

# İşaret İşleme

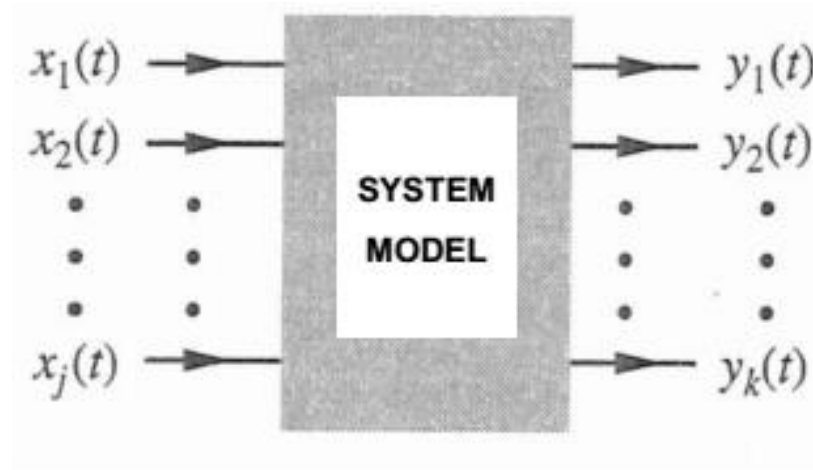
## Zaman Domaini Analizi

(Birim darbe cevabı  
&  
Sıfır durum cevabı)

### H5CD1

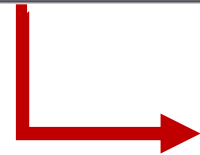
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## Bir sistemin toplam tepkisi - (Total response)



Remember that for a Linear System

**Total response = zero-input response + zero-state response**



Önceki derslerimizde sistemin  
sıfır giriş cevabının nasıl  
hesaplanacağını öğrenmiştik

# Sıfır Giriş Cevabı (SGC)-(Zero input response)

In this lecture, we will focus on a linear system's **zero-input response**,  $y_0(t)$ , which is the solution of the system equation when input  $x(t) = 0$ .



$$(D^N + a_1 D^{N-1} + \dots + a_{N-1} D + a_N) y(t) = (b_{N-M} D^M + b_{N-M+1} D^{M-1} + \dots + b_{N-1} D + b_N) x(t)$$



$$\Rightarrow Q(D)y(t) = P(D)x(t)$$

$$\Rightarrow Q(D)y_0(t) = 0$$

$$\Rightarrow (D^N + a_1 D^{N-1} + \dots + a_{N-1} D + a_N) y_0(t) = 0$$

# Characteristic Polynomial of a system

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$Q(\lambda)$  is called the **characteristic polynomial** of the system

$Q(\lambda) = 0$  is the **characteristic equation** of the system

The **roots** to the characteristic equation  $Q(\lambda) = 0$ , i.e.  $\lambda_1, \lambda_2, \dots, \lambda_N$ , are extremely important.

They are called by different names:

- Characteristic values
- **Eigenvalues**
- **Natural frequencies**

The exponentials  $e^{\lambda_i t}$  ( $i = 1, 2, \dots, n$ ) are the **characteristic modes** (also known as **natural modes**) of the system

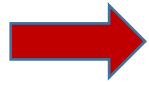
Characteristics modes determine the system's behaviour

$Q(\lambda)$  is called the **characteristic polynomial** of the system

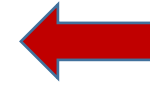
The **roots** to the characteristic equation  $Q(\lambda) = 0$ , i.e.  $\lambda_1, \lambda_2, \dots, \lambda_N$ , are extremely important.

- **NOT:**
  - **Sistemin karakteristik polinomuna ait kökler ( $\lambda$ ) 3 farklı durumda olabilir.**
    - Katsız (tekrar etmeyen) kök
    - Katlı (tekrar eden) kök
    - Kompleks kök
  - **Her 3 durum için sistemin sıfır giriş cevabı farklı genel çözümlerle bulunur.**

- Sistemin karakteristik polinomuna ait kökler ( $\lambda_i$ ) **Katsız (tekrar etmeyen) kökler** olduğunda sistemin sıfır giriş cevabına ait genel çözüm;



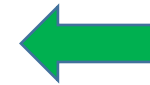
$$y_0(t) = c_1 e^{\lambda_1 t} + c_2 e^{\lambda_2 t} + \dots + c_N e^{\lambda_N t}$$



- Sistemin karakteristik polinomuna ait kökler ( $\lambda_i$ ) **Katlı (tekrar eden) kökler** olduğunda sistemin sıfır giriş cevabına ait genel çözüm;



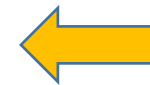
$$y_0(t) = (c_1 + c_2 t + \dots + c_r t^{r-1}) e^{\lambda t}$$



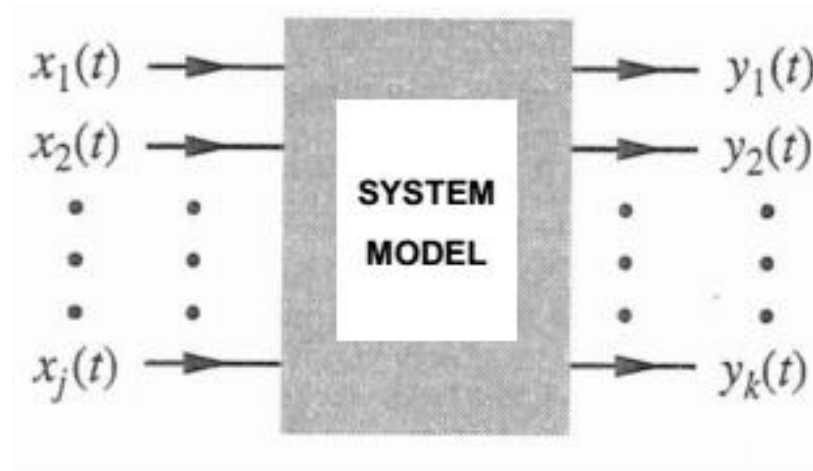
- Sistemin karakteristik polinomuna ait kökler ( $\lambda_i$ ) **Kompleks kökler** olduğunda sistemin sıfır giriş cevabına ait genel çözüm;



$$\begin{aligned} y_0(t) &= \frac{c}{2} e^{j\theta} e^{(\alpha + j\beta)t} + \frac{c}{2} e^{-j\theta} e^{(\alpha - j\beta)t} \\ &= \frac{c}{2} e^{\alpha t} [e^{j(\beta t + \theta)} + e^{-j(\beta t + \theta)}] \\ &= c e^{\alpha t} \cos(\beta t + \theta) \end{aligned}$$



## Bir sistemin toplam tepkisi - (Total response)



Remember that for a Linear System

**Total response = zero-input response + zero-state response**

**Sistemin sıfır durum cevabını bulmak için önce  
birim darbe cevabı hesaplanmalıdır.**

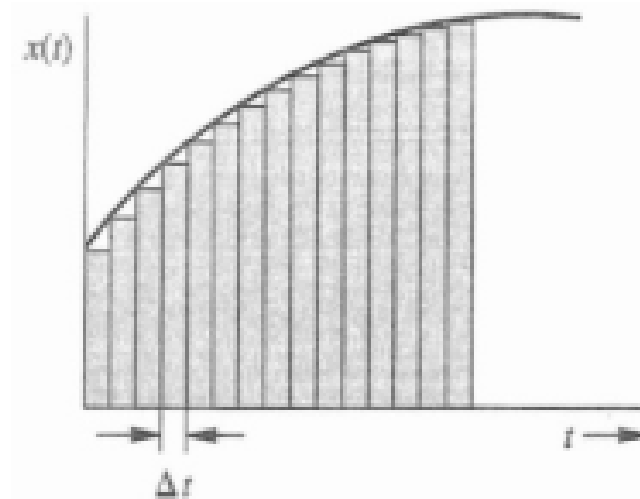
# Birim Darbe Cevabı

## (Unit Impulse Response)



# The importance of Impulse Response $h(t)$

- ◆ **Zero-state response** assumes that the system is in “rest” state, i.e. all internal system variables are zero.
- ◆ Deriving and understanding zero-state response depends on knowing the **impulse response  $h(t)$**  to a system.
- ◆ Any input  $x(t)$  can be broken into many **narrow rectangular pulses**. Each pulse produces a system response.
- ◆ Since the system is linear and time invariant, the system response to  $x(t)$  is the sum of its responses to all the impulse components.
- ◆  $h(t)$  is the system response to the rectangular pulse at  $t=0$  as the pulse **width approaches zero**.



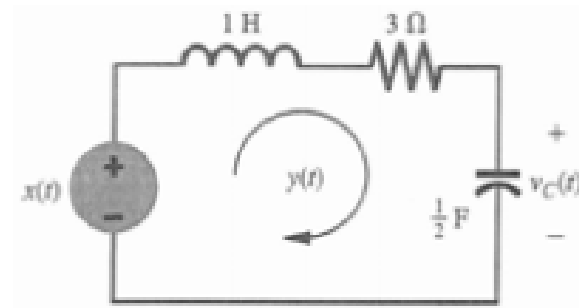
## How to determine the unit impulse response $h(t)$ ? (1)

Given that a system is specified by the following differential equation, determine its unit impulse response  $h(t)$ .

$$\frac{d^2 y}{dt^2} + 3 \frac{dy}{dt} + 2y(t) = \frac{dx}{dt}$$

Remember the general system equation:

$$Q(D)y(t) = P(D)x(t)$$



It can be shown that the impulse response  $h(t)$  is given by:

$$h(t) = [P(D)y_n(t)] u(t) \quad \dots\dots (4.3.1)$$

where  $u(t)$  is the unit step function, and  $y_n(t)$  is a linear combination of the characteristic modes of the system.

$$y_n(t) = c_1 e^{\lambda_1 t} + c_2 e^{\lambda_2 t} + \dots\dots\dots + c_N e^{\lambda_N t}$$

## How to determine the unit impulse response $h(t)$ ? (2)

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The constants  $c_i$  are determined by the following initial conditions:



$$y_n(0) = \dot{y}_n(0) = \ddot{y}_n(0) = \dots = y_n^{(N-2)}(0) = 0, \quad y_n^{(N-1)}(0) = 1.$$

Note  $y_n^{(k)}(0)$  is the  $k^{\text{th}}$  derivative of  $y_n(t)$  at  $t = 0$ .

The above is true if  $M$ , the order of  $P(D)$ , is less than  $N$ , the order of  $Q(D)$  (which is generally the case for most stable systems).

## The Example (1)

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Determine the impulse response for the system:  $(D^2 + 3D + 2) y(t) = Dx(t)$

This is a second-order system (i.e.  $N=2$ ,  $M=1$ ) and the characteristic polynomial is:

$$(\lambda^2 + 3\lambda + 2) = (\lambda + 1)(\lambda + 2)$$

The characteristic roots are  $\lambda = -1$  and  $\lambda = -2$ .

Therefore :  $y_n(t) = c_1 e^{-t} + c_2 e^{-2t}$

Differentiating this equation yields:  $\dot{y}_n(t) = -c_1 e^{-t} - 2c_2 e^{-2t}$

The initial conditions are

$$\dot{y}_n(0) = 1 \quad \text{and} \quad y_n(0) = 0$$

## The Example (2)

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Setting  $t = 0$  and substituting the initial conditions yield:

$$0 = c_1 + c_2$$

$$1 = -c_1 - 2c_2$$

The solution of these equations are:

$$c_1 = 1 \quad \text{and} \quad c_2 = -1$$

Therefore we obtain

$$y_n(t) = e^{-t} - e^{-2t}$$

Remember that  $h(t)$  is given by:

$$h(t) = [P(D)y_n(t)]u(t)$$

and  $P(D) = D$  in this case.

Therefore

$$h(t) = [P(D)y_n(t)]u(t) = (-e^{-t} + 2e^{-2t})u(t)$$

$$P(D)y_n(t) = Dy_n(t) = \dot{y}_n(t) = -e^{-t} + 2e^{-2t}$$

# Sıfır Durum Cevabı (Zero State Response)

## Zero-state Response (1)

We now consider how to determine the **system response**  $y(t)$  to an input  $x(t)$  when system is in zero state.

Define a pulse  $p(t)$  of unit height and width  $\Delta\tau$  at  $t=0$ :

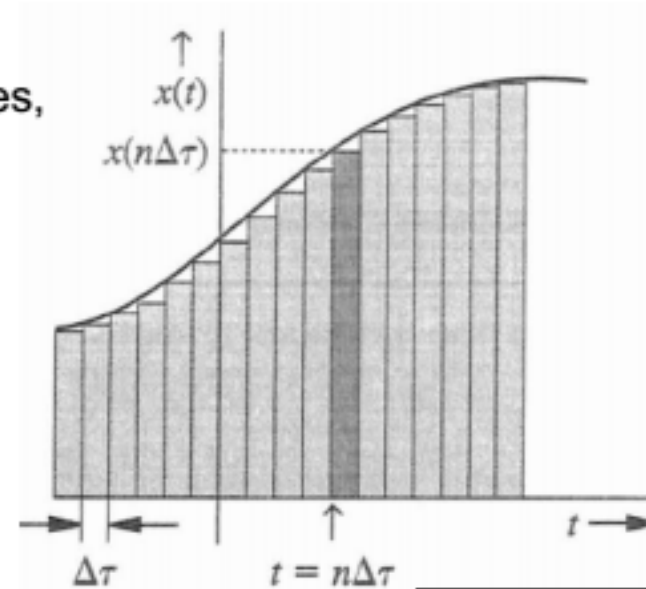
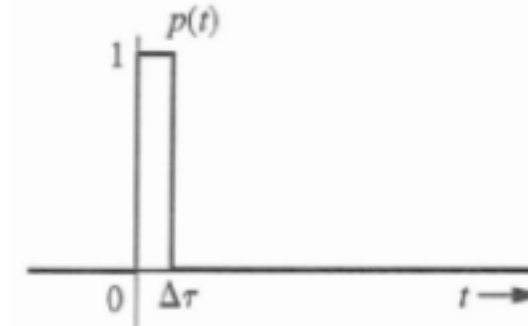
Input  $x(t)$  can be represented as sum of narrow rectangular pulses.

The pulse at  $t = n\Delta\tau$  has a height  $x(t) = x(n\Delta\tau)$ .

This can be expressed as  $x(n\Delta\tau) p(t - n\Delta\tau)$ .

Therefore  $x(t)$  is the sum of all  $[x(n\Delta\tau)/\Delta\tau]$  such pulses, i.e.

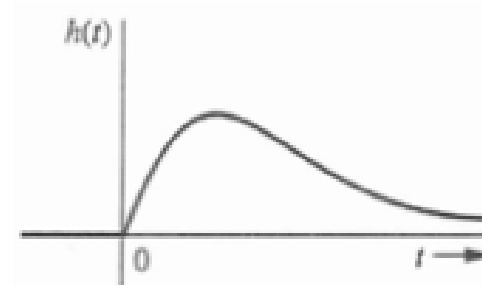
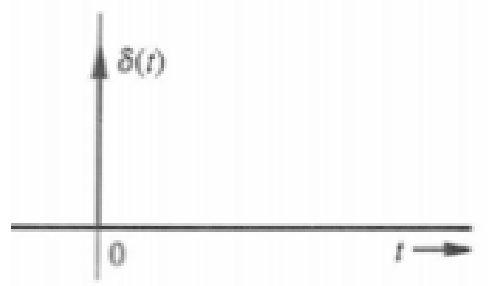
$$\begin{aligned} x(t) &= \lim_{\Delta\tau \rightarrow 0} \sum_r x(n\Delta\tau) p(t - n\Delta\tau) \\ &= \lim_{\Delta\tau \rightarrow 0} \sum_r \left[ \frac{x(n\Delta\tau)}{\Delta\tau} \right] p(t - n\Delta\tau) \Delta\tau \end{aligned}$$



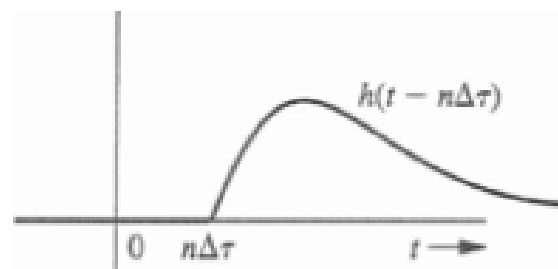
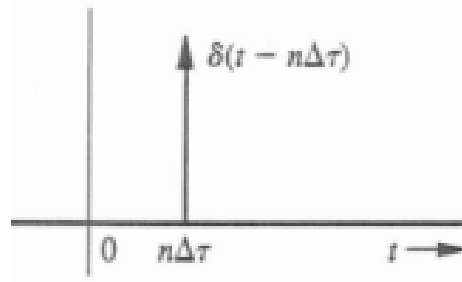
## Zero-state Response (2)

input  $\Rightarrow$  output

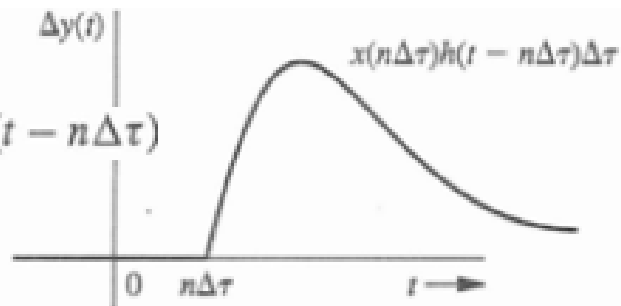
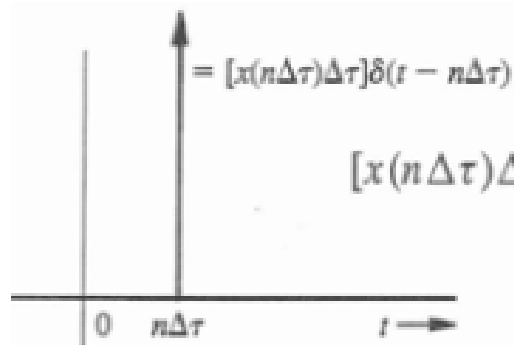
$$\delta(t) \Rightarrow h(t)$$



$$\delta(t - n\Delta\tau) \Rightarrow h(t - n\Delta\tau)$$



$$[x(n\Delta\tau)\Delta\tau]\delta(t - n\Delta\tau) \Rightarrow [x(n\Delta\tau)\Delta\tau]h(t - n\Delta\tau)$$

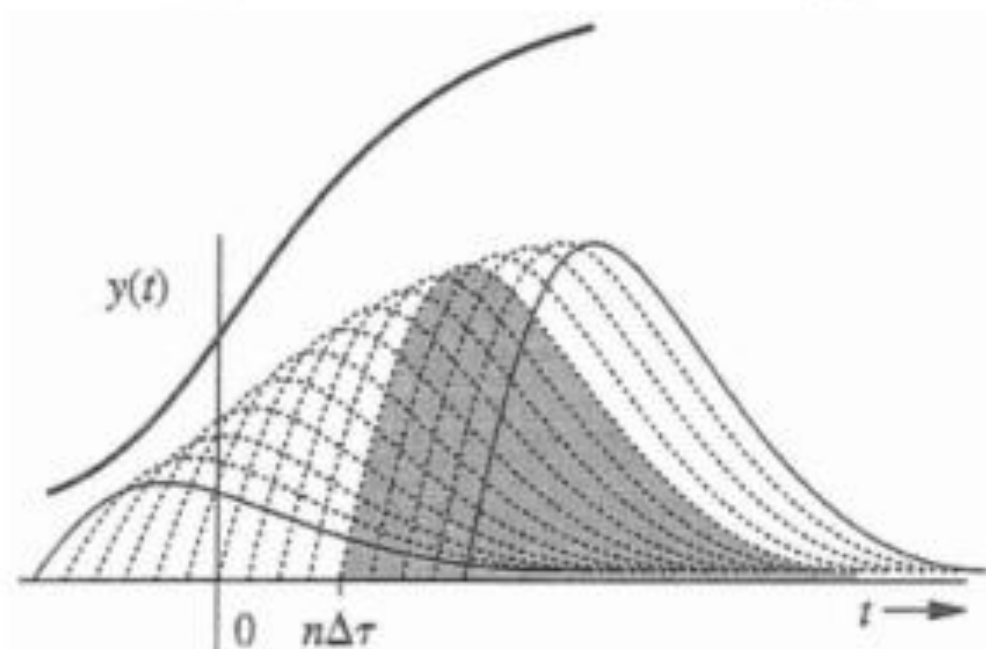




## Zero-state Response (3)

input  $\Rightarrow$  output

$$\underbrace{\lim_{\Delta\tau \rightarrow 0} \sum_{\tau} x(n\Delta\tau) \delta(t - n\Delta\tau) \Delta\tau}_{x(t)} \Rightarrow \underbrace{\lim_{\Delta\tau \rightarrow 0} \sum_{\tau} x(n\Delta\tau) h(t - n\Delta\tau) \Delta\tau}_{y(t)}$$

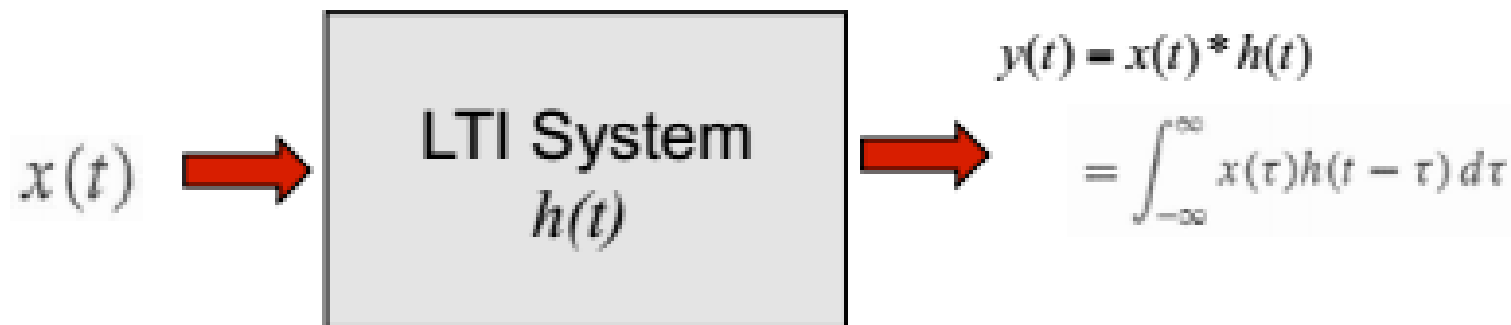


## Zero-state Response (4)

- ◆ Therefore,

$$\begin{aligned} y(t) &= \lim_{\Delta\tau \rightarrow 0} \sum_{\tau} x(n\Delta\tau)h(t - n\Delta\tau)\Delta\tau \\ &= \int_{-\infty}^{\infty} x(\tau)h(t - \tau) d\tau \end{aligned}$$

- ◆ Knowing  $h(t)$ , we can determine the response  $y(t)$  to any input  $x(t)$ .
- ◆ Observe the all-pervasive nature of the system's characteristic modes, which determines the impulse response of the system.



# The Convolution Integral

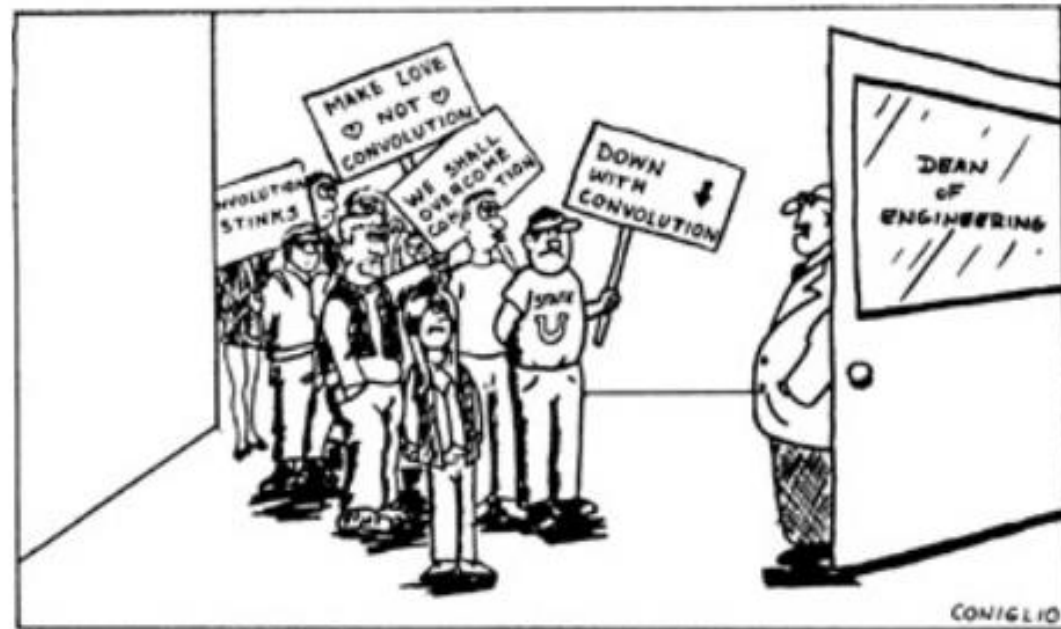
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- ◆ The derived integral equation occurs frequently in physical sciences, engineering and mathematics.
- ◆ It is given the name: the convolution integral.
- ◆ The convolution integral of two functions  $x_1(t)$  and  $x_2(t)$  is denoted symbolically as

$$x_1(t) * x_2(t) \equiv \int_{-\infty}^{\infty} x_1(\tau) x_2(t - \tau) d\tau$$

- ◆ Note that the convolution operator is linear, i.e. it obeys the principle of superposition.

# Time-domain analysis: Convolution



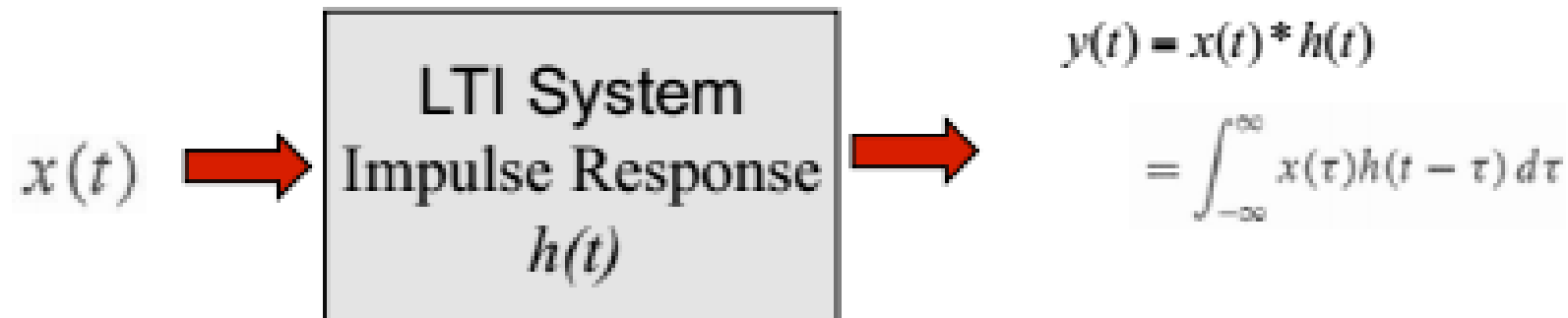
Convolution: its bark is worse than its bite!

# Convolution Integral

- ◆ Convolution Integral:

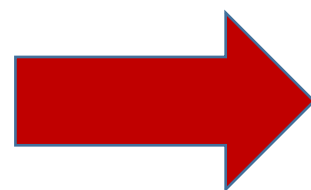
$$y(t) = x(t) * h(t) = \int_{-\infty}^{\infty} x(\tau) h(t - \tau) d\tau$$

- ◆ System output (i.e. zero-state response) is found by convolving input  $x(t)$  with System's impulse response  $h(t)$ .



**Table 2.1: Convolution Table**[→ Open table as spreadsheet](#)

No.	$x_1(t)$	$x_2(t)$	$x_1(t)*x_2(t) = x_2(t)*x_1(t)$
1	$x(t)$	$\delta(t - T)$	$x(t - T)$
2	$e^{\lambda t}u(t)$	$u(t)$	$\frac{1 - e^{\lambda t}}{-\lambda} u(t)$
3	$u(t)$	$u(t)$	$tu(t)$
4	$e^{\lambda_1 t}u(t)$	$e^{\lambda_2 t}u(t)$	$\frac{e^{\lambda_1 t} - e^{\lambda_2 t}}{\lambda_1 - \lambda_2} u(t) \quad \lambda_1 \neq \lambda_2$
5	$e^{\lambda t}u(t)$	$e^{\lambda t}u(t)$	$te^{\lambda t}u(t)$
6	$te^{\lambda t}u(t)$	$e^{\lambda t}u(t)$	$\frac{1}{2}t^2e^{\lambda t}u(t)$
7	$t^N u(t)$	$e^{\lambda t}u(t)$	$\frac{N! e^{\lambda t}}{\lambda^{N+1}} u(t) - \sum_{k=0}^N \frac{N! t^{N-k}}{\lambda^{k+1} (N-k)!} u(t)$
8	$t^M u(t)$	$t^N u(t)$	$\frac{M!N!}{(M+N+1)!} t^{M+N+1} u(t)$



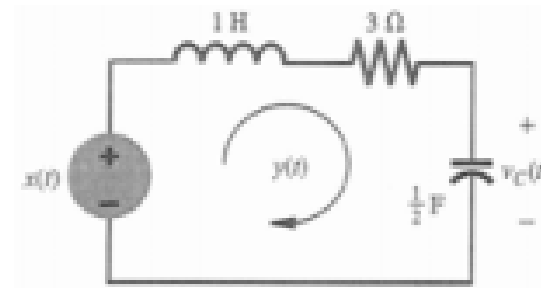
9	$te^{\lambda_1 t}u(t)$	$e^{\lambda_2 t}u(t)$	$\frac{e^{\lambda_2 t} - e^{\lambda_1 t} + (\lambda_1 - \lambda_2)te^{\lambda_1 t}}{(\lambda_1 - \lambda_2)^2} u(t)$
10	$t^M e^{\lambda t}u(t)$	$t^N e^{\lambda t}u(t)$	$\frac{M! N!}{(N + M + 1)!} t^{M+N+1} e^{\lambda t} u(t)$
11	$t^M e^{\lambda_1 t}u(t)$ $\lambda_1 \neq \lambda_2$	$t^N e^{\lambda_2 t}u(t)$	$\sum_{k=0}^M \frac{(-1)^k M!(N+k)! t^{M-k} e^{\lambda_1 t}}{k!(M-k)!(\lambda_1 - \lambda_2)^{N+k+1}} u(t)$ $+ \sum_{k=0}^N \frac{(-1)^k N!(M+k)! t^{N-k} e^{\lambda_2 t}}{k!(N-k)!(\lambda_2 - \lambda_1)^{M+k+1}} u(t)$
12	$e^{-\alpha t} \cos(\beta t + \theta)u(t)$	$e^{\lambda_1 t}u(t)$	$\frac{\cos(\theta - \phi)e^{\lambda_1 t} - e^{-\alpha t} \cos(\beta t + \theta - \phi)}{\sqrt{(\alpha + \lambda)^2 + \beta^2}} u(t)$
13	$e^{\lambda_1 t}u(t)$	$e^{\lambda_2 t}u(-t)$	$\frac{e^{\lambda_1 t}u(t) + e^{\lambda_2 t}u(-t)}{\lambda_2 - \lambda_1} \quad \text{Re } \lambda_2 > \text{Re } \lambda_1$
14	$e^{\lambda_1 t}u(-t)$	$e^{\lambda_2 t}u(-t)$	$\frac{e^{\lambda_1 t} - e^{\lambda_2 t}}{\lambda_2 - \lambda_1} u(-t)$

# Total Response

Total response = zero-input response + zero-state response

$$\text{total response} = \underbrace{\sum_{k=1}^N c_k e^{\lambda_k t}}_{\text{zero-input component}} + \underbrace{x(t) * h(t)}_{\text{zero-state component}}$$

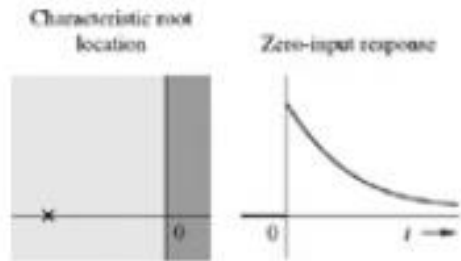
- Let us put everything together, using our RLC circuit as an example.
- Let us assume  $x(t) = 10e^{-3t}u(t)$ ,  $y(0) = 0$ ,  $\dot{y}(0) = -5$ .
- In earlier slides, we have shown that



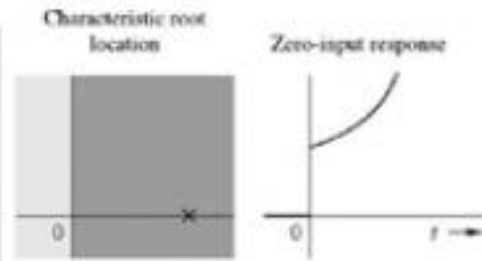
$$\text{total current} = \underbrace{(-5e^{-t} + 5e^{-2t})}_{\text{zero-input current}} + \underbrace{(-5e^{-t} + 20e^{-2t} - 15e^{-3t})}_{\text{zero-state current}} \quad t \geq 0$$



# Internal (Asymptotic) Stability



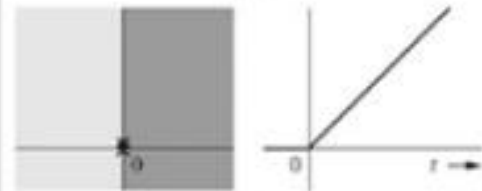
(a)



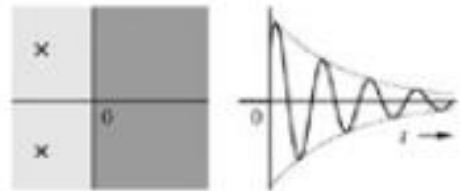
(b)



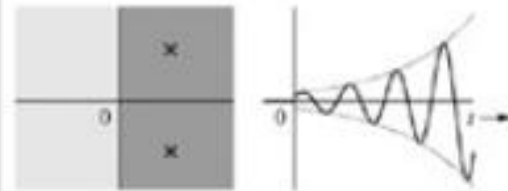
(c)



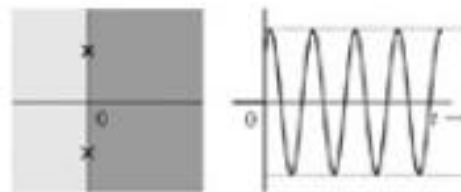
(d)



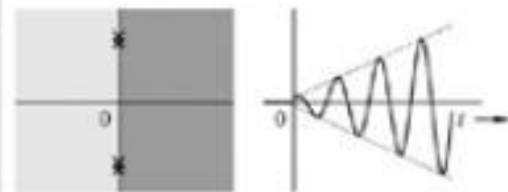
(e)



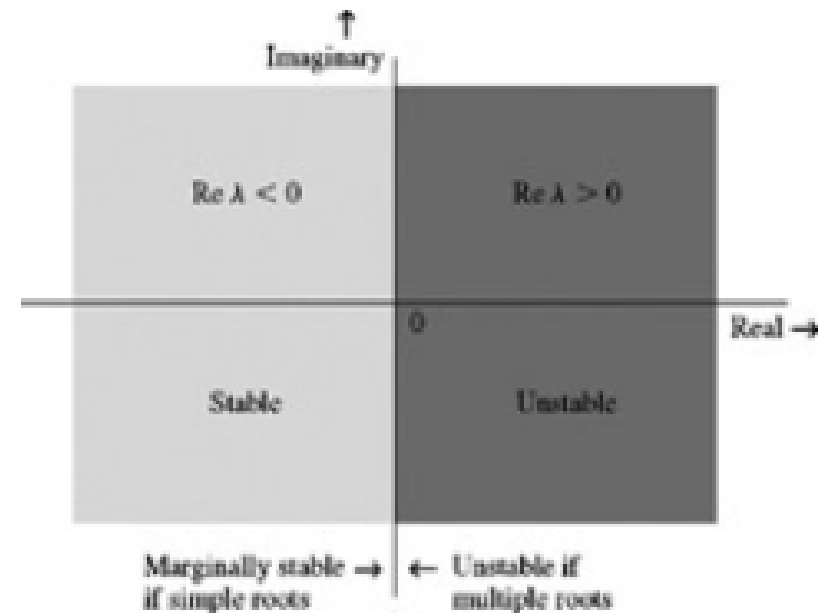
(f)



(g)



(h)



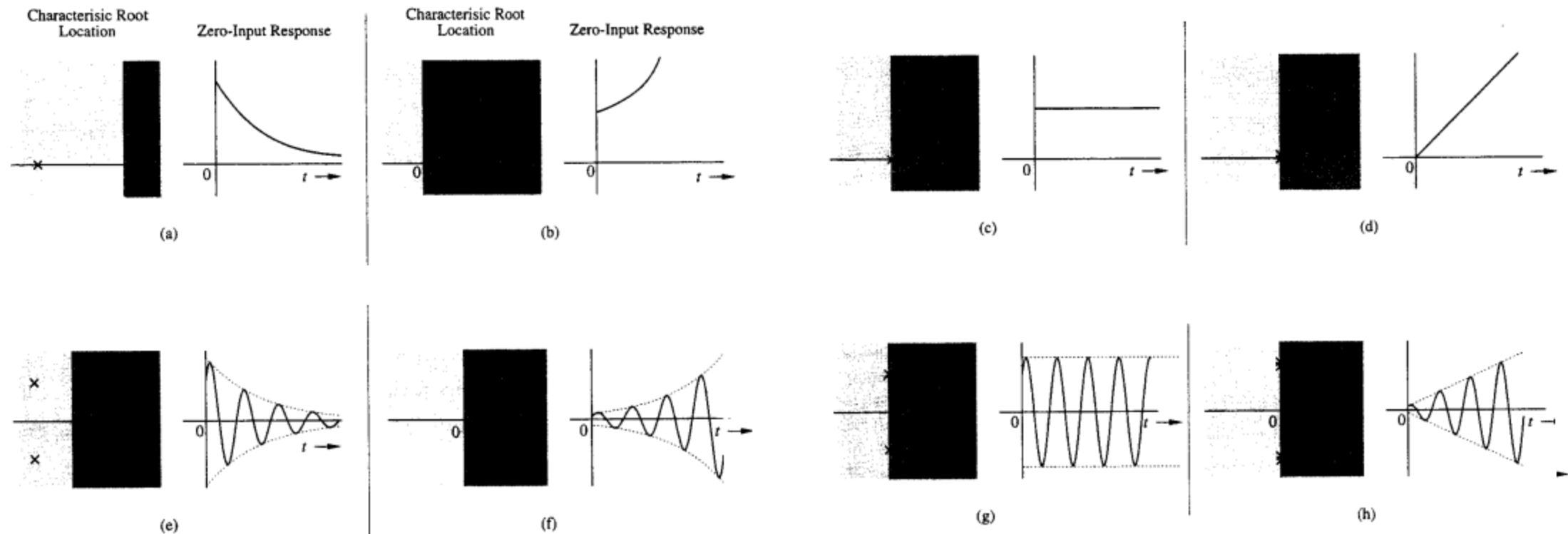


Fig. Location of characteristic roots and the corresponding characteristic modes.

# Sürekli zamanda sistem kararlılığı örnekleri

Investigate the asymptotic and the BIBO stability of LTIC system described by the following equations, assuming that the equations are internal system description.

a.  $(D + 1)(D^2 + 4D + 8)y(t) = (D-3)x(t)$

b.  $(D - 1)(D^2 + 4D + 8)y(t) = (D+2)x(t)$

c.  $(D + 2)(D^2 + 4)y(t) = (D^2 + D + 1)x(t)$

d.  $(D + 1)(D^2 + 4)^2y(t) = (D^2 + 2D + 8)x(t)$



# Sürekli zamanda sistem kararlılığı örnekleri-devam

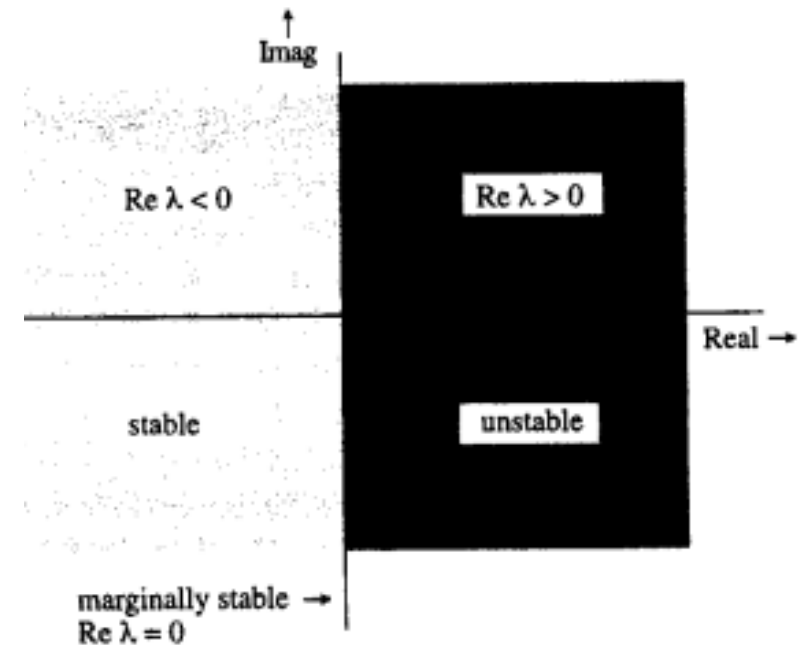
The characteristic polynomials of these systems are

a.  $(\lambda + 1)(\lambda^2 + 4\lambda + 8) = (\lambda + 1)(\lambda + 2 - j2)(\lambda + 2 + j2)$

b.  $(\lambda - 1)(\lambda^2 + 4\lambda + 8) = (\lambda - 1)(\lambda + 2 - j2)(\lambda + 2 + j2)$

c.  $(\lambda + 2)(\lambda^2 + 4) = (\lambda + 2)(\lambda - j2)(\lambda + j2)$

d.  $(\lambda + 1)(\lambda^2 + 4)^2 = (\lambda + 2)(\lambda - j2)^2(\lambda + j2)^2$



Characteristic roots location and system stability.

# Sürekli zamanda sistem kararlılığı örnekleri-devam

a.  $(\lambda + 1)(\lambda^2 + 4\lambda + 8) = (\lambda + 1)(\lambda + 2 - j2)(\lambda + 2 + j2)$

b.  $(\lambda - 1)(\lambda^2 + 4\lambda + 8) = (\lambda - 1)(\lambda + 2 - j2)(\lambda + 2 + j2)$

c.  $(\lambda + 2)(\lambda^2 + 4) = (\lambda + 2)(\lambda - j2)(\lambda + j2)$

d.  $(\lambda + 1)(\lambda^2 + 4)^2 = (\lambda + 1)(\lambda - j2)^2(\lambda + j2)^2$

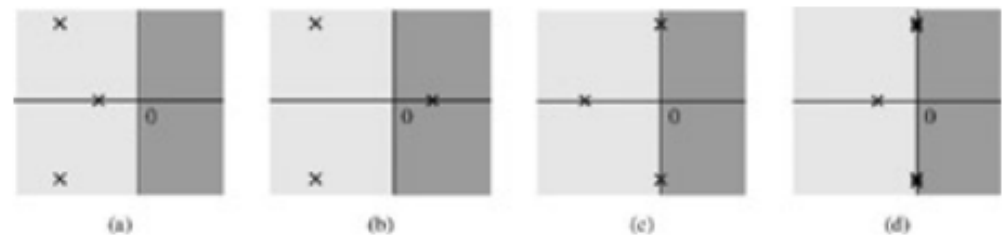
Consequently, the characteristic roots of the systems are (see Fig. 2.20):

a.  $-1, -2 \pm j2$

b.  $1, -2 \pm j2$

c.  $-2 \pm j2$

d.  $1, -\pm j2, \pm j2$



# Bu ders notu için faydalanılan kaynaklar

## Lecture 4

### **Time-domain analysis: Zero-state Response** (Lathi 2.3-2.4.1)

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