

1. Let's start with the separate-variable ansatz for the  $\rho < a$  and  $\rho > a$  region respectively:

$$E_z = E(\rho) e^{im\phi} e^{ikz} \quad H_z = H(\rho) e^{im\phi} e^{ikz} \quad (1)$$

Within the core  $\rho < a$ , we have  $\nabla_t n_1^2 = 0$ , which turns (8.127) into

$$\nabla_t^2 [\psi(\rho) e^{im\phi}] + \gamma^2 \psi(\rho) e^{im\phi} = 0 \quad \Rightarrow \quad \frac{1}{\rho} \frac{d}{d\rho} (\rho \psi) + \left( \gamma^2 - \frac{m^2}{\rho} \right) \psi = 0 \quad \gamma^2 = \frac{n_1^2 \omega^2}{c^2} - k^2 \quad (2)$$

where  $\psi(\rho)$  can be either  $E_z(\rho)$  or  $H_z(\rho)$ . This is the Bessel equation (see (3.75)), whose solution is the linear combination of  $J_m(\gamma\rho)$  and  $N_m(\gamma\rho)$ . Since the core contains the axis where  $\rho = 0$ ,  $N_m(\gamma\rho)$  must be rejected, giving the solution form

$$E_z = A_e J_m(\gamma\rho) e^{im\phi} \quad H_z = A_h J_m(\gamma\rho) e^{im\phi} \quad \text{for } \rho < a \quad (3)$$

For the cladding region, let

$$\beta^2 = k^2 - \frac{n_2^2 \omega^2}{c^2} \quad (4)$$

then for  $\rho > a$  where  $\nabla_t n_2^2 = 0$ , (8.127) has the form

$$\nabla_t^2 [\psi(\rho) e^{im\phi}] - \beta^2 \psi(\rho) e^{im\phi} = 0 \quad \Rightarrow \quad \frac{1}{\rho} \frac{d}{d\rho} (\rho \psi) - \left( \beta^2 + \frac{m^2}{\rho} \right) \psi = 0 \quad (5)$$

which is the modified Bessel equation (see (3.98)), whose solution is the linear combination of  $I_m(\beta\rho)$  and  $K_m(\beta\rho)$ . We reject  $I_m(\beta\rho)$  for its divergence at the infinity, hence

$$E_z = B_e K_m(\beta\rho) e^{im\phi} \quad H_z = B_h K_m(\beta\rho) e^{im\phi} \quad \text{for } \rho > a \quad (6)$$

The corresponding gradients are

$$\text{for } \rho < a \quad \nabla_t E_z = A_e \left[ \gamma J'_m(\gamma\rho) \hat{\rho} + \frac{im}{\rho} J_m(\gamma\rho) \hat{\phi} \right] e^{im\phi} \quad \nabla_t H_z = A_h \left[ \gamma J'_m(\gamma\rho) \hat{\rho} + \frac{im}{\rho} J_m(\gamma\rho) \hat{\phi} \right] e^{im\phi} \quad (7)$$

$$\text{for } \rho > a \quad \nabla_t E_z = B_e \left[ \beta K'_m(\beta\rho) \hat{\rho} + \frac{im}{\rho} K_m(\beta\rho) \hat{\phi} \right] e^{im\phi} \quad \nabla_t H_z = B_h \left[ \beta K'_m(\beta\rho) \hat{\rho} + \frac{im}{\rho} K_m(\beta\rho) \hat{\phi} \right] e^{im\phi} \quad (8)$$

With  $\hat{z} \times \hat{\rho} = \hat{\phi}$ ,  $\hat{z} \times \hat{\phi} = -\hat{\rho}$  and (8.126), we have for the core region  $\rho < a$ ,

$$\begin{aligned} \mathbf{E}_t &= \frac{i}{\gamma^2} (k \nabla_t E_z - \omega \mu_0 \hat{z} \times \nabla_t H_z) \\ &= \frac{i}{\gamma^2} \left\{ k A_e \left[ \gamma J'_m(\gamma\rho) \hat{\rho} + \frac{im}{\rho} J_m(\gamma\rho) \hat{\phi} \right] e^{im\phi} - \omega \mu_0 A_h \left[ \gamma J'_m(\gamma\rho) \hat{\phi} - \frac{im}{\rho} J_m(\gamma\rho) \hat{\rho} \right] e^{im\phi} \right\} \\ &= \hat{\rho} \left[ \frac{ik A_e}{\gamma} J'_m(\gamma\rho) - \frac{m \omega \mu_0 A_h}{\gamma^2 \rho} J_m(\gamma\rho) \right] e^{im\phi} - \hat{\phi} \left[ \frac{mk A_e}{\gamma^2 \rho} J_m(\gamma\rho) + \frac{i \omega \mu_0 A_h}{\gamma} J'_m(\gamma\rho) \right] e^{im\phi} \end{aligned} \quad (9)$$

$$\begin{aligned} \mathbf{H}_t &= \frac{i}{\gamma^2} (k \nabla_t H_z + \omega \epsilon_0 n_1^2 \hat{z} \times \nabla_t E_z) \\ &= \frac{i}{\gamma^2} \left\{ k A_h \left[ \gamma J'_m(\gamma\rho) \hat{\rho} + \frac{im}{\rho} J_m(\gamma\rho) \hat{\phi} \right] e^{im\phi} + \omega \epsilon_0 n_1^2 A_e \left[ \gamma J'_m(\gamma\rho) \hat{\phi} - \frac{im}{\rho} J_m(\gamma\rho) \hat{\rho} \right] e^{im\phi} \right\} \\ &= \hat{\rho} \left[ \frac{ik A_h}{\gamma} J'_m(\gamma\rho) + \frac{m \omega \epsilon_0 n_1^2 A_e}{\gamma^2 \rho} J_m(\gamma\rho) \right] e^{im\phi} - \hat{\phi} \left[ \frac{mk A_h}{\gamma^2 \rho} J_m(\gamma\rho) - \frac{i \omega \epsilon_0 n_1^2 A_e}{\gamma} J'_m(\gamma\rho) \right] e^{im\phi} \end{aligned} \quad (10)$$

Note that the definition of  $\beta^2$  differs from  $\gamma^2$  by a minus sign, we must replace  $\gamma^2 \rightarrow -\beta^2$  in (8.126) to obtain the cladding's transverse fields, hence for  $\rho > a$ ,

$$\mathbf{E}_t = -\hat{\rho} \left[ \frac{ik B_e}{\beta} K'_m(\beta\rho) - \frac{m \omega \mu_0 B_h}{\beta^2 \rho} K_m(\beta\rho) \right] e^{im\phi} + \hat{\phi} \left[ \frac{mk B_e}{\beta^2 \rho} K_m(\beta\rho) + \frac{i \omega \mu_0 B_h}{\beta} K'_m(\beta\rho) \right] e^{im\phi} \quad (11)$$

$$\mathbf{H}_t = -\hat{\rho} \left[ \frac{ik B_h}{\beta} K'_m(\beta\rho) + \frac{m \omega \epsilon_0 n_2^2 B_e}{\beta^2 \rho} K_m(\beta\rho) \right] e^{im\phi} + \hat{\phi} \left[ \frac{mk B_h}{\beta^2 \rho} K_m(\beta\rho) - \frac{i \omega \epsilon_0 n_2^2 B_e}{\beta} K'_m(\beta\rho) \right] e^{im\phi} \quad (12)$$

Boundary conditions dictate that normal  $\mathbf{D}$  and  $\mathbf{B}$ , as well as tangential  $\mathbf{E}$  and  $\mathbf{H}$  be continuous across  $\rho = a$

$$\text{normal } \mathbf{B} : \quad \frac{ikA_h}{\gamma} J'_m(\gamma a) + \frac{m\omega\epsilon_0 n_1^2 A_e}{\gamma^2 a} J_m(\gamma a) = - \left[ \frac{ikB_h}{\beta} K'_m(\beta a) + \frac{m\omega\epsilon_0 n_2^2 B_e}{\beta^2 a} K_m(\beta a) \right] \quad (13)$$

$$\text{normal } \mathbf{D} : \quad n_1^2 \left[ \frac{ikA_e}{\gamma} J'_m(\gamma a) - \frac{m\omega\mu_0 A_h}{\gamma^2 a} J_m(\gamma a) \right] = -n_2^2 \left[ \frac{ikB_e}{\beta} K'_m(\beta a) - \frac{m\omega\mu_0 B_h}{\beta^2 a} K_m(\beta a) \right] \quad (14)$$

$$\text{tangential } (\hat{\mathbf{z}}) \mathbf{H} : \quad A_h J_m(\gamma a) = B_h K_m(\beta a) \quad (15)$$

$$\text{tangential } (\hat{\phi}) \mathbf{H} : \quad \frac{mkA_h}{\gamma^2 a} J_m(\gamma a) - \frac{i\omega\epsilon_0 n_1^2 A_e}{\gamma} J'_m(\gamma a) = - \left[ \frac{mkB_h}{\beta^2 a} K_m(\beta a) - \frac{i\omega\epsilon_0 n_2^2 B_e}{\beta} K'_m(\beta a) \right] \quad (16)$$

$$\text{tangential } (\hat{\mathbf{z}}) \mathbf{E} : \quad A_e J_m(\gamma a) = B_e K_m(\beta a) \quad (17)$$

$$\text{tangential } (\hat{\phi}) \mathbf{E} : \quad \frac{mkA_e}{\gamma^2 a} J_m(\gamma a) + \frac{i\omega\mu_0 A_h}{\gamma} J'_m(\gamma a) = - \left[ \frac{mkB_e}{\beta^2 a} K_m(\beta a) + \frac{i\omega\mu_0 B_h}{\beta} K'_m(\beta a) \right] \quad (18)$$

Eliminating the  $B$ 's in (16) and (18) using (15) and (17), we get

$$\begin{aligned} \frac{mkA_h}{\gamma^2 a} J_m - \frac{i\omega\epsilon_0 n_1^2 A_e}{\gamma} J'_m &= - \left[ \frac{mkA_h}{\beta^2 a} J_m - \frac{i\omega\epsilon_0 n_2^2 A_e}{\beta} \frac{K'_m}{K_m} J_m \right] \implies \\ \left( \frac{1}{\gamma^2} + \frac{1}{\beta^2} \right) \frac{mkA_h}{a} &= \left( \frac{n_1^2}{\gamma} \frac{J'_m}{J_m} + \frac{n_2^2}{\beta} \frac{K'_m}{K_m} \right) i\omega\epsilon_0 A_e \end{aligned} \quad (19)$$

$$\begin{aligned} \frac{mkA_e}{\gamma^2 a} J_m + \frac{i\omega\mu_0 A_h}{\gamma} J'_m &= - \left[ \frac{mkA_e}{\beta^2 a} J_m + \frac{i\omega\mu_0 A_h}{\beta} \frac{K'_m}{K_m} J_m \right] \implies \\ \left( \frac{1}{\gamma^2} + \frac{1}{\beta^2} \right) \frac{mkA_e}{a} &= - \left( \frac{1}{\gamma} \frac{J'_m}{J_m} + \frac{1}{\beta} \frac{K'_m}{K_m} \right) i\omega\mu_0 A_h \end{aligned} \quad (20)$$

When  $m \neq 0$ , we can further eliminate  $A_e, A_h$  from (19) and (20)

$$\left( \frac{1}{\gamma^2} + \frac{1}{\beta^2} \right)^2 \frac{m^2}{a^2} k^2 = \left( \frac{n_1^2}{\gamma} \frac{J'_m}{J_m} + \frac{n_2^2}{\beta} \frac{K'_m}{K_m} \right) \left( \frac{1}{\gamma} \frac{J'_m}{J_m} + \frac{1}{\beta} \frac{K'_m}{K_m} \right) \frac{\omega^2}{c^2} \quad (21)$$

Finally, from (2) and (4), we can express  $k^2, \omega^2/c^2$  in terms of  $\gamma^2, \beta^2$ ,

$$k^2 = \frac{n_2^2 \gamma^2 + n_1^2 \beta^2}{n_1^2 - n_2^2} \quad \frac{\omega^2}{c^2} = \frac{\gamma^2 + \beta^2}{n_1^2 - n_2^2} \quad (22)$$

and (21) is turned into the desired form

$$\frac{m^2}{a^2} \left( \frac{1}{\gamma^2} + \frac{1}{\beta^2} \right) \left( \frac{n_1^2}{\gamma^2} + \frac{n_2^2}{\beta^2} \right) = \left( \frac{n_1^2}{\gamma} \frac{J'_m}{J_m} + \frac{n_2^2}{\beta} \frac{K'_m}{K_m} \right) \left( \frac{1}{\gamma} \frac{J'_m}{J_m} + \frac{1}{\beta} \frac{K'_m}{K_m} \right) \quad (23)$$

It is worth noting that we have not used (13) and (14) when we derive (21), this is because they are redundant as a result of the ansatz satisfying the Maxwell equations. To verify this, (13) and (14) can be rewritten

$$ikA_h \left( \frac{1}{\gamma} \frac{J'_m}{J_m} + \frac{1}{\beta} \frac{K'_m}{K_m} \right) = - \frac{m\omega\epsilon_0 A_e}{a} \left( \frac{n_1^2}{\gamma^2} + \frac{n_2^2}{\beta^2} \right) \quad (24)$$

$$ikA_e \left( \frac{n_1^2}{\gamma} \frac{J'_m}{J_m} + \frac{n_2^2}{\beta} \frac{K'_m}{K_m} \right) = \frac{m\omega\mu_0 A_h}{a} \left( \frac{n_1^2}{\gamma^2} + \frac{n_2^2}{\beta^2} \right) \quad (25)$$

which would have required

$$k^2 \left( \frac{1}{\gamma} \frac{J'_m}{J_m} + \frac{1}{\beta} \frac{K'_m}{K_m} \right) \left( \frac{n_1^2}{\gamma} \frac{J'_m}{J_m} + \frac{n_2^2}{\beta} \frac{K'_m}{K_m} \right) = \frac{m^2}{a^2} \frac{\omega^2}{c^2} \left( \frac{n_1^2}{\gamma^2} + \frac{n_2^2}{\beta^2} \right)^2 \quad (26)$$

which is equivalent to the eigenequation (23).

2. For  $m = 0$ , (19) and (20) still hold. We have a TM mode and TE mode:

$$\text{TE mode : } A_h \neq 0 \implies \frac{1}{\gamma} \frac{J'_0}{J_0} + \frac{1}{\beta} \frac{K'_0}{K_0} = 0 \quad \text{TM mode : } A_e \neq 0 \implies \frac{n_1^2}{\gamma} \frac{J'_0}{J_0} + \frac{n_2^2}{\beta} \frac{K'_0}{K_0} = 0 \quad (27)$$

At cutoff, we require  $\beta = 0$  so there is no radiation outside of the core. For the eigenequation (27) to make sense, we must have  $J_0(\gamma a) = 0$ . It is easy to verify that when  $\beta = 0$  and  $\gamma a = x_{01}$ ,  $V = n_1 \omega a \sqrt{2\Delta}/c = x_{01} = 2.405$ .

3. Omitted (this problem is covered in details in section 12-9 in *Optical Waveguide Theory* by A.W. Snyder and J.D. Love).