

A Homotopy method for motion planning

M.-A. Belabbas
Electrical and Computer Engineering Department
Coordinated Science Lab
University of Illinois, Urbana-Champaign

Motion planning can mean a lot of things to a lot of people



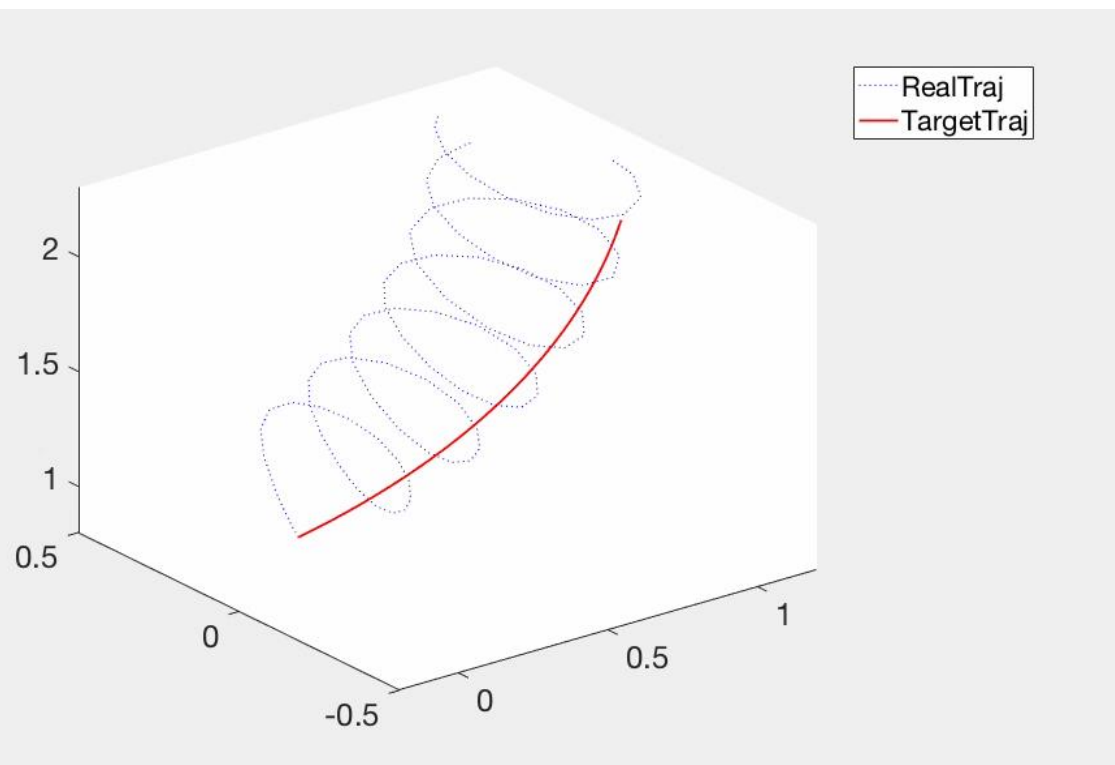
- Changing, unknown environment
- **Goal:** find controls to reach final destination
- High-level control: send 'move to (x,y)' commands, algorithmic solutions

- Addresses the *difficult* problem of planning with *non-holonomic* dynamics

$$\dot{x} = \sum_i u_i f_i(x)$$

$$\dot{x} = \sqrt{\frac{1}{\varepsilon}} \cos\left(\frac{t}{\varepsilon}\right) f_1(x) + \sqrt{\frac{1}{\varepsilon}} \sin\left(\frac{t}{\varepsilon}\right) f_2(x) \Leftrightarrow \dot{x} = [f_1, f_2](x)$$

- **Goal:** find *controls* to follow target trajectory.
- Provides: Analytic solutions



Motion planning = find controls to drive you to a desired destination

New method for motion planning for nonlinear systems

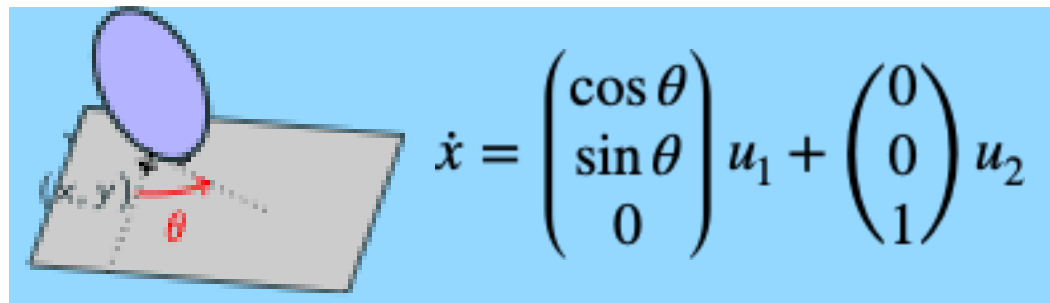
in:

1. Description of environment
2. Description of dynamics
3. Desired final location/state

out:

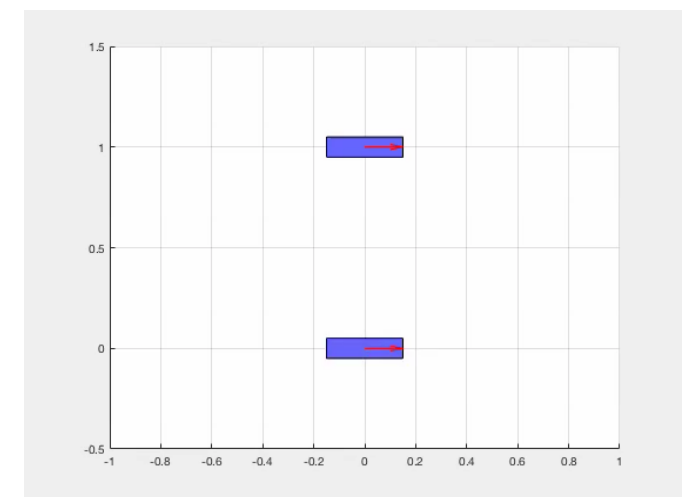
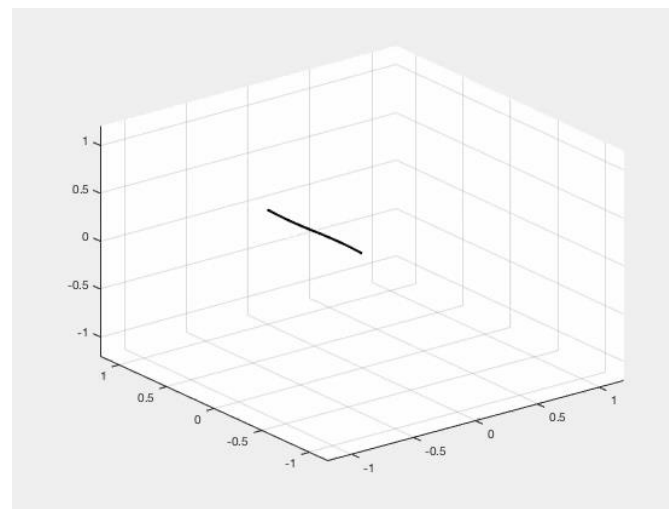
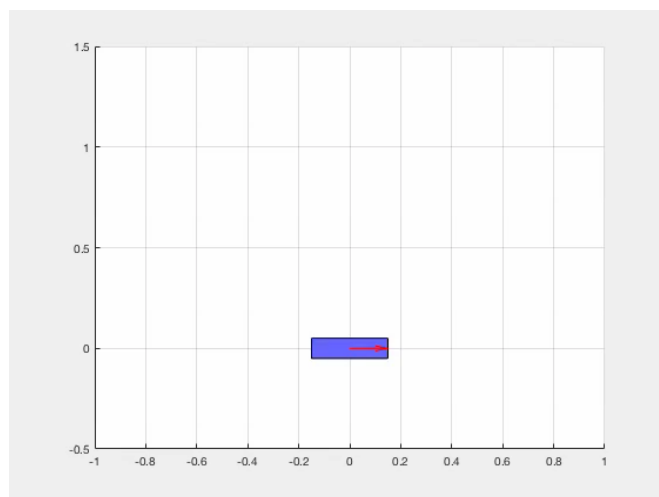
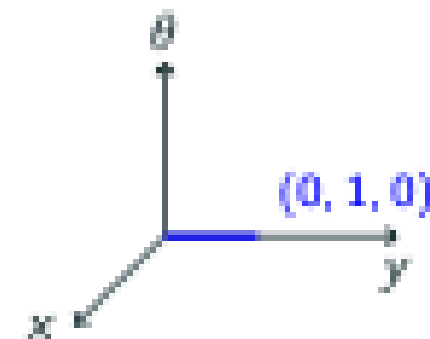
Controls that send you to destination

- Handles holonomic, nonholonomic, obstacle constraints
- Provides an algorithm, and strong guarantees of convergence
- Yields *natural* motions



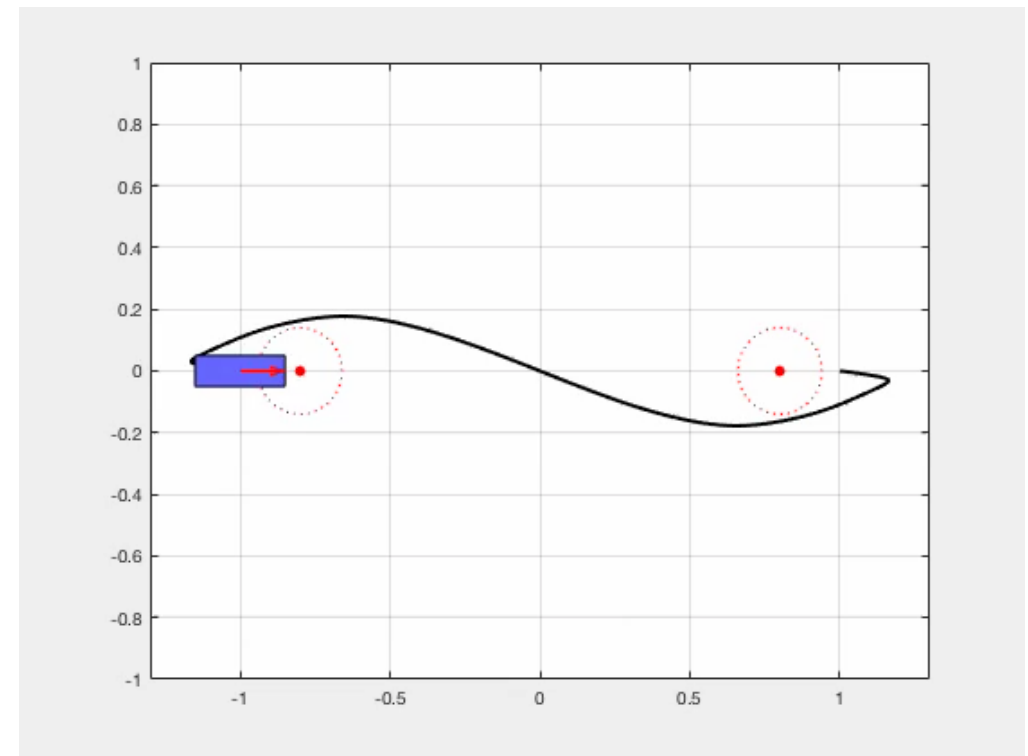
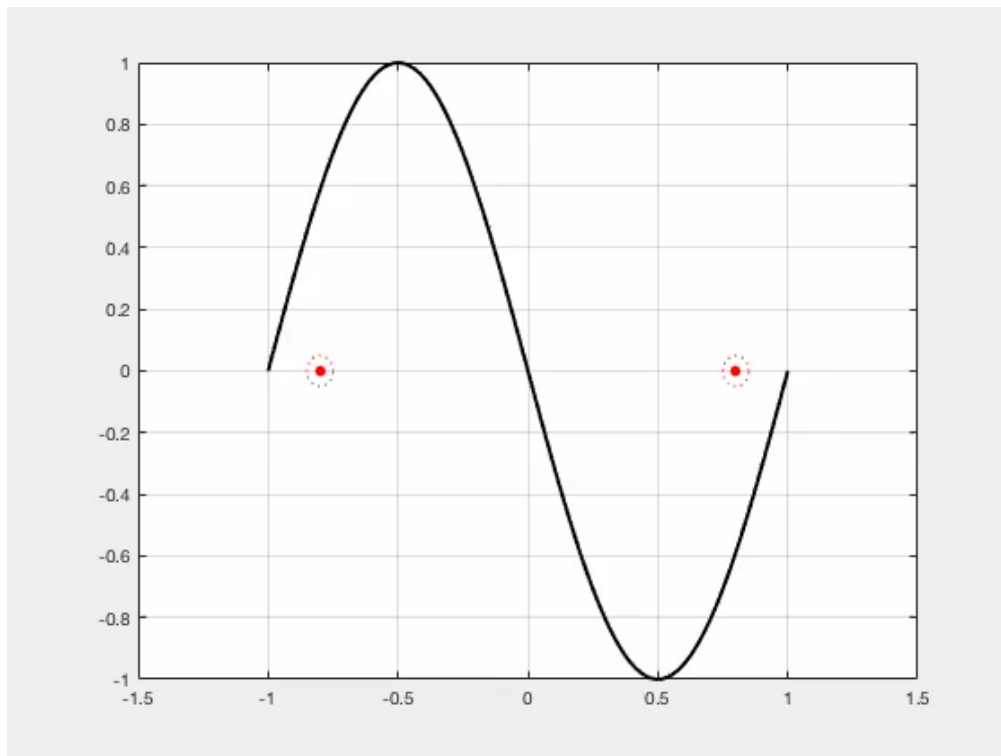
Goal: move unicycle from $(0,0,0)$ to $(0,1,0)$

Initial trajectory



With obstacles

- Warning: homotopies always take place in configuration space and are differentiable
- We show a projection onto 2D workspace



Outline of the presentation

1. Introduction and motivation
2. Presentation of the method
3. Complexity, drift and bounded controls
4. Case study: wheeled vehicles
5. Sketch of proof of convergence

Three steps of the method

1. The constraints: think local

When at a point in configuration space, what are good directions to follow?

2. Homotopy

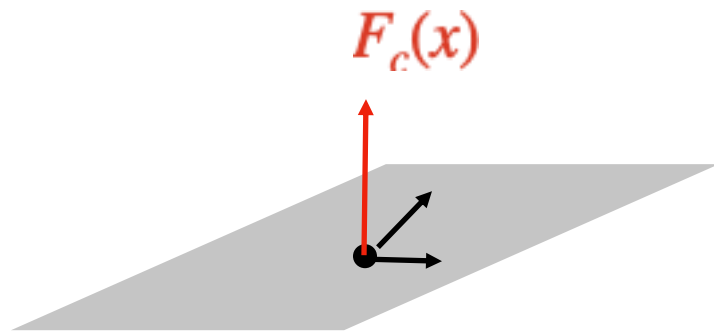
Transform an initial path to one that meets constraints

3. Extract controls

Think local!

- From a **local** perspective: 2 **types** of constraints

Hard constraints



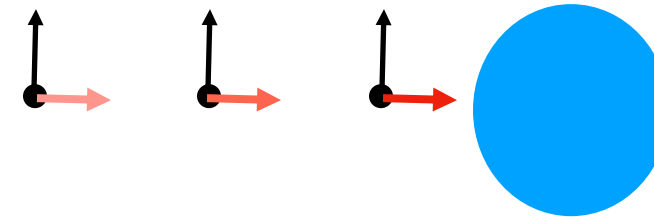
- Holonomic/non-holonomic:
motion in some direction not allowed

Mathematically, create a matrix

$$F_c(x) = \begin{pmatrix} | & | & \cdots & | \\ f_1 & f_2 & \cdots & f_p \\ | & | & \cdots & | \end{pmatrix}$$

where the columns span the forbidden motion

Soft constraints



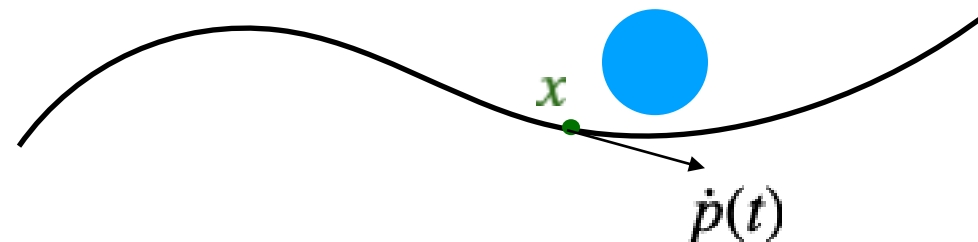
- Obstacle:
unless exactly at boundary, no restriction on motion

Mathematically, described by
“barrier” function $r(x)$

$$\mathcal{O} = \{x \in Q \mid r(x) \geq 0\}$$

Naive approach: minimize integral cost of forbidden directions

- Let $p(t)$ be a trajectory in configuration space joining initial to desired final states
- How much is the trajectory using constrained motions at x ?



- Motion at $x=p(t)$ is given by $\dot{p}(t)$
- Constrained motions are $F_c(x)$
- Proximity to obstacle is given by $\left| \frac{1}{\varepsilon + r(x)} \right|$, where ε is a tolerance parameter

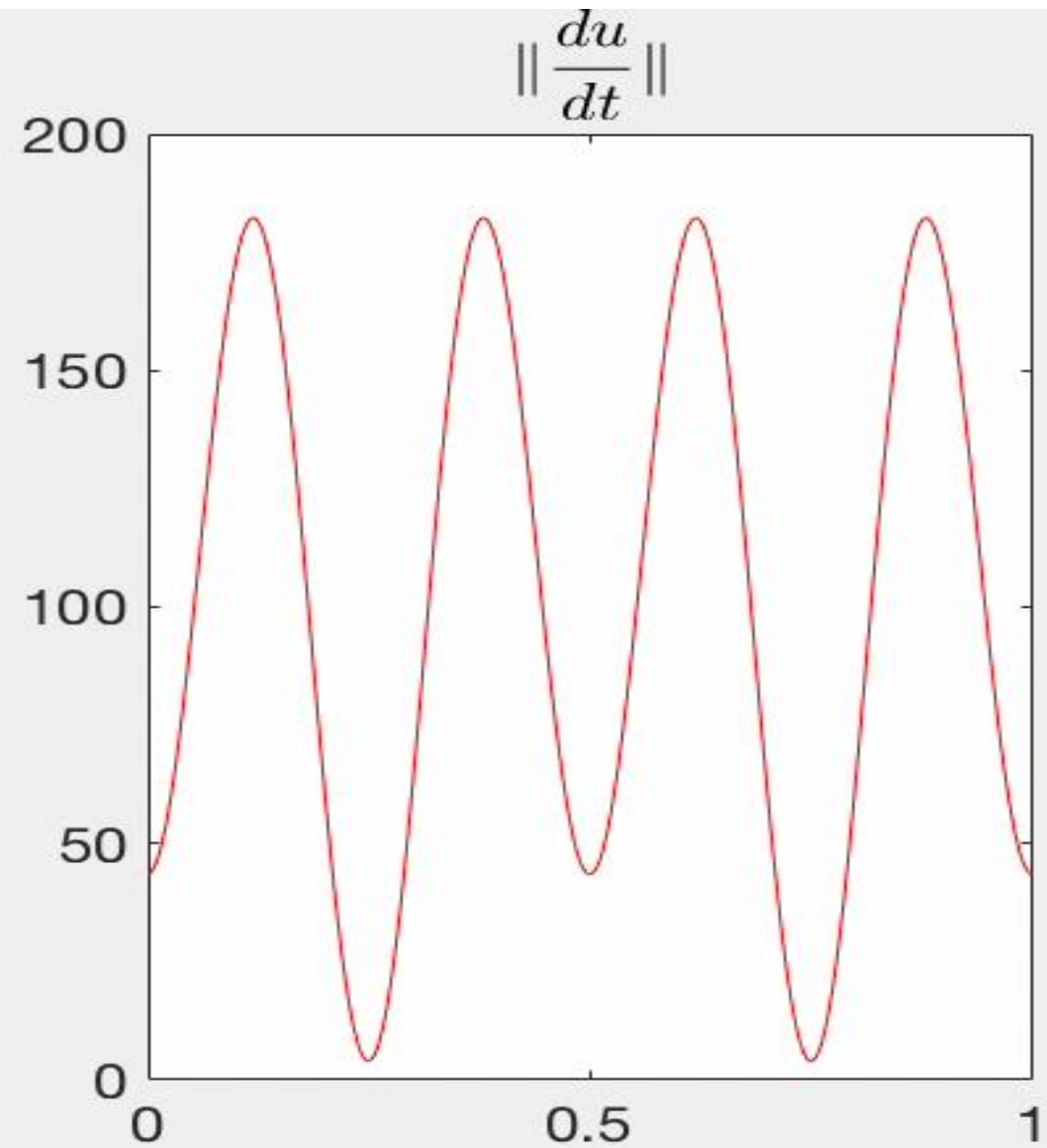
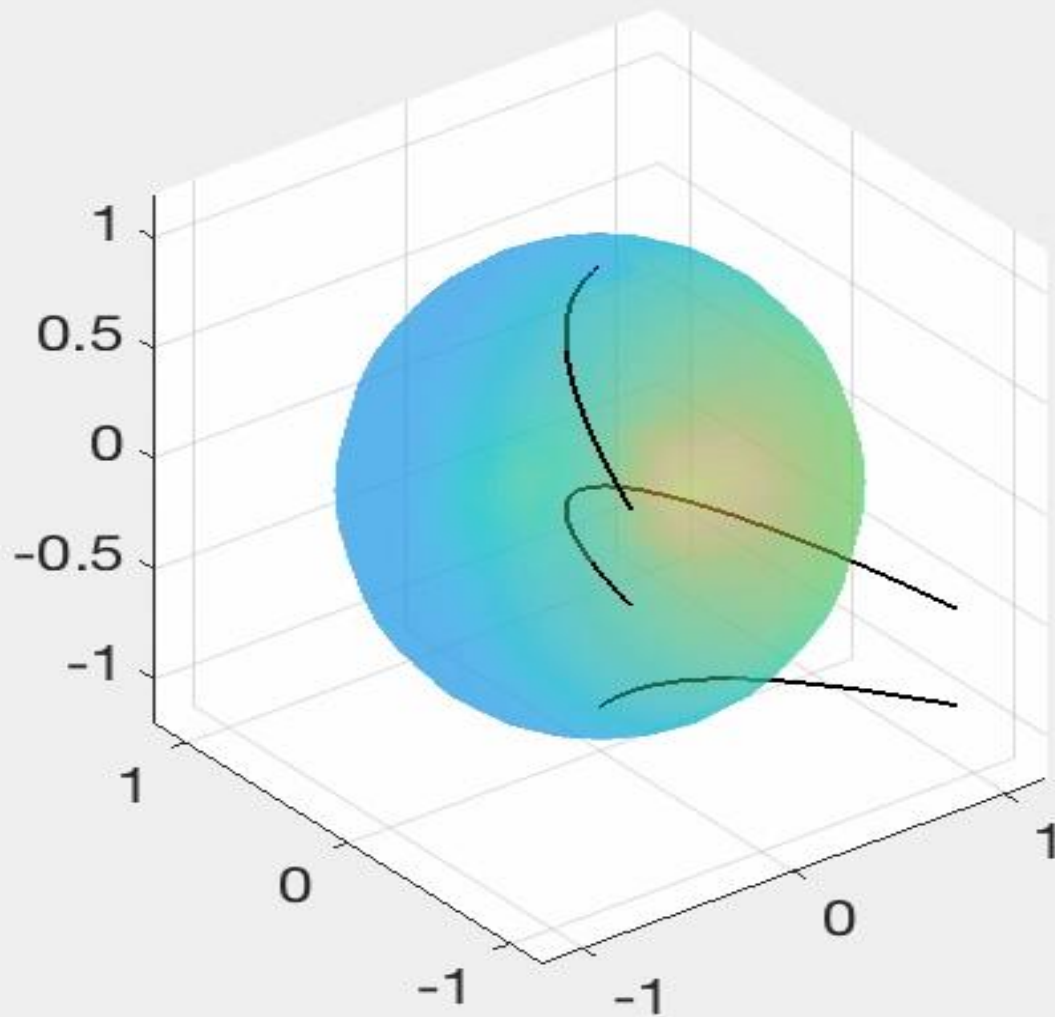
The quantity $\|F_c^\top(x)\dot{p}(t)\|^2 \left| \frac{1}{\varepsilon + r(x)} \right|^2$ measures how much “bad directions” are used at $p(t)$

Naive approach: minimize cost of forbidden directions

- We assign the cost J to a path $p(t)$:

$$J(p) := \int_0^{t_f} \|F_c^\top(p(t))\dot{p}(t)\|^2 \left| \frac{1}{\varepsilon + r(p(t))} \right|^2 dt$$

- Derive the *gradient flow* for this functional, in path space



- Converges to a *discontinuous* path in general

The fix: “regularization”

- Discontinuous curve \Leftrightarrow large derivative
- \rightarrow Penalize the norm of the derivative

$$\text{minimize } E_k(p) := J(p) + \frac{1}{k} \int_0^{t_f} \|\dot{p}\|^2 dt$$

- **The good:** minima are continuous
- **The bad:** when $k < \infty$, we are *not* solving our original problem
- **The ugly:** we can try to solve for k large and hope to have p close to minima of J , but we know that for $k = \infty$, we converge to a discontinuous p .

Theorem: Let $p_k(t)$ be a minimizer of E_k . Then $\lim_{k \rightarrow \infty} p_k(t)$ is continuous.

Riemannian geometry naturally appears when dealing with localized constraints

Observations: 1. we can always find a G so that the functional E can be expressed as

$$E(p) := J(p) + \frac{1}{k} \int_0^{t_f} \|\dot{p}\|^2 dt \quad \longrightarrow \quad E(p) = \int_0^{t_f} \dot{p}^\top G(p(t)) \dot{p} dt$$

2. This is the energy functional, whose minimizers are **geodesics** for the metric associated with G !

Admissible paths \leftarrow geodesics for “good metric”

The method in three steps redux



1. Localize the constraints

→ Encode in a positive definite matrix

2. Homotopy

Transform an initial path which does *not* meet the constraints to one that meets constraints

Becomes a Geometric Heat Flow (GHF)

3. Extract controls

Encoding the constraints in an inner product

Set $F_f(x) \leftarrow F_c^\perp(x)$ and $F(x) = \begin{pmatrix} | & | \\ F_c & F_f \\ | & | \end{pmatrix}$ F is square and invertible.

- Denote by p the number of columns of $F_c(x)$

- Set $b(x) := \left| \frac{1}{\varepsilon + r(x)} \right|$

- Define the family of inner products (metrics)

$$G_k(x) := F(x) \begin{pmatrix} k & 0 & \dots & & 0 \\ 0 & k & 0 & \dots & 0 \\ \vdots & & \ddots & & \vdots \\ 0 & \dots & & b(x) & 0 \\ \vdots & & & & \ddots & \vdots \\ 0 & \dots & & & & b(x) \end{pmatrix} F^\top(x)$$

The method in three steps redux

1. Localize the constraints

When at a point in configuration space, what are good directions to follow?

Add regularization for complementary directions

→ Riemannian inner product

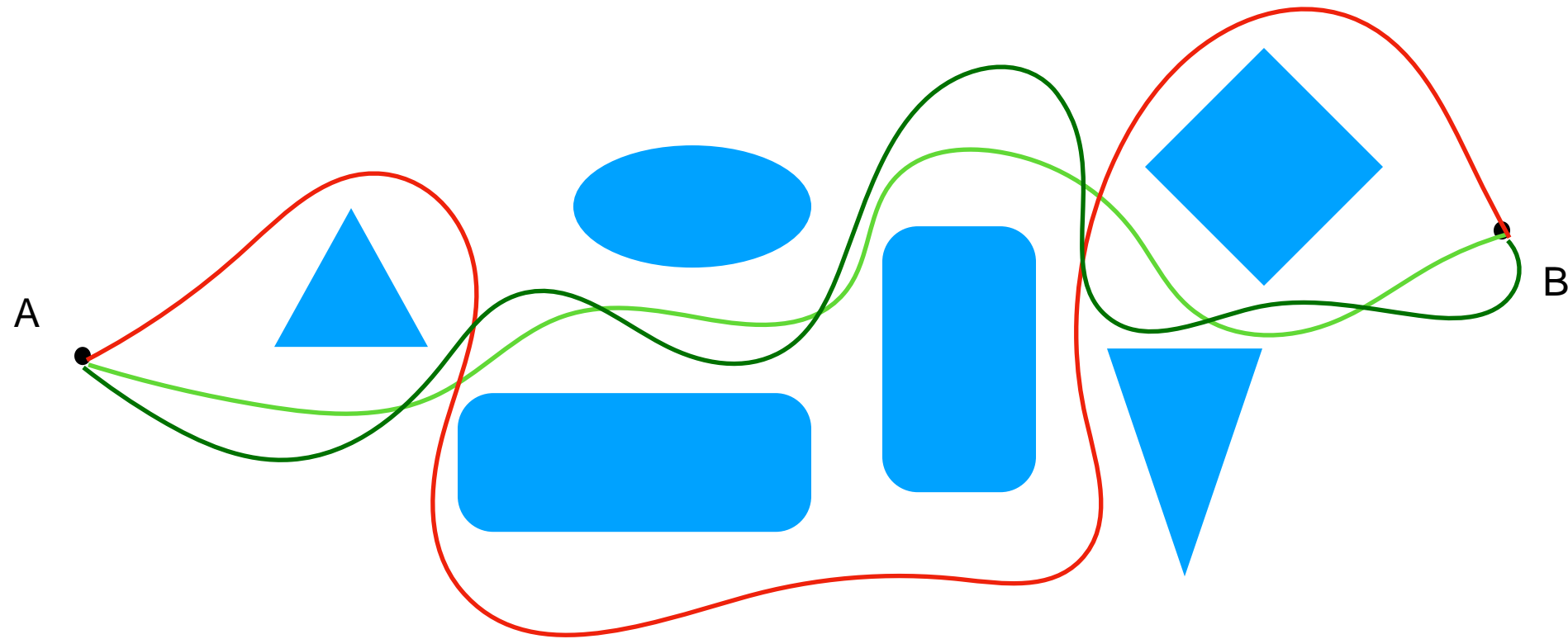
→ 2. Homotopy

Transform an initial path which does *not* meet the constraints to one that meets constraints

Becomes a Geometric Heat Flow (GHF)

3. Extract controls

Why use homotopy of paths?



Homotopic paths have similar “macroscopic” characteristics

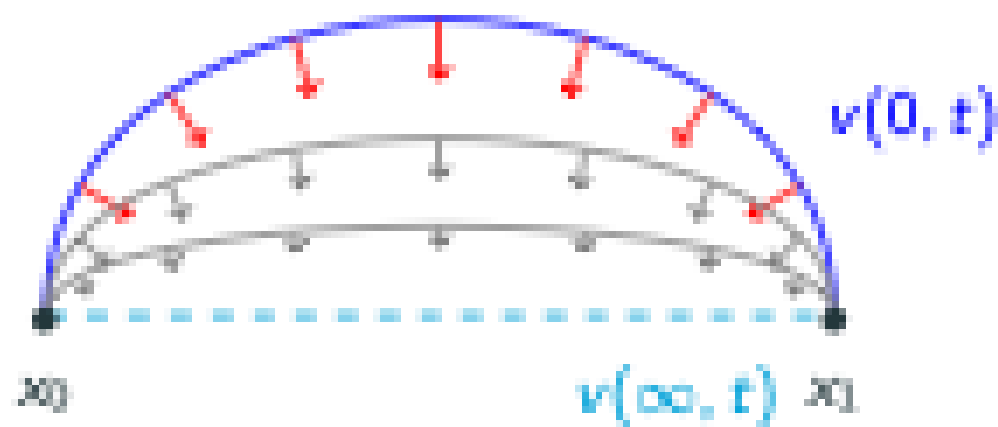
1. + : if you need to insure properties of paths
Integrate prior knowledge into initial trajectory
2. - : if you want to optimize global properties.
Need preprocessing to find optimal homotopy class

Homotopy through geometric heat flow

- In our problem, we are given
 1. Fixed initial and final states
 2. An initial path between these states that avoid obstacles, but does not meet constraints necessarily.
- **Goal:** minimize length for $G(x)$ amongst differentiable paths joining these states

Large body of research in the area, under the name of *curve shortening flows* or *Geometric heat flows*

[Angenent, Huisken, Grayson, Altschuler, Abresch, Langer (between 1986-1991)]



Homotopy

$$v(s, t) : [0, \infty] \times [0, t_f] \rightarrow Q \text{ with } v(s, 0) = x_0, v(s, t_f) = x_1$$

Curve shortening: move in direction of inner normal

$$\frac{\partial v(s, t)}{\partial s} = \dot{v} = \kappa N$$

In general case

$$\frac{\partial}{\partial s} v_i(s, t) = \frac{\partial^2}{\partial t^2} v_i(s, t) + \sum_{j,k} \Gamma_{jk}^i \frac{\partial v_j}{\partial t} \frac{\partial v_k}{\partial t}$$

This is the geometric heat flow we solve

Where, we recall the *Christoffels symbols*

$$\Gamma_{jk}^i(x) := \frac{1}{2} \sum_{l=1}^n G_{il}^{-1} \left(\frac{\partial G_{lj}}{\partial x_k} + \frac{\partial G_{lk}}{\partial x_j} - \frac{\partial G_{jk}}{\partial x_l} \right)$$

The method in three steps redux

1. Localize the constraints

When at a point in configuration space, what are good directions to follow?

Add regularization for complementary directions

→ Riemannian inner product

2. Homotopy

Transform an initial path which does *not* meet the constraints to one that meets constraints

Becomes a Geometric Heat Flow (GHF)

3. Extract controls



Extract controls and convergence guarantee

- Assume system is given by $\dot{x} = \sum_{i=1}^l u_i b_i(x)$, and the desired final state is \bar{x}_{t_f}
- Let $B(x)$ be the matrix with columns $b_i(x)$

Let $p_{k,s}(t)$ be the solution using our method with integration time s and metric $G_k(x)$

Note that $\lim_{s \rightarrow \infty} p_{k,s}(t) = \arg \min \int_0^{t_f} \dot{p}^\top G_k \dot{p} dt$

$$\text{Set } \bar{u}_{k,s}(t) = B^\dagger F_f F_f^\dagger \dot{p}_{k,s}(t) \longrightarrow \dot{x}_{s,k}^*(t) = \sum_{i=1}^p \bar{u}_{i,s,k} b_i(x^*)$$

Under some assumptions (controllability), the following hold

Theorem : We have $\lim_{s,k \rightarrow \infty} p_{s,k}(t)$ is continuous

Theorem [Consistency]: We have $\lim_{s,k \rightarrow \infty} x_{s,k}^*(t) = \lim_{s,k \rightarrow \infty} p_{s,k}(t)$

Theorem: For all $\varepsilon > 0$, there exists s_m, k_m so that for all $s \geq s_m, k \geq k_m, \|x_{s,k}^*(t_f) - \bar{x}(t_f)\| < \varepsilon$

Outline of the presentation

1. Introduction and motivation
2. Presentation of the method
3. Complexity, drift and bounded controls
4. Case study: wheeled vehicles
5. Sketch of proof of convergence

On complexity

- Computationally *intensive* part: numerical solution of the GHF
- Good news: this is a *parabolic PDE*. Fast, parallel algorithm exist.
- It is of *much* lower complexity than solving the *Hamilton-Jacobi-Bellman* (HJB) equation

Hamilton-Jacobi-Bellman

$$-\frac{\partial V(t, x)}{\partial t} = -\min_u \left[\frac{\partial V}{\partial x} f(x, u) + c(x, u) \right]$$

- *Complexity*: dimension of *domain* of V increases linearly in dimension of Q
 - 1 equation with domain scaling with number of dimensions of Q
 - complexity is *exponential* in dimension of domain
- + : Provides *feedback* control
- - : Feedback control may not exist, no clean stopping rule

Geometric Heat Flow

$$\frac{\partial}{\partial s} v_i(s, t) = \frac{\partial^2}{\partial t^2} v_i(s, t) + \sum_{j,k} \Gamma_{jk}^i \frac{\partial v_j}{\partial t} \frac{\partial v_k}{\partial t}$$

- *Complexity*: domain is (s, t) : always two-dimensional.
 - Number of PDEs increases with dimension of Q
 - complexity increases *polynomially* in dimension Q
- Provides open loop control

Systems with drift and constrained controls

$$\dot{x} = f_d(x) + \sum_i u_i b_i(x)$$

$u \in \mathcal{U}$ a set of admissible controls

- Deciding controllability for systems with drift is *far* more complex
- From **local** point of view: set of allowable motions is not a *vector* space, but an *affine* space

- We use instead the functional:

$$\tilde{E}(p) := \int_0^{t_f} (\dot{p}^\top - f_{drift}) G(p(t)) (\dot{p} - f_{drift}) dt$$

- **Constraints** on the controls are handled via **obstacles** and added state variables

$$\dot{x} = u_1 f_1 + u_2 f_2$$

$$u_1 \geq 0$$



$$\dot{x} = z_1 f_1 + u_2 f_2$$

$$\dot{z}_1 = u_1$$

and obstacle $z_1 \geq 0$

Systems with drift and constrained controls

Legged robot 2D planning // parallel legs

Configuration space: position and orientation (x, y, θ)

Inputs: ground reaction force u_x u_y

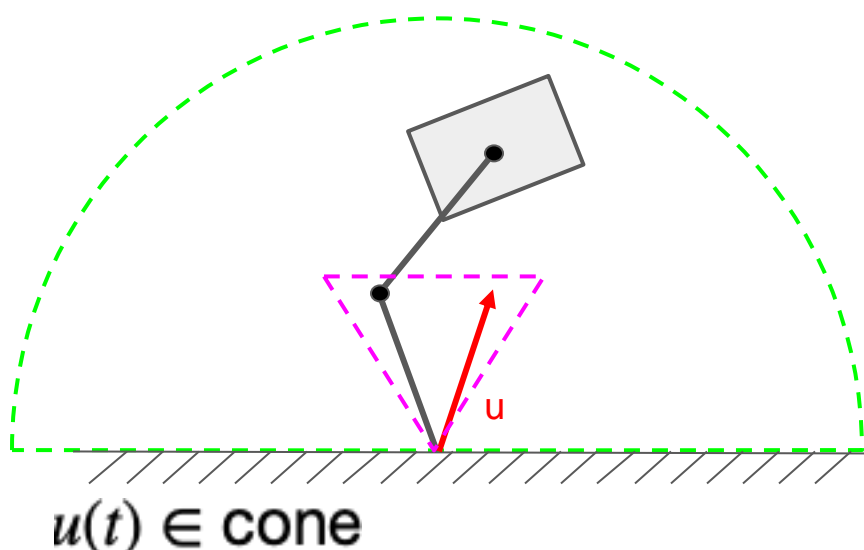
Massless: inputs to legs joint torque: $\tau = J^T \begin{bmatrix} u_x \\ u_y \end{bmatrix}$

Goal:

find a trajectory for x, y, θ, u_x, u_y with given initial and final condition.

Constraints:

- Kinematics constraints at joints
- Input constraints: friction cone



EoM: (assuming $m=1$)

$$\ddot{x} = u_x$$

$$\ddot{y} = u_y - g$$

$$\ddot{\theta} = u_x y - u_y x$$

$$X = [x \quad y \quad \theta \quad \dot{x} \quad \dot{y} \quad \dot{\theta}]^T$$

$$\dot{X} = \underbrace{\begin{bmatrix} X(4) \\ X(5) \\ X(6) \\ 0 \\ -g \\ 0 \end{bmatrix}}_{\substack{f(X) \\ \text{drift term}}} + \underbrace{\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \\ X(2) & -X(1) \end{bmatrix}}_{\substack{F_f(X) \\ \text{admissible direction}}} u$$

Systems with drift and positivity constraints

To implement the constraints, modify the system:
add the control as states

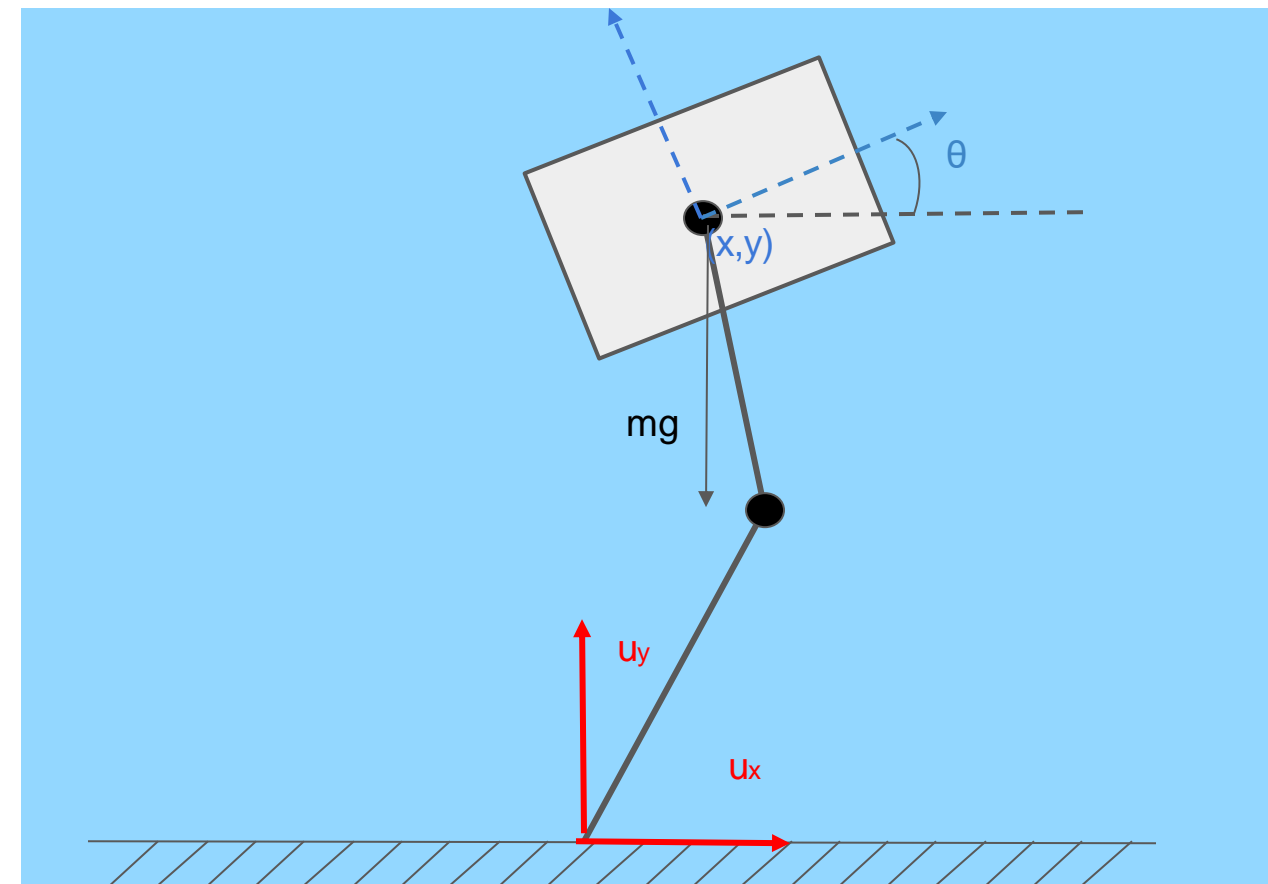
$$X = [x \quad y \quad \theta \quad \dot{x} \quad \dot{y} \quad \dot{\theta} \quad \boxed{u_x \quad u_y}]^T$$

Update the dynamics

$$\dot{X} = \begin{bmatrix} X(4) \\ X(5) \\ X(6) \\ X(7) \\ X(8) - g \\ -X(1)X(8) + X(2)X(7) \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} u$$

$\underbrace{\begin{bmatrix} X(4) \\ X(5) \\ X(6) \\ X(7) \\ X(8) - g \\ -X(1)X(8) + X(2)X(7) \\ 0 \\ 0 \end{bmatrix}}_{f(X)} \quad \underbrace{\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}}_{F_f}$

Set obstacles on the control states to implement the friction cone



EoM: (assuming $m=1$)

$$\ddot{x} = u_x$$

$$\ddot{y} = u_y - g$$

$$X = [x \quad y \quad \theta \quad \dot{x} \quad \dot{y} \quad \dot{\theta}]^T$$

$$\ddot{\theta} = u_x y - u_y x$$

$$\dot{X} = \begin{bmatrix} X(4) \\ X(5) \\ X(6) \\ 0 \\ -g \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \\ X(2) & -X(1) \end{bmatrix} u$$

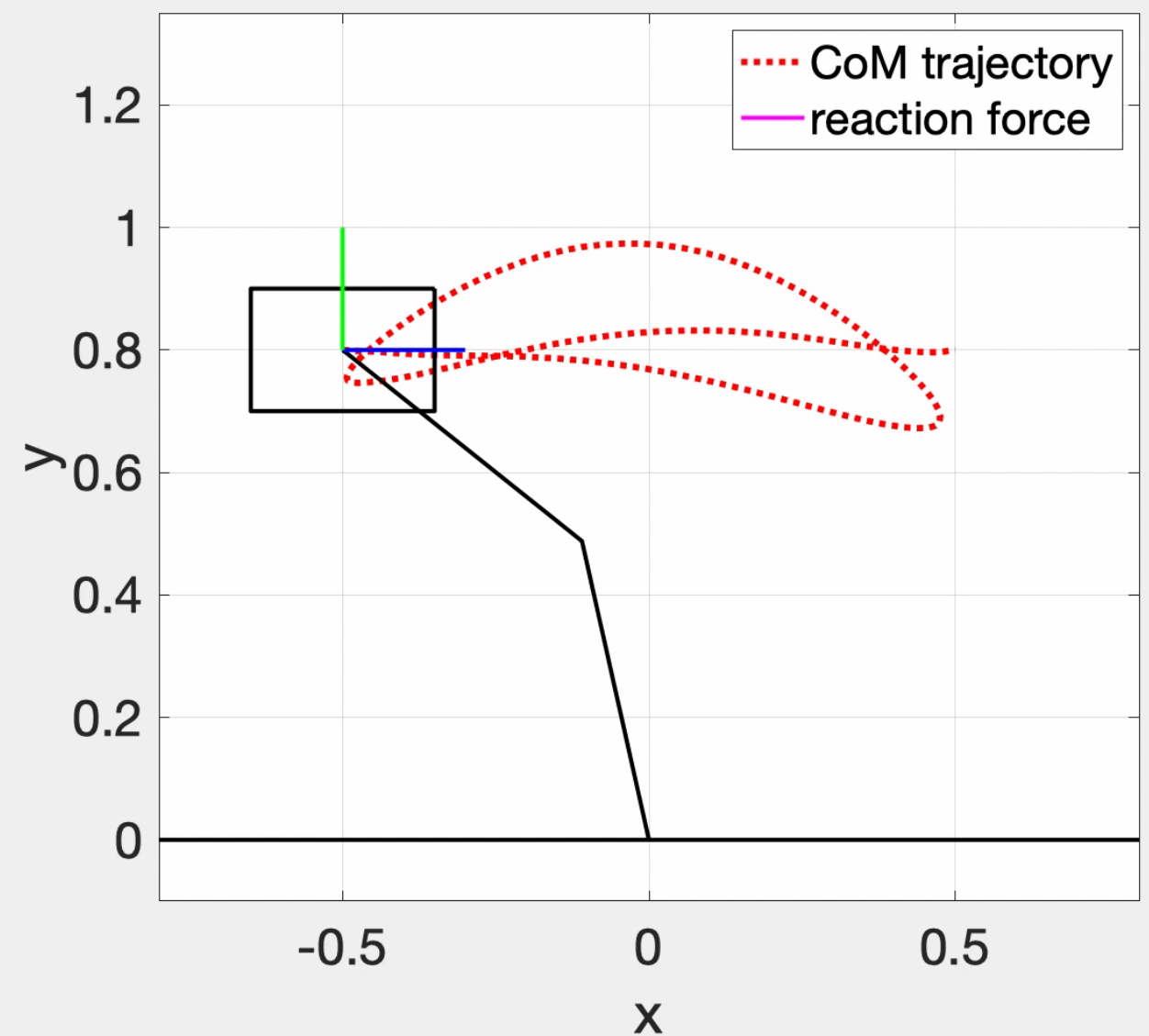
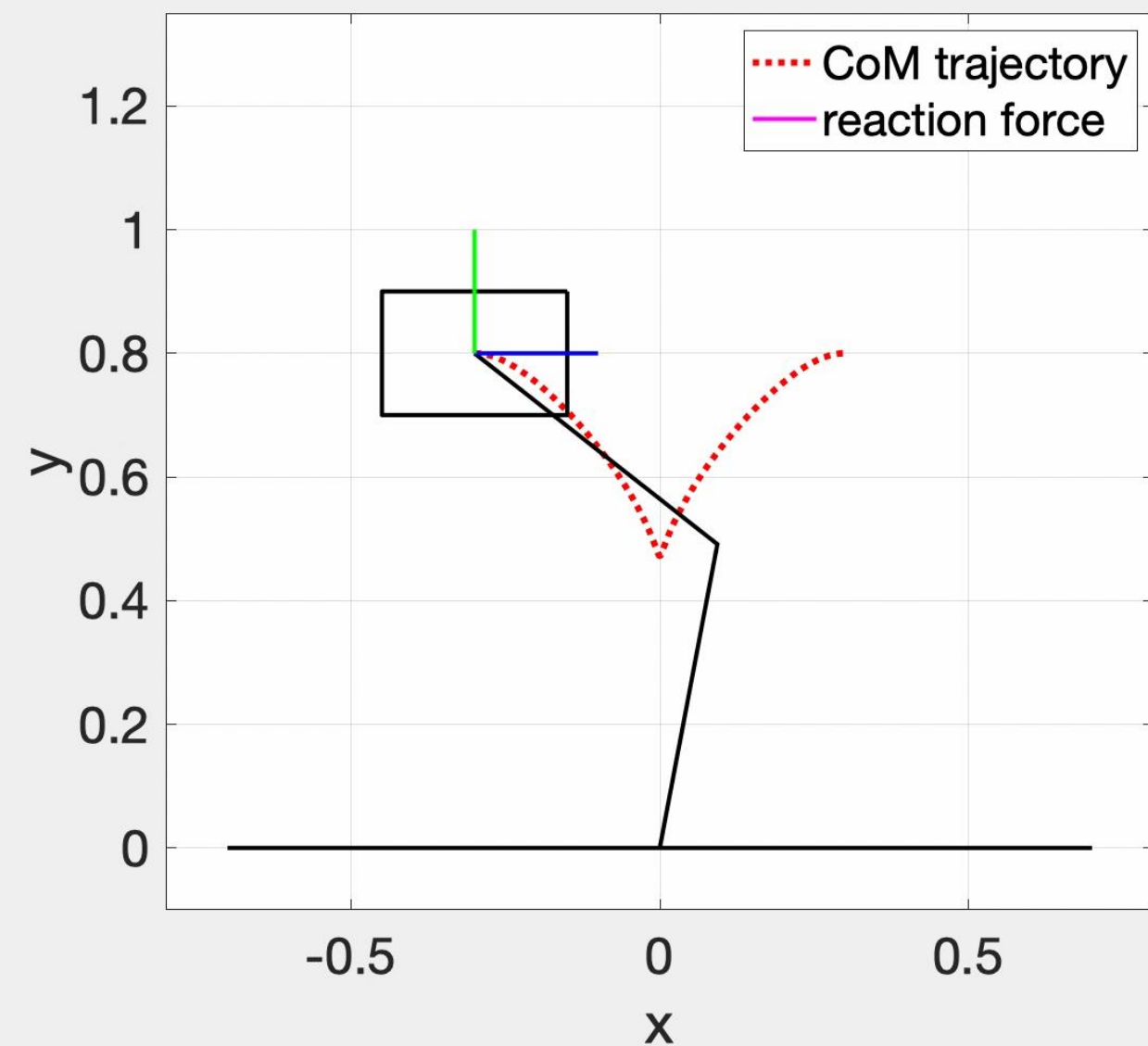
$\underbrace{\begin{bmatrix} X(4) \\ X(5) \\ X(6) \\ 0 \\ -g \\ 0 \end{bmatrix}}_{\substack{f(X) \\ \text{drift term}}} \quad \underbrace{\begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \\ X(2) & -X(1) \end{bmatrix}}_{\substack{F_f(X) \\ \text{admissible direction}}} u$

Systems with drift and positive constraints

Transfer body from $(-.25, .8, 0)$ to $(.25, .8, 0)$

Transfer body from $(-.5, .8, 0)$ to $(.5, .8, 0)$

Allowed time: 1.5 sec

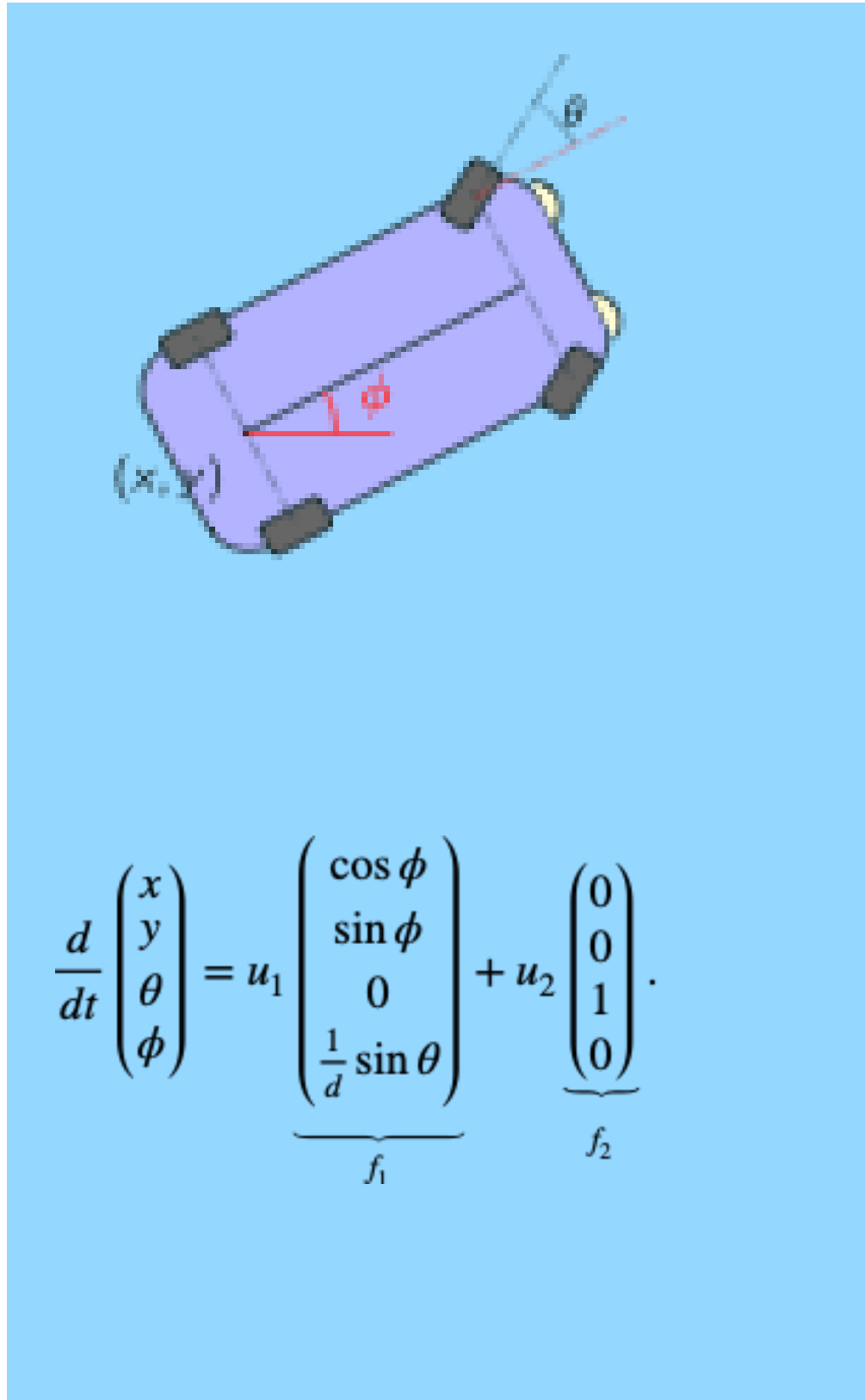


Outline of the presentation

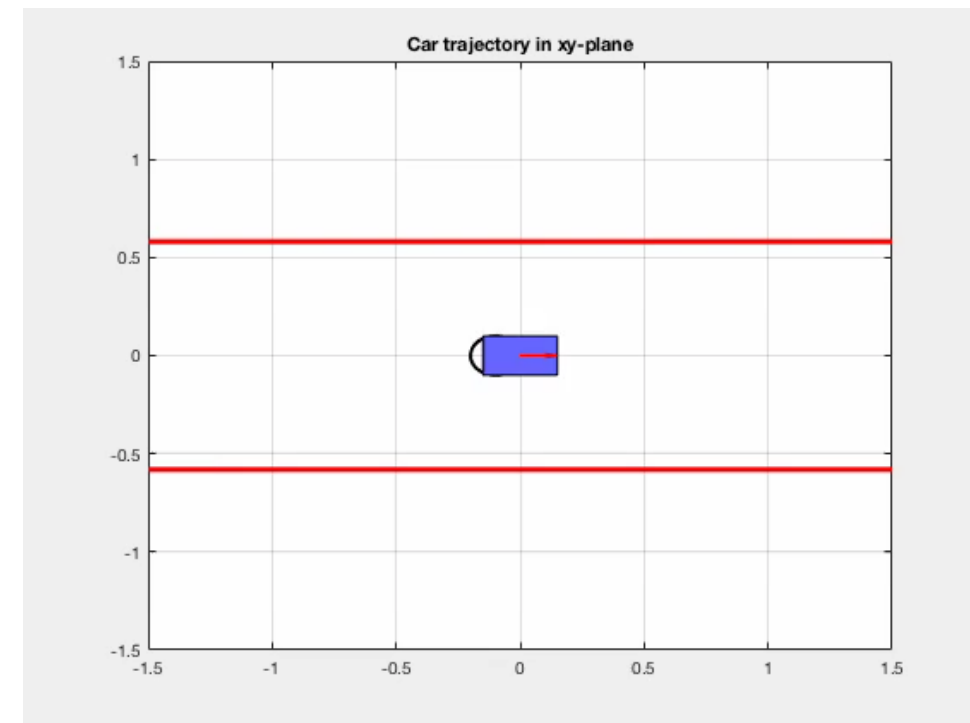
1. Introduction and motivation
2. Presentation of the method
3. Complexity, drift and bounded controls
4. Case study: wheeled vehicles
5. Sketch of proof of convergence

Case study: car maneuvers

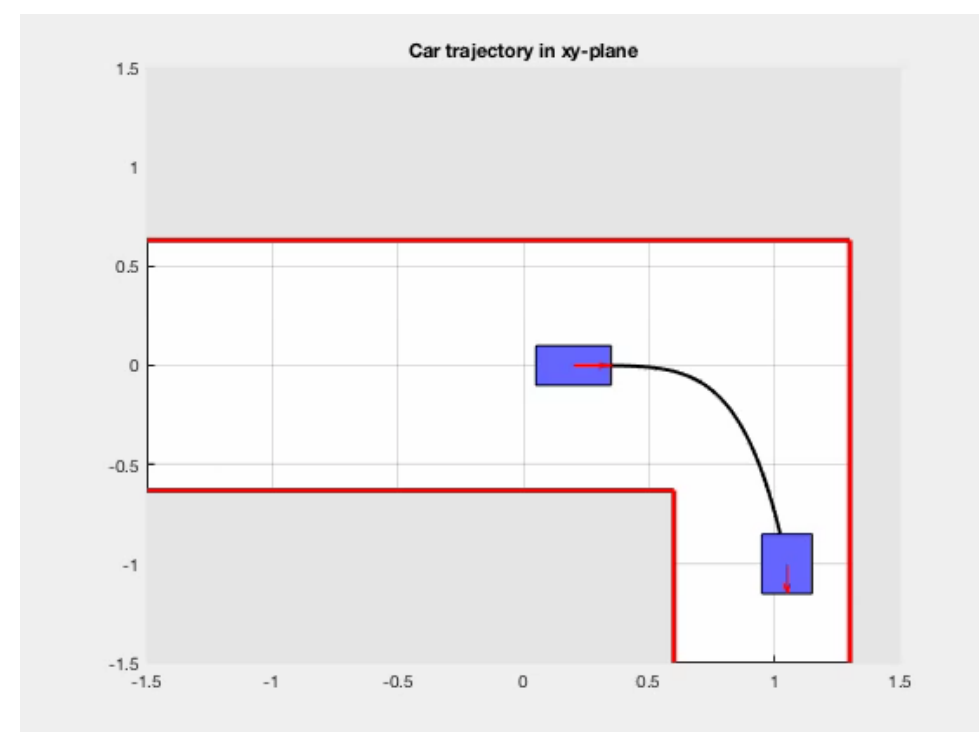
Model



Initial trajectories: 180 turn

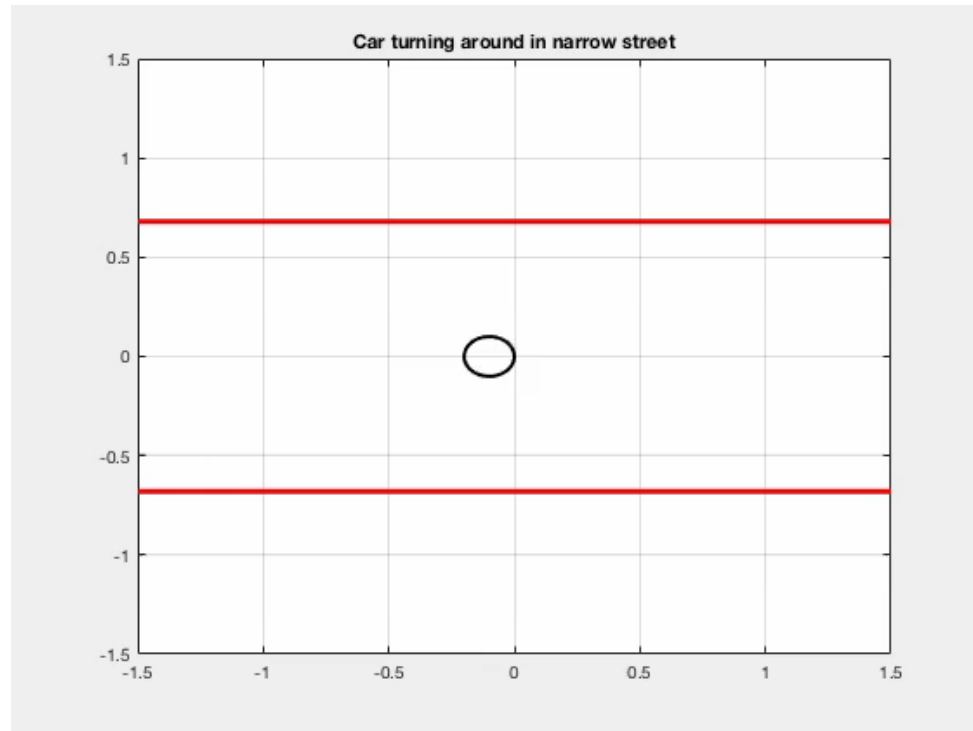


Initial trajectories: street turn

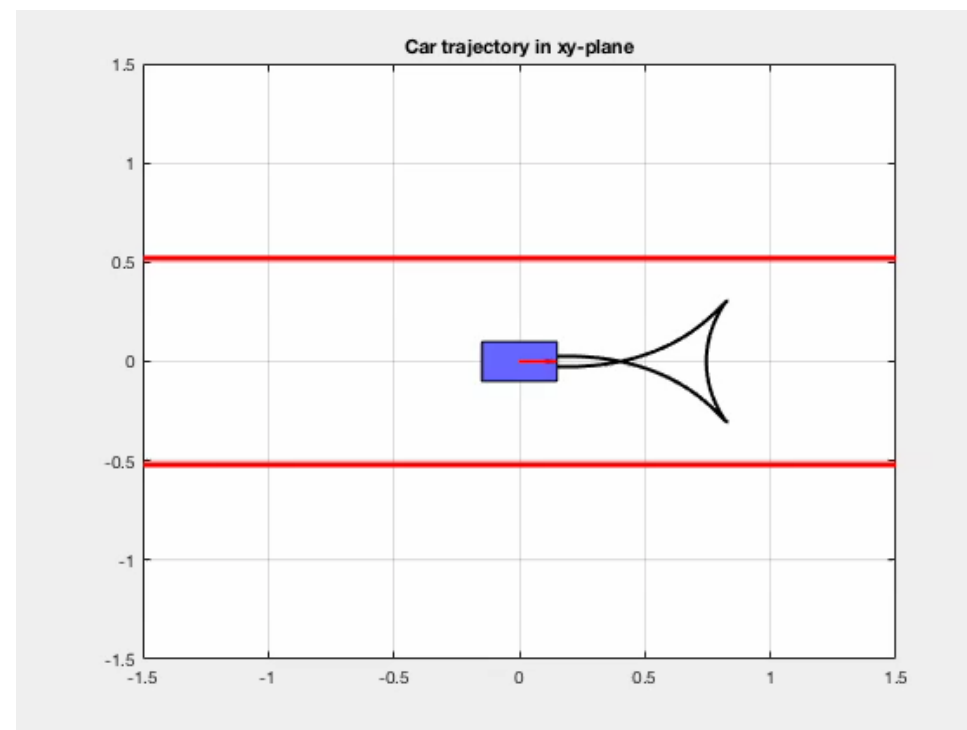
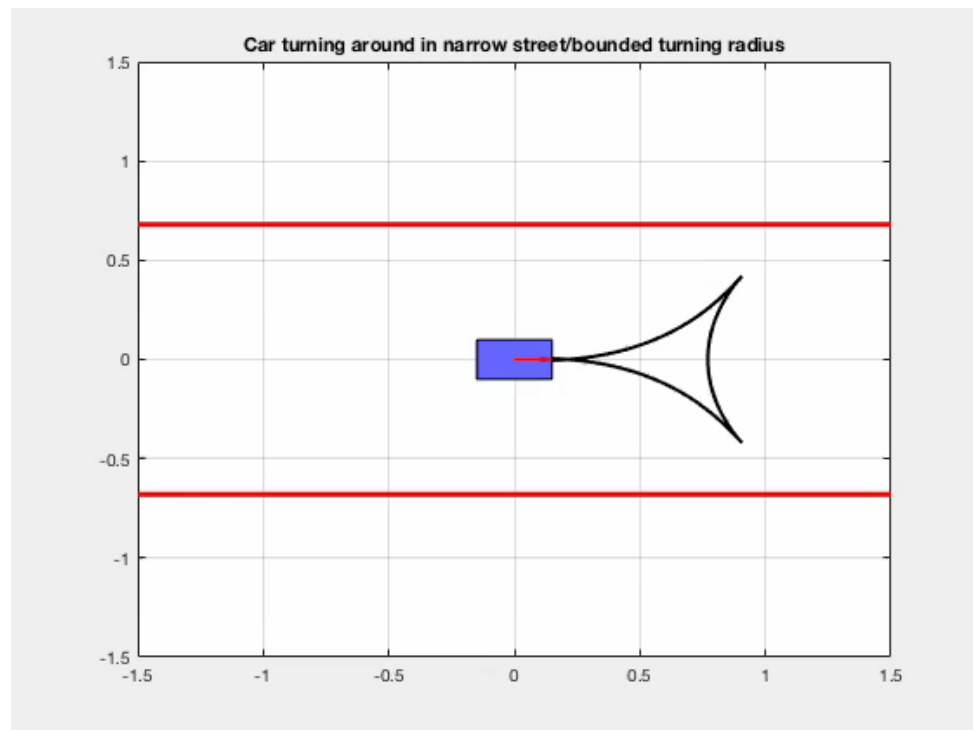
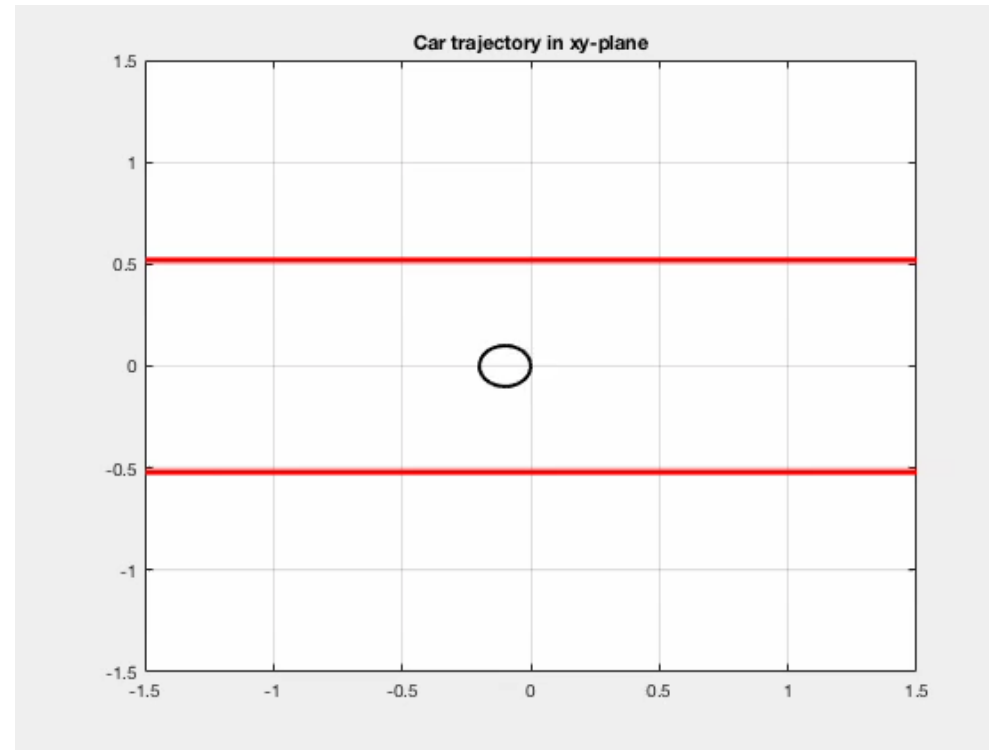


Car maneuvers: 180 turn

Wide street

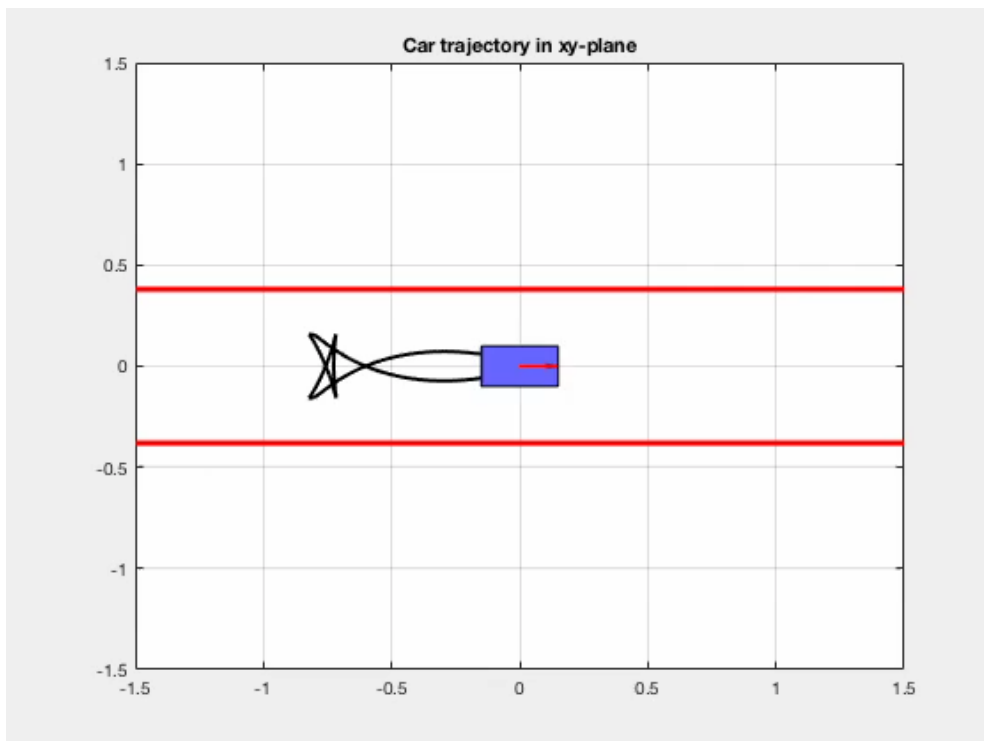
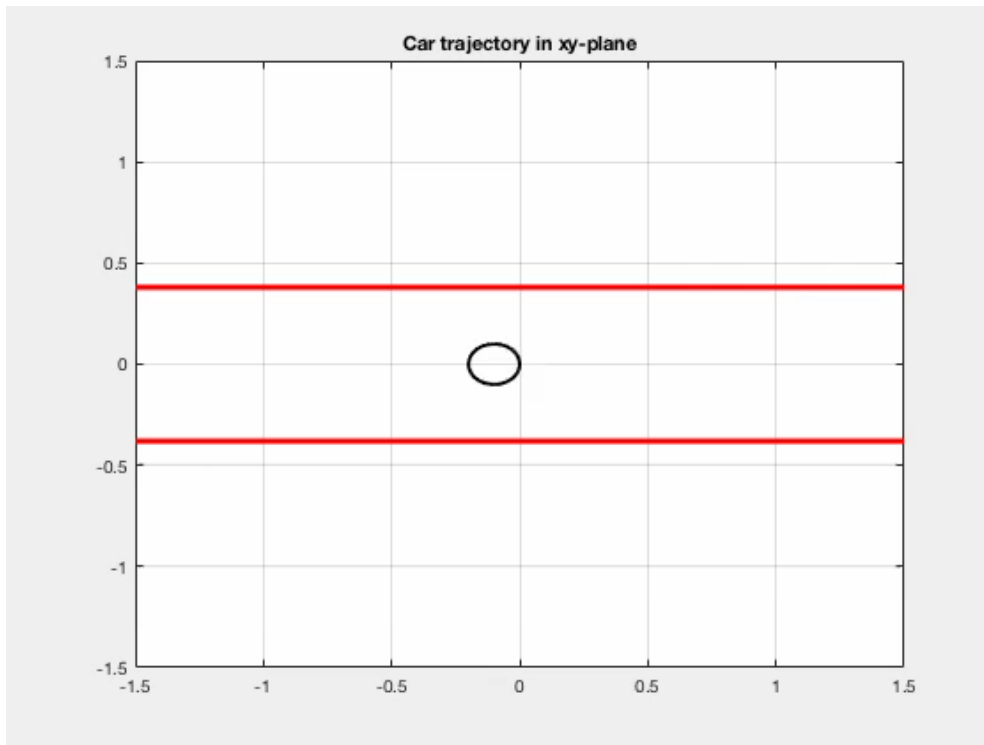


Narrow street

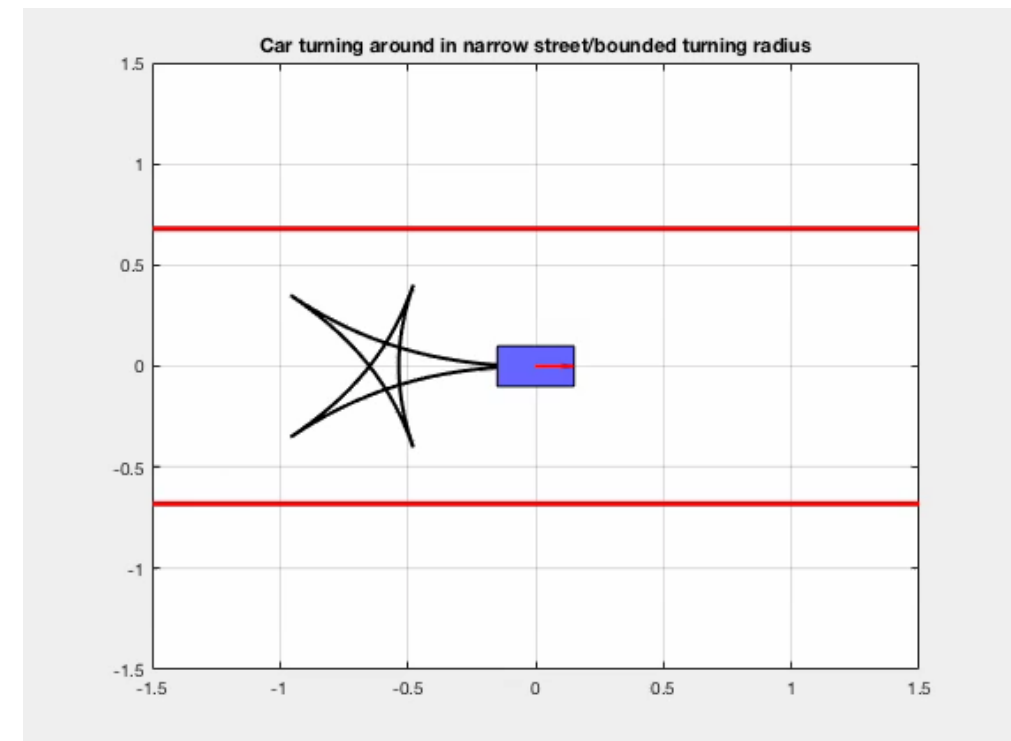
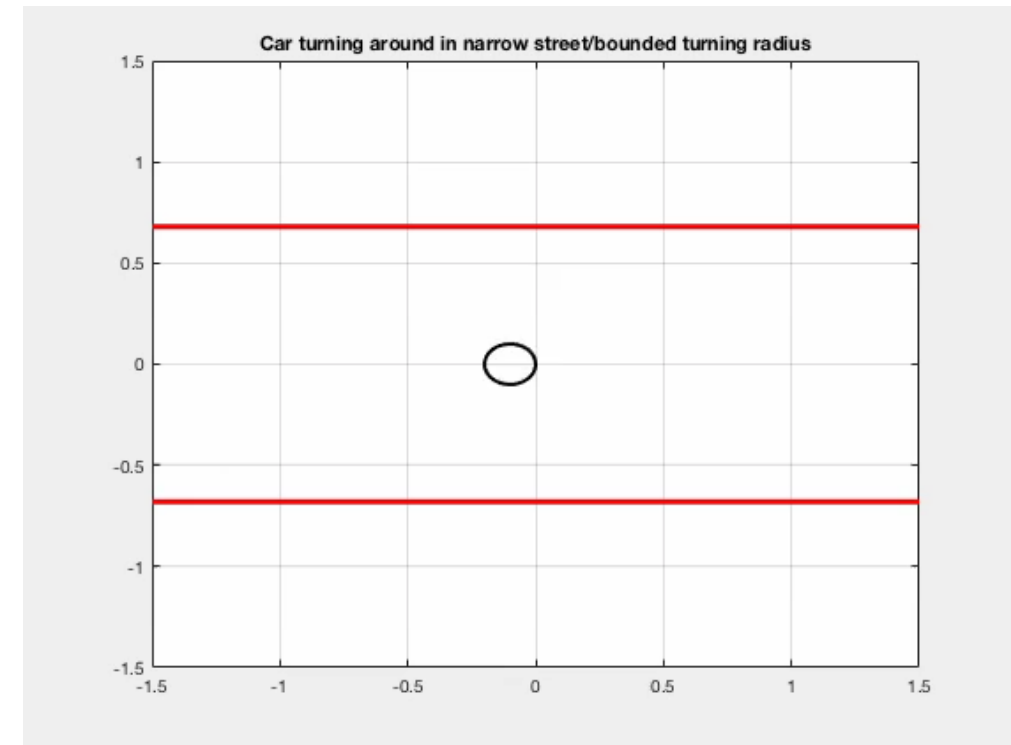


Car maneuvers: 180 turn

1. Narrower street

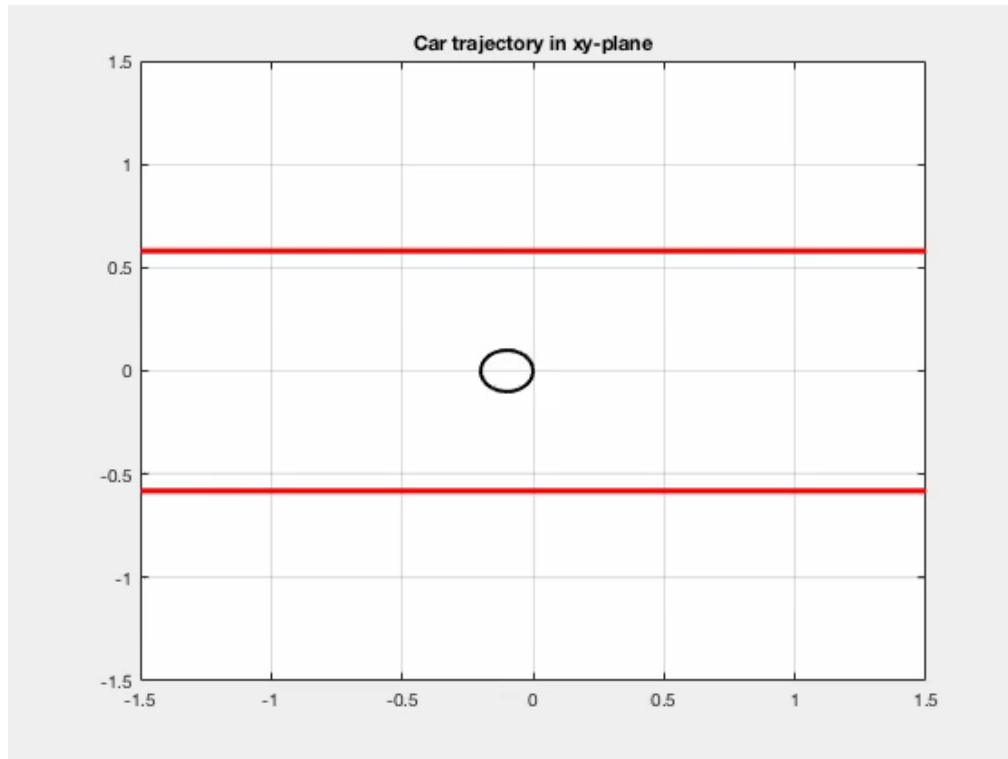


1. Bounding turning angle

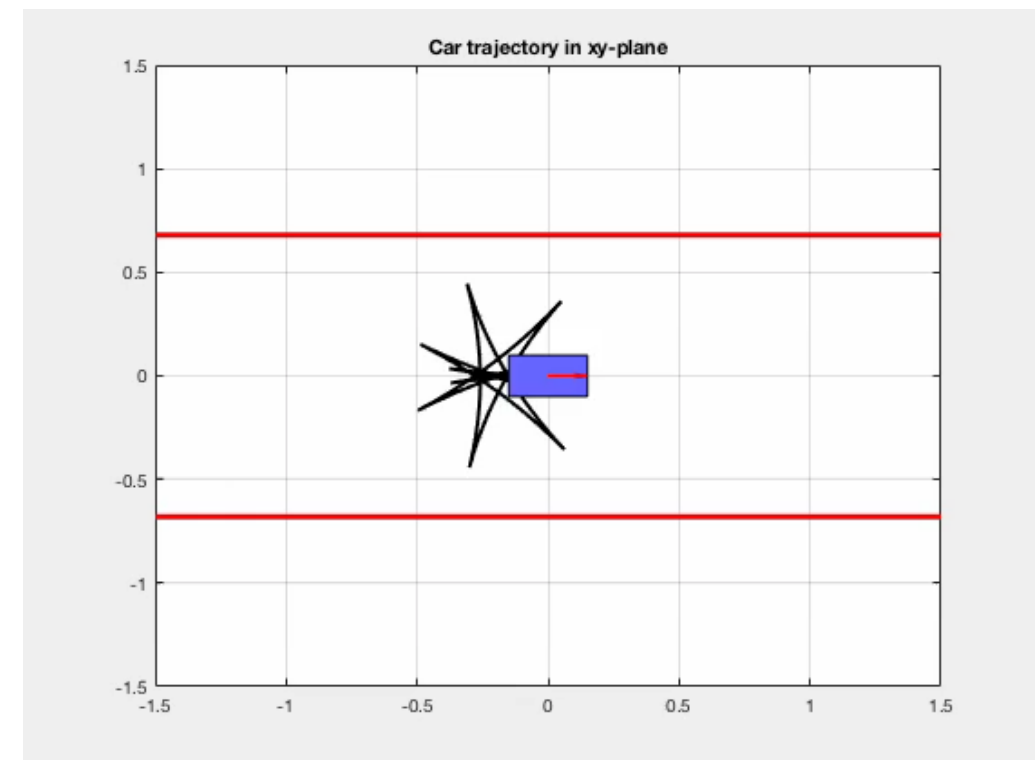
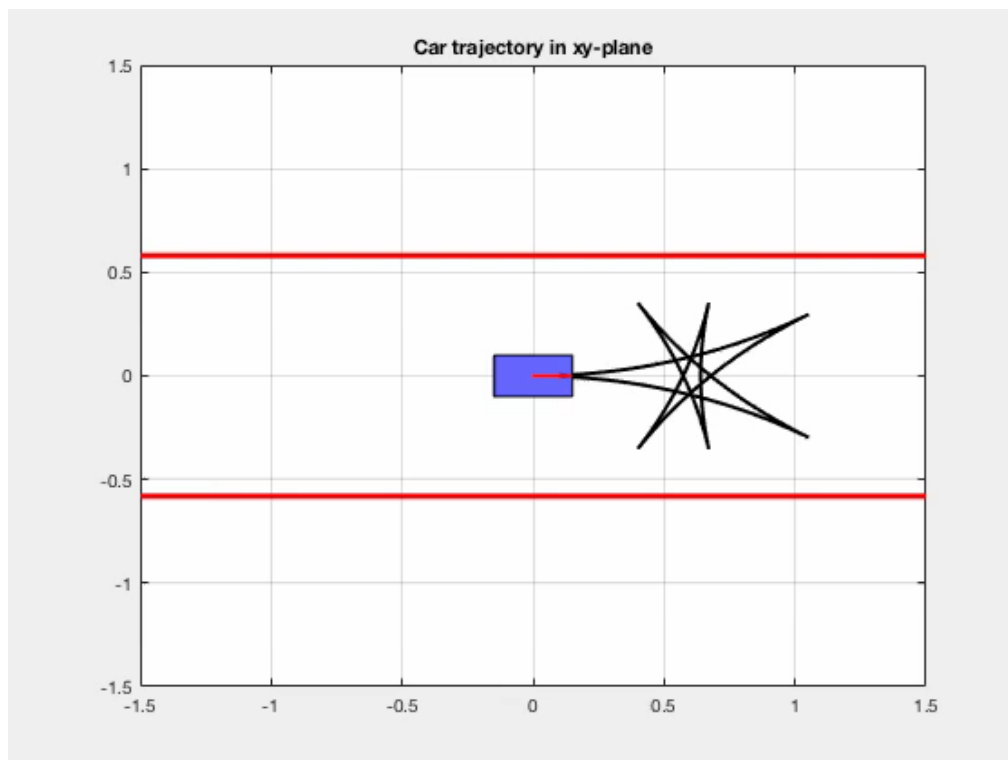
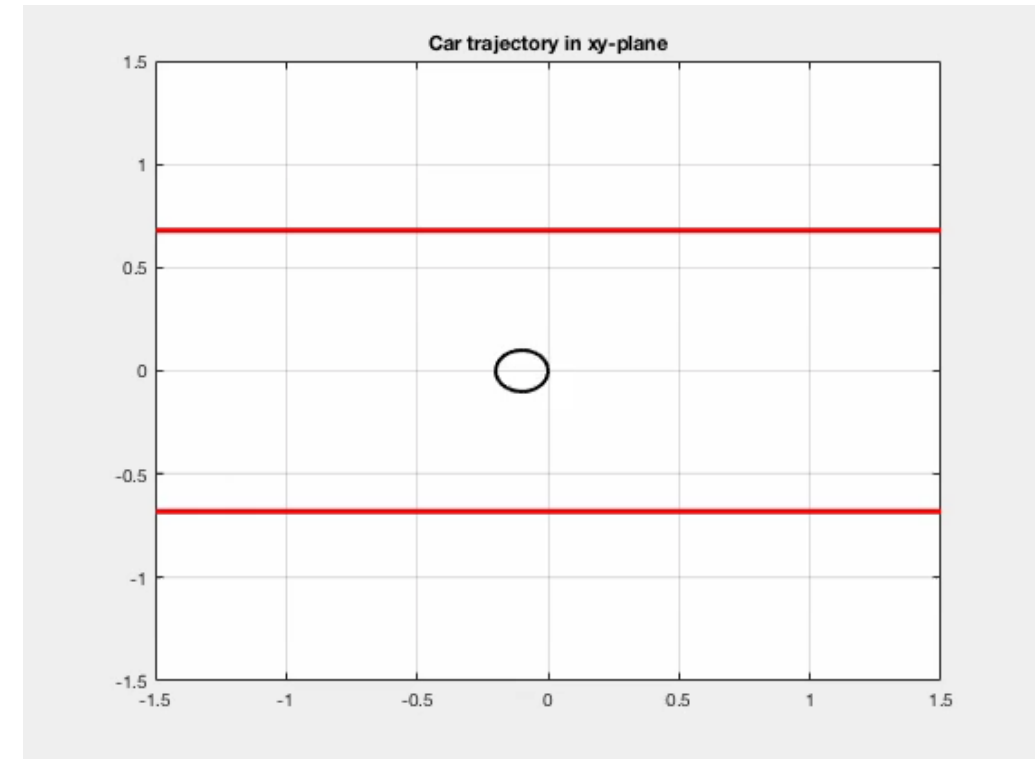


Car maneuvers: 180 turn

1. Smaller turning angle

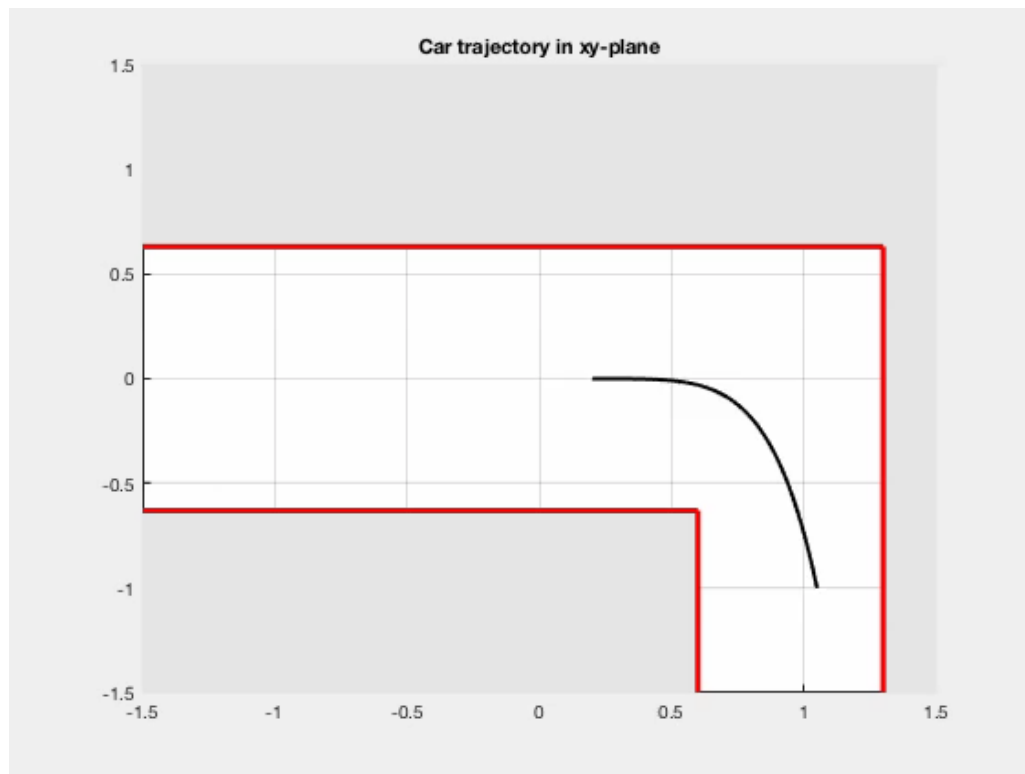


1. Even smaller turning angle

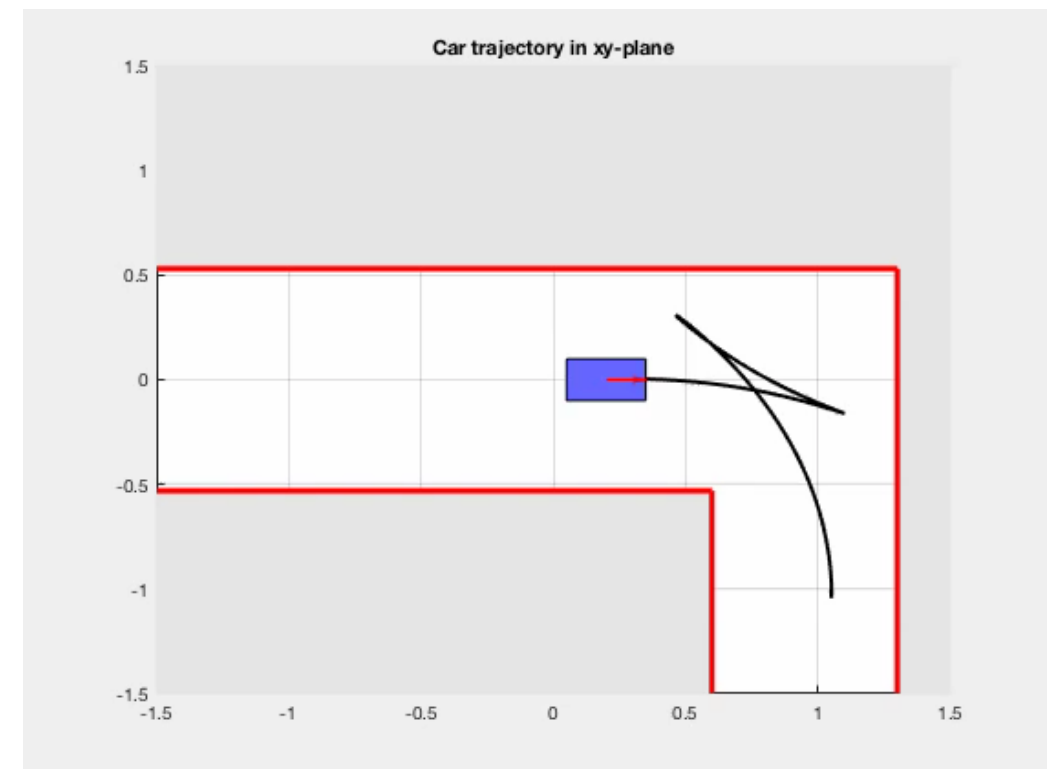
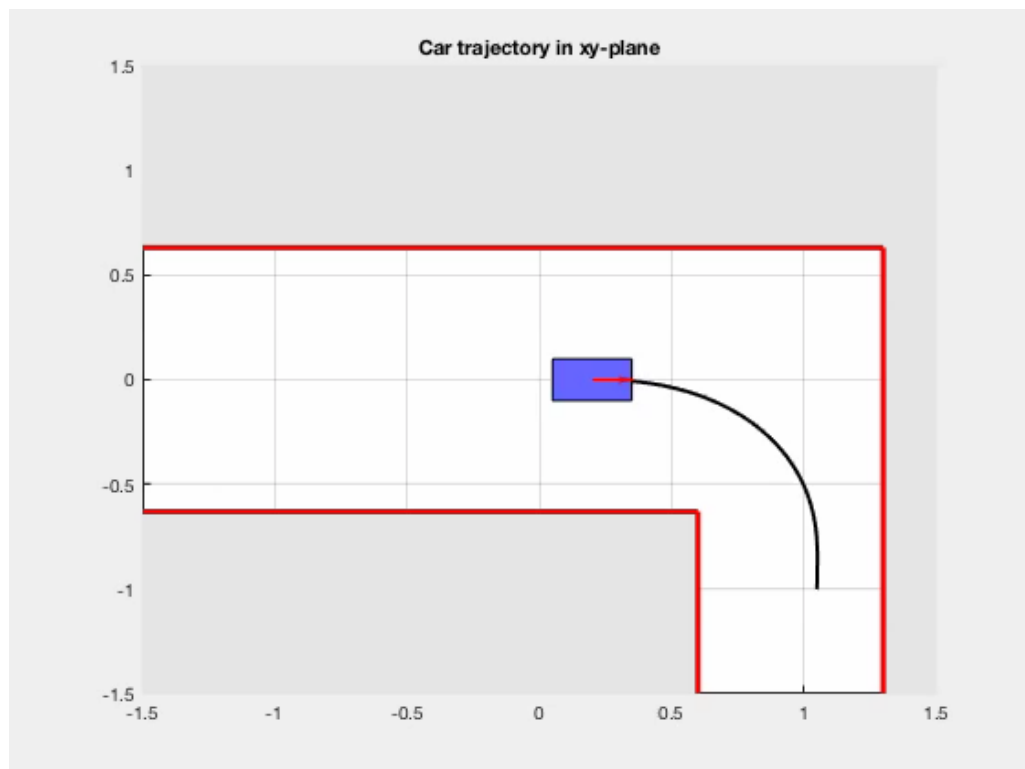
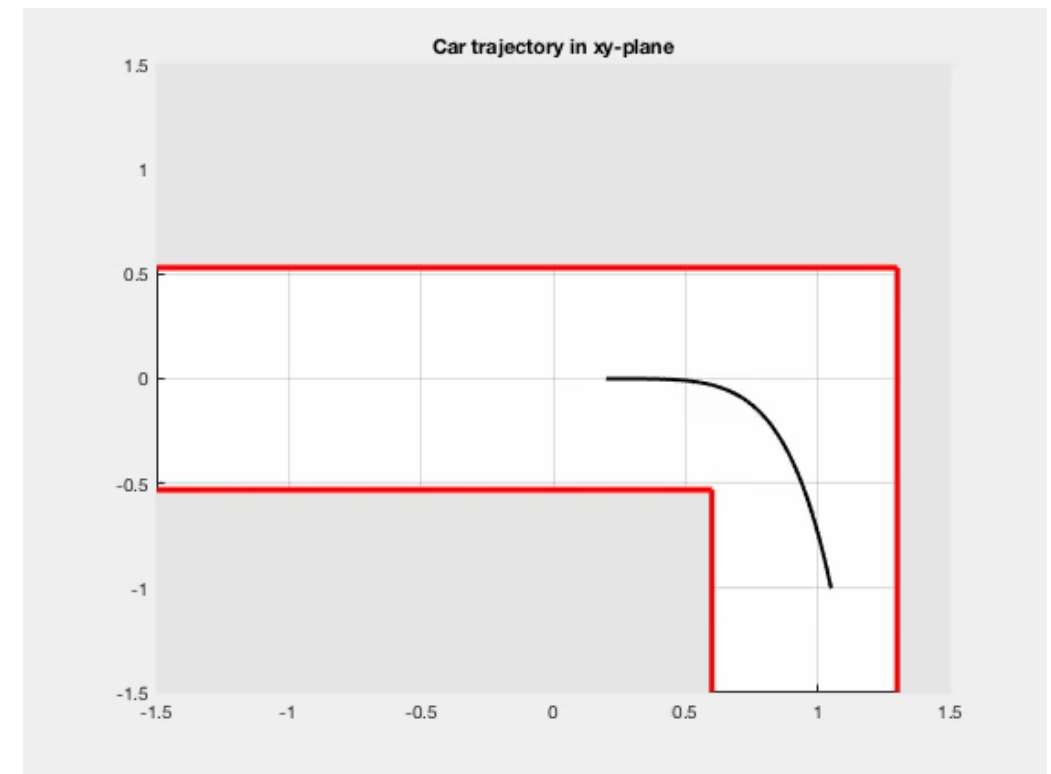


Car maneuvers: 180 turn

1. 90 degree turn



1. bounded turning angle



Car maneuvers: parking lot

This is obtained using **fixed** waypoints

Outline of the presentation

1. Introduction and motivation
2. Presentation of the method
3. Complexity, drift and bounded controls
4. Case study: wheeled vehicles
5. Sketch of proof of convergence

Theoretical guarantee

Set $\Delta = \text{span}\{f_{\text{holo}}\} \cap \text{span}\{f_{\text{nonholo}}\}$.

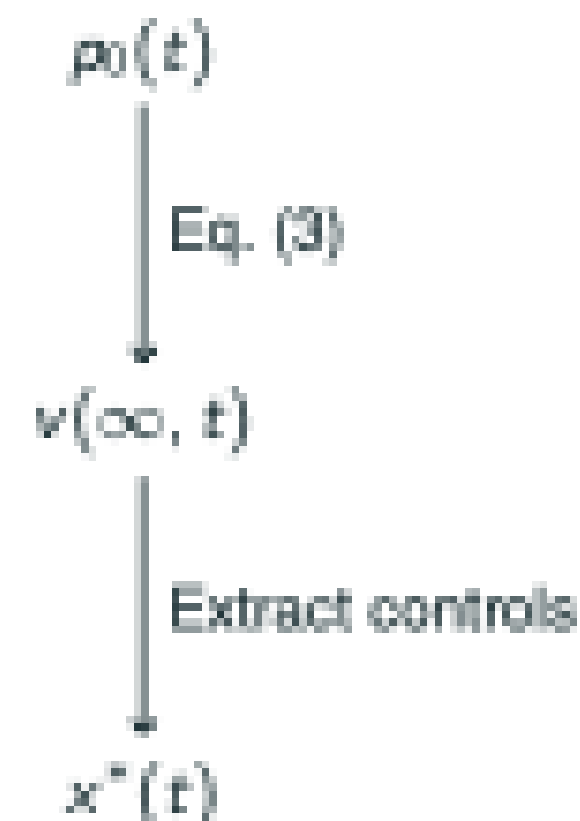
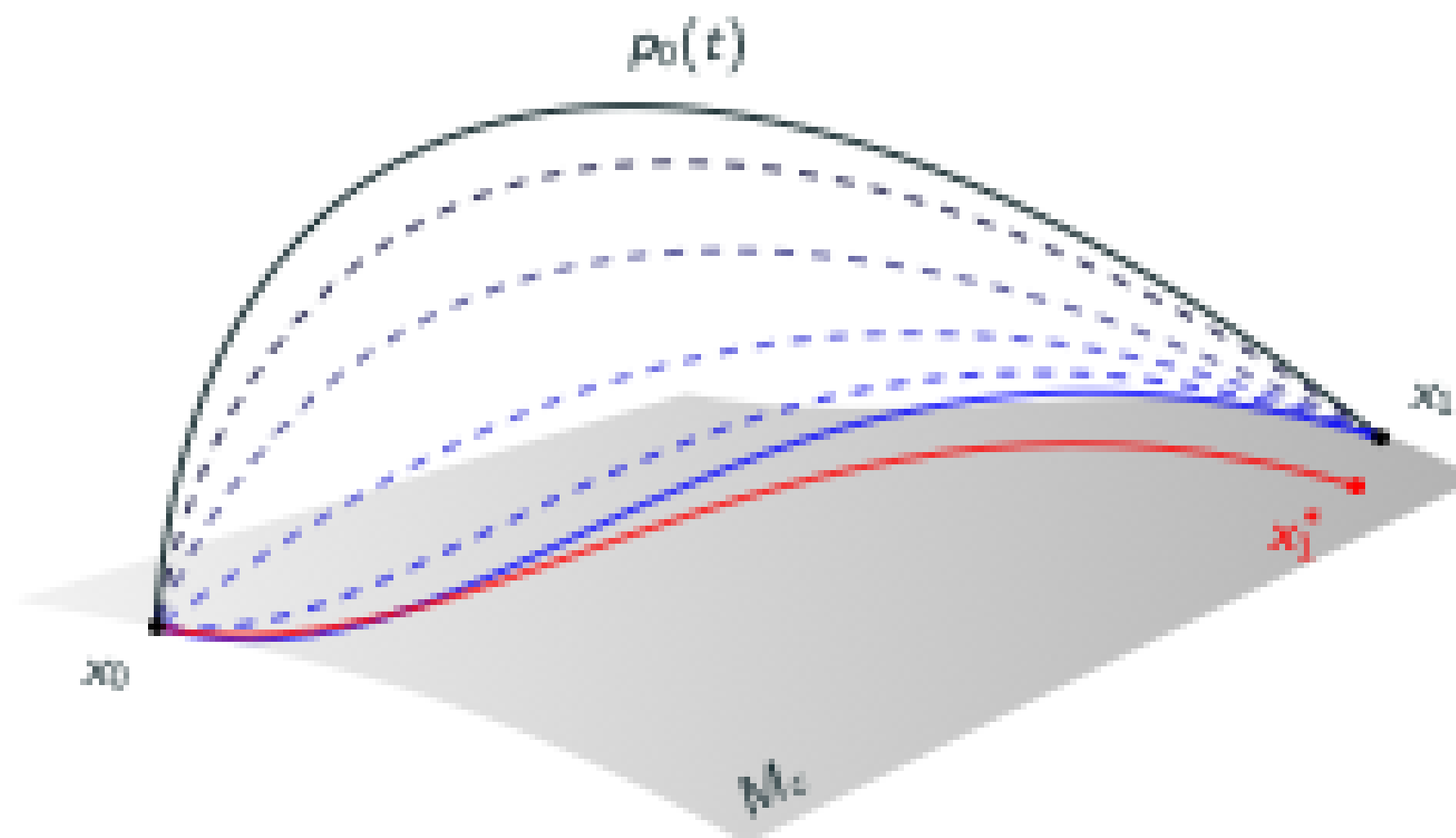
Definition: Constraints are **satisfiable** if the distribution Δ satisfies the LARC.

Theorem

Assume that the constraints are satisfiable and all functions/vector fields are smooth. Then our method provides controls $\bar{u}(t)$ so that the solution $x^*(t)$ of $\dot{x} = \sum_i \bar{u}_i f_i$ has the properties:

1. It satisfies the holonomic and non-holonomic constraints
2. For $\varepsilon > 0$, $\exists k > 0$ such that $\|x^*(1) - x_0\| < \varepsilon$ and all obstacles are avoided.

Theoretical guarantee



- $p_0(t)$: init. curve
- $v(\infty, t)$: sol. of PDE
- $x^*(t)$: system traj.
- M_c : admissible traj.

The trajectory x^* is so that $\|x^*(1) - x_1\| \searrow 0$ as $k \nearrow \infty$.

Sketch of the proof

- Set F_I so that $\text{span}\{F_I\} = \Delta$ and F_c to be the orthogonal complement of F_I .
- Set $p(t) := \lim_{s \rightarrow \infty} v(s, t)$: solution to the PDE (3).
- Define $x(t) := \text{Proj}_\Delta \dot{p}(t)$.
- We can set \bar{u} s.t. $x(t) = F_I(p)\bar{u}$.
- Because $\Delta \subseteq \text{span}\{f_i\}$, there exists $\bar{u}(t)$ so that

$$x(t) = \sum_i \bar{u}_i f_i(p).$$

→ By construction, $x^*(t)$ meets both holonomic and non-holonomic constraints.

- We can express

$$\dot{p} = F_I(p)\bar{u} + F_c(p)u_c$$

Sketch of the proof

- Consider the **energy** of p :

$$\begin{aligned} E(p) &= \int_0^1 \dot{p}(t)^T G(p(t)) \dot{p}(t) dt \\ &= \int_0^1 |F_r(p)^T \tilde{u}(t)|^2 + k |F_c(p)^T u_c(t)|^2 dt \end{aligned}$$

- By Chow-Rashevski, an **admissible trajectory** ending at x_1 exists. Denote it by \bar{p} . Notice that $E(\bar{p})$ is independent of k because $F_c^T \dot{\bar{p}} = 0 \rightarrow E(\bar{p})$ is a finite constant.
- The solution of the PDE minimizes $E(\cdot)$, hence

$$\int_0^1 |F_r(p)^T \tilde{u}(t)|^2 + k |F_c(p)^T u_c(t)|^2 dt = E(p) \leq E(\bar{p})$$

Sketch of the proof

- Without loss of generality with F_f, F_c are normalized, we have

$$\int_0^1 |\tilde{u}(t)|^2 + k|u_c(t)|^2 dt \leq E(\bar{p}),$$

which leads to the **two inequalities**:

$$\int_0^1 |\tilde{u}(t)|^2 dt \leq E(\bar{p}),$$

$$\int_0^1 |u_c(t)|^2 dt \leq \frac{E(\bar{p})}{k}$$

- Define** the error $e(t) := p(t) - x^*(t)$. It satisfies

$$e(0) = 0, \dot{e}(t) = (F_f(p) - F_f(x^*))\tilde{u}(t) + F_c(p)u_c(t)$$

Sketch of the proof

- We can show that F_f is **Lipschitz** with constant L in the domain of interest. Applying Cauchy-Schwartz inequality and Grönwall's lemma,

$$\begin{aligned} |e(t)|^2 &= \left| \int_0^t (F_f(p) - F_c(x^*)) \bar{u}(\tau) + F_c(p) u_c(\tau) d\tau \right|^2 \\ &\leq 2t \int_0^t L^2 |\bar{u}(\tau)|^2 |e(\tau)|^2 d\tau + 2t \int_0^t |u_c(\tau)|^2 d\tau \end{aligned}$$

$$\Rightarrow |e(t)|^2 \leq 2t \int_0^1 |u_c(\tau)|^2 d\tau \exp \left(2tL^2 \int_0^1 |\bar{u}(\tau)|^2 d\tau \right)$$

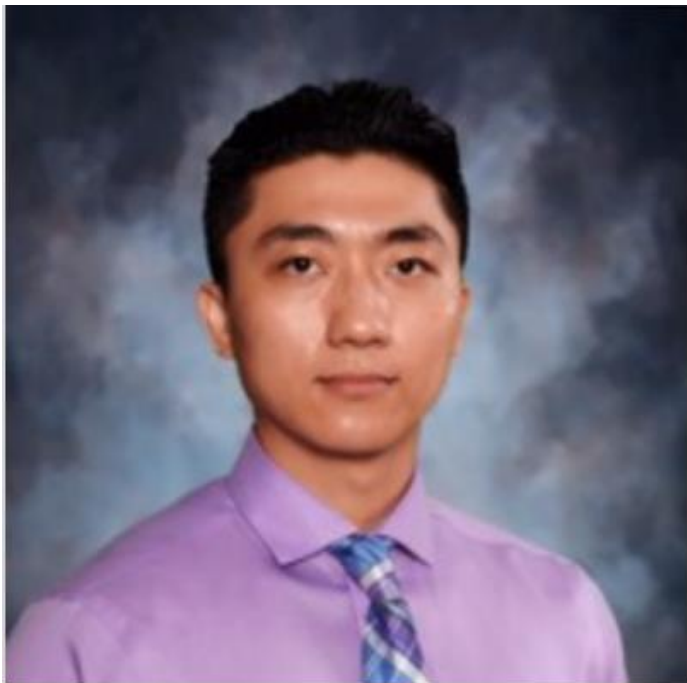
- Plugin the **two inequalities** from previous slide,

$$|e(t)| \leq \sqrt{\frac{2tE(\bar{p})}{k}} e^{L^2 E(\bar{p})}$$

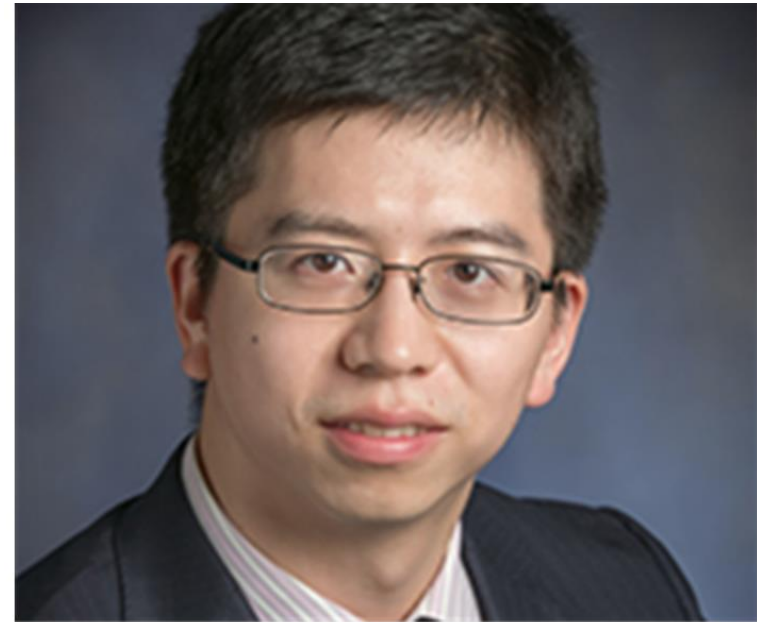
- In particular, $|x^*(1) - x_1| = |e(1)| \leq \sqrt{\frac{2E(\bar{p})}{k}} e^{L^2 E(\bar{p})} \rightarrow 0$ as $k \rightarrow \infty$, meaning we get **arbitrarily close** to x_1 by taking k **sufficiently large**.

Summary and outlook

1. New method for **motion planning** for nonlinear systems
 2. Handles **holonomic/non-holonomic and obstacle** constraints
 3. Provides natural motions
 4. Can plan motion for **multi-vehicles** systems
 5. Theoretical guarantees of convergence are provided
1. Streamline **encoding** of constraints
 2. **Parallelize** GHF solver
 3. Investigate **regularity** properties of solutions
 4. **Ensemble control** and harmonic surfaces



Yinai Fan



Shenyu Liu