

# RIT Formula SAE Senior Design



# Agenda

- Project Description
- Customer Needs
- Engineering Specifications
- Budget
- Risk Assessment
- Preliminary Testing Results
- Finalized Intake Design Details

# Project Introduction

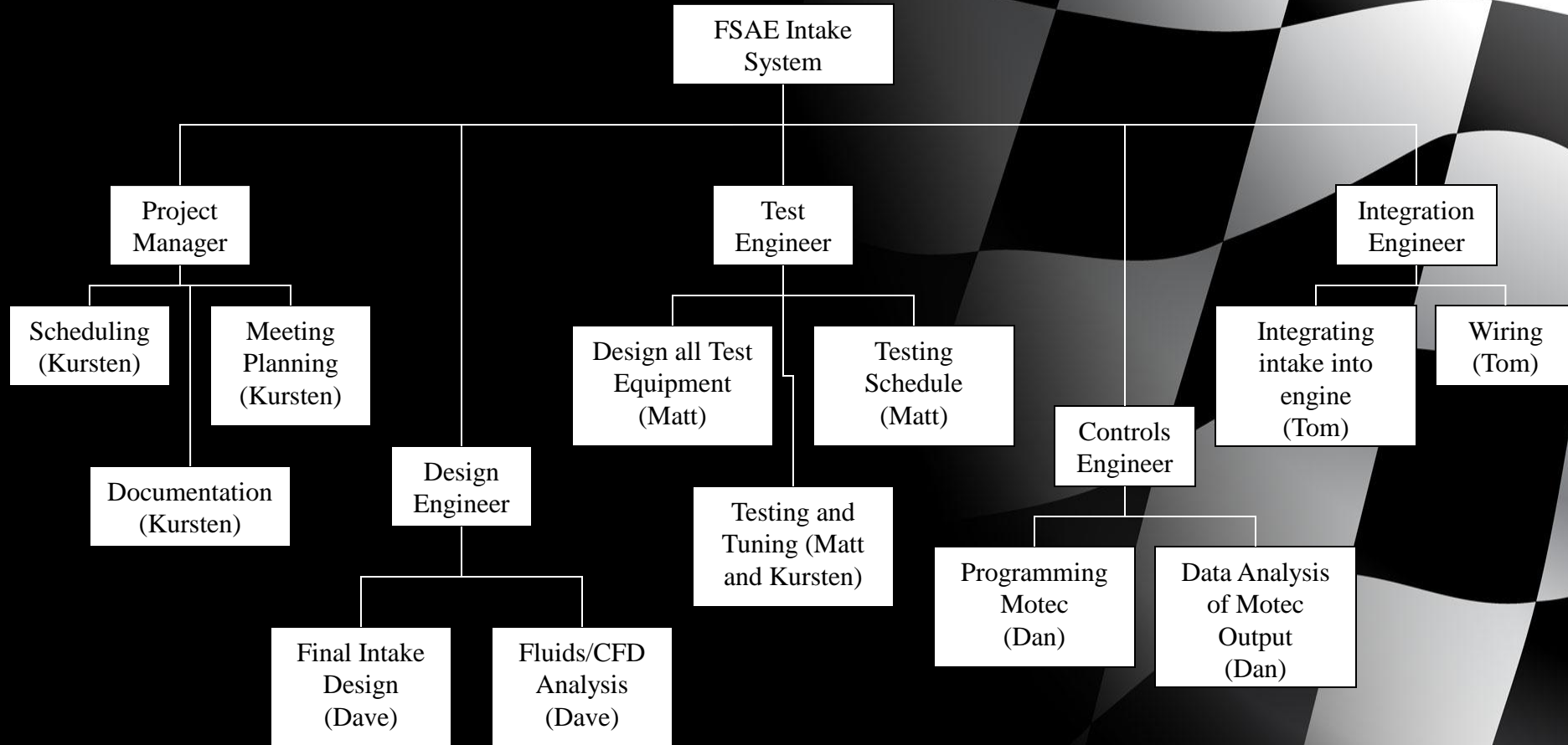
- As each competition passes, fuel efficiency and technical superiority becomes much more prevalent in competition scoring. To advance the RIT Formula SAE Racing Team in the engine subsystem, the variable intake system will prove to be innovative and technically competitive.
- Problem Statement: This senior design project will develop a variable intake system for the Formula SAE race car that will allow for increased fuel efficiency, design advancements and a greener methodology to produce more engine power.

# Project Introduction

## Project Scope:

1. Measure the fuel efficiency of the engine
2. Improve power and torque
3. Packaging the system with simplicity to allow for ease of installation and maintenance
4. Design and build for the non-professional, weekend and competition market

# Work Breakdown



# Customer Needs

Customer Need #	Importance	Description
		<b>Volumetric Efficiency</b>
CN1	4	Increased Air Inductance
		<b>Fuel Efficiency</b>
CN2	7	Optimized usage of race fuel
		<b>Power/Torque</b>
CN3	5	Increased HP Output
CN4	5	Increased Torque Output
		<b>Drivability</b>
CN5	6	Ease of length of change while driving
		<b>Weight</b>
CN6	3	No significant weight gain
		<b>Reliability</b>
CN7	7	Low maintenance
		<b>Manufacturability</b>
CN8	1	Simplistic
		<b>Serviceability</b>
CN9	2	Computer programming
CN10	2	Assembly
		<b>Cost</b>
CN11	0	Low cost

Importance: 10 = Highest Importance  
0 = Lowest Importance

# Specifications

Engr. Spec. #	Importance	Source	Specification (description)	Unit of Measure	Marginal Value	Ideal Value	Comments/Status
ES1	2	Weight	The overall weight of the system compared to non-adjustable	lbs	4.0	1.85	Current system 1.478 lbs
ES2	1	Performance	The reduction of lap times due to system performance	sec	1	2	Will vary depending on event
ES3	3	Fuel Economy	The impact this system has on fuel consumption	lbs/hr	0	-2	
ES4	7	Manufacturing Time	Time required to produce a working unit	days	20	10	
ES5	5	Current Draw	Current required by the system to operate	amps	5	1	
ES6	4	Actuation Time	Time required to change position	milliseconds	200	100	
ES8	5	Voltage Draw	Voltage required to produce a working system	volts	12	12	



# Concept Screening

Concept Screening		
	2-Stroke	Infinitely
Selection Criteria		
<i>Volumetric Efficiency</i>		
Increased Air Inductance	+	+
<i>Fuel Efficiency</i>		
Optimized usage of race fuel	+	+
<i>Power/Torque</i>		
Increased HP Output	+	+
Increased Torque Output	+	+
<i>Drivability</i>		
Ease of length of change while driving	-	+
<i>Weight</i>		
No significant weight gain	0	0
<i>Reliability</i>		
Low maintenance	0	0
<i>Manufacturability</i>		
Simplistic	+	-
<i>Serviceability</i>		
Computer programming	+	-
Assembly	+	-
<i>Cost</i>		
Low cost	0	0
Sum +'s	7	5
Sum 0's	2	2
Sum -'s	1	3
Net Score	6	2
Rank	1	2

Based on the customer needs, the best intake system for the race car is the two-position as it allows for a greater number of benefits compared to an infinitely variable system given the time frame, tools and manufacturing capabilities available.



# Budget

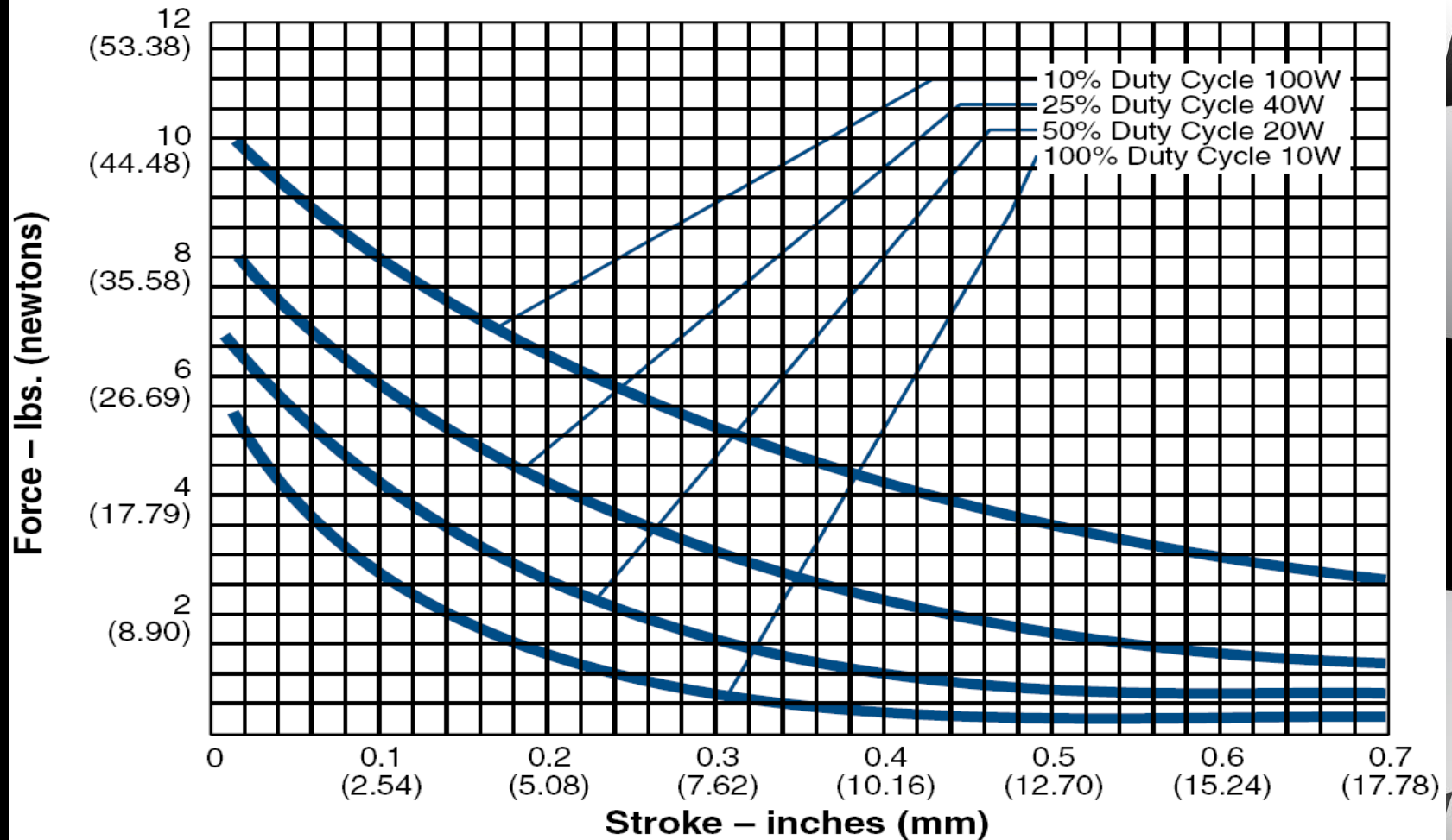
Product	Manufacturer	Part Number	Unit Price	Quantity	Total Price	Comments
<i>Testing and Verification</i>						
<i>Testing Materials</i>						
93 Octane Fuel	-	-	\$ 3.00	20	\$ 60.00	gallons
100 Octane Fuel	-	-	\$ 6.00	20	\$ 120.00	gallons
Tires	Competition Tire East	D2696	\$ 180.00	4	\$ 720.00	Goodyear Tires
<i>Miscellaneous Dyno Materials</i>	-	-	-	-	-	
Thermocouples	Omega	KMQSS-062U-6	\$ 26.00	8	\$ 208.00	
<i>Manufacturing and Assembly</i>						
<i>Electric Actuation</i>						
Electric Solenoid	Allied Electronics	Ledex 195204-230	\$ 19.97	3	\$ 59.91	2 for testing, 1 for manufacturing
Extension Spring	McMaster-Carr	9657K33	\$ 6.86	1	\$ 6.86	Package of 12
<i>Pneumatic Actuation</i>						
Three Way Solenoid	Skinner	3131BEN1EN00RRT1J1C1	\$ 57.50	2	\$ 115.00	Three Way Valve
Pneumatic Cylinder	Bimba	010.5-NRENT	\$ 20.15	2	\$ 40.30	Single Acting .5" Stroke, non rotating, 7/16 bore
Pressure Regulator	Parker	14RJ110C	\$ 18.99	1	\$ 18.99	
<i>System Materials</i>						
Aluminum Plate	McMaster Carr	8975K439	\$ 10.94	2	\$ 21.88	Size: 0.125 x 6 x 12, for Base Flange
Aluminum Tube	McMaster Carr	89965K123	\$ 18.18	1	\$ 18.18	Size: 1.5 x 0.035 x 36, for Static Runners
Aluminum Sheet	McMaster Carr	89015K14	\$ 12.63	1	\$ 12.63	Size: 0.050 x 12 x 12, for Plenum Shell
Aluminum Sheet	McMaster Carr	89015K18	\$ 26.29	1	\$ 26.29	Size: 0.125 x 12 x 12, for Plenum Base
ABS Plastic Rod	McMaster Carr	8587K52	\$ 57.57	1	\$ 57.57	Size: 3 Round x 12, for Diverter
ABS Plastic Rod	McMaster Carr	8587K49	\$ 22.53	2	\$ 45.06	Size: 2 Round x 12, for Dynamic Runners
<i>Miscellaneous System Materials</i>						
Air Filter	K&N Filters	RU-0981	\$ 29.99	1	\$ 29.99	Size: 2 Round x 12, for Dynamic Runners
			Total		\$ 1,391.26	
			Maximum Total		\$ 1,500.00	
			Balance		\$ 108.74	
	Purchased					
	To Be Purchased					
	To Be Returned					

# Risks

Please see handout for list

# Solenoid Force Curve

## Typical Force @ 20°C



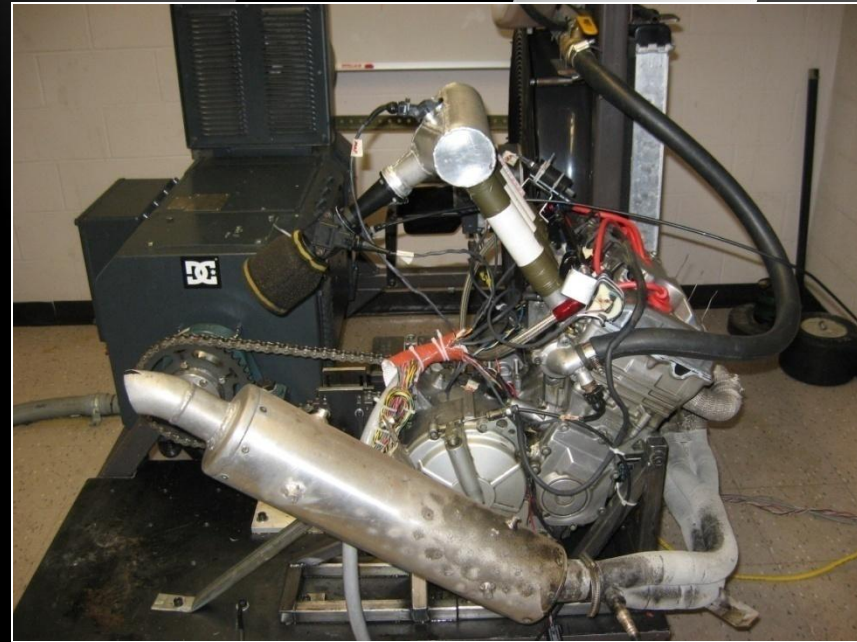
# Testing Equipment

## **Test Equipment available**

Machine shop equipment  
DC Dynamometer  
Chassis Dynamometer  
Honda CBR 600 test engine  
RIT FSAE race car  
Electronic test equipment  
Computers

## **Test Equipment needed but not available**

Advanced Vehicle based data acquisition system (DAQ)



# Testing

## Sub-System Breakdown

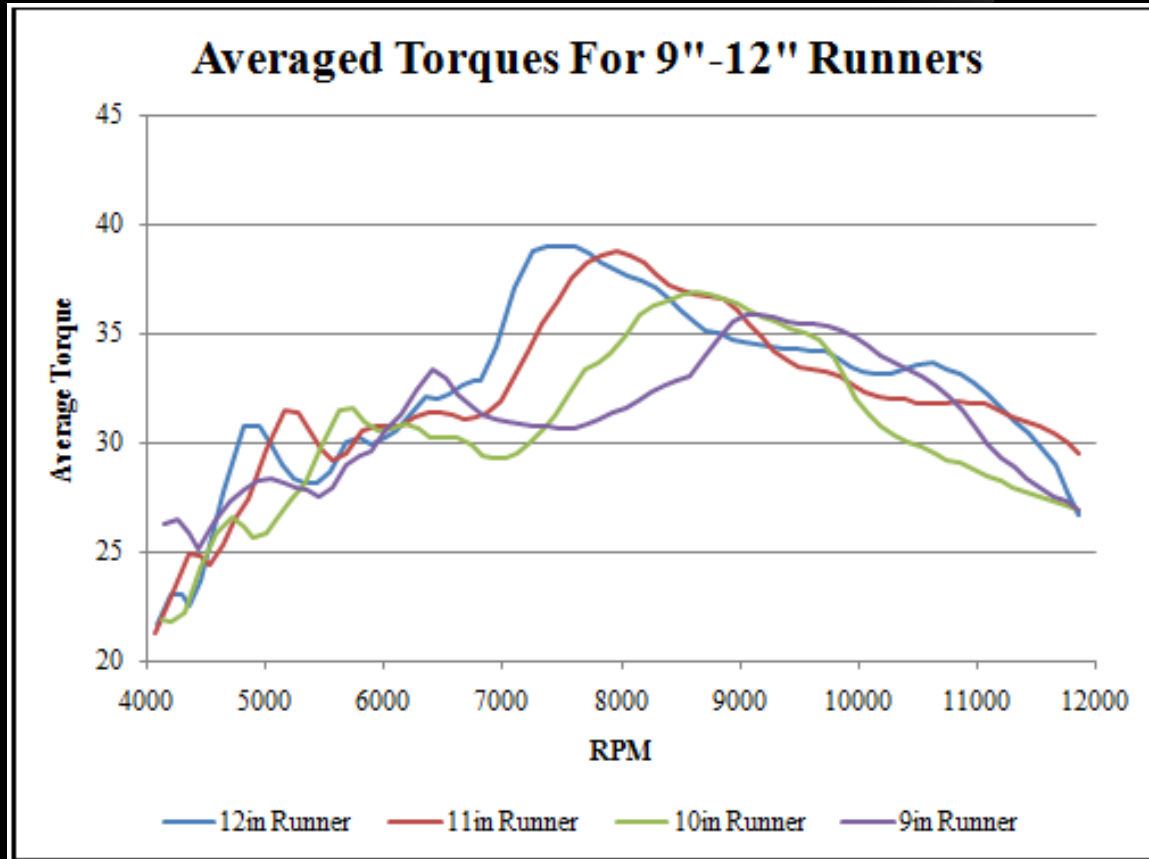
- *Mechanical System*
- The mechanical system is comprised of the sliding interface that allows the change in runner length and the plenum that the runners interact with. This system must allow for the desired change in length, not leak, maintain desired plenum volume, and comply with the FSAE rulebook.
- *Actuation System*
- The actuation system will move the mechanical system based on inputs from the control system. Actuation speed is critical for this application as transient times must be kept under 100ms. This system must also be able to gauge the system's location.
- *Control System*
- The controls for this system will be fully integrated into the engine control unit (ECU) for the vehicle. Using inputs such as RPM, throttle position, manifold pressure and current runner length the control system will output a desired runner length to be achieved by the actuation system.
- *Supporting Systems*
- The variable intake will interface with the engine on one end and a throttle/ restrictor assembly on the other. Sufficient information on the flow characteristics of the throttle/ restrictor assembly will be needed to design and tune this system.
- The electrical requirements of the actuation system will be provided by the vehicle's stator. There is a limited amount of power available from this system, which must be taken into account.

# Current Draw Analysis

Component	Max Limits (A)	Duty Cycle	Average (A)
Motec and Sensors	2.5	1	2.5
MW Power	6	1	6
Dash	2	1	2
Brake Light	0.5	0.2	0.1
Fuel Pump	5.4	1	5.4
Fan	7.4	1	7.4
Shift Solenoids	0.5	0.2	0.1
TCMX	1	1	1
Wheel Speed Sensors	0.8	1	0.8
Intake Actuation System	0.5	0.5	0.25
Totals	26.6	7.9	25.55



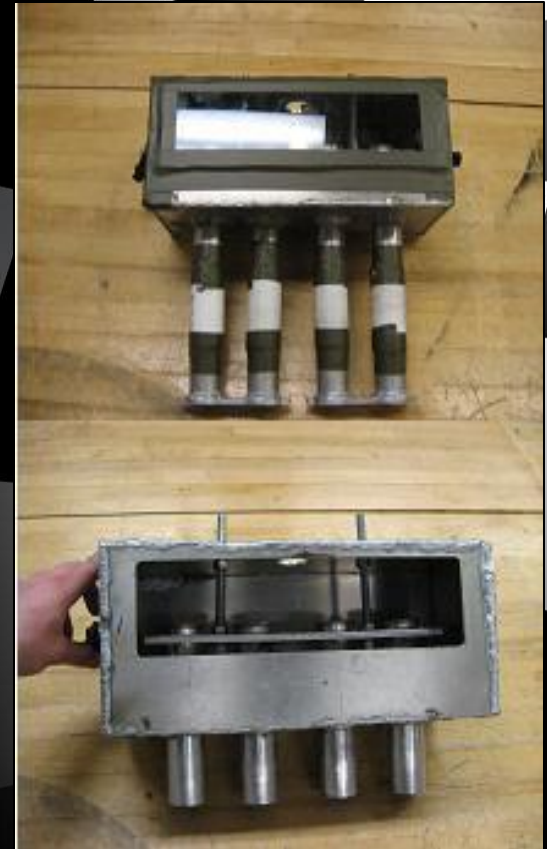
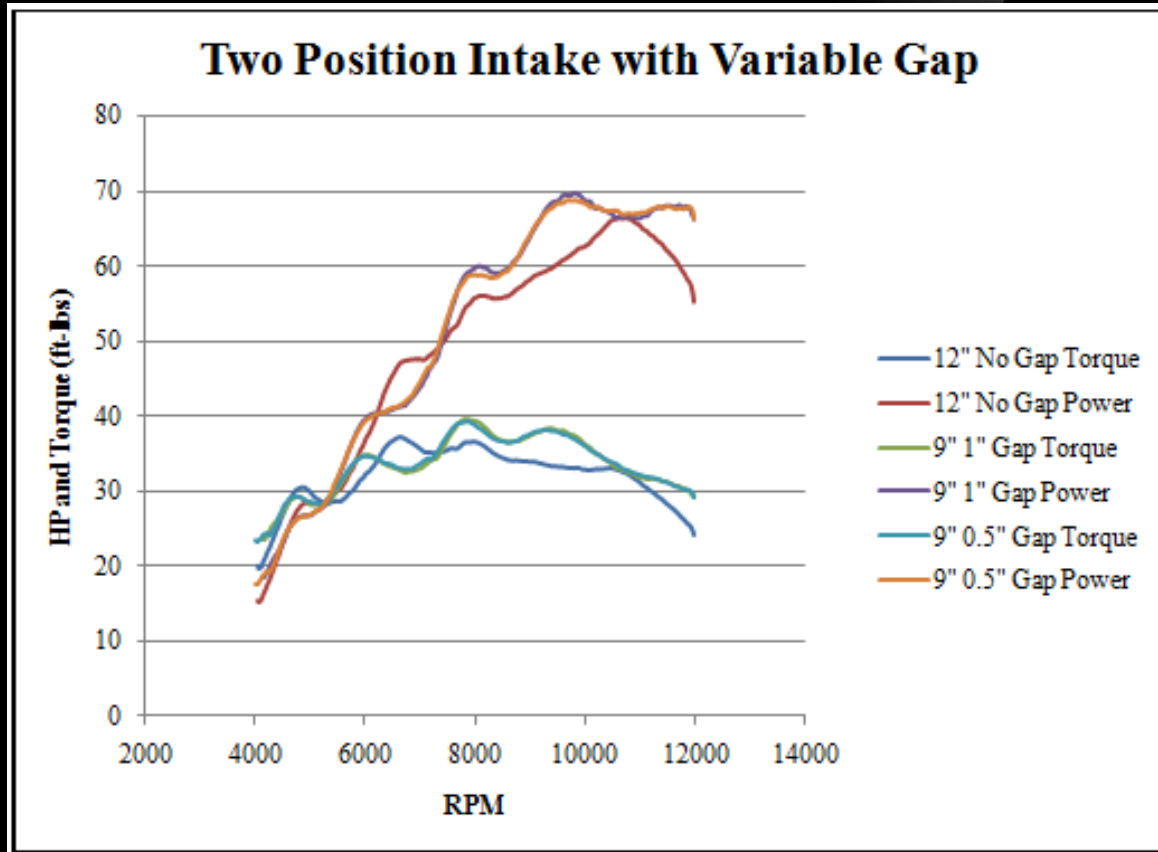
# Preliminary Testing Results



To find the runner lengths that achieved the best possible torque and horsepower, we modified a previous intake into our first prototype so that the runner length was adjustable. Testing was performed at inch increments from 6" through 12". As you can see from the graph above, the best resulting lengths are 12", 11" and 9". Using this data, a second prototype was created.

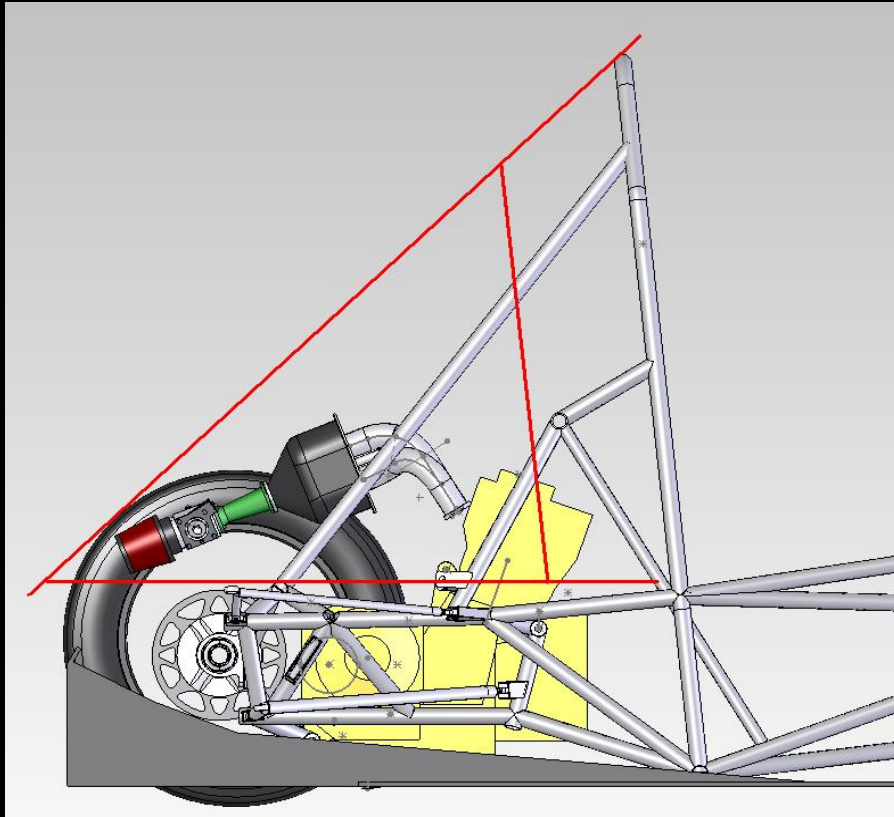


# Preliminary Testing Results



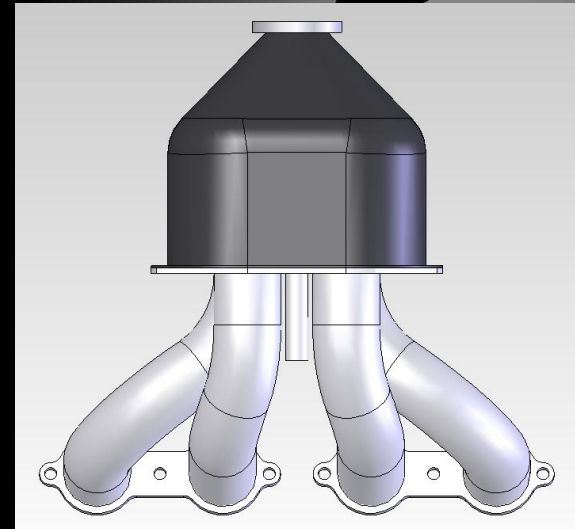
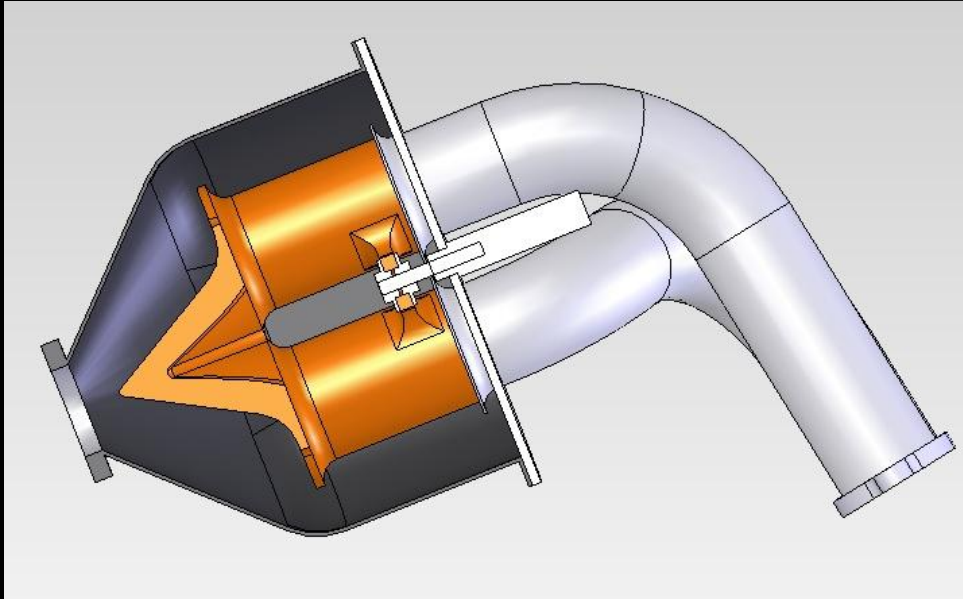
To mimic a two position system with the desired torque and horsepower peaks, we modified an existing plenum to fit the extending runners with an adjustable gap. When the intake was in long mode, the gap was closed and the total runner length was 12 inches. When the intake was in short mode, the gap was open and the total runner length was 9 inches. The open gap length was tested a multiple length in order to determine differences in yielding horsepower and torque. As a result, the optimal gap length to be used in the final design is 0.5 inches.

# Finalized Intake Design



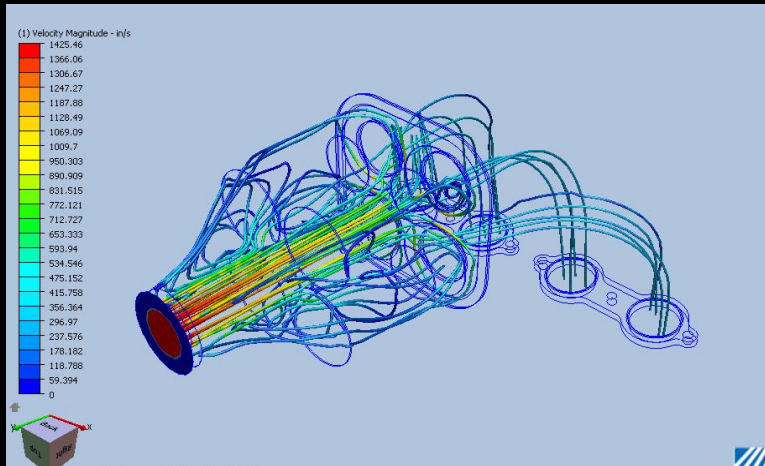
Packaging: The geometry of the chassis, as well as the governing rulebook, defines the packaging area for the intake system. The intake must lie within the area outlined below.

# Finalized Intake Design

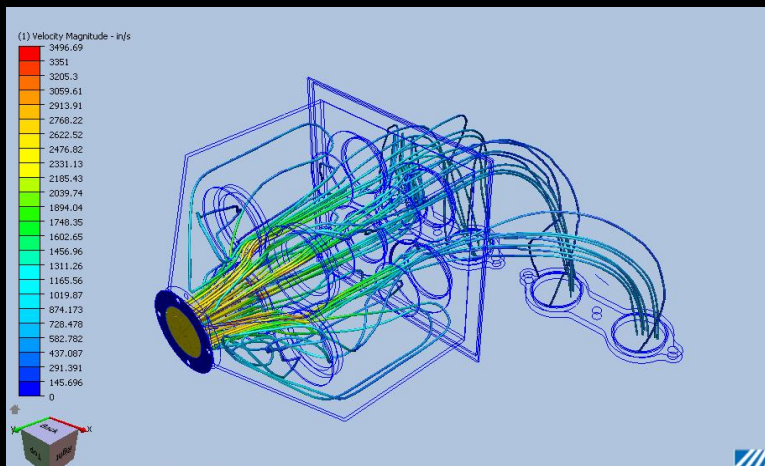


# Finalized Intake Design

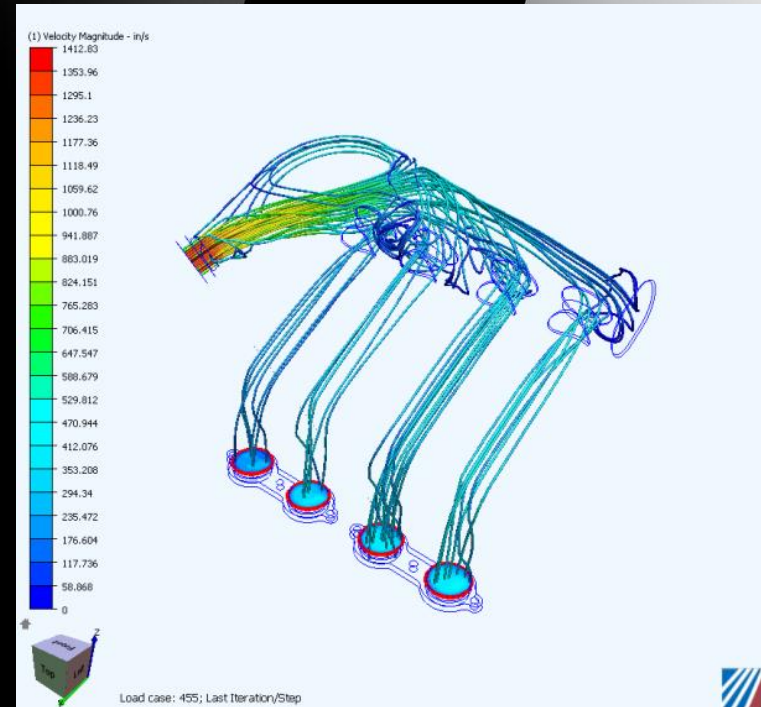
## CFD Analysis



Intake System without Spike to Direct Flow into Runners



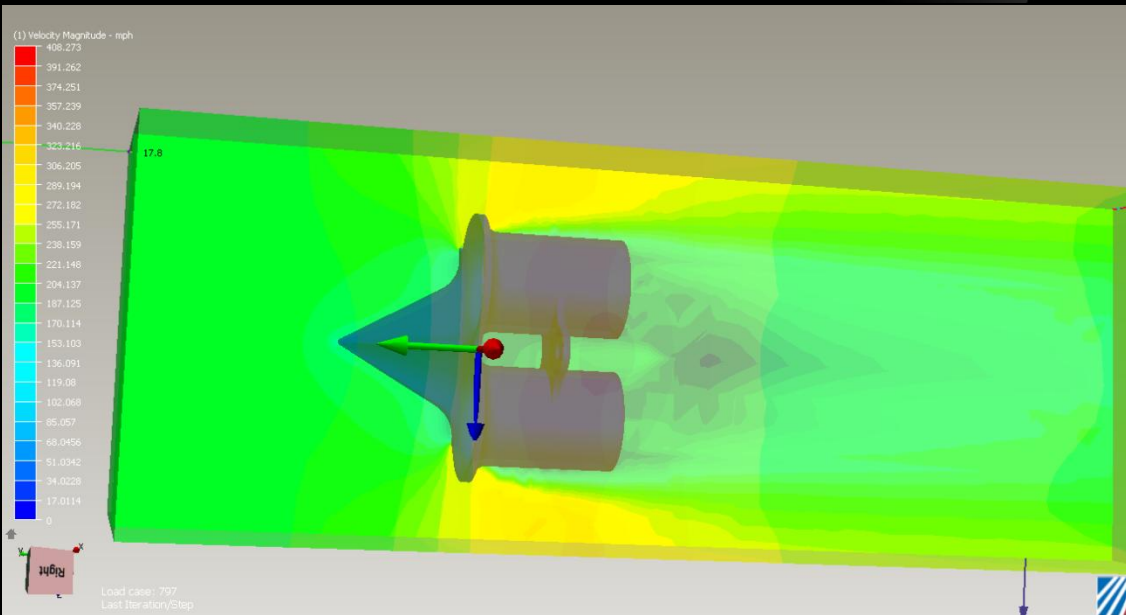
Intake System with Spike to Direct Flow into Runners



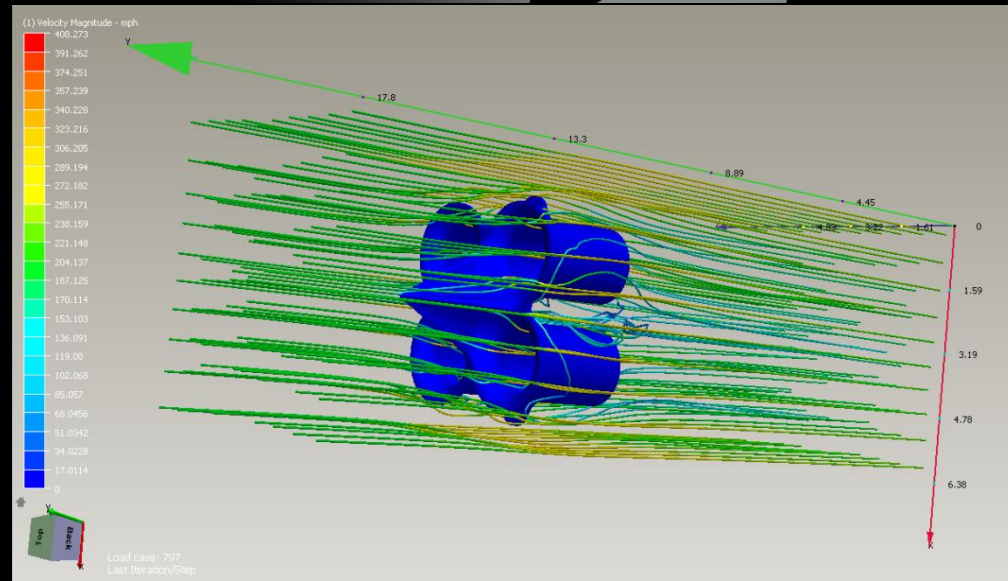
Previous Design



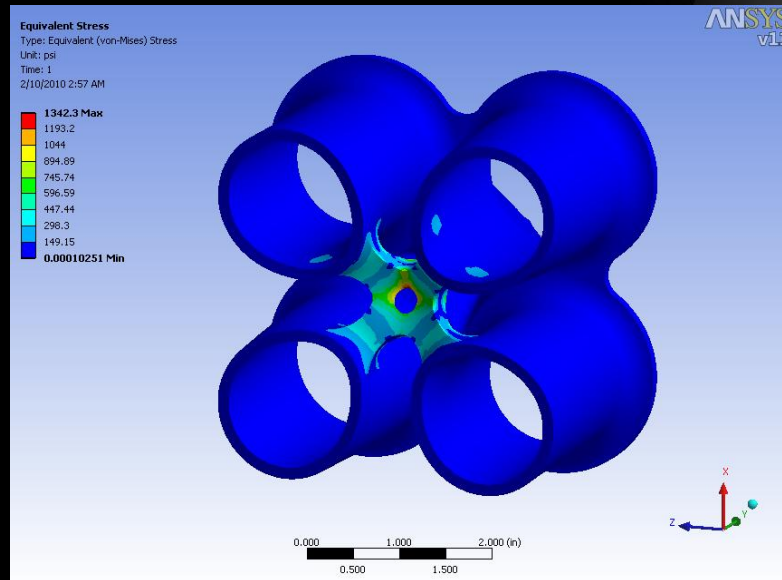
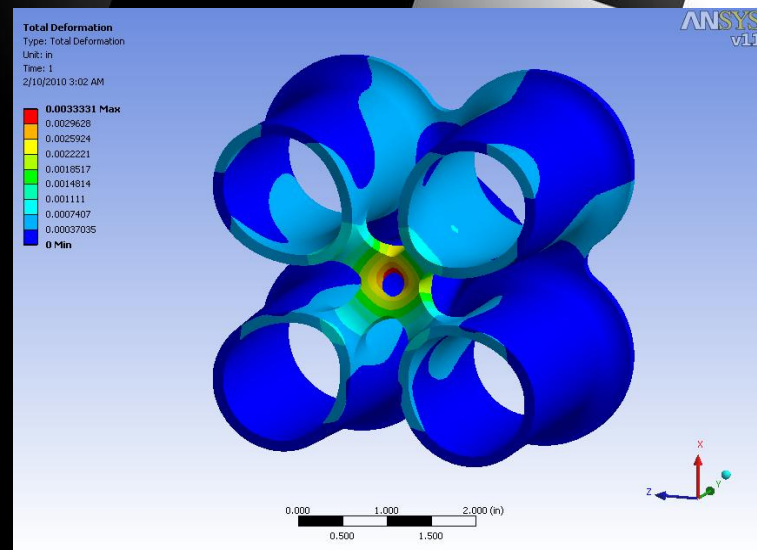
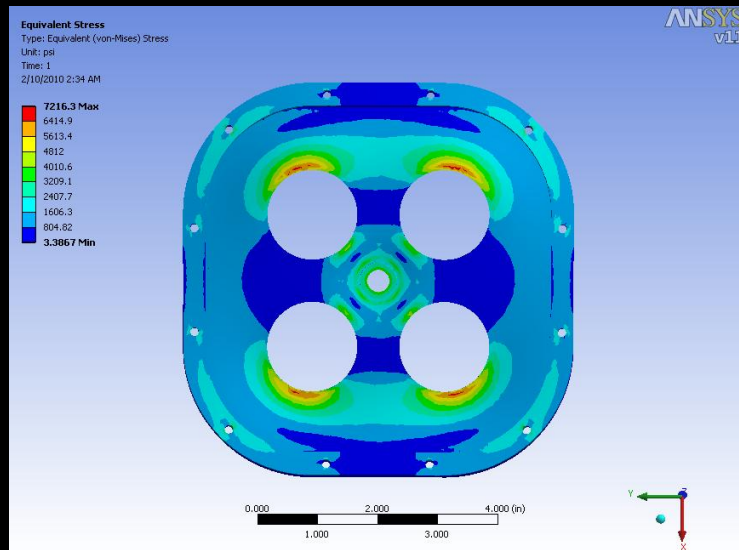
# Finalized Intake Design



## CFD Analysis

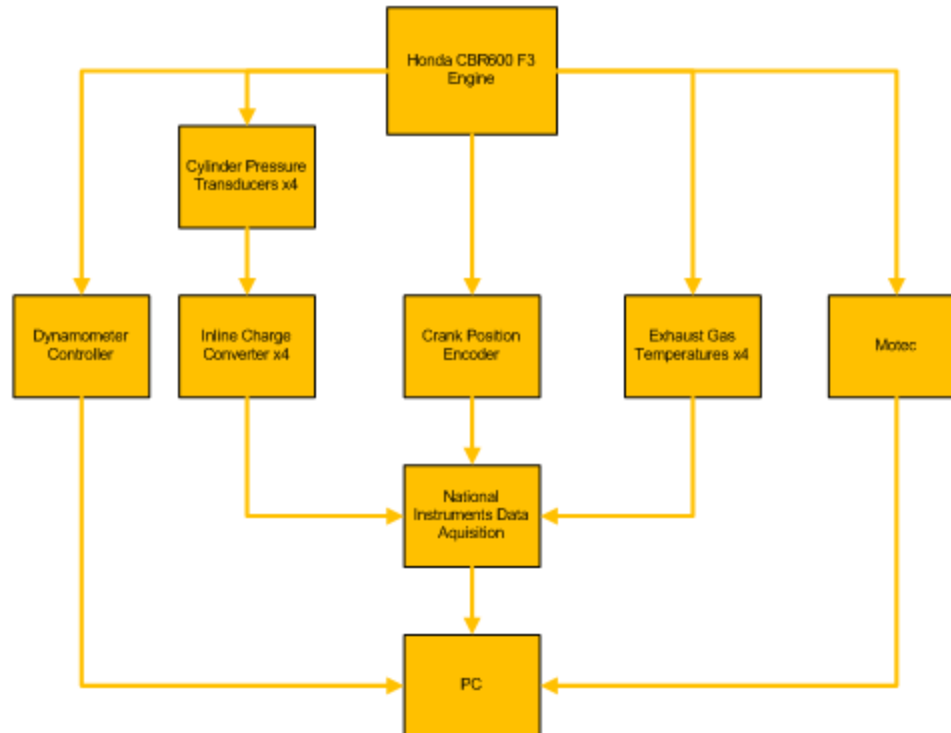


# Finalized Intake Design



# Electrical Integration and Assembly

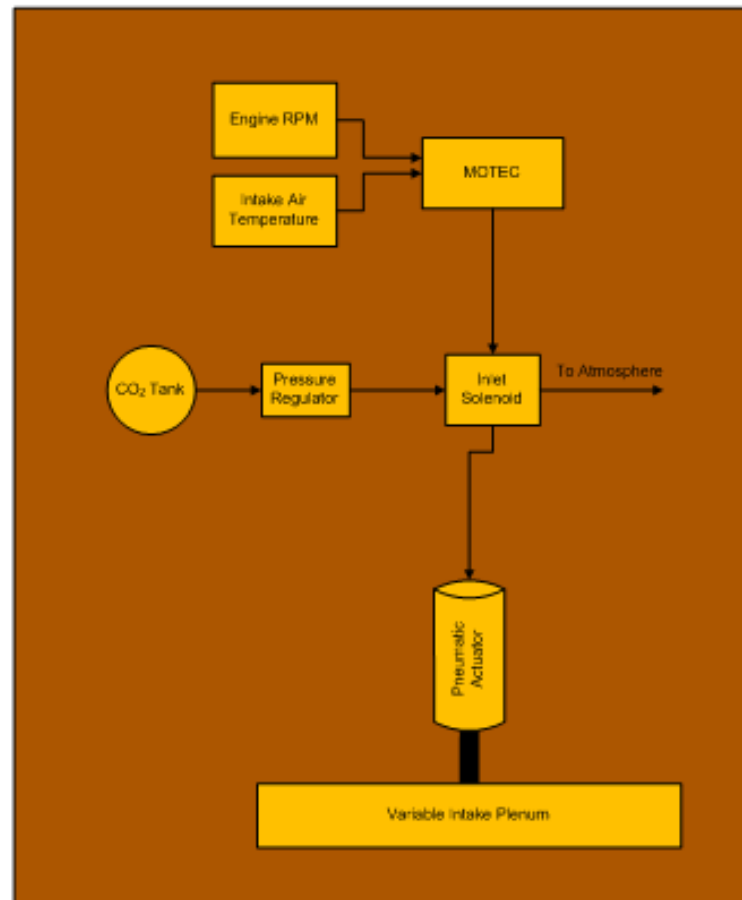
Dynamometer Test Layout



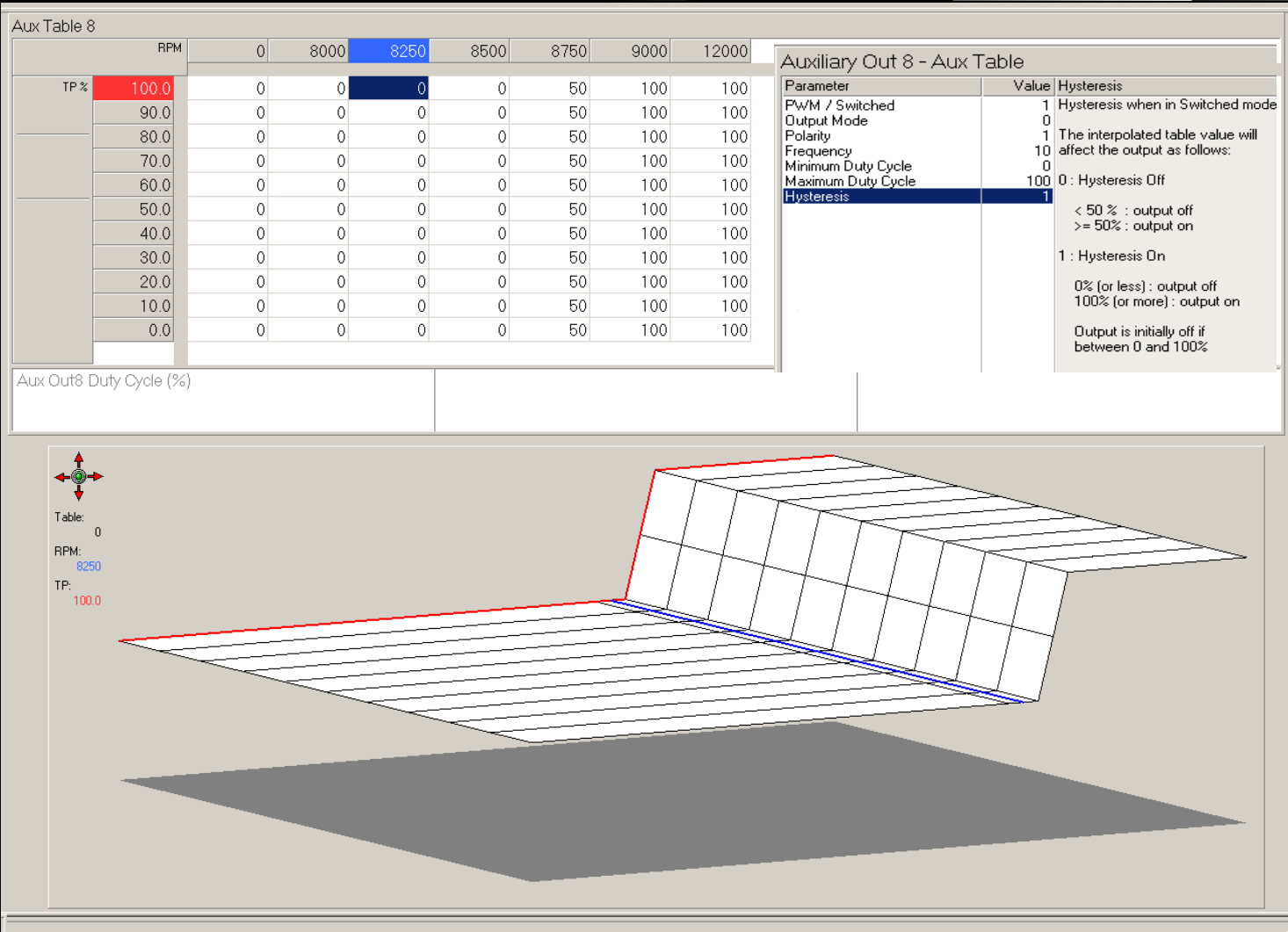


# Electrical Integration and Assembly

## Intake System Design



# Intake Actuation Map



# Next Steps...Manufacturing

Rapid Prototyping



Composites



Aluminum



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# Questions?

