

We will give the most general solution to this three-media reflection/transmission problem, where we assume arbitrary incident angle and permeability of the media.

Let $\mathbf{E}_1/\mathbf{B}_1$ be the incident wave. We expect it to generate a reflected wave $\mathbf{E}'_1/\mathbf{B}'_1$ and a transmitted wave $\mathbf{E}_2/\mathbf{B}_2$ at the n_1/n_2 boundary. Then $\mathbf{E}_2/\mathbf{B}_2$ is going to generate a reflected wave and a transmitted wave $\mathbf{E}'_2/\mathbf{B}'_2$ and $\mathbf{E}_3/\mathbf{B}_3$ at the n_2/n_3 boundary.

All the $\mathbf{E}, \mathbf{B}, \mathbf{k}$ vectors have the wave form

$$\mathbf{E}(\mathbf{x}, t) = \mathbf{E}e^{i\mathbf{k}\cdot\mathbf{x} - i\omega t} \quad (1)$$

$$\mathbf{B}(\mathbf{x}, t) = \sqrt{\mu\epsilon} \frac{\mathbf{k} \times \mathbf{E}(\mathbf{x}, t)}{|\mathbf{k}|} \quad (2)$$

$$|\mathbf{k}| = \omega\sqrt{\mu\epsilon} = \frac{n\omega}{c} \quad (3)$$

The boundary conditions are given by the Maxwell's equations:

n_1/n_2 boundary

$$[\epsilon_1(\mathbf{E}_1 + \mathbf{E}'_1) - \epsilon_2(\mathbf{E}_2 + \mathbf{E}'_2)] \cdot \mathbf{n}_{12} = 0$$

$$(\mathbf{k}_1 \times \mathbf{E}_1 + \mathbf{k}'_1 \times \mathbf{E}'_1 - \mathbf{k}_2 \times \mathbf{E}_2 - \mathbf{k}'_2 \times \mathbf{E}'_2) \cdot \mathbf{n}_{12} = 0$$

$$(\mathbf{E}_1 + \mathbf{E}'_1 - \mathbf{E}_2 - \mathbf{E}'_2) \times \mathbf{n}_{12} = 0$$

$$\left[\frac{1}{\mu_1} (\mathbf{k}_1 \times \mathbf{E}_1 + \mathbf{k}'_1 \times \mathbf{E}'_1) - \frac{1}{\mu_2} (\mathbf{k}_2 \times \mathbf{E}_2 + \mathbf{k}'_2 \times \mathbf{E}'_2) \right] \times \mathbf{n}_{12} = 0 \quad (4)$$

n_2/n_3 boundary

$$[\epsilon_2(\mathbf{E}_2 + \mathbf{E}'_2) - \epsilon_3\mathbf{E}_3] \cdot \mathbf{n}_{23} = 0 \quad (5)$$

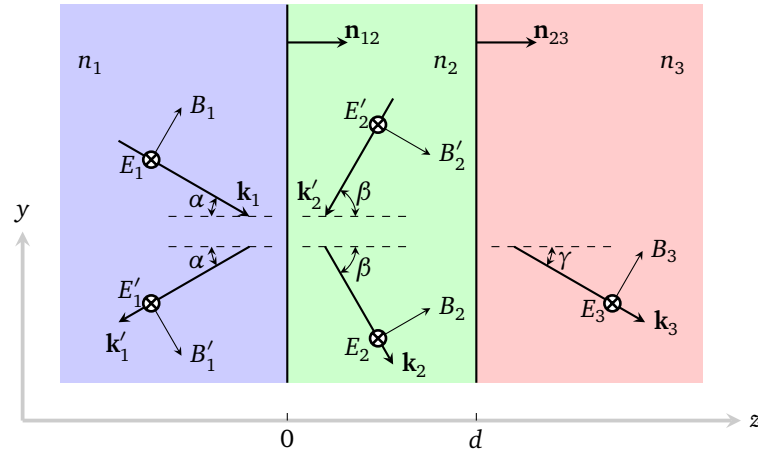
$$(\mathbf{k}_2 \times \mathbf{E}_2 + \mathbf{k}'_2 \times \mathbf{E}'_2 - \mathbf{k}_3 \times \mathbf{E}_3) \cdot \mathbf{n}_{23} = 0 \quad (6)$$

$$(\mathbf{E}_2 + \mathbf{E}'_2 - \mathbf{E}_3) \times \mathbf{n}_{23} = 0 \quad (7)$$

$$\left[\frac{1}{\mu_2} (\mathbf{k}_2 \times \mathbf{E}_2 + \mathbf{k}'_2 \times \mathbf{E}'_2) - \frac{1}{\mu_3} (\mathbf{k}_3 \times \mathbf{E}_3) \right] \times \mathbf{n}_{23} = 0 \quad (8)$$

Similar to the text, we are going to treat the two linear polarization cases separately.

1. \mathbf{E} is perpendicular to the plane of incidence.



Consider (6) for the n_2/n_3 boundary,

$$(E_2 e^{i\mathbf{k}_2 \cdot \mathbf{x}} + E'_2 e^{i\mathbf{k}'_2 \cdot \mathbf{x}} - E_3 e^{i\mathbf{k}_3 \cdot \mathbf{x}}) e^{-i\omega t} = 0 \quad \text{for all } t \text{ and all } \mathbf{x} \text{ on } z = d \text{ plane} \quad (9)$$

This implies

$$E_2 e^{ik_{2z}d} e^{i(k_{2x}x + k_{2y}y)} + E'_2 e^{ik'_{2z}d} e^{i(k'_{2x}x + k'_{2y}y)} - E_3 e^{ik_{3z}d} e^{i(k_{3x}x + k_{3y}y)} = 0 \quad \text{for all } x, y \quad (10)$$

Now for the fixed complex numbers $E_2 e^{ik_{2z}d}, E'_2 e^{ik'_{2z}d}, E_3 e^{ik_{3z}d}$, the only way for (9) to be consistent for all x, y is for the phase factors to be identical, i.e.,

$$\begin{aligned} k_{2x}x + k_{2y}y &= k'_{2x}x + k'_{2y}y = k_{3x}x + k_{3y}y & \implies \\ \mathbf{k}_2 \cdot (\mathbf{x} - d\hat{\mathbf{z}}) &= \mathbf{k}'_2 \cdot (\mathbf{x} - d\hat{\mathbf{z}}) = \mathbf{k}_3 \cdot (\mathbf{x} - d\hat{\mathbf{z}}) & \text{for all } \mathbf{x} \text{ on } z = d \text{ plane} \end{aligned} \quad (11)$$

This is just the expected reflection symmetry and Snell's law.

(9) is now turned into

$$E_2 e^{ik_2 d \cos \beta} + E'_2 e^{-ik_2 d \cos \beta} - E_3 e^{ik_3 d \cos \gamma} = 0 \quad (11)$$

With this, we can rewrite (7) for n_2/n_3 boundary as

$$\sqrt{\frac{\epsilon_2}{\mu_2}} \cos \beta (E_2 e^{ik_2 d \cos \beta} - E'_2 e^{-ik_2 d \cos \beta}) - \sqrt{\frac{\epsilon_3}{\mu_3}} \cos \gamma (E_3 e^{ik_3 d \cos \gamma}) = 0 \quad (12)$$

(11) and (12) are essentially (7.38) since they describe the same two-media reflection and transmission, aside from the phase factor which is due to the origin shift. This allows us to use (7.39) to express E'_2 and E_3 in terms of E_2 :

$$E_3 = E_2 \overbrace{\left(\frac{2n_2 \cos \beta}{n_2 \cos \beta + \frac{\mu_2}{\mu_3} n_3 \cos \gamma} \right)}^{t_{23}} e^{i(k_2 \cos \beta - k_3 \cos \gamma)d} \quad (13)$$

$$E'_2 = E_2 \underbrace{\left(\frac{n_2 \cos \beta - \frac{\mu_2}{\mu_3} n_3 \cos \gamma}{n_2 \cos \beta + \frac{\mu_2}{\mu_3} n_3 \cos \gamma} \right)}_{r_{23}} e^{i2k_2 d \cos \beta} \quad (14)$$

Coming back to the n_1/n_2 boundary, (6) gives

$$(E_1 e^{ik_1 \cdot \mathbf{x}} + E'_1 e^{ik'_1 \cdot \mathbf{x}} - E_2 e^{ik_2 \cdot \mathbf{x}} - E'_2 e^{ik'_2 \cdot \mathbf{x}}) e^{-i\omega t} = 0 \quad \text{for all } t \text{ and all } \mathbf{x} \text{ on } z = 0 \text{ plane} \quad (15)$$

With similar arguments, we obtain

$$\mathbf{k}_1 \cdot \mathbf{x} = \mathbf{k}'_1 \cdot \mathbf{x} = \mathbf{k}_2 \cdot \mathbf{x} = \mathbf{k}'_2 \cdot \mathbf{x} \quad \text{for all } \mathbf{x} \text{ on } z = 0 \text{ plane} \quad (16)$$

which again gives the reflection symmetry and Snell's law.

(15) and (7) are equivalent to the restrictions

$$E_1 + E'_1 - E_2 - E'_2 = 0 \quad (17)$$

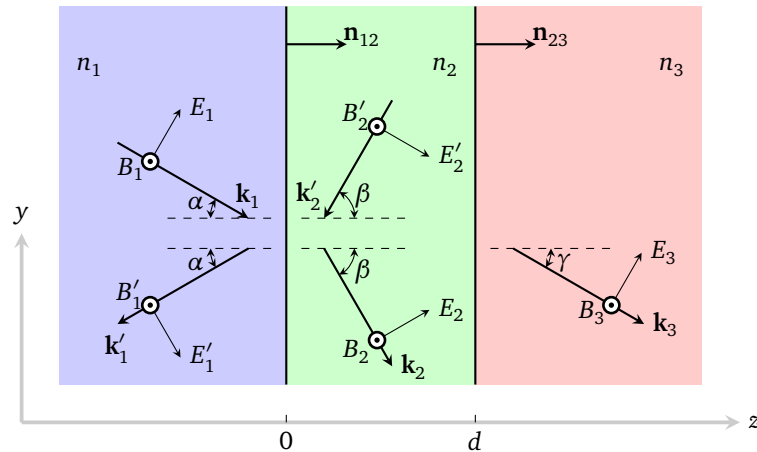
$$\sqrt{\frac{\epsilon_1}{\mu_1}} \cos \alpha (E_1 - E'_1) - \sqrt{\frac{\epsilon_2}{\mu_2}} \cos \beta (E_2 - E'_2) = 0 \quad (18)$$

We can get the solution using (14):

$$E'_1 = E_1 \left[\frac{(1 + r_{23}) n_1 \cos \alpha - \frac{\mu_1}{\mu_2} (1 - r_{23}) n_2 \cos \beta}{(1 + r_{23}) n_1 \cos \alpha + \frac{\mu_1}{\mu_2} (1 - r_{23}) n_2 \cos \beta} \right] \quad (19)$$

$$E_2 = E_1 \left[\frac{2n_1 \cos \alpha}{(1 + r_{23}) n_1 \cos \alpha + \frac{\mu_1}{\mu_2} (1 - r_{23}) n_2 \cos \beta} \right] \quad (20)$$

2. \mathbf{E} is parallel to the plane of incidence.



The process that determines reflection symmetry and Snell's law is similar to the perpendicular case above. Then (6) and (7) for the n_2/n_3 boundary require

$$\cos \beta (E_2 e^{ik_2 d \cos \beta} - E'_2 e^{-ik_2 d \cos \beta}) - \cos \gamma E_3 e^{ik_3 d \cos \gamma} = 0 \quad (21)$$

$$\sqrt{\frac{\epsilon_2}{\mu_2}} (E_2 e^{ik_2 d \cos \beta} + E'_2 e^{-ik_2 d \cos \beta}) - \sqrt{\frac{\epsilon_3}{\mu_3}} E_3 e^{ik_3 d \cos \gamma} = 0 \quad (22)$$

This can be solved using (7.41)

$$E_3 = E_2 \overbrace{\left(\frac{2n_2 \cos \beta}{\frac{\mu_2}{\mu_3} n_3 \cos \beta + n_2 \cos \gamma} \right)}^{t_{23}} e^{i(k_2 \cos \beta - k_3 \cos \gamma)d} \quad (23)$$

$$E'_2 = E_2 \underbrace{\left(\frac{\frac{\mu_2}{\mu_3} n_3 \cos \beta - n_2 \cos \gamma}{\frac{\mu_2}{\mu_3} n_3 \cos \beta + n_2 \cos \gamma} \right)}_{r_{23}} e^{i2k_2 d \cos \beta} \quad (24)$$

For the n_1/n_2 boundary, (6) and (7) require

$$\cos \alpha (E_1 - E'_1) - \cos \beta (E_2 - E'_2) = 0 \quad (25)$$

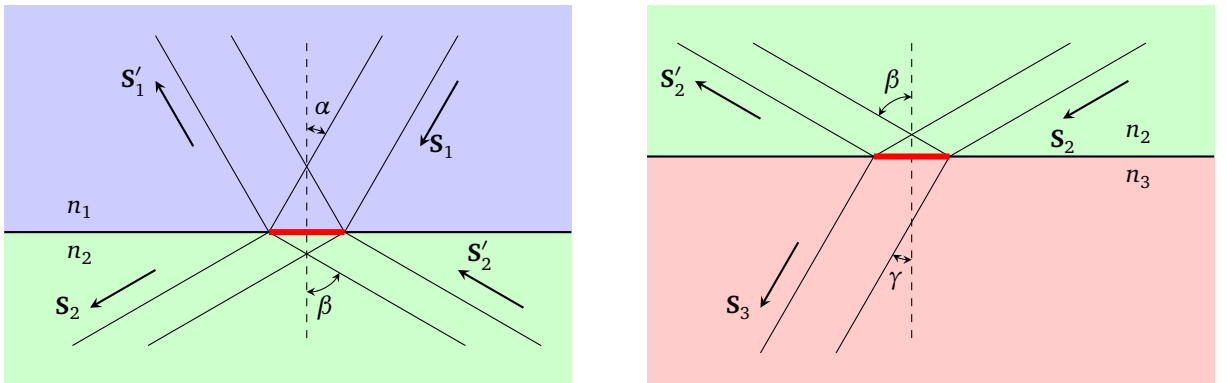
$$\sqrt{\frac{\epsilon_1}{\mu_1}} (E_1 + E'_1) - \sqrt{\frac{\epsilon_2}{\mu_2}} (E_2 + E'_2) = 0 \quad (26)$$

of which the solution is

$$E'_1 = E_1 \left[\frac{\frac{\mu_1}{\mu_2} (1 + r_{23}) n_2 \cos \alpha - (1 - r_{23}) n_1 \cos \beta}{\frac{\mu_1}{\mu_2} (1 + r_{23}) n_2 \cos \alpha + (1 - r_{23}) n_1 \cos \beta} \right] \quad (27)$$

$$E_2 = E_1 \left[\frac{2n_1 \cos \alpha}{\frac{\mu_1}{\mu_2} (1 + r_{23}) n_2 \cos \alpha + (1 - r_{23}) n_1 \cos \beta} \right] \quad (28)$$

3. We will now show how the Poynting flux is involved in the energy conservation of the reflection and transmission.



Let A be an area patch on the n_1/n_2 boundary. The energy incoming onto and outgoing from A are

| | |
|--|---------------------------------|
| incoming from n_1 as incident wave: | $ \mathbf{S}_1 A \cos \alpha$ |
| outgoing to n_1 as reflected wave: | $ \mathbf{S}'_1 A \cos \alpha$ |
| incoming from n_2 as reflected wave: | $ \mathbf{S}'_2 A \cos \beta$ |
| outgoing to n_2 as transmitted wave: | $ \mathbf{S}_2 A \cos \beta$ |

where \mathbf{S} is the Poynting vector of the corresponding wave

$$\mathbf{S} = \frac{1}{2} \mathbf{E} \times \mathbf{H}^* = \frac{1}{2c} \frac{n}{\mu} |E|^2 \hat{\mathbf{k}} \quad (29)$$

Thus for patch A, energy conservation means

$$\frac{n_1}{\mu_1} |E_1|^2 \cos \alpha + \frac{n_2}{\mu_2} |E_2'|^2 \cos \beta = \frac{n_1}{\mu_1} |E_1'|^2 \cos \alpha + \frac{n_2}{\mu_2} |E_2|^2 \cos \beta \quad (30)$$

Similarly for a patch A' on the n_2/n_3 boundary, three waves are involved, and energy conservation means

$$\frac{n_2}{\mu_2} |E_2|^2 \cos \beta = \frac{n_2}{\mu_2} |E_2'|^2 \cos \beta + \frac{n_3}{\mu_3} |E_3|^2 \cos \gamma \quad (31)$$

To see that our calculations agree with energy conservation, let's consider the perpendicular polarization case. Rewriting (17) and (18), and taking the complex conjugation for one of them, we get

$$E_1 + E_1' = E_2 + E_2' \quad (32)$$

$$\frac{n_1}{\mu_1} \cos \alpha (E_1^* - E_1'^*) = \frac{n_2}{\mu_2} \cos \beta (E_2^* - E_2'^*) \quad (33)$$

Multiplying (32) and (33) gives

$$\frac{n_1}{\mu_1} \cos \alpha (|E_1|^2 - |E_1'|^2 + E_1' E_1^* - E_1 E_1'^*) = \frac{n_2}{\mu_2} \cos \beta (|E_2|^2 - |E_2'|^2 + E_2' E_2^* - E_2 E_2'^*) \quad (34)$$

Since $E_1' E_1^* - E_1 E_1'^*$ and $E_2' E_2^* - E_2 E_2'^*$ are purely imaginary, (30) is obtained by taking the real part of (34).

The parallel polarization case can be proved similarly by rewriting (25) and (26). Same for the n_2/n_3 conservation equation (31).

Lastly, adding (30) and (31) will give

$$\frac{n_1}{\mu_1} |E_1|^2 \cos \alpha = \frac{n_1}{\mu_1} |E_1'|^2 \cos \alpha + \frac{n_3}{\mu_3} |E_3|^2 \cos \gamma \quad (35)$$

This is just a claim about the overall energy conservation while we ignore the role of the middle layer.

4. Solution to problem 7.2.

(a) Here we apply the simplifying assumption that $\mu_i = 1$ and $\alpha = \beta = \gamma = 0$, i.e., normal incidence.

i. For the perpendicular polarization (use (13)-(20)):

$$r_{23} = \frac{n_2 - n_3}{n_2 + n_3} e^{i2n_2\omega/\omega_0} \quad \text{where } \omega_0 \equiv \frac{c}{d} \quad (36)$$

$$\begin{aligned} |E_1'|^2 &= |E_1|^2 \left| \frac{(1 + r_{23})n_1 - (1 - r_{23})n_2}{(1 + r_{23})n_1 + (1 - r_{23})n_2} \right|^2 \implies \\ R &= \frac{|E_1'|^2}{|E_1|^2} = \left| \frac{(1 + r_{23})n_1 - (1 - r_{23})n_2}{(1 + r_{23})n_1 + (1 - r_{23})n_2} \right|^2 \end{aligned} \quad (37)$$

$$\begin{aligned} |E_3|^2 &= |E_1|^2 \left(\frac{2n_2}{n_2 + n_3} \right)^2 \left| \frac{2n_1}{(1 + r_{23})n_1 + (1 - r_{23})n_2} \right|^2 \implies \\ T &= \frac{n_3 |E_3|^2}{n_1 |E_1|^2} = \left(\frac{2n_2}{n_2 + n_3} \right)^2 \frac{4n_1 n_3}{|(1 + r_{23})n_1 + (1 - r_{23})n_2|^2} \end{aligned} \quad (38)$$

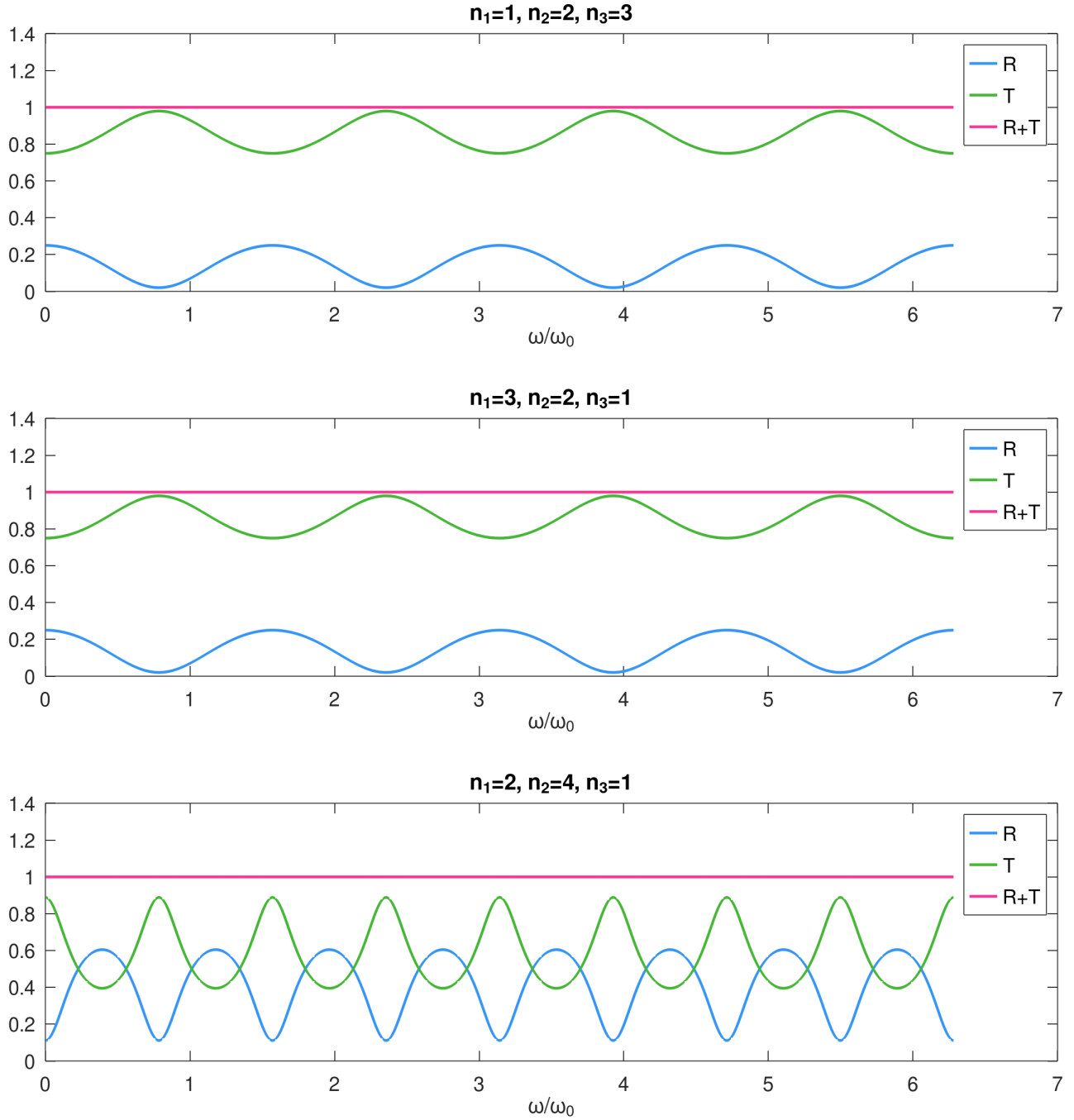
ii. For the parallel polarization (use (23)-(28)):

$$r_{23} = \frac{n_3 - n_2}{n_2 + n_3} e^{i2n_2\omega/\omega_0} \quad (39)$$

$$\begin{aligned} |E_1'|^2 &= |E_1|^2 \left| \frac{(1 + r_{23})n_2 - (1 - r_{23})n_1}{(1 + r_{23})n_2 + (1 - r_{23})n_1} \right|^2 \implies \\ R &= \frac{|E_1'|^2}{|E_1|^2} = \left| \frac{(1 + r_{23})n_2 - (1 - r_{23})n_1}{(1 + r_{23})n_2 + (1 - r_{23})n_1} \right|^2 \end{aligned} \quad (40)$$

$$\begin{aligned} |E_3|^2 &= |E_1|^2 \left(\frac{2n_2}{n_2 + n_3} \right)^2 \left| \frac{2n_1}{(1 + r_{23})n_2 + (1 - r_{23})n_1} \right|^2 \implies \\ T &= \frac{n_3 |E_3|^2}{n_1 |E_1|^2} = \left(\frac{2n_2}{n_2 + n_3} \right)^2 \frac{4n_1 n_3}{|(1 + r_{23})n_2 + (1 - r_{23})n_1|^2} \end{aligned} \quad (41)$$

Numerically, the two polarizations produce the same R and T because r_{23} 's in each case have opposite signs. The plots for different combination of refractive indices are shown below.



(b) Using the perpendicular polarization formula (36)-(38), in order for R to be zero, we need

$$(1 + r_{23})n_1 = (1 - r_{23})n_2 \quad \Rightarrow \quad \frac{n_2 - 1}{n_2 + 1} e^{i2n_2\omega/\omega_0} = r_{23} = \frac{n_2 - n_1}{n_2 + n_1} \quad (42)$$

For this to be true, we must have

$$\frac{n_2 - 1}{n_2 + 1} = \pm \frac{n_2 - n_1}{n_2 + n_1} \quad (43)$$

The + sign is untenable since it entails $n_2 = 0$. The – sign yields

$$n_2 = \sqrt{n_1} \quad \text{and} \quad \frac{2n_2\omega d}{c} = (2k + 1)\pi \quad \Rightarrow \quad d = \frac{(2k + 1)\pi c}{2\sqrt{n_1}\omega} \quad (44)$$