

1. Consider a thin slice of cross section at $z' \to z' + dz'$, let $C_{z'}$ denote its boundary loop which lies in the z = z' plane. Its contribution to the field at $\mathbf{x} = (x, y, z)$ is

$$d\mathbf{B}_{z'} = \frac{\mu_0 N I dz'}{4\pi} \oint_{C_{z'}} d\mathbf{l}' \times \frac{\mathbf{x} - \mathbf{x}'}{|\mathbf{x} - \mathbf{x}'|^3}$$
(1)

Integrating (1) with $z':-\infty\to\infty$ gives the field

$$\mathbf{B}(\mathbf{x}) = \frac{\mu_0 NI}{4\pi} \int_{-\infty}^{\infty} dz' \oint_{C_{z'}} d\mathbf{l}' \times \frac{\mathbf{x} - \mathbf{x}'}{|\mathbf{x} - \mathbf{x}'|^3}$$
(2)

whose *k*-th component is

$$B_k = \frac{\mu_0 NI}{4\pi} \int_{-\infty}^{\infty} dz' \epsilon_{ijk} \oint_{C_i} dl_i' \frac{x_j - x_j'}{|\mathbf{x} - \mathbf{x}'|^3}$$
 (3)

Since the current flows parallel to the x-y plane, all loops $C_{z'}$ are actually planer loops, whose dl'_3 component is zero, thus we can exchange the integration order to obtain

$$B_k = \frac{\mu_0 NI}{4\pi} \epsilon_{ijk} \oint_C dl_i' \int_{-\infty}^{\infty} dz' \frac{x_j - x_j'}{|\mathbf{x} - \mathbf{x}'|^3} \tag{4}$$

where *C* is taken to be in the z = 0 plane without loss of generality. Furthermore, the inner integral vanishes for j = 3 due to its odd parity. This reduces (4) to

$$B_1 = B_2 = 0 (5)$$

$$B_{3} = \frac{\mu_{0}NI}{4\pi} \epsilon_{ij3} \oint_{C} dl'_{i} \left(x_{j} - x'_{j}\right) \overbrace{\int_{-\infty}^{\infty} \frac{dz'}{\left|\mathbf{x} - \mathbf{x}'\right|^{3}}}^{I}$$
 (6)

where

$$I = \int_{-\infty}^{\infty} \frac{dz'}{\sqrt{\underbrace{(x - x')^2 + (y - y')^2}_{\equiv \rho^2} + (z - z')^2}}$$

$$= \int_{-\pi/2}^{\pi/2} \frac{\rho/\cos^2 \xi d\xi}{\rho^3/\cos^3 \xi} = \frac{2}{\rho^2}$$
(let $z' - z \equiv \rho \tan \xi$)
(7)

Now (6) becomes

$$B_3 = \frac{\mu_0 NI}{2\pi} \left(\oint_C d\mathbf{l}' \times \frac{\boldsymbol{\rho}}{\rho^2} \right)_3 \qquad \text{where } \boldsymbol{\rho} = (x - x', y - y', 0)$$
 (8)

From the 2D figure above on the right, it's clear that $|d\mathbf{l}' \times \boldsymbol{\rho}|$ is, as viewed from the eye at (x, y, 0), the area sweeped by the differential line segment $d\mathbf{l}'$, hence $|d\mathbf{l}' \times \boldsymbol{\rho}|/\rho^2$ is the sweeped angle. Therefore the integral in (8) gives the total sweeped angle as the eye traces the loop for one round. So for \mathbf{x} enclosed in the solenoid, this integral produces 2π , but vanishes if \mathbf{x} is outside.

In summary

$$\mathbf{H} = \frac{\mathbf{B}}{\mu_0} = \begin{cases} NI\hat{\mathbf{z}} & \text{for inside points} \\ 0 & \text{for outside points} \end{cases}$$
 (9)

2. With a "realistic" solenoid, a single wire is arranged in a helix shape where it slowly stacks up in the z-direction. Consider a plane parallel to the x-y plane, the coil's wire intersects with this plane at one point, which means the current through this plane (hence in the z-direction) is I. If we integrate the field along a circle with radius b outside of the solenoid, we will have

$$B_{\phi} 2\pi b = \mu_0 I \qquad \Longrightarrow \qquad B_{\phi} = \frac{\mu_0 I}{2\pi b} \tag{10}$$

I.e., we have a tangential field in the $\hat{\phi}$ direction outside of the solenoid, this is the same field generated by the current I flowing in the z direction.