

From problem 8.2, we have determined the form of the fields in TEM mode,

$$\mathbf{E}(\mathbf{x}) = \frac{C\hat{\rho}}{\rho} \quad \mathbf{B} = \frac{\hat{\mathbf{z}} \times \mathbf{E}}{c} \quad (1)$$

For the voltage between the inner and outer conductors to be V , we must have

$$\int_a^b \frac{C}{\rho} d\rho = V \quad \Rightarrow \quad C = \frac{V}{\ln\left(\frac{b}{a}\right)} \quad (2)$$

giving

$$\mathbf{E} = \frac{V}{\ln\left(\frac{b}{a}\right)} \frac{\hat{\rho}}{\rho} \quad c\mathbf{B} = \frac{V}{\ln\left(\frac{b}{a}\right)} \frac{\hat{\phi}}{\rho} \quad (3)$$

We use Smythe-Kirchhoff approximation (10.109) to estimate the radiation-zone field on the other side of the infinite screen,

$$\mathbf{E}(\mathbf{x}) = \frac{ie^{ikr}}{2\pi r} \mathbf{k} \times \int_{\text{ring}} \hat{\mathbf{z}} \times \mathbf{E}(\mathbf{x}') e^{-ik\mathbf{x} \cdot \mathbf{x}'} da' \quad (4)$$

We can parameterize \mathbf{k}, \mathbf{x}' by the following

$$\mathbf{k} = k(\sin\beta \cos\gamma \hat{\mathbf{x}} + \sin\beta \sin\gamma \hat{\mathbf{y}} + \cos\beta \hat{\mathbf{z}}) \quad \mathbf{x}' = \rho \cos\phi \hat{\mathbf{x}} + \rho \sin\phi \hat{\mathbf{y}} \quad (5)$$

then the integrand becomes

$$\begin{aligned} \hat{\mathbf{z}} \times \mathbf{E}(\mathbf{x}') e^{-ik\mathbf{x} \cdot \mathbf{x}'} &= \frac{\hat{\phi}}{\rho} \frac{V}{\ln\left(\frac{b}{a}\right)} e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \\ &= \frac{V}{\ln\left(\frac{b}{a}\right)} \left(\frac{-\sin\phi \hat{\mathbf{x}} + \cos\phi \hat{\mathbf{y}}}{\rho} \right) e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \end{aligned} \quad (6)$$

We can use the integral representation of the Bessel function (see problem 3.16 (d))

$$J_m(x) = \frac{1}{2\pi i^m} \int_0^{2\pi} e^{ix \cos\alpha - im\alpha} d\alpha \quad (7)$$

and its parity property

$$J_m(-x) = J_{-m}(x) = (-1)^m J_m(x) \quad (8)$$

to get

$$\begin{aligned} \int_0^{2\pi} e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \cos\phi d\phi &= \int_0^{2\pi} e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \left(\frac{e^{i\phi} + e^{-i\phi}}{2} \right) d\phi \quad \text{let } \alpha = \phi - \gamma \\ &= \int_0^{2\pi} e^{-ik\rho \sin\beta \cos\alpha} \left[\frac{e^{i(\alpha+\gamma)} + e^{-i(\alpha+\gamma)}}{2} \right] d\alpha \\ &= \frac{1}{2} [-2\pi i e^{i\gamma} J_{-1}(-k\rho \sin\beta) + 2\pi i e^{-i\gamma} J_1(-k\rho \sin\beta)] \\ &= -2\pi i \cos\gamma J_1(k\rho \sin\beta) \end{aligned} \quad (9)$$

$$\begin{aligned} \int_0^{2\pi} e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \sin\phi d\phi &= \int_0^{2\pi} e^{-ik\rho \sin\beta \cos(\phi-\gamma)} \left(\frac{e^{i\phi} - e^{-i\phi}}{2i} \right) d\phi \\ &= \int_0^{2\pi} e^{-ik\rho \sin\beta \cos\alpha} \left[\frac{e^{i(\alpha+\gamma)} - e^{-i(\alpha+\gamma)}}{2i} \right] d\alpha \\ &= \frac{1}{2i} [-2\pi i e^{i\gamma} J_{-1}(-k\rho \sin\beta) - 2\pi i e^{-i\gamma} J_1(-k\rho \sin\beta)] \\ &= -2\pi i \sin\gamma J_1(k\rho \sin\beta) \end{aligned} \quad (10)$$

Thus (4) becomes

$$\begin{aligned}
 \mathbf{E}(\mathbf{x}) &= \frac{ie^{ikr}}{2\pi r} \cdot \frac{V}{\ln\left(\frac{b}{a}\right)} (-2\pi i) \overbrace{\mathbf{k} \times (-\sin\gamma\hat{\mathbf{x}} + \cos\gamma\hat{\mathbf{y}})}^{k\hat{\mathbf{r}} \times \hat{\boldsymbol{\phi}} = -k\hat{\boldsymbol{\theta}}} \int_a^b J_1(k\rho \sin\beta) d\rho \quad \text{use } J_1(x) = -J'_0(x) \\
 &= \frac{e^{ikr}}{r} \frac{V}{\ln\left(\frac{b}{a}\right)} \left[\frac{J_0(kb \sin\beta) - J_0(ka \sin\beta)}{\sin\beta} \right] \hat{\boldsymbol{\theta}} \quad (11)
 \end{aligned}$$

The angular distribution of power is obtained by the usual routine

$$\frac{dP}{d\Omega} = \frac{1}{2Z_0} |\mathbf{E}|^2 r^2 = \frac{V^2}{2Z_0 \ln^2\left(\frac{b}{a}\right)} \left[\frac{J_0(kb \sin\beta) - J_0(ka \sin\beta)}{\sin\beta} \right]^2 \quad (12)$$

and the total radiated power is obtained by integrating (12) over $\beta \in [0, \pi/2]$ and $\gamma \in [0, 2\pi]$, which does not seem to have closed forms,

$$P = \int \frac{dP}{d\Omega} d\Omega = \frac{\pi V^2}{Z_0 \ln^2\left(\frac{b}{a}\right)} \int_0^{\pi/2} \frac{[J_0(kb \sin\beta) - J_0(ka \sin\beta)]^2}{\sin\beta} d\beta \quad (13)$$