

4.1.1 $F_* = \frac{SL}{u_{\infty}}$, $F_* = 1 \rightarrow u_{\infty} = SL$

$\frac{\omega \phi}{u_{\infty}} = 0.075 \xrightarrow{\text{substitute } u_{\infty}} \frac{2\pi \phi}{SL} \xrightarrow{\text{simplify}} \frac{2\pi \phi}{L} = 0.075 \rightarrow \frac{\phi}{L} = \frac{0.075}{2\pi} = 0.0119$

4.1.2 $\frac{\delta}{\phi} = 10 \therefore \frac{\delta}{\phi} \frac{\phi}{L} = \frac{\delta}{L} = 0.119$

4.5.1 Optimum Spacing = 0.86

$$\frac{1}{\theta} = 4, \quad \frac{\omega \theta}{U_{\infty}} = 0.12$$

$$\lambda_x = \frac{2\pi}{\omega}$$

$$\omega = \frac{U_{\infty}}{\theta} \cdot 0.12 \rightarrow \lambda_x = \frac{2\pi}{\left(\frac{U_{\infty}}{\theta}\right) \cdot 0.12} = 52.36 \left(\frac{\theta}{U_{\infty}}\right)$$

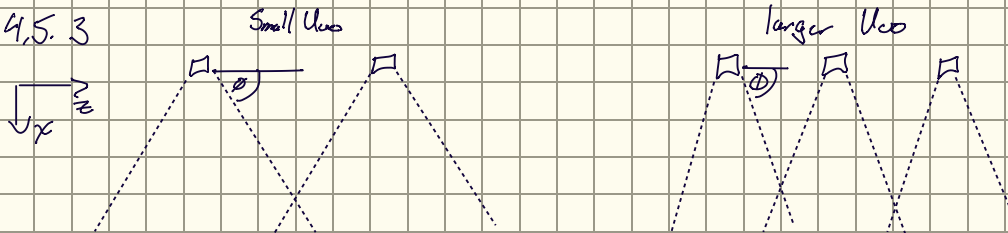
4.5.2 $\theta \approx 0.1$ Assuming $\lambda_z = 0.86$

$$\theta = \tan^{-1}\left(\frac{\lambda_z}{\lambda_x}\right) = \tan^{-1}\left(\frac{0.86}{52.36 \frac{\theta}{U_{\infty}}}\right) = \tan^{-1}\left(\frac{0.8 \cdot 10^4}{52.36 \frac{\theta}{U_{\infty}}}\right) = \tan^{-1}\left(\frac{1.8 U_{\infty}}{62.8}\right)$$

U_{∞}	θ (deg)
5	32.4
10	56.8
15	66.4
20	71.9

$$\lambda_z = \frac{4.56}{u}$$

4.5.3



At larger U_{∞} the wave angle is larger and the waves are more 3D. Therefore the vortices travel a smaller spanwise distance and therefore more are needed to effectively mix the boundary layer.

4.6.1

$$L \geq T_c \cdot d_{\text{geo}}$$

$$T_c = 1.5 \text{ ms} \rightarrow 0.0015 \text{ s}$$

$$V_{\text{ao}} = 68 \text{ m/s}$$

$$V_j = 3 \text{ (conservative)}$$

$$L \geq 0.0015 \cdot 68 \Rightarrow L \geq 0.102 \text{ m} \quad \text{minimum required length}$$

4.6.2

$$V_j/V_{\text{ao}} > 0.8 \quad T_c = d/V_j \Rightarrow \frac{T_c}{V_j} = d$$

$$\frac{T_c}{V_j} = \frac{0.0015}{3} = \frac{T_{c_{\text{new}}}}{0.8 \cdot 68} \rightarrow T_{c_{\text{new}}} = 0.0272 \text{ s}$$

$$L \geq T_{c_{\text{new}}} \cdot 68 = 1.85 \text{ m}$$

4.6.3

This justifies the relatively small holes needed for wall jets because they are parallel at these states and therefore much less restrictive than the plasma actuators.

4.2.1

Section: $\frac{\partial}{\partial x}$ Favorable pressure gradient, the Boundary layer to gain momentum and increase the Velocity gradient.

Blowing: $\frac{\partial}{\partial x}$ Adverse pressure gradient, causing the Boundary layer to Billow and the Velocity gradient near the wall to approach zero.

4.2.2

The profile $\frac{\partial}{\partial x}$ changes the Magnitude of Amplification and the most Amplified Frequency of the shear layer instability. Based on Fig 4.13. The Magnitude of Amplification increases as the shear layer separates. The Frequency however, increases until the shear layer separates and the most Amplified Frequency decreases slightly. The effects are ~~not the~~ the same for wall normal section and tangential Blowing.

4.2.3

Wall section:

1.) Reduction of Boundary layer thickness.

2.) Increased momentum Near Wall and increasing the Velocity gradient near the Wall.

3.) Delay of Adverse Pressure gradients and therefore delays Separation.

Tangential Blowing:

1.) Enhancement of Shear stress at the wall, which works to prevent separation.

2.) Thickening of Boundary layer through addition of momentum into flow.

3.) Suppression of Vortical structures.