

# Development of piecewise-polynomial approximation $u(x)$

For a partition  $\Omega$  into a number of elements,  $u$  can be expressed as

$$u_h(x) = \sum_{j=1}^N u_j \phi_j(x), \quad (1)$$

where  $\phi_j(x)$  is associated with the entity indexed by  $j$ .

The finite element bases are constructed so that  $\phi_j(x)$  is nonzero only on elements containing entity  $j$ .

In one dimension, finite element bases are constructed implicitly in an element-by-element manner in terms of “shape function”:

**Piecewise-linear** Lagrange polynomial approximation

$$\phi_j(x) = \begin{cases} \frac{x-x_{j-1}}{x_j-x_{j-1}}, & \text{if } x_{j-1} \leq x < x_j \\ \frac{x_{j+1}-x}{x_{j+1}-x_j}, & \text{if } x_j \leq x < x_{j+1} \\ 0, & \text{otherwise} \end{cases}$$

on the mesh  $x_0 < x_1 < \dots < x_N$

## Piecewise-quadratic Lagrange polynomial approximation

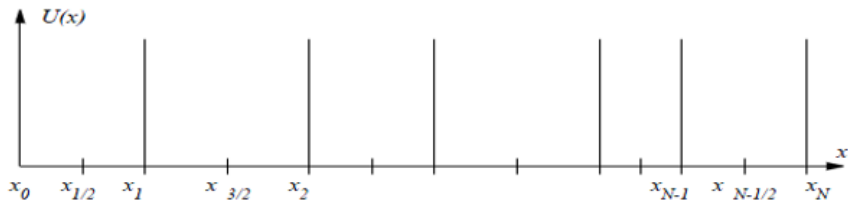
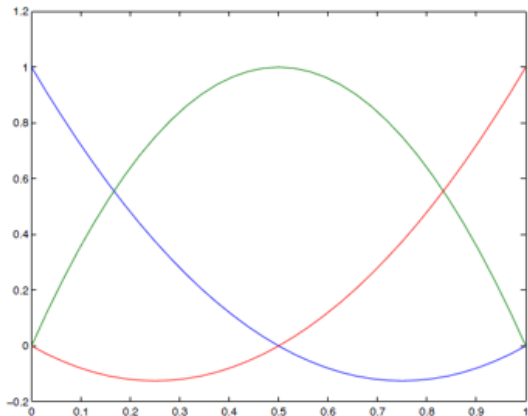


Figure: Quadratic Element

On the element  $\Omega_j = [x_{j-1}, x_j]$ ,

$$\phi_{j-1}(x) = 1 - 3 \left( \frac{x-x_{j-1}}{x_j-x_{j-1}} \right) + 2 \left( \frac{x-x_{j-1}}{x_j-x_{j-1}} \right)^2, \quad \phi_{j-\frac{1}{2}}(x) = 1 - 4 \left( \frac{x-x_{j-\frac{1}{2}}}{x_j-x_{j-1}} \right)^2,$$

$$\phi_j(x) = 1 + 3 \left( \frac{x-x_j}{x_j-x_{j-1}} \right) + 2 \left( \frac{x-x_j}{x_j-x_{j-1}} \right)^2,$$



**Figure:** The three quadratic Lagrangian shape functions on the element  $\Omega_1$  when  $x_{j-1} = 0$ ,  $x_{j-\frac{1}{2}} = 0.5$ ,  $x_j = 1$ .

# 1D Element Transformation

A 1D Lagrange polynomial shape function of degree 1 is constructed on  $\Omega_e$  using two vertex nodes.

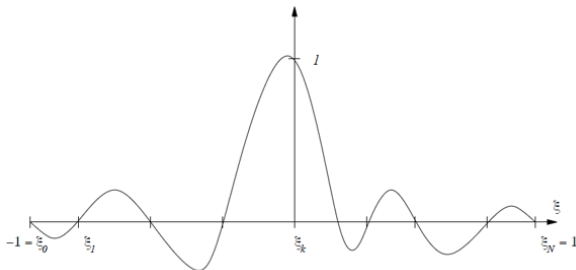
We map an arbitrary element

$$\Omega_e = [x_{j-1}, x_j] \quad \text{onto} \quad -1 \leq \xi \leq 1$$

by the linear transformation

$$T : x = x(\xi) = \frac{1 - \xi}{2} x_{j-1} + \frac{1 + \xi}{2} x_j.$$

A 1D Lagrange polynomial shape function of degree  $p$  is constructed on  $\Omega_e$  using two vertex nodes and  $p - 1$  nodes interior to the element.



**Figure:** An element  $\Omega_e$  used to construct a  $p$ th-degree Lagrangian shape function.

The nodes

$$\xi_0 = -1, \xi_1, \dots, \xi_{p-1}, \xi_p = 1$$

are mapped to the actual physical nodes

$$x_{j-1}, x_{j-1+1/p}, \dots, x_j$$

on an element  $\Omega$

The Lagrangian shape function  $\psi_k$  of degree  $p$  has a unit value at node  $k$  of element and vanishes at all other nodes, thus for  $\ell = 0, 1, \dots, p$

$$\psi_k(\xi_\ell) = \delta_{k\ell} = \begin{cases} 1 & \text{if } k = \ell \\ 0 & \text{otherwise} \end{cases}$$

which implies that

$$\psi_k(\xi) = \frac{(\xi - \xi_0)(\xi - \xi_1) \cdots (\xi - \xi_{k-1})(\xi - \xi_{k+1}) \cdots (\xi - \xi_{k-p})}{(\xi_k - \xi_0)(\xi_k - \xi_1) \cdots (\xi_k - \xi_{k-1})(\xi_k - \xi_{k+1}) \cdots (\xi_k - \xi_{k-p})}.$$

We now have

$$U(\xi) = \sum_{k=1}^p c_k \psi_k(\xi).$$

## Exercise

- Construct the quadratic Lagrange shape function on the master element for  $p=1$ , and

$$\xi_0 = -1, \text{ and } \xi_1 = 1.$$

Find  $\psi_0(\xi)$  and  $\psi_1(\xi)$ .

- Construct the quadratic Lagrange shape function on the master element for  $p=2$ , and

$$\xi_0 = -1, \xi_1 = 0 \text{ and } \xi_2 = 1.$$

Find  $\psi_0(\xi)$ ,  $\psi_1(\xi)$  and  $\psi_2(\xi)$ .



## 2D Element Transformation

Calculation of element matrices in  $x, y$  coordinates is awkward as integration region is complex and limit of integration changes from element to element. If we can find a transformation

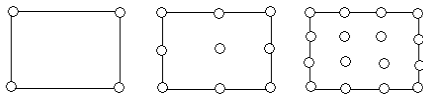
$$T_e : \begin{cases} x = x(\xi, \eta) = \sum_i x_i \psi_i(\xi, \eta) \\ y = y(\xi, \eta) = \sum_i y_i \psi_i(\xi, \eta) \end{cases}$$

which maps an arbitrarily chosen element  $e$  into a standard (master) element  $\bar{\Omega}$ , then the calculation of element matrices can be standardized using numerical quadrature.

# Square element

## Square element

The geometry of the master element is chosen as simple as possible, eg. the square as shown.



**Figure:** Square elements with 4 nodes (linear element), 9 nodes (quadratic element) and 16 nodes (cubic element)

For a linear master element, shape function at node  $i$  is

$$\psi_i(\xi, \eta) = \frac{1}{4}(1 + \xi\xi_i)(1 + \eta\eta_i).$$

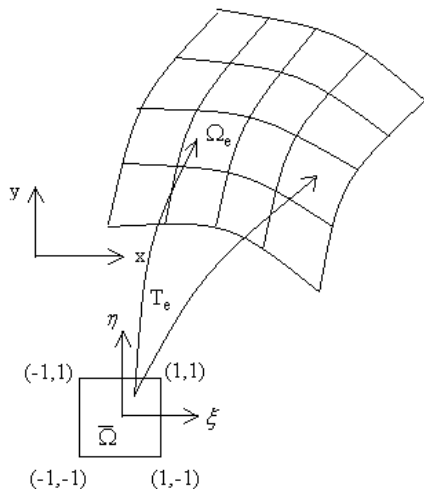
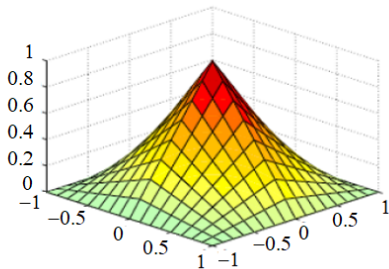
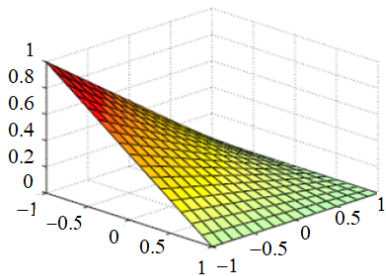
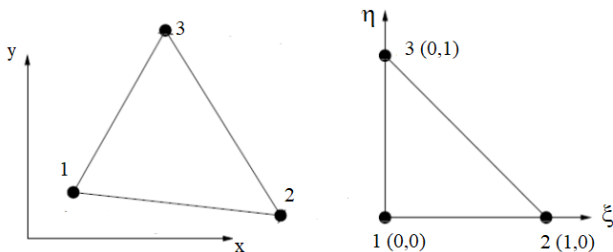


Figure: Square Element transformation  $T_e$



**Figure:** Bilinear shape function  $\psi_1$  (left) and bilinear basis function at the intersection of four square elements (right)

# Triangular element Transformation



For a linear master element, shape function at node  $i$  is

$$T_e : \begin{cases} x = (1 - \xi - \eta)x_1 + \xi x_2 + \eta x_3, \\ y = (1 - \xi - \eta)y_1 + \xi y_2 + \eta y_3 \end{cases}$$

# Triangular element Transformation

$$\xi = \frac{\det \begin{bmatrix} 1 & x & y \\ 1 & x_1 & y_1 \\ 1 & x_3 & y_3 \end{bmatrix}}{\det \begin{bmatrix} 1 & x_2 & y_2 \\ 1 & x_1 & y_1 \\ 1 & x_3 & y_3 \end{bmatrix}}, \quad \eta = \frac{\det \begin{bmatrix} 1 & x & y \\ 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \end{bmatrix}}{\det \begin{bmatrix} 1 & x_3 & y_3 \\ 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \end{bmatrix}}.$$

As a check, evaluate the determinants and verify that

$$(x_1, y_1) \rightarrow (0, 0),$$

$$(x_2, y_2) \rightarrow (1, 0),$$

$$(x_3, y_3) \rightarrow (0, 1).$$

# Element Calculation

- A point  $P(\xi = \alpha, \eta = \beta)$  in the standard element  $\bar{\Omega}$  is mapped into a point

$$P[x(\alpha, \beta), y(\alpha, \beta)]$$

in local element  $\Omega_e$ .

- A line ( $\xi = \alpha$ ) in  $\bar{\Omega}$  is mapped into a curve

$$[x = x(\alpha, \eta), y = y(\alpha, \eta)]$$

in the plane, which is called the curvilinear coordinate line ( $\xi = \alpha$ ).

# Element Calculation

- A finite element mesh can be viewed as a sequence of transformation  $\{T_1, T_2, \dots, T_E\}$  of the fixed master element. Each element  $\Omega_e$  is the image of the master element  $\bar{\Omega}$  under a coordinate map  $T_e$ .
- All properties of a given type of elements (number and location of nodes, shape functions, stiffness and etc) can be prescribed for the fixed element  $\bar{\Omega}$ , and then carried to any  $\Omega_e$  in the mesh by using the map  $T_e$ .



Relations between  $dx$ ,  $dy$  with  $d\xi$  and  $d\eta$

Suppose  $x(\xi, \eta)$  and  $y(\xi, \eta)$  are continuously differentiable, then

$$dx = \frac{\partial x}{\partial \xi} d\xi + \frac{\partial x}{\partial \eta} d\eta \text{ and}$$

$$dy = \frac{\partial y}{\partial \xi} d\xi + \frac{\partial y}{\partial \eta} d\eta$$

$$\text{or} \quad \begin{bmatrix} dx \\ dy \end{bmatrix} = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial x}{\partial \eta} \\ \frac{\partial y}{\partial \xi} & \frac{\partial y}{\partial \eta} \end{bmatrix} \begin{bmatrix} d\xi \\ d\eta \end{bmatrix} = J \begin{bmatrix} d\xi \\ d\eta \end{bmatrix}, \quad (2)$$

where  $J$  = Jacobian matrix of the transformation.

# Properties of Coordinate Transformation

If at point  $(\xi, \eta)$  we have  $|J| = \det(J) \neq 0$   
then an inverse map  $T_e^{-1}(x, y \rightarrow \xi, \eta)$  exists at this point and thus

$$\begin{bmatrix} d\xi \\ d\eta \end{bmatrix} = J^{-1} \begin{bmatrix} dx \\ dy \end{bmatrix} \quad (3)$$

and

$$T_e^{-1} : \begin{array}{l} \xi = \xi(x, y) \\ \eta = \eta(x, y) \end{array} \quad (4)$$

defines a map  $(x, y) \rightarrow (\xi, \eta)$ .

# Element Calculation

As in (2), we have

$$\begin{bmatrix} d\xi \\ d\eta \end{bmatrix} = \begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \xi}{\partial y} \\ \frac{\partial \eta}{\partial x} & \frac{\partial \eta}{\partial y} \end{bmatrix} \begin{bmatrix} dx \\ dy \end{bmatrix}. \quad (5)$$

Hence, by equating terms in (5) and (3), we have the following relations

$$\frac{\partial \xi}{\partial x} = \frac{1}{|J|} \frac{\partial y}{\partial \eta}, \quad \frac{\partial \xi}{\partial y} = -\frac{1}{|J|} \frac{\partial x}{\partial \eta}, \quad \frac{\partial \eta}{\partial x} = -\frac{1}{|J|} \frac{\partial y}{\partial \xi}, \quad \frac{\partial \eta}{\partial y} = \frac{1}{|J|} \frac{\partial x}{\partial \xi} \quad (6)$$

### (3) Construction of the Transformations $T_e$

#### Criteria for selection of $T_e$

- (i) Within  $\Omega_e$ ,  $\xi(x, y)$  and  $\eta(x, y)$  must be invertible and continuously differentiable.
- (ii)  $\{T_e\}_{e=1}^E$  must generate a mesh with no spurious gaps between elements and with no element overlapping another.
- (iii)  $T_e$  should be easy to construct from the geometric data of the element.

### (3) Construction of the Transformations $T_e$

#### Construction of $T_e$

The transformation  $T_e$  is constructed based on the element shape functions.

Let  $\psi_j$  be the shape function defined on  $\bar{\Omega}$  for  $j = 1, 2, \dots, N$ , where  $N$  is the total number of nodes in  $\bar{\Omega}$ .

Then, any function  $g = g(\xi, \eta)$  in  $\bar{\Omega}$  can be approximated by

$$\bar{g}(\xi, \eta) = \sum g_j \psi_j(\xi, \eta). \quad (7)$$

### (3) Construction of the Transformations $T_e$

Let  $g = x$  and  $g = y$  respectively, from (7) we have

$$\begin{aligned} T_e : \quad x &= \sum_{j=1}^N x_j \psi_j(\xi, \eta), \\ y &= \sum_{j=1}^N y_j \psi_j(\xi, \eta), \end{aligned} \tag{8}$$

which maps  $\bar{\Omega}$  to  $\Omega_e$ . To see this, consider a node  $i$  in  $\bar{\Omega}$ , the coordinates is  $(\xi_i, \eta_i)$ . From (8), this point is mapped into point  $x = x_i$ ,  $y = y_i$  in the  $x - y$  plane i.e, node  $i$ .

## Remark

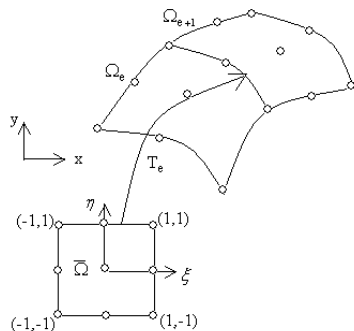
- 1) Criterion (iii) is easily verified.  $T_e$  is readily constructed from element data  $(x_i, y_i, \dots)$ .
- 2) Criterion (ii) is usually not difficult to satisfy.
- 3) For  $T_e$  to be invertible, we require  $\det(J) \neq 0$ . In addition, from the integration theory,

$$dx dy = |J| d\xi d\eta.$$

Clearly, for the mapping defined by (4) to be acceptable, we must have positive values of  $|J|$  at all points in  $\bar{\Omega}$ . The satisfaction of this condition is not assured in general for all maps of the form (8). Each set of shape functions must be examined to ensure that  $|J| > 0$  throughout  $\bar{\Omega}$ .

## Straight sides of $\bar{\Omega}$ map to curved sides of $\Omega_e$

The quadratic shape function on the master square maps the element to the corresponding elements  $\Omega_e$  in the  $x - y$  plane in such a way that straight sides of the  $\bar{\Omega}$  are mapped to quadratic curved sides of  $\Omega_e$ . On a given curved side between  $\Omega_e$  and  $\Omega_{e+1}$ , the maps  $T_e$  and  $T_{e+1}$  reduce to the same quadratic functions.



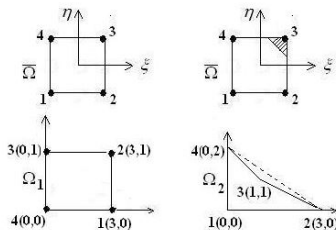


## Example

The following figure shows a 4-node master element  $\bar{\Omega}$  and 2 elements  $\Omega_1$  and  $\Omega_2$  generated from it using the map (8). The shape function defined on  $\bar{\Omega}$  are

$$\psi_i = \frac{1}{4}(1 + \xi\xi_i)(1 + \eta\eta_i), \quad (i = 1, \dots, 4)$$

where  $(\xi_i, \eta_i)$  are coordinates of node  $i$ .



## Element Calculation

In this example, straight lines  $\xi = \text{constant}$  or  $\eta = \text{constant}$  in  $\bar{\Omega}$  map to corresponding straight lines in  $\Omega_e$ .

For  $\Omega_1$

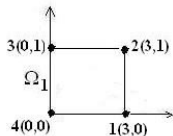
$$x = 3\psi_1 + 3\psi_2 + (0)\psi_3 + (0)\psi_4 = \frac{3}{2}(1 - \eta)$$

$T_e$  :

$$y = \psi_2 + \psi_3 = \frac{1}{2}(1 + \xi).$$

$$|J| = \det \begin{bmatrix} 0 & -\frac{3}{2} \\ \frac{1}{2} & 0 \end{bmatrix} = \frac{3}{4} > 0$$

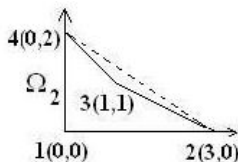
Therefore, the map is invertible.



# Element Calculation

For  $\Omega_2$

$$|J| = \frac{1}{8}(5-3\xi-4\eta) \quad \left\{ \begin{array}{l} = 0 \text{ along } L : \xi = \frac{5}{3} - \frac{4}{3}\eta \\ > 0 \text{ below } L \\ < 0 \text{ above } L. \end{array} \right.$$



The region above  $L$  is mapped outside of  $\Omega_2$  by  $T_2$ . Clearly,  $\Omega_2$  is unacceptable.

# Finite Element Calculations

The key to the finite element approximation is the calculation of the element matrices for each element in the mesh. To calculate the following integrals

$$k_{ij}^e = \int_{\Omega_e} \left[ k \left( \frac{\partial \phi_i}{\partial x} \frac{\partial \phi_j}{\partial x} + \frac{\partial \phi_i}{\partial y} \frac{\partial \phi_j}{\partial y} \right) + b \phi_i \phi_j \right] dx dy,$$
$$f_i^e = \int_{\Omega_e} f \phi_i dx dy, \tag{9}$$

$$p_i^e = \int_{\partial \Omega_{2e}} p \phi_i \phi_j ds,$$

and

$$\gamma_i^e = \int_{\partial \Omega_{2e}} P \hat{u} \phi_i ds,$$

we begin by choosing the master element  $\bar{\Omega}$  with geometry as simple as possible, such as square.

# Finite Element Calculation

For a chosen  $\Omega$ , we need to

- identify  $M$  nodes and shape function  $\varphi$  to define the coordinates map  $T_e$ ,
- identify  $N$  nodes and shape function  $\bar{\varphi}$  for local approximation of the unknown function.

**Remarks:**  $M$  and  $N$  need not to be the same.

- If  $M > N_e$ , then it is super-parametric map.
- If  $M = N_e$ , then it is iso-parametric map (iso-parametric element).
- If  $M < N_e$ , then it is sub-parametric map.

# Element Calculation

In the following, we will consider only the iso-parametric element. Having selected  $\bar{\Omega}$  and  $\varphi_j$ , we perform the following steps:

## (1) Element map

$$\begin{aligned} T_e : \quad x &= \sum_{j=1}^N x_j \psi_j(\xi, \eta) \\ y &= \sum_{j=1}^N y_j \psi_j(\xi, \eta) \end{aligned} \quad (10)$$

## Transformation of shape functions

As  $T_e$  is invertible,  $\xi = \xi(x, y)$ ,  $\eta = \eta(x, y)$  and the element shape functions are

$$\phi_j(x, y) = \psi_j[\xi(x, y), \eta(x, y)] \quad (11)$$

Therefore,

$$\frac{\partial \phi_j}{\partial x} = \frac{\partial \psi_j}{\partial \xi} \frac{\partial \xi}{\partial x} + \frac{\partial \psi_j}{\partial \eta} \frac{\partial \eta}{\partial x}, \quad \frac{\partial \phi_j}{\partial y} = \frac{\partial \psi_j}{\partial \xi} \frac{\partial \xi}{\partial y} + \frac{\partial \psi_j}{\partial \eta} \frac{\partial \eta}{\partial y}.$$

# Transformation of shape functions

According to (10)

$$\frac{\partial x}{\partial \xi} = \sum_1^{N_e} x_k \frac{\partial \psi_k}{\partial \xi}(\xi, \eta), \quad \frac{\partial x}{\partial \eta} = \sum_1^{N_e} x_k \frac{\partial \psi_k}{\partial \eta}(\xi, \eta),$$

$$\frac{\partial y}{\partial \xi} = \sum_1^{N_e} y_k \frac{\partial \psi_k}{\partial \xi}(\xi, \eta), \quad \frac{\partial y}{\partial \eta} = \sum_1^{N_e} y_k \frac{\partial \psi_k}{\partial \eta}(\xi, \eta),$$

Thus, using (6) and (10), equation (11) becomes

$$\frac{\partial \phi_j}{\partial x} = \frac{1}{|J|} \left\{ \frac{\partial \psi_j}{\partial \xi} \sum_{k=1}^N y_k \frac{\partial \psi_k}{\partial \eta}(\xi, \eta) - \frac{\partial \psi_j}{\partial \eta} \sum_{k=1}^N y_k \frac{\partial \psi_k}{\partial \xi}(\xi, \eta) \right\}$$

$$\frac{\partial \phi_j}{\partial y} = \frac{1}{|J|} \left\{ \frac{\partial \psi_j}{\partial \xi} \sum_{k=1}^N x_k \frac{\partial \psi_k}{\partial \eta}(\xi, \eta) - \frac{\partial \psi_j}{\partial \eta} \sum_{k=1}^N x_k \frac{\partial \psi_k}{\partial \xi}(\xi, \eta) \right\}$$

## Remarks

- (a) The partial derivatives of  $\phi_j$  w.r.t.  $x$  and  $y$  are completely determined by calculation defined only on  $\bar{\Omega}$ .
- (b) From (9), for 4-node element,  $K^e$  is a  $4 \times 4$  matrix which can be expressed as

$$K^e = \int_{\Omega_e} (k(D\phi)^T (D\phi) + b\phi^T \phi) d\Omega \quad (12)$$

where  $\phi = (\phi_1, \phi_2, \phi_3, \phi_4)$  and

$$D\phi = \begin{bmatrix} \frac{\partial \phi_1}{\partial x} & \frac{\partial \phi_2}{\partial x} & \frac{\partial \phi_3}{\partial x} & \frac{\partial \phi_4}{\partial x} \\ \frac{\partial \phi_1}{\partial y} & \frac{\partial \phi_2}{\partial y} & \frac{\partial \phi_3}{\partial y} & \frac{\partial \phi_4}{\partial y} \end{bmatrix}.$$



# Integration

Let  $I = \int_{\Omega_e} g(x, y) \, dx dy$

then  $I = \int_{\bar{\Omega}} G(\xi, \eta) \, d\xi d\eta$ ,

where

$$G(\xi, \eta) = g\left(\sum_1^N x_j \psi_j(\xi, \eta), \sum_1^N y_j \psi_j(\xi, \eta)\right) |J(\xi, \eta)| \quad (13)$$

Numerical quadrature (such as the Gaussian quadrature) are usually used to evaluate the integrals. Quadrature rules for quadrilateral elements are usually derived from the 1-D quadrature by treating the integration over  $\bar{\Omega}$  as a double integral.

Thus, using the 1-D quadrature rule of order N,

$$I = \int_{\bar{\Omega}} G(\xi, \eta) d\xi d\eta = \int_{-1}^1 \left[ \int_{-1}^1 G(\xi, \eta) d\xi \right] d\eta \approx \sum_{k=1}^N \left[ \sum_{\ell=1}^N G(\xi_{\ell}, \eta_k) w_{\ell} \right] w_k$$

# Integration

For 9-point Gaussian quadrature ( 1-D of order 3).

$$N = 3, \quad w_1 = 5/9, \quad w_2 = 8/9, \quad w_3 = 5/9,$$

$$\xi_1 = \eta_1 = -\sqrt{3/5}, \quad \xi_2 = \eta_2 = 0, \quad \xi_3 = \eta_3 = \sqrt{3/5}.$$

If  $k = k(x, y)$ ,  $b = b(x, y)$  and  $f = f(x, y)$  are not constant over an element, we may use

$$k(x, y) \approx \sum_{j=1}^N k_j \phi_j(x, y), \quad b(x, y) \approx \sum_{j=1}^N b_j \phi_j(x, y), \quad f(x, y) \approx \sum_{j=1}^N f_j \phi_j(x, y).$$

Then the calculations of  $a_{ij}^e$  and  $f_i^e$  only require the nodal values of  $k$ ,  $b$  and  $f$ .

# Boundary Integrals

The calculation of the boundary integrals in (9) is carried out by integrating along those sides of  $\bar{\Omega}$  that are mapped onto the sides of  $\partial\Omega_{2e}$  along which natural boundary conditions are prescribed.

For definiteness, we suppose that the sides  $\xi = 1$  of a master square is to be mapped onto  $\partial\Omega_{2h}$ . Let  $\theta_j$  denote the restriction of the master-element shape function  $\psi_j$  to side  $\xi = 1$ , i.e.,

$$\theta_j(\eta) = \psi_j(1, \eta), \quad j = 1, 2, \dots, N.$$

We thus have

$$\int_{\partial\Omega_{2e}} p \phi_i \phi_j \, ds = \int_{-1}^1 p \theta_i(\eta) \theta_j(\eta) |J| \, d\eta$$

# Integration

Since

$$ds = \sqrt{\left(\frac{\partial x}{\partial \eta}(1, \eta)\right)^2 + \left(\frac{\partial y}{\partial \eta}(1, \eta)\right)^2} d\eta,$$

we have

$$|J(\eta)| = \sqrt{\left(\frac{\partial x}{\partial \eta}(1, \eta)\right)^2 + \left(\frac{\partial y}{\partial \eta}(1, \eta)\right)^2}$$

where  $x(\xi, \eta)$  and  $y(\xi, \eta)$  are defined in (10). The integral can be evaluated numerically.

## Example

Let  $\Omega$  be a square region, consider

$$\left\{ \begin{array}{ll} \nabla \cdot k(x) \nabla T + Q = 0 & \text{on } \Omega \\ T = x & \text{on } y = 0 \\ T = 3 + x^2 & \text{on } y = 3 \\ T = y & \text{on } x = 0 \\ \frac{\partial T}{\partial x} = 1 - 0.2T & \text{on } x = 3 \end{array} \right.$$

# Finite Element mesh

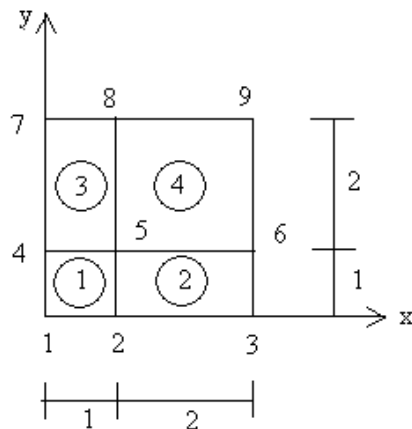


Figure: Finite element mesh

# Variational Statement

Find  $T \in H^1(\Omega)$  such that  $T = x$  on  $y = 0$ ,  $T = 3 + x^2$  on  $y = 3$ ,  $T = y$  on  $x = 0$  and

$$a(T, v) = L(v), \quad \forall v \in H_0^1(\Omega)$$

where  $H_0^1(\Omega) = \{v : v \in H^1(\Omega) \text{ and } v = 0 \text{ on } x = 0, y = 0 \text{ and } y = 3\}$

$$a(T, v) = \int_0^3 0.2 T(3, y) v(3, y) dy + \int_{\Omega} \nabla T \cdot \nabla v d\Omega$$

$$L(v) = \int_0^3 v(3, y) dy + \int_{\Omega} 2v d\Omega$$

# Variational Statement

Finite element equations is a system

$$\mathbf{AT} = \mathbf{F},$$

where

$$\mathbf{A} = \{a_{ij}\}, \text{ with } a_{ij} = \sum_{e=1}^E \int_{\Omega_e} \nabla \phi_i \cdot \nabla \phi_j \, d\Omega + \sum_{e=1}^B \int_{\partial\Omega_e} 0.2 \phi_i \phi_j \, dy$$

$$\mathbf{F} = \{f_i\} \text{ with } f_i = \sum_{e=1}^E \int_{\Omega_e} 2\phi_i \, d\Omega + \sum_{e=1}^B \int_{\partial\Omega_e} \phi_i \, dy,$$

$B$  is the number of elements with natural boundary condition.



# Solution of Sparse Systems of Linear Equations

This chapter concerns with a unique solution of the finite element linear system

$$\mathbf{Ax} = \mathbf{b}, \quad (14)$$

where

- the  $n \times n$  matrix  $\mathbf{A}$  is large, sparse, and symmetric,
- $\mathbf{b}$  and  $\mathbf{x}$  are both  $n \times m$  ( $m \geq 1$ ) matrices.

# Positive - Definite Systems

For a positive-definite matrix  $\mathbf{A}$

- Gauss elimination process can be performed without row interchange and the computation is stable wrt growth of rounding error.
- $\text{LDL}^T$  factorization method can be used to solve the system

$$\mathbf{Ax} = \mathbf{b}$$

Note: An  $n \times n$  matrix  $A$  with real entries is called positive definite if

$$\mathbf{x}^T \mathbf{Ax} > 0.$$

In FEM, the nonzero entries of  $A$  are often clustered in a small number of diagonals surrounding the main diagonal. Thus, we can use special techniques to improve computation efficiency by avoiding operating involving zero operands, and reduce storage requirement.

# Positive - Definite Systems

The algorithm is follows:

*Factorization* :  $d_1 = a_{11}$

*For*  $i=1,2,\dots,n$

$$\ell_{ij} = \frac{1}{d_j} [a_{ij} - \sum_{k=1}^{j-1} \ell_{ik} \ell_{jk} d_k], \quad j = 1, 2, \dots, i-1$$

$$d_i = a_{ii} - \sum_{k=1}^{i-1} \ell_{ik}^2 d_k$$

*substitution* : *For*  $i=1,\dots,n$

$$y_i = n_i - \sum_{k=1}^{i-1} \ell_{ik} y_k$$

*For*  $i=n,n-2,\dots,1$

$$x_i = \frac{y_i}{d_i} - \sum_{k=i+1}^n \ell_{ki} x_k$$

# Band Methods

Let  $m_A$  be the smallest integer such that  $a_{ij} = 0$  for  $|i - j| > m_A$ , then

- the portion of  $A$  containing exactly those entries  $a_{ij}$  satisfying  $|i - j| \leq m_A$  called the band of  $A$ ,
- $m_A$  is called the bandwidth by storing mainly the nonzero entries.

In the  $LDL^T$  method, none of the entries of the matrix  $A$  can ever be nonzero unless  $|i - j| \leq m_A$ . This fact can be used to modify the algorithm, so that only the entries of the band are ever used.

# Algorithm

LDL<sup>T</sup>:  $d_1 = a_{11}$

For  $i = 2, \dots, n$

$$\ell_{ij} = \frac{1}{d_j} \left[ a_{ij} - \sum_{k=\max(i-m_A, j-m_A)}^{j-1} \ell_{ik} \ell_{jk} d_k \right], \quad j = 1, 2, \dots,$$

$$d_i = a_{ii} - \sum_{k=i-m_A}^{i-1} \ell_{ik}^2 d_k$$

Subst:  $y_i = b_i - \sum_{k=i-m_A}^{i-1} \ell_{ik} y_k, \quad i = 1, \dots, N$

$$y_i = \frac{y_i}{d_i} - \sum_{k=i+1}^{\min(i+m_A, n)} \ell_{ki} x_k, \quad i = n, n-1, \dots, 1.$$

## Remarks:

Let  $m_i$  be the smallest integer such that

$$a_{ij} = 0 \quad (j < i) \quad \text{if} \quad i - j > m \text{ (or } j < i - m)$$

. It can be shown that, the algorithm for such problem is similar to the one above. Except for the backward substitution formula, we can replace

- $i \pm m_A$  by  $i \pm m_i$
- $j \pm m_A$  by  $j \pm m_j$ .

# Storage Structure

Rules:

- a) Store the matrix  $A_{n \times n}$  row by row into a one-dimensional array  $A1$ .
- b) For each row, store the elements from the 1st nonzero entry to the diagonal element.
  - Use  $IA(i)_{i=1 \text{ to } N}$  to identify the storage location of  $A(i, i)$  in the 1-D array  $A1$ . Thus,
    - The elements in  $i$ th row (from the 1st nonzero element to the diagonal element) are stored into  $A1[IA(i-1) + 1], A1[IA(i-1) + 2], \dots, A1[IA(i)]$
    - The number of nonzero elements (from the 1st nonzero elements to the diagonal but not include the diagonal element)

$$m_i = IA(i) - IA(i-1) - 1$$

- The element  $A(i, j)$  is stored into  $A1(ij)$  where

$$ij = IA(i) - (i - j).$$

# Example

For  $A = \begin{bmatrix} a_{11} & a_{12} & 0 & 0 \\ a_{21} & a_{22} & a_{23} & a_{24} \\ 0 & a_{32} & a_{33} & 0 \\ 0 & a_{42} & 0 & a_{44} \end{bmatrix}$  (assume symmetric)

We will construct  $A1$  and  $IA$  as follows:

$k$	1	2	3	4	5	6	7	8
$A1(k)$	$a_{11}$	$a_{21}$	$a_{22}$	$a_{32}$	$a_{33}$	$a_{42}$	0	$a_{44}$



$IA(i)_{i=1 \text{ to } N}$  identifies the storage location of  $A(i, i)$  in the 1-D array  $A1$ .

$i$	1	2	3	4
$IA(i)$	1	3	5	8

# Programming using 1-D Storage Structure

A: an array, contain matrix  $A(1-D)$ . On exit, contain LD in 1-D form.

For  $i = 2, N$

$$m_i = IA(i) - IA(i - 1) - 1$$

$$i1 = \max(i - m_i, 1)$$

For  $j = i1, i$

$$m_j = IA(j) - IA(j - 1)$$

$$j1 = \max(j - m_j, 1)$$

$$sum = 0$$

For  $k = \max(i1, j1), j - 1$

$$ik = Trans(i, k)$$

$$jk = Trans(j, k)$$

$$kk = Trans(k, k)$$

$$sum = sum + A(ik) * A(jk) * A(kk)$$

# Programming using 1-D Storage Structure

$ij = \text{Trans}(i, j)$

$jj = \text{Trans}(j, j)$

If  $(i \neq j)$  then  $A(ij) = (A(ij) - \text{sum})/A(jj)$

else  $A(ij) = a(ij) - \text{sum}$

END

# Exercise

Given the list of nodal points and their coordinates and the list of elements and their node numbers below:

- sketch the finite element mesh  $\Omega_h$
- sketch the  $\xi, \eta$  -axes in each element and verify that the maps  $T_e, e = 1, 2, \dots, 5$ , produce a connected region  $\Omega_h$
- sketch the global basis function  $\phi_e$  for node 4 of the mesh.

Node	x	y
1	0	1
2	0.7	0.7
3	1	0
4	0	2
5	1.5	1.5
6	2	0
7	0	3
8	1.5	3
9	3	3

Element	Nodes
1	1, 2, 5, 4
2	3, 6, 5, 2
3	5, 8, 7, 4
4	5, 10, 9, 8
5	6, 11, 10, 5