

1. Prob 12.3

- (a) Without loss of generality, let z -axis be aligned with the direction of \mathbf{E}_0 , and let x -axis be aligned with the initial velocity \mathbf{v}_0 . From the equation of motion (12.1), (12.2), we have

$$\frac{d(\gamma m v_z)}{dt} = eE_0 \quad (1)$$

$$\frac{d(\gamma mc^2)}{dt} = e v_z E_0 \quad (2)$$

Multiplying both sides of (2) by γm , we get

$$\begin{aligned} \frac{(mc)^2}{2} \frac{d\gamma^2}{dt} &= eE_0 (\gamma m v_z) && \text{take } d/dt \text{ and use (1)} && \Rightarrow \\ \frac{(mc)^2}{2} \frac{d^2\gamma^2}{dt^2} &= (eE_0)^2 && && (3) \end{aligned}$$

This means that as a function of t , γ^2 is quadratic in t :

$$\gamma^2(t) = A + Bt + Ct^2 \quad (4)$$

We can use (3) to find C , and use the value of γ^2 at $t = 0$ to find A , and the value at $t = 0$ of (2) to find B . The result is

$$\gamma^2(t) = \frac{\overbrace{1}^{\gamma_0^2}}{1 - v_0^2/c^2} + \left(\frac{eE_0}{mc}\right)^2 t^2 \quad (5)$$

$v_z(t)$ can be found via (1)

$$v_z(t) = \left(\frac{eE_0}{m}\right) \frac{t}{\gamma} = \frac{\left(\frac{eE_0}{m}\right) t}{\sqrt{\gamma_0^2 + \left(\frac{eE_0}{mc}\right)^2 t^2}} \quad (6)$$

Integrating (6) yields

$$z(t) = \frac{mc^2}{eE_0} \left[\sqrt{\gamma_0^2 + \left(\frac{eE_0}{mc}\right)^2 t^2} - \gamma_0 \right] \quad (7)$$

In the x direction, momentum is conserved, so we have

$$v_x(t) = \frac{\gamma_0 m v_0}{\gamma(t) m} = \frac{\gamma_0 v_0}{\sqrt{\gamma_0^2 + \left(\frac{eE_0}{mc}\right)^2 t^2}} \quad (8)$$

hence

$$x(t) = \frac{\gamma_0 m v_0 c}{eE_0} \sinh^{-1} \left(\frac{eE_0 t}{\gamma_0 mc} \right) \quad (9)$$

- (b) Inverting (9) gives

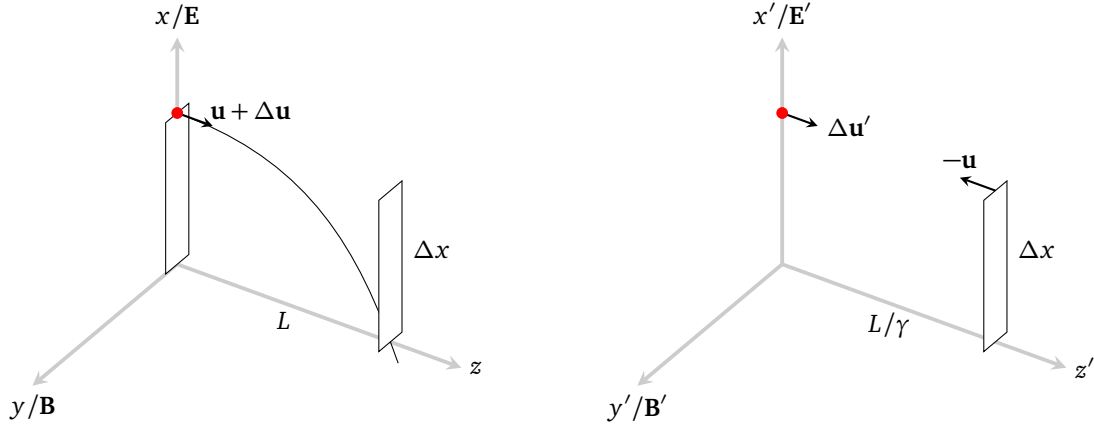
$$t = \frac{\gamma_0 mc}{eE_0} \sinh \left(\frac{eE_0 x}{\gamma_0 m v_0 c} \right) \quad (10)$$

Then by (7),

$$z(x) = \frac{\gamma_0 mc^2}{eE_0} \left[\cosh \left(\frac{eE_0 x}{\gamma_0 m v_0 c} \right) - 1 \right] \quad (11)$$

From (9), we can define a characteristic time $T = \gamma_0 mc / eE_0$. When $t \ll T$, we have $x \propto t$ and $z \propto t^2$, the trajectory is approximately parabolic. When $t \gg T$, $x \propto \ln t$ and $z \propto t$, the trajectory is approximately exponential.

2. Prob 12.4



Let \mathbf{E} be in the x direction, and let \mathbf{B} be in the y direction, and let the particle move into the device with velocity $(u + \Delta u)\hat{\mathbf{z}}$, where $u = cE/B$ is the drift velocity. At the drift velocity, the electric force and the magnetic force balance out. The extra Δu gives rise to a net force of $-e\Delta u B/c\hat{\mathbf{x}}$. With $\Delta u \ll u$, we can treat the z -direction velocity as constant (even though the net force in the $-x$ direction will give the particle some x velocity over time, which will result in an z -acceleration due to magnetic force, the increase in z velocity is of higher order of Δu). The equation of motion in x direction says

$$\frac{dp_x}{dt} = -\frac{e\Delta u B}{c} \quad \Rightarrow \quad \frac{dv_x}{dt} = -\frac{e\Delta u B}{c\gamma m} \quad (12)$$

This is also treating γ as approximately constant which is true given the small Δu . With this, the opening Δx must be no smaller than the x displacement of the particle as it travels the distance L in the z direction, i.e.,

$$\frac{1}{2} \left(\frac{e\Delta u B}{c\gamma m} \right) \left(\frac{L}{u} \right)^2 \leq \Delta x \quad \Rightarrow \quad \Delta u \leq \frac{2c\gamma m u^2 \Delta x}{eBL^2} \quad (13)$$

We can do this calculation in the inertial frame moving at velocity \mathbf{u} (see above figure on the right). In this frame, we have $\mathbf{E}' = 0$, $\mathbf{B}' = \mathbf{B}/\gamma$ by (12.44). The particle's velocity in this frame is given by

$$\Delta u' = \frac{(u + \Delta u) - u}{1 - \frac{(u + \Delta u)u}{c^2}} \approx \gamma^2 \Delta u \quad (14)$$

The opposing opening is moving towards the particle with velocity $-\mathbf{u}$ from a contracted distance L/γ . Since $\Delta u' \ll u$, the time for them to meet is approximately

$$t' \approx \frac{L}{\gamma u} \quad (15)$$

The equation of motion in the x' direction requires

$$\frac{dp'_x}{dt'} = -\frac{e\Delta u' B'}{c} \quad \Rightarrow \quad \frac{dv'_x}{dt'} \approx -\frac{e\Delta u' B'}{cm} \quad (16)$$

where we have treated the Lorentz factor due to $\Delta u'$ to be approximately unity.

The condition for velocity selection is thus

$$\frac{1}{2} \left(\frac{e\Delta u' B'}{cm} \right) t'^2 \leq \Delta x \quad \Rightarrow \quad \frac{1}{2} \left[\frac{e(\gamma^2 \Delta u)(B/\gamma)}{cm} \right] \left(\frac{L}{\gamma u} \right)^2 \leq \Delta x \quad (17)$$

which gives the same constraint on Δu as (13).

3. Prob 12.5

(a) For $\mathbf{E} \perp \mathbf{B}$ and $|\mathbf{E}| < |\mathbf{B}|$, section 12.3 has shown that in a frame K' moving at velocity

$$\mathbf{u} = c \frac{\mathbf{E} \times \mathbf{B}}{B^2} \quad (18)$$

the electric field vanishes, and magnetic field is scaled down by a factor of

$$\gamma = \sqrt{\frac{B^2}{B^2 - E^2}} \quad (19)$$

Translating (12.41) into the coordinate axis given in this problem, i.e., $\epsilon_3 = \hat{\mathbf{y}}, \epsilon_1 = \hat{\mathbf{z}}, \epsilon_2 = \hat{\mathbf{x}}$, we have

$$\mathbf{x}'(t') = \mathbf{X}'_0 + v'_y t' \hat{\mathbf{y}} + a \sin \omega t' \hat{\mathbf{z}} + a \cos \omega t' \hat{\mathbf{x}} \quad (20)$$

where

$$a = \frac{cp'_\perp}{eB'} = \frac{c\gamma' m \sqrt{v'^2_z + v'^2_x}}{eB'} \quad \gamma' = \frac{1}{\sqrt{1 - v'^2/c^2}} \quad \omega = \frac{eB'}{\gamma' mc} \quad (21)$$

Applying the Lorentz transformation to (20) gives the parametric trajectory in the lab frame

$$z(t') = \gamma [z'(t') + ut'] = \gamma (z'_0 + a \sin \omega t' + ut') \quad (22)$$

$$x(t') = x'(t') = x'_0 + a \cos \omega t' \quad (23)$$

$$y(t') = y'(t') = y'_0 + v'_y t' \quad (24)$$

Note that the parameter for the trajectory is the time in frame K' .

(b) If $|\mathbf{E}| > |\mathbf{B}|$, we transform into frame K' that moves with velocity

$$\mathbf{u} = c \frac{\mathbf{E} \times \mathbf{B}}{E^2} \quad (25)$$

In this frame, there is only electric field of strength $\mathbf{E}' = \mathbf{E}/\gamma$, and the magnetic field is zero. We can use the result of problem 12.3 by properly choosing the zero time at which the velocity along x direction is zero and velocities along y and z are v'_{y0} and v'_{z0} . In this case

$$x'(t') = \frac{mc^2}{eE'} \left[\sqrt{\gamma'^2_0 + \left(\frac{eE'}{mc} \right)^2 t'^2} - \gamma'_0 \right] \quad (26)$$

$$y'(t') = \frac{\gamma'_0 m v'_{y0} c}{eE'} \sinh^{-1} \left(\frac{eE' t'}{\gamma'_0 mc} \right) \quad (27)$$

$$z'(t') = \frac{\gamma'_0 m v'_{z0} c}{eE'} \sinh^{-1} \left(\frac{eE' t'}{\gamma'_0 mc} \right) \quad (28)$$

where

$$\gamma'_0 = \frac{1}{\sqrt{1 - v'^2_0/c^2}} \quad v'_0 = \sqrt{v'^2_{y0} + v'^2_{z0}} \quad (29)$$

Applying Lorentz transformation back to K gives the parametric trajectory

$$x(t') = x'(t') = \frac{mc^2}{eE'} \left[\sqrt{\gamma'^2_0 + \left(\frac{eE'}{mc} \right)^2 t'^2} - \gamma'_0 \right] \quad (30)$$

$$y(t') = y'(t') = \frac{\gamma'_0 m v'_{y0} c}{eE'} \sinh^{-1} \left(\frac{eE' t'}{\gamma'_0 mc} \right) \quad (31)$$

$$z(t') = \gamma [z'(t') + ut'] = \gamma \left[\frac{\gamma'_0 m v'_{z0} c}{eE'} \sinh^{-1} \left(\frac{eE' t'}{\gamma'_0 mc} \right) + ut' \right] \quad (32)$$

4. Prob 12.6

- (a) From problem 11.15, we see that when \mathbf{E} and \mathbf{B} are not already parallel, we can always change into a frame K' where \mathbf{E}' and \mathbf{B}' are parallel. The relative velocity of K' to the original frame is along the direction of $\mathbf{E} \times \mathbf{B}$. Once we solve the equation of motion in K' , applying the Lorentz transformation back to K will give the trajectory in K . In part (b) we will derive such solution in K' .
- (b) Let \mathbf{E}, \mathbf{B} be parallel and along the z direction. The equation of motion is

$$\frac{d(\gamma m \mathbf{u})}{dt} = e \left(\mathbf{E} + \frac{\mathbf{u} \times \mathbf{B}}{c} \right) \quad (33)$$

$$\frac{d(\gamma m c^2)}{dt} = e \mathbf{u} \cdot \mathbf{E} \quad (34)$$

Their component forms are

$$\frac{d(\gamma m u_z)}{dt} = eE \quad \frac{d(\gamma m c^2)}{dt} = e u_z E \quad (35)$$

$$\frac{d(\gamma m u_x)}{dt} = \left(\frac{eB}{c} \right) u_y \quad \frac{d(\gamma m u_y)}{dt} = - \left(\frac{eB}{c} \right) u_x \quad (36)$$

We can properly choose the starting time at which $u_z(0) = 0$. The solution of (35) is already obtained in problem 12.3. Rewriting (5) and (6) gives

$$\gamma^2(t) = \gamma_0^2 + \lambda^2 t^2 \quad \text{where} \quad \lambda = \frac{eE}{mc} \quad \gamma_0 = \frac{1}{\sqrt{1 - u_{\perp 0}^2/c^2}} \quad (37)$$

$$u_z(t) = \frac{\lambda c t}{\gamma} \quad (38)$$

From the definition of γ , we have

$$\frac{1}{\gamma^2} = 1 - \left(\frac{u_z^2 + u_{\perp}^2}{c^2} \right) \quad \Rightarrow \quad u_{\perp}^2 = \frac{c^2(\gamma_0^2 - 1)}{\gamma^2} \quad (39)$$

Note from (36), we have

$$u_x \frac{d(\gamma m u_x)}{dt} + u_y \frac{d(\gamma m u_y)}{dt} = 0 \quad \Rightarrow \quad \frac{d\gamma}{dt} u_{\perp}^2 + \frac{\gamma}{2} \frac{du_{\perp}^2}{dt} = 0 \quad \Rightarrow \quad \frac{du_{\perp}^2}{u_{\perp}^2} = -2 \frac{d\gamma}{\gamma} \quad (40)$$

which is consistent with (39).

Let ϕ be the angle made between \mathbf{u}_{\perp} and the x -axis, i.e.,

$$u_x = u_{\perp} \cos \phi \quad u_y = u_{\perp} \sin \phi \quad (41)$$

Using the fact that γu_{\perp} is a constant (by (39)), we see that (36) implies

$$\left. \begin{aligned} \frac{d(\gamma m u_{\perp} \cos \phi)}{dt} &= \left(\frac{eB}{c} \right) u_{\perp} \sin \phi \\ \frac{d(\gamma m u_{\perp} \sin \phi)}{dt} &= - \left(\frac{eB}{c} \right) u_{\perp} \cos \phi \end{aligned} \right\} \quad \Rightarrow \quad \frac{d\phi}{dt} = - \frac{\mu}{\gamma} \quad \text{where} \quad \mu = \frac{eB}{mc} \quad (42)$$

Plugging (37) into (42) gives

$$\frac{d\phi}{dt} = - \frac{\mu}{\sqrt{\gamma_0^2 + \lambda^2 t^2}} = - \frac{1}{\sqrt{\left(\frac{\gamma_0}{\mu} \right)^2 + \left(\frac{\lambda}{\mu} \right)^2 t^2}} \quad (43)$$

the solution of which is

$$\phi(t) = - \left(\frac{\mu}{\lambda} \right) \sinh^{-1} \left(\frac{\lambda t}{\gamma_0} \right) = - \left(\frac{B}{E} \right) \sinh^{-1} \left(\frac{eEt}{\gamma_0 mc} \right) \quad (44)$$

assuming the x axis is aligned with the direction of $\mathbf{u}_{\perp}(0)$.

Inverting (44) yields

$$t(\phi) = -\frac{\gamma_0 mc}{eE} \sinh \left[\left(\frac{E}{B} \right) \phi \right] \quad (45)$$

If we define

$$R = \frac{mc^2}{eB} \quad \rho = \frac{E}{B} \quad (46)$$

(45) can be written in the desired form

$$ct = -\frac{R}{\rho} \gamma_0 \sinh(\rho \phi) \quad (47)$$

In these variables, the z -displacement (7) can be written as

$$z = \frac{R}{\rho} \gamma_0 [\cosh(\rho \phi) - 1] \quad (48)$$

Note these are the same as the form in the problem after some translation in z and reversing the rotation direction ϕ .

We can obtain the x displacement by the integration

$$\begin{aligned} x &= \int u_x dt = \int u_{\perp} \cos \phi dt && \text{use (39)} \\ &= \int c \sqrt{\gamma_0^2 - 1} \cos \phi \frac{dt}{\gamma} && \text{by (42) } \frac{dt}{\gamma} = -\frac{d\phi}{\mu} \\ &= -\frac{c}{\mu} \sqrt{\gamma_0^2 - 1} \sin \phi \\ &= -R \sqrt{\gamma_0^2 - 1} \sin \phi \end{aligned} \quad (49)$$

and similarly for the y displacement

$$y = \int u_y dt = R \sqrt{\gamma_0^2 - 1} \cos \phi \quad (50)$$

after conveniently choosing the origin in the x - y plane to eliminate the integration constant.

The A in the problem statement is just $\sqrt{\gamma_0^2 - 1}$, which cannot be arbitrary but has to be determined by the initial transverse velocity $\mathbf{u}_{\perp}(0)$.

The statement that ϕ is c/R times the proper time can be seen from (42).

It is rather surprising that despite persistent acceleration by the electric field, the particle's projected trajectory in the x - y plane remains a perfect circle. As t increases, by (44), the angular displacement grows approximately via $\phi \sim \ln t$.