

# EEC 130A: Homework 2

Due: 3:30 pm, Jan. 24, 2012

1. (4 points) (FAE P2.1) A transmission line of length  $l$  connects a load to a sinusoidal voltage source with an oscillation frequency  $f$ . Assuming that the velocity of wave propagation on the line is  $c$ , for which of the following situations is it reasonable to ignore the presence of the transmission line in the solution of the circuit (and **why?**):

- (a)  $l = 20$  cm,  $f = 20$  kHz
- (b)  $l = 50$  km,  $f = 60$  Hz
- (c)  $l = 20$  cm,  $f = 600$  MHz
- (d)  $l = 1$  mm,  $f = 100$  GHz

2. (4 points) (FAE P2.3) Show that the transmission-line model shown in Fig. 1 yields the same telegrapher's equations given by Eqs. (2.14) and (2.16) in the textbook.

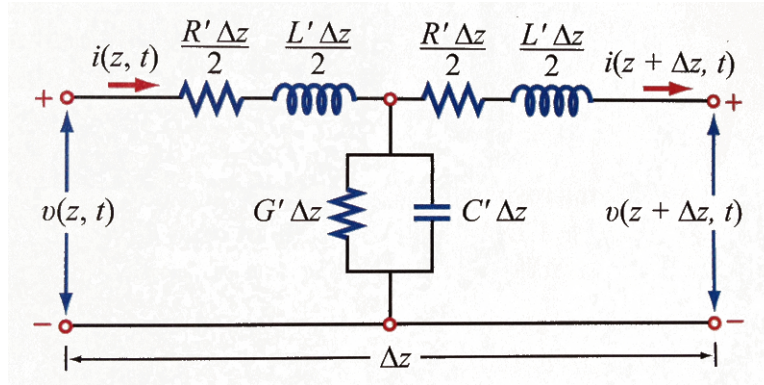


Figure 1: Transmission-line model for Problem 2.

3. (4 points) (FAE P2.4) A 1-GHz parallel-plate transmission line consists of 1.2-cm-wide copper strips separated by a 0.15-cm-thick layer of polystyrene. Appendix B gives  $\mu_c = \mu_0 = 4\pi \times 10^{-7}$  (H/m) and  $\sigma_c = 5.8 \times 10^7$  (S/m) for copper, and  $\epsilon_r = 2.6$  for polystyrene. Use Table. 1 to determine the line parameters of the transmission line. Assume that  $\mu = \mu_0$  and  $\sigma \simeq 0$  for polystyrene.

The relevant part of Fig.2-4 from FAE is reprinted here for your reference.

4. (4 points) (FAE P2.13) In addition to not dissipating power, a lossless line has two important features: (1) it is dispersionless ( $u_p$  is independent of frequency); and (2) its characteristic impedance  $Z_0$  is purely real. Sometimes, it is not possible to design a transmission

Table 1: (Table 2-1 from FAE) Transmission-line parameters  $R'$ ,  $L'$ ,  $G'$ , and  $C'$  for three types of lines.

**Table 2-1:** Transmission-line parameters  $R'$ ,  $L'$ ,  $G'$ , and  $C'$  for three types of lines.

Parameter	Coaxial	Two-Wire	Parallel-Plate	Unit
$R'$	$\frac{R_s}{2\pi} \left( \frac{1}{a} + \frac{1}{b} \right)$	$\frac{2R_s}{\pi d}$	$\frac{2R_s}{w}$	$\Omega/\text{m}$
$L'$	$\frac{\mu}{2\pi} \ln(b/a)$	$\frac{\mu}{\pi} \ln \left[ (D/d) + \sqrt{(D/d)^2 - 1} \right]$	$\frac{\mu h}{w}$	$\text{H}/\text{m}$
$G'$	$\frac{2\pi\sigma}{\ln(b/a)}$	$\frac{\pi\sigma}{\ln \left[ (D/d) + \sqrt{(D/d)^2 - 1} \right]}$	$\frac{\sigma w}{h}$	$\text{S}/\text{m}$
$C'$	$\frac{2\pi\epsilon}{\ln(b/a)}$	$\frac{\pi\epsilon}{\ln \left[ (D/d) + \sqrt{(D/d)^2 - 1} \right]}$	$\frac{\epsilon w}{h}$	$\text{F}/\text{m}$

Notes: (1) Refer to Fig. 2-4 for definitions of dimensions. (2)  $\mu$ ,  $\epsilon$ , and  $\sigma$  pertain to the insulating material between the conductors. (3)  $R_s = \sqrt{\pi f \mu_c / \sigma_c}$ . (4)  $\mu_c$  and  $\sigma_c$  pertain to the conductors. (5) If  $(D/d)^2 \gg 1$ , then  $\ln \left[ (D/d) + \sqrt{(D/d)^2 - 1} \right] \simeq \ln(2D/d)$ .

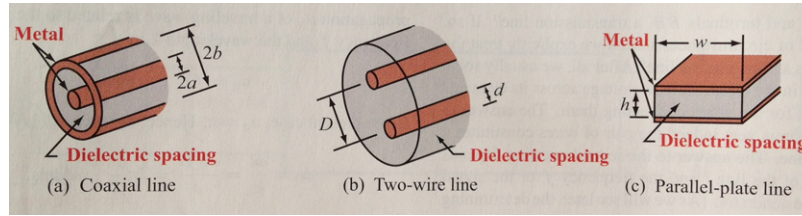


Figure 2: (Fig.2-4 from FAE) A few examples of transmission lines.

line such that  $R' \ll \omega L'$  and  $G' \ll \omega C'$ , but it is possible to choose the dimensions of the line and its material properties so as to satisfy the condition

$$R'C' = L'G' \quad \text{distortionless line}$$

Such a line is called a distortionless line, because despite the fact that it is not lossless, it nonetheless possesses the previously mentioned features of the lossless line. Show that for a distortionless line,

$$\alpha = R' \sqrt{\frac{C'}{L'}} = \sqrt{R'G'},$$

$$\beta = \omega \sqrt{L'C'},$$

$$Z_0 = \sqrt{\frac{L'}{C'}}.$$

5. (4 points) (FAE P.2.12) Generate a plot of  $Z_0$  as a function of strip width  $w$ , over the range from 0.05 mm to 5 mm, for a microstrip line fabricated on a 0.7-mm-thick substrate with  $\epsilon_r = 9.8$ .