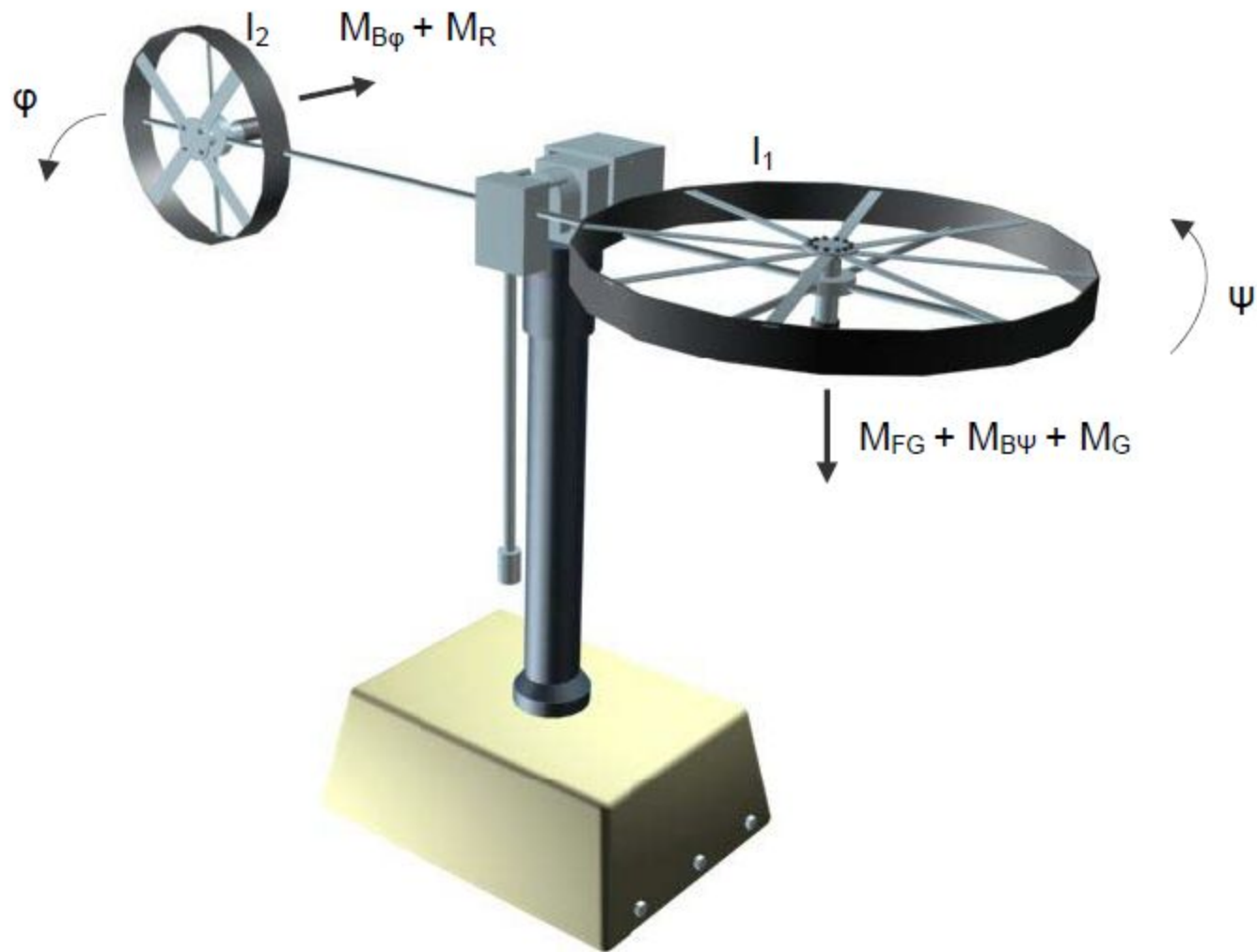


Controle TRMS

Aluno: Matheus Bawden Silverio de Castro
Matricula: 222105990



Características do sistema

- MIMO;
- Não Linear;
- Dependendo da trajetória o sistema muda com o tempo.

Equações:

$$I_1 \cdot \ddot{\psi} = M_1 - M_{FG} - M_{B\psi} - M_G, \quad (1)$$

$$M_1 = a_1 \cdot \tau_1^2 + b_1 \cdot \tau_1, \quad - \text{nonlinear static characteristic} \quad (2)$$

$$M_{FG} = M_g \cdot \sin \psi, \quad - \text{gravity momentum} \quad (3)$$

$$M_{B\psi} = B_{1\psi} \cdot \dot{\psi} + B_{2\psi} \cdot \text{sign}(\dot{\psi}), \quad - \text{friction forces momentum} \quad (4)$$

$$M_G = K_{gy} \cdot M_1 \cdot \dot{\phi} \cdot \cos \psi. \quad - \text{gyroscopic momentum} \quad (5)$$

Equações:

$$I_2 \cdot \ddot{\phi} = M_2 - M_{B\phi} - M_R$$

$$M_2 = a_2 \cdot \tau_2^2 + b_2 \cdot \tau_2, \quad - \text{nonlinear static characteristic}$$

$$M_{B\psi} = B_{1\phi} \cdot \dot{\psi} + B_{2\phi} \cdot \text{sign}(\dot{\phi}), \quad - \text{friction forces momentum}$$

$$\tau_1 = \frac{k_1}{T_{11}s + T_{10}} \cdot u_1.$$

$$\tau_2 = \frac{k_2}{T_{21}s + T_{20}} \cdot u_2.$$

Matriz A e B linearizados na trajetória

$$\begin{aligned}
 & \begin{bmatrix} 0, & 1, & 0, & 0, & 0, & 0; \\ \alpha_1, -B_1P/l_1, & 0, & \alpha_2, & \alpha_3, & 0; \\ 0, & 0, & 0, & 1, & 0, 0; \\ 0, & 0, & 0, & -B_1Y/l_2, & \alpha_4, & \alpha_5; \\ 0, & 0, & 0, & 0, & -T_{10}/T_{11}, & 0; \\ 0, & 0, & 0, & 0, & 0, & -T_{20}/T_{21} \end{bmatrix} B = \begin{bmatrix} 0, & 0; \\ 0, & 0; \\ 0, & 0; \\ k_1/T_{11}, & 0; \\ 0, & k_2/T_{21} \end{bmatrix}
 \end{aligned}$$

$$\alpha_1 = -(2*B_2P*\cos(2*x_1d)*x_4d^2 - K_{gy}*\sin(x_1d)*(a_1*x_5d^2 + b_1*x_5d)*x_4d + M_g*\cos(x_1d))/l_1, -B_1P/l_1;$$

$$\alpha_2 = -(2*B_2P*x_4d*\sin(2*x_1d) + K_{gy}*\cos(x_1d)*(a_1*x_5d^2 + b_1*x_5d))/l_1;$$

$$\alpha_3 = (b_1 + 2*a_1*x_5d - K_{gy}*x_4d*\cos(x_1d)*(b_1 + 2*a_1*x_5d))/l_1;$$

$$\alpha_4 = -(K_c*T_O*(b_1 + 2*a_1*x_5d))/(l_2*T_P);$$

$$\alpha_5 = (b_2 + 2*a_2*x_6d)/l_2;$$

Matrix Ck

$$C = [B(1) A*B - \text{diff}(B(1)) A*B*B - \text{diff}(B(1),2) B(1) A*B - \text{diff}(B(1)) A*B*B - \text{diff}(B(1),2)$$

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[0      0 ,      alpha_1,      1,      0,      0;
 0,      alpha_2,      alpha_3,      0,      0,      alpha_4;
 0,      0,      Alpha_5, 0,0,(k2*(b_2 + 2*a_2*x6d))/(l_2*T21);
 0,      alpha_5,      Alpha_6,      0,      alpha_7, alpha8;
 k1/T11,-(T10*k1)/T11^2,(T10^2*k1)/T11^3,      0,      0,      0;
 0,      0,      0, k2/T21, -(T20*k2)/T21^2,(T20^2*k2)/T21^3
```

Determinante de C

$$\begin{aligned} & (k_1^3 k_2^3 (b_2 + 2a_2 x_6 d)^2 (b_1 + 2a_1 x_5 d \\ & - K_{gy} b_1 x_4 d \cos(x_1 d) \\ & - 2K_{gy} a_1 x_4 d x_5 d \cos(x_1 d))^2) / (I_1^2 I_2^2 T_{11}^3 T_{21}^3) \end{aligned}$$

Existe regiões não controláveis mas no repouso é controlável:

$$k_1^3 k_2^3 (b_2)^2 (b_1) / (I_1^2 I_2^2 T_{11}^3 T_{21}^3)$$

Saidas Planas

$$FO1 = Cte*Psi = Cte*X1$$

$$FO1_1p = Cte*X1$$

$$FO1_2p = a3*X1+b3*X2+c3*X3+d3*X4+e3*X5+f3*X6$$

$$FO1_3p = a4*X1+b4*X2+c4*X3+d4*X4+e4*X5+f4*X6+ g4*U1+h4*U2$$

$$FO2 = Cte*Psi + Cte*Yaw = Cte*X1 + Cte*X3$$

$$FO2_1p = a6*X1+b6*X2+c6*X3+d6*X4+e6*X5+f6*X6$$

$$FO2_2p = a7*X1+b7*X2+c7*X3+d7*X4+e7*X5+f7*X6$$

$$FO2_3p = a8*X1+b8*X2+c8*X3+d8*X4+e8*X5+f8*X6+ g8*U1+h8*U2$$