

## MATH5004 LAB 8

## 2D FEM: The plane truss element

The plane truss element has modulus of elasticity  $E$ , cross-sectional area  $A$ , and length  $L$ . The plane truss element has four degrees of freedom. Let  $C = \cos \theta$  and  $S = \sin \theta$  and the element stiffness matrix is given by

$$k^e = \frac{EA}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ -CS & -S^2 & CS & S^2 \end{bmatrix},$$

The force for each element is

$$f^e = \frac{EA}{L} [-C \quad -S \quad C \quad S] \mathbf{u}^e,$$

where  $\mathbf{u}^e = [u_{1x}, u_{1y}, u_{2x}, u_{2y}]^T$  is element displacement vector. If  $n$  is number of nodes in the area  $A$ , the global stiffness matrix  $\mathbf{K}$  has dimension  $2n \times 2n$ . The element stress is obtained by dividing the element force by the cross sectional area  $A$ . Assemble all element matrices and element force vectors, we obtain a global system of equations

$$\mathbf{KU} = \mathbf{F}.$$

If there is an inclined support at one of the nodes of the truss then the global stiffness matrix needs to be modified using the following equation:

$$\mathbf{K}_{new} = \mathbf{T} \mathbf{K}_{new} \mathbf{T}^T,$$

where  $\mathbf{T}$  is a  $2n \times 2n$  transformation matrix that is obtained by making a call to the MATLAB function *PlaneTrussInclinedSupport*.

**Example.** Consider the plane truss with modulus of elasticity  $E = 210 \text{ GPa}$  and cross-sectional area  $A = 1 \times 10^{-4} \text{ m}^2$ .

Find:

1. the global stiffness matrix for the structure.
2. the horizontal displacement at node 2.
3. the horizontal and vertical displacements at node 3.
4. the reactions at nodes 1 and 2.
5. the stress in each element.

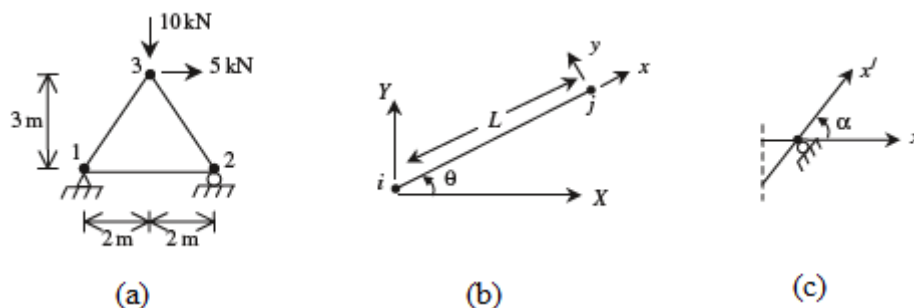


Fig 1. Plane Truss with Three Elements (a), and two nodal truss element (b) with inclined support (c).

## MATLAB Functions

The following MATLAB functions are used for this problem:

- *PlaneTrussElementLength.m*
- *PlaneTrussElementStiffness.m*,
- *PlaneTrussAssemble.m*
- *PlaneTrussElementForce.m*
- *PlaneTrussElementStress.m*
- *PlaneTrussInclinedSupport.m*

```
function y = PlaneTrussElementLength(x1,y1,x2,y2)
%PlaneTrussElementLength This function returns the length of the
% plane truss element whose first node has
% coordinates (x1, y1) and second node has
% coordinates (x2, y2).
y = sqrt((x2-x1)*(x2-x1) + (y2-y1)*(y2-y1));
```

```
function y = PlaneTrussAssemble(K,k,i,j)
%PlaneTrussAssemble This function assembles the element stiffness
% matrix k of the plane truss element with nodes
% i and j into the global stiffness matrix K.
% This function returns the global stiffness
% matrix K after the element stiffness matrix
% k is assembled.
K(2*i-1,2*i-1) = K(2*i-1,2*i-1) + k(1,1) ;
K(2*i-1,2*i) = K(2*i-1,2*i) + k(1,2) ;
K(2*i-1,2*j-1) = K(2*i-1,2*j-1) + k(1,3) ;
K(2*i-1,2*j) = K(2*i-1,2*j) + k(1,4) ;
K(2*i,2*i-1) = K(2*i,2*i-1) + k(2,1) ;
K(2*i,2*i) = K(2*i,2*i) + k(2,2) ;
K(2*i,2*j-1) = K(2*i,2*j-1) + k(2,3) ;
K(2*i,2*j) = K(2*i,2*j) + k(2,4) ;
K(2*j-1,2*i-1) = K(2*j-1,2*i-1) + k(3,1) ;
K(2*j-1,2*i) = K(2*j-1,2*i) + k(3,2) ;
K(2*j-1,2*j-1) = K(2*j-1,2*j-1) + k(3,3) ;
K(2*j-1,2*j) = K(2*j-1,2*j) + k(3,4) ;
K(2*j,2*i-1) = K(2*j,2*i-1) + k(4,1) ;
K(2*j,2*i) = K(2*j,2*i) + k(4,2) ;
K(2*j,2*j-1) = K(2*j,2*j-1) + k(4,3) ;
K(2*j,2*j) = K(2*j,2*j) + k(4,4) ;
y = K;
```

```
function y = PlaneTrussElementStiffness(E,A,L, theta)
%PlaneTrussElementStiffness This function returns the element
% stiffness matrix for a plane truss
% element with modulus of elasticity E,
% cross-sectional area A, length L, and
% angle theta (in degrees).
% The size of the element stiffness
% matrix is 4 x 4.
x = theta*pi/180;
C = cos(x);
S = sin(x);
y = E*A/L*[C*C C*S -C*C -C*S ; C*S S*S -C*S -S*S ;
           -C*C -C*S C*C C*S ; -C*S -S*S C*S S*S] ;
```

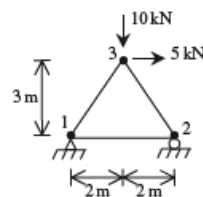
```
function y = PlaneTrussElementForce(E,A,L,theta,u)
%PlaneTrussElementForce This function returns the element force
% given the modulus of elasticity E, the
% cross-sectional area A, the length L,
% the angle theta (in degrees), and the
% element nodal displacement vector u.
x = theta* pi/180;
C = cos(x);
S = sin(x);
y = E*A/L*[-C -S C S]* u;
```

```
function y = PlaneTrussElementStress(E,L,theta,u)
%PlaneTrussElementStress This function returns the element stress
% given the modulus of elasticity E, the length L, the angle theta (in
% degrees), and the element nodal displacement vector u.
x = theta * pi/180;
C = cos(x);
S = sin(x);
y = E/L*[-C -S C S]* u;
```

```
function y = PlaneTrussInclinedSupport(T,i,alpha)
%PlaneTrussInclinedSupport This function calculates the tranformation
% matrix T of the inclined support at node i with angle of
% inclination alpha (in degrees).
x = alpha*pi/180;
T(2*i-1,2*i-1) = cos(x) ;
T(2*i-1,2*i) = sin(x) ;
T(2*i,2*i-1) = -sin(x) ;
T(2*i,2*i) = cos(x) ;
y = T;
```

### Step 1 Discretizing the Domain

Element Number	Node i	Node j
1	1	2
2	1	3
3	2	3



### Step 2 Writing the Element Stiffness Matrices

The tool **PlaneTrussElementStiffness.m** are used to obtain three element stiffness matrices  $k^{(1)}$ ,  $k^{(2)}$ , and  $k^{(3)}$ .

```
» E=210e6
```

```
E =
```

```
2100000000
```

```
» A=1e-4
```

```
A =
```

```
1.0000e-004
```

```
» L1=4
```

```
L1 =
```

```
4
```

```
» L2=PlaneTrussElementLength(0,0,2,3)
```

```
L2 =
```

```
3.6056
```

```
» L3=PlaneTrussElementLength(0,0,-2,3)
```

```
L3 =
```

```
3.6056
```

```
» k1=PlaneTrussElementStiffness(E,A,L1,0)
```

```
k1 =
```

```
5250    0   -5250    0
    0    0     0     0
-5250    0    5250    0
    0    0     0     0
```

```
» theta2=atan(3/2)*180/pi
```

```
theta2 =
```

```
56.3099
```

```
» theta3=180-theta2
```

```
theta3 =
```

```
123.6901
```

```
» k2=PlaneTrussElementStiffness(E,A,L2,theta2)
```

```
k2 =
```

```
1.0e+003 *
```

```
1.7921  2.6882 -1.7921 -2.6882
2.6882  4.0322 -2.6882 -4.0322
-1.7921 -2.6882  1.7921  2.6882
-2.6882 -4.0322  2.6882  4.0322
```

```
» k3=PlaneTrussElementStiffness(E,A,L3,theta3)
```

```
k3 =
```

```
1.0e+003 *
```

```
1.7921 -2.6882 -1.7921  2.6882
-2.6882  4.0322  2.6882 -4.0322
-1.7921  2.6882  1.7921 -2.6882
2.6882 -4.0322 -2.6882  4.0322
```

```
» K=PlaneTrussAssemble(K,k2,1,3)
```

```
K =
```

```
1.0e+003 *
```

```
7.0421  2.6882 -5.2500  0 -1.7921 -2.6882
2.6882  4.0322  0  0 -2.6882 -4.0322
```

### Step 3 Assembling the Global Stiffness Matrix

As the structure has three nodes, each node has two degree of freedoms (displacements in x and y direction), the size of the global stiffness matrix is  $6 \times 6$ . We firstly initialize a zero matrix  $K$  of size  $6 \times 6$ .

```
» K=zeros(6,6)
```

```
K =
```

```
0  0  0  0  0  0
0  0  0  0  0  0
0  0  0  0  0  0
0  0  0  0  0  0
0  0  0  0  0  0
0  0  0  0  0  0
```

We then make three calls to the MATLAB function *PlaneTrussAssemble.m*

```
» K=PlaneTrussAssemble(K,k1,1,2)
```

K =

```

5250    0   -5250    0    0    0
    0    0        0    0    0    0
-5250    0    5250    0    0    0
    0    0        0    0    0    0
    0    0        0    0    0    0
    0    0        0    0    0    0
```

```
» K=PlaneTrussAssemble(K,k2,1,3)
```

K =

1.0e+003 \*

```

7.0421    2.6882   -5.2500    0   -1.7921   -2.6882
2.6882    4.0322        0    0   -2.6882   -4.0322

-5.2500        0    5.2500    0        0        0
    0        0        0    0        0        0
-1.7921   -2.6882        0    0    1.7921    2.6882
-2.6882   -4.0322        0    0    2.6882    4.0322
```

```
» K=PlaneTrussAssemble(K,k3,2,3)
```

K =

1.0e+003 \*

```

7.0421    2.6882   -5.2500        0   -1.7921   -2.6882
2.6882    4.0322        0        0   -2.6882   -4.0322
-5.2500        0    7.0421   -2.6882   -1.7921    2.6882
    0        0   -2.6882    4.0322    2.6882   -4.0322
-1.7921   -2.6882   -1.7921    2.6882    3.5842    0.0000
-2.6882   -4.0322    2.6882   -4.0322    0.0000    8.0645
```

#### Step 4 Applying the Boundary Conditions

The boundary conditions are

$$U1x = U1y = U2y = 0, \quad F2x = 0, \quad F3x = 5, \quad F3y = -10$$

Imposing BCs to the global stiffness matrix  $\mathbf{K}$  obtained in the previous step:

$$\mathbf{KU} = \mathbf{F},$$

where

$$\mathbf{U} = \begin{bmatrix} U_{1x} \\ U_{1y} \\ U_{2x} \\ U_{2y} \\ U_{3x} \\ U_{3y} \end{bmatrix} \text{ and } \mathbf{F} = \begin{bmatrix} F_{1x} \\ F_{1y} \\ F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \end{bmatrix}.$$

We then obtain

$$10^3 \begin{bmatrix} 7.041 & 2.6882 & -5.2500 & 0 & -1.7921 & -2.6882 \\ 2.6882 & 4.0322 & 0 & 0 & -2.6882 & -4.0322 \\ -5.2500 & 0 & 7.0421 & -2.6882 & -1.7921 & 2.6882 \\ 0 & 0 & -2.6882 & 4.0322 & 2.6882 & -4.0322 \\ -1.7921 & -2.6882 & -1.7921 & 2.6882 & 3.5842 & 0 \\ -2.6882 & -4.0322 & 2.6882 & -4.0322 & 0 & 8.0645 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ U_{2x} \\ 0 \\ U_{3x} \\ U_{3y} \end{bmatrix} = \begin{bmatrix} F_{1x} \\ F_{1y} \\ 0 \\ F_{2y} \\ 5 \\ -10 \end{bmatrix}$$

### Step 5 Solving the Equations

The solution of the following system

$$10^3 \begin{bmatrix} 7.0421 & -1.7921 & 2.6882 \\ -1.7921 & 3.5842 & 0 \\ 2.6882 & 0 & 8.0645 \end{bmatrix} \begin{bmatrix} U_{2x} \\ U_{3x} \\ U_{3y} \end{bmatrix} = \begin{bmatrix} 0 \\ 5 \\ -10 \end{bmatrix}$$

is obtained using MATLAB code as follows:

```
» k=[K(3,3) K(3,5:6) ; K(5:6,3) K(5:6,5:6)]
```

```
k =
```

```
1.0e+003 *
```

```
    7.0421    -1.7921    2.6882
   -1.7921    3.5842    0.0000
    2.6882    0.0000    8.0645
```

```
» f=[0 ; 5 ; -10]
```

```
f =
```

```
    0
    5
   -10
```

```

» u=k\f
u =
    0.0011
    0.0020
   -0.0016

```

which means that the horizontal displacement at node 2 is 0.0011 m, and the horizontal and vertical displacements at node 3 are 0.0020m and  $-0.0016$ m, respectively.

### Step 6 *Post-processing*

This step is to determine the reactions at nodes 1 and 2, and the stress in each element.

- set up the global nodal displacement vector  $\mathbf{U}$ , then we calculate the global nodal force vector  $\mathbf{F}$ .

```

» U=[0 ; 0 ; u(1) ; 0 ; u(2:3)]
U =
     0
     0
    0.0011
     0
    0.0020
   -0.0016

» F=K*U
F =
   -5.0000
    1.2500
   -0.0000
    8.7500
    5.0000
   -10.0000

```

The result  $\mathbf{F}$  indicates that

- the horizontal and vertical reactions at node 1 are forces of 5 kN (directed to the left) and 1.25 kN (directed upwards).
  - The vertical reaction at node 2 is a force of 8.75N (directed upwards).
- Set up the element nodal displacement vectors  $\mathbf{u}^{(1)}$ ,  $\mathbf{u}^{(2)}$ , and  $\mathbf{u}^{(3)}$

```

» u1=[U(1) ; U(2) ; U(3) ; U(4)]
u1 =
     0
     0
    0.0011
     0

```



```
» u2=[U(1) ; U(2) ; U(5) ; U(6)]
```

```
u2 =
```

```

    0
    0
  0.0020
 -0.0016

```

```
» u3=[U(3) ; U(4) ; U(5) ; U(6)]
```

```
u3 =
```

```

  0.0011
    0
  0.0020
 -0.0016

```

- Use the tool *PlaneTrussElementStress.m* to Calculate the element stresses  $\sigma_1$ ,  $\sigma_2$ , and  $\sigma_3$ .

```
» sigma1=PlaneTrussElementStress(E,L1,0,u1)
```

```
sigma1 =
```

```
5.8333e+004
```

```
» sigma2=PlaneTrussElementStress(E,L2,theta2,u2)
```

```
sigma2 =
```

```
-1.5023e+004
```

```
» sigma3=PlaneTrussElementStress(E,L3,theta3,u3)
```

```
sigma3 =
```

```
-1.0516e+005
```

We conclude that the stress in each element as follows:

- In element 1, the stress is 1 58.3333MPa (tensile),
- In element 2, the stress is 15.023MPa (compressive),
- In element 3, the stress is 105.16MPa (compressive).

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