ME 233 Advance Control II

Lecture 15

Deterministic Input/Output Approach to SISO Discrete Time Systems

Pole Placement, Disturbance Rejection and Tracking Control

SISO ARMA models

· SISO State space model

$$x(k+1) = Ax(k) + Bu(k)$$
$$y(k) = Cx(k) + Du(k)$$

Where all inputs and outputs are scalars:

- $u(k) \in \mathcal{R}$ control input
- $y(k) \in \mathcal{R}$ output
- $x(k) \in \mathbb{R}^n$ state

SISO transfer function

$$Y(z) = \left[C(sI - A)^{-1}B + D \right] U(z) = \frac{B^*(z)}{A^*(z)} U(z)$$

$$A^*(z) = det\{(zI - A)\} = z^n + a_1 z^{n-1} + \dots + a_n$$

$$B^*(z) = CAdj\{(sI - A)\}B + D$$

= $b_0 z^m + b_1 z^{n-1} + \dots + b_m$

$$d = n - m \ge 0$$
 relative degree

ARMA Models

- Define the $\emph{back-step}$ operator q^{-1} such that

$$y(k-1) = q^{-1}y(k)$$

· the polynomials

$$A(q^{-1}) = q^{-n} A^*(q) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

$$B(q^{-1}) = q^{-m} B^*(q) = b_o + b_1 q^{-1} + \dots + b_m q^{-m}$$

relative degree (pure time delay)

$$d = n - m$$

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) u(k)$$

$$y(k) = b_0 u(k-d) + \dots + b_m u(k-n)$$
$$-a_1 y(k-1) - \dots - a_n y(k-n)$$

SISO ARMA models with persistent disturbances

SISO ARMA model with disturbance

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) [u(k) + d(k)]$$

Where all inputs and outputs are scalars:

- u(k)control input
- d(k)persistent (deterministic) but unknown disturbance
- y(k)output

Deterministic SISO ARMA models

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) [u(k) + d(k)]$$

Where polynomials:

$$A(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

$$B(q^{-1}) = b_0 + b_1 q^{-1} + \dots + b_m q^{-m}$$

are co-prime and **d** is the **known** pure time delay

Polynomials in q-1

· Monic polynomial

$$A(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$
non-delay coefficient is 1

$$A^*(q) = q^n A(q^{-1})$$

$$A^*(q) = q^n + a_1 q^{n-1} + \dots + a_n$$
leading coefficient is 1

$$A(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

$$B(q^{-1}) = b_o + b_1 q^{-1} + \dots + b_m q^{-m}$$

are co-prime if and only if

for all $p \in \mathcal{C}$ such that A(p) = 0

$$B(p) \neq 0$$

Polynomials in q^{-1}

- Schur polynomials in $q^{\text{-}1}$ have all roots outside the unit circle

$$A(q^{-1}) = 1 + a_1q^{-1} + \dots + a_nq^{-n}$$

is Schur if and only if, for all sequences $\{y(k)\} \in \mathcal{R}$

such that
$$A(q^{-1})y(k) = 0$$

$$\lim_{k \to \infty} y(k) = 0$$

Polynomials in q^{-1}

• Schur polynomials in $q^{\text{-}1}$ have all roots outside the unit circle

$$A(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

is Schur if and only if,

for all $p \in \mathcal{C}$ such that $A(p^{-1}) = 0$, |p| < 1

$$A^*(p) = 0$$
 $A^*(q) = q^n A(q^{-1})$

Factorization of the zero polynomial $B(q^{-1})$

The m order zero polynomial:

$$B^*(q) = q^m B(q^{-1}) = 0$$

has

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- m_u zeros which we do not wish to cancel.
- m_s zeros inside the unite circle (asymptotically stable) which we wish to cancel.

$$B(q^{-1}) = B^{s}(q^{-1}) B^{u}(q^{-1})$$

$$B^s(q^{-1})$$
 is Schur

$$B^{u*}(q) = q^{m_u}B^u(q^{-1})$$
 has zeros which we do not wish to cancel

Example

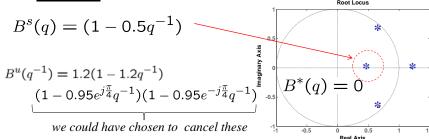
$$B^*(q) = 1.2(q - 0.5)(q - 1.2)(q - 0.95e^{j\frac{\pi}{4}})(q - 0.95e^{-j\frac{\pi}{4}})$$

$$B(q^{-1}) = 1.2(1 - 0.5q^{-1})(1 - 1.2q^{-1})$$

$$(1 - 0.95e^{j\frac{\pi}{4}}q^{-1})(1 - 0.95e^{-j\frac{\pi}{4}}q^{-1})$$

$$= B^{s}(q^{-1})B^{u}(q^{-1})$$

Example



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Control Objectives

- 1. <u>Pole Placement</u>: The poles of the closed loop system must be placed at specific locations in the complex plane.
- Closed loop pole polynomial:

$$A_c(q^{-1}) = B^s(q^{-1}) A'_c(q^{-1})$$

Where:

- $B^s(q^{-1})$ cancelable plant zeros
- $A_c^{'}(q^{-1})$ monic Schur polynomial chosen by the designer $A_c^{'}(q^{-1})=1+a_{c1}^{'}q^{-1}+\cdots+a_{cn_c}^{'}q^{-n_c^{'}}$

Deterministic SISO ARMA models

The zero polynomial:

$$B(q^{-1}) = B^{s}(q^{-1}) B^{u}(q^{-1})$$

Without loss of generality, we will assume that

$$B^{s}(q^{-1}) = 1 + \dots + b_{m_s}^{s} q^{-m_s}$$

$$B^{u}(q^{-1}) = b_{o} + \dots + b_{m_{u}}^{u} q^{-m_{u}}$$

i.e. the Schur polynomial $B^s(q^{-1})$ is monic

Control Objectives

- 2. **Tracking**: The output sequence y(k) must follow a **reference** sequence $y_d(k)$ which is known
- Reference model:

$$A_m(q^{-1})y_d(k) = q^{-d} B_m(q^{-1}) u_d(k)$$

Where:

- $y_d(k)$ reference output sequence, which is known in advance (i.e. $y_d(k+L)$ is available at instance k for some $L{>}0$).
- $A_m(q^{-1})$ monic Schur polynomial chosen by the designer
- $B_m(q^{-1})$ polynomial chosen by the designer

Control Objectives

- **3.** <u>Disturbance rejection</u>: The closed loop system must reject a class of <u>persistent</u> disturbances d(k)
- Disturbance model:

$$A_d(q^{-1})d(k) = 0$$

Where

- $A_d(q^{-1})$ is a **known** annihilating polynomial with roots on the unit circle
- $A_d(q^{-1}), B(q^{-1})$ are co-prime

Deterministic disturbance examples

a) Constant disturbance:

$$d(k) = d(k-1)$$

Then,

$$A_d(q^{-1}) = 1 - q^{-1}$$

b) Sinusoidal disturbance of **known** frequency:

$$d(k) = D \sin(\omega k + \phi)$$

Then,

$$A_d(q^{-1}) = 1 - 2\cos(\omega) q^{-1} + q^{-2}$$

Deterministic disturbance examples

c) Periodic disturbance of \underline{known} period N

$$d(k) = d(k - N)$$

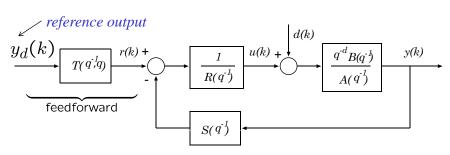
Then,

$$A_d(q^{-1}) = 1 - q^{-N}$$

In all of these three examples, the polynomial $A_d(q^{-1})$ has its roots on the unit circle.

Control Law

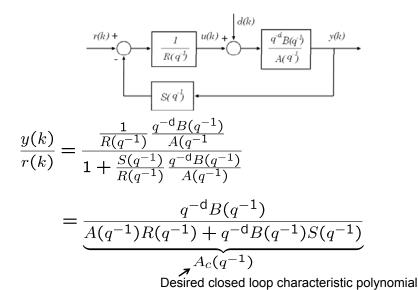
· Feedback and feedforward actions:



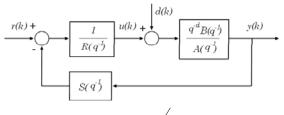
$$u(k) = \frac{1}{R(q^{-1})} \left[r(k) - S(q^{-1})y(k) \right]$$

$$r(k) = T(q^{-1}, q) y_d(k)$$
 Feedforward action (a-causal)

Close Loop TF from r(k) to y(k)



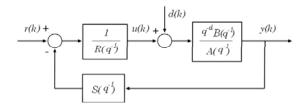
Close Loop TF from r(k) to y(k)



$$\frac{y(k)}{r(k)} = \frac{q^{-\mathsf{d}}B(q^{-1})}{A_c(q^{-1})} = \frac{B^s(q^{-1})}{B^s(q^{-1})} \frac{q^{-\mathsf{d}}B^u(q^{-1})}{A'_c(q^{-1})}$$

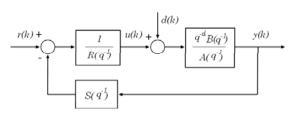
Since
$$\begin{cases} B(q^{-1}) = B^{s}(q^{-1}) B^{u}(q^{-1}) \\ A_{c}(q^{-1}) = B^{s}(q^{-1}) A'_{c}(q^{-1}) \end{cases}$$

Close Loop TF from r(k) to y(k)



$$\left[\underbrace{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})}_{A_c(q^{-1})}\right]y(k) = q^{-\mathsf{d}}B(q^{-1})\,r(k)$$
 Desired closed loop polynomial

Close Loop TF from r(k) to y(k)



$$\left[A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1}) \right] y(k) = q^{-\mathsf{d}}B(q^{-1}) r(k)$$

We need to find polynomials $R(q^{-1})$ and $S(q^{-1})$ so that

$$A(q^{-1})R(q^{-1}) + q^{-d}B(q^{-1})S(q^{-1}) = A_c(q^{-1})$$

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The Diophantine (Bezout) equation

• Given the co-prime polynomials

$$\mathcal{A}(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

$$\mathcal{B}(q^{-1}) = b_0 + b_1 q^{-1} + \dots + b_m q^{-m}$$

- $\mathcal{A}(q^{-1})$ is monic and order n
- $\mathcal{B}(q^{-1})$ is order m
- ullet and a monic polynomial of order $\,n_{\mathcal{C}}$

$$C(q^{-1}) = 1 + c_1 q^{-1} + \dots + c_{n_c} q^{-n_c}$$

The Diophantine (Bezout) equation

We wish to find the polynomials

same order as $\beta(q^{-1})$

$$\mathcal{R}(q^{-1}) = 1 + r_1 q^{-1} + \dots + r_m q^{-m}$$

$$\mathcal{S}(q^{-1}) = s_0 + \dots + s_{n_0} q^{-n_0}$$

which satisfy the Diophantine equation:

$$C(q^{-1}) = A(q^{-1}) R(q^{-1}) + q^{-1} B(q^{-1}) S(q^{-1})$$
given

The Diophantine (Bezout) equation

Expanding in terms of q^{-1} coefficients:

$$\frac{\mathcal{C}(q^{-1}) = \mathcal{A}(q^{-1}) \mathcal{R}(q^{-1}) + q^{-1} \mathcal{B}(q^{-1}) \mathcal{S}(q^{-1})}{\uparrow}$$
order order order
$$n_{c} \qquad n + m \qquad m + n_{s} + 1$$

$$n_s = \max\{n-1, n_c-m-1\}$$

The Diophantine (Bezout) equation

Expanding in terms of q^{-1} coefficients:

$$C(q^{-1}) = A(q^{-1}) R(q^{-1}) + q^{-1} B(q^{-1}) S(q^{-1})$$

We obtain:

Where the matrix $D \in \mathcal{R}^{(n_s+1+m)\times(n_s+1+m)}$ is given by:

The Diophantine (Bezout) equation

Theorem: D is nonsingular iff the polynomials $\mathcal{A}(q^{-1})$ and $q^{-1}\mathcal{B}(q^{-1})$ are co-prime.

The solution to the Diophantine equation is:

$$\begin{bmatrix} r_1 \\ r_2 \\ \vdots \\ r_m \\ s_o \\ \vdots \\ s_{n_s} \end{bmatrix} = D^{-1} \left\{ \begin{bmatrix} c_1 \\ c_2 \\ \vdots \\ c_{nc-1} \\ c_{nc} \\ \vdots \\ 0 \end{bmatrix} - \begin{bmatrix} a_1 \\ a_2 \\ \vdots \\ a_n \\ 0 \\ \vdots \\ 0 \end{bmatrix} \right\}.$$

Example:
$$\mathcal{C}(q^{-1}) = \mathcal{A}(q^{-1}) \, \mathcal{R}(q^{-1}) + q^{-1} \, \mathcal{B}(q^{-1}) \mathcal{S}(q^{-1})$$
 Let

$$\mathcal{C}(q^{-1}) = (1 - 0.5q^{-1})(1 - 0.8q^{-1})$$
 order $n_c = 2$
= $(1 - 1.3q^{-1}0.4q^{-2})$

$$\mathcal{A}(q^{-1}) = (1 - q^{-1})(1 - 1.2q^{-1})$$
 order $n = 2$
= $(1 - 2.2q^{-1} + 1.2q^{-2})$

$$\mathcal{B}(q^{-1}) = (2q^{-1} + 2.4q^{-2}) \qquad \text{order } m = 2$$

Solve for
$$\begin{cases} & \mathcal{R}(q^{-1}) = 1 + r_1q^{-1} + r_2q^{-2} & \text{order } m = 2 \\ & \mathcal{S}(q^{-1}) & \text{order } n_s \end{cases}$$

$$n_s = \max\{n-1, n_c - m - 1\} = \max\{2 - 1, 2 - 2 - 1\} = 1$$

$$\underbrace{(1 - 1.3q^{-1}0.4q^{-2})}_{\mathcal{C}(q^{-1})} = \underbrace{(1 - 2.2q^{-1} + 1.2q^{-2})}_{\mathcal{A}(q^{-1})} \underbrace{(1 + r_1q^{-1} + r_2q^{-2})}_{\mathcal{R}(q^{-1})}$$

Example: $C(q^{-1}) = A(q^{-1}) \mathcal{R}(q^{-1}) + q^{-1} \mathcal{B}(q^{-1}) \mathcal{S}(q^{-1})$

4 equations and 4 unknowns

Example:
$$C(q^{-1}) = A(q^{-1}) \mathcal{R}(q^{-1}) + q^{-1} \mathcal{B}(q^{-1}) \mathcal{S}(q^{-1})$$

Equating coefficients of powers of q^{-1}

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ -2.2 & 1 & 2 & 0 \\ 1.2 & -2.2 & 2.4 & 2 \\ 0 & 1.2 & 0 & 2.4 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \\ s_0 \\ s_1 \end{bmatrix} = \begin{bmatrix} -1.3 \\ 0.4 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} -2.2 \\ 1.2 \\ 0 \\ 0 \end{bmatrix}$$

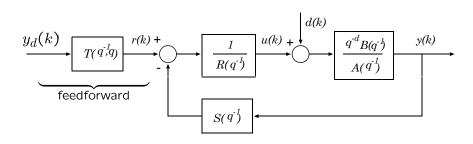
Solution:

$$\mathcal{R}(q^{-1}) = 1 + 0.9q^{-1} + 0.57q^{-2}$$

$$S(q^{-1}) = 0.31 - 0.28q^{-1}$$

Control Law

Feedback and feedforward actions:



$$u(k) = \frac{1}{R(q^{-1})} \left[r(k) - S(q^{-1})y(k) \right]$$

$$r(k) = T(q^{-1}, q) y_d(k)$$
 Feedforward (a-causal)

Feedback Controller

Diophantine equation: Obtain polynomials $R(q^{-1})$, $S(q^{-1})$ which satisfy:

$$A_{c}(q^{-1}) = A(q^{-1}) R(q^{-1}) + q^{-d}B(q^{-1}) S(q^{-1})$$

$$\uparrow \qquad \qquad \uparrow \qquad \qquad \uparrow$$

$$Close \ loop \qquad Plant \ poles \qquad plant \ zeros$$

$$poles$$

$$A_{c}(q^{-1}) = \underline{B^{s}(q^{-1})} A'_{c}(q^{-1})$$

$$R(q^{-1}) = R'(q^{-1}) \underline{A_{d}(q^{-1})} \underline{B^{s}(q^{-1})}$$

We will factor out the $B^s(q^{-1})$ polynomial next

Controller Diophantine equation

Factor out $B^s(q^{-1})$ polynomial $A_c(q^{-1}) = B^s(q^{-1}) A_c'(q^{-1})$ $R(q^{-1}) = R'(q^{-1}) A_d(q^{-1}) B^s(q^{-1})$

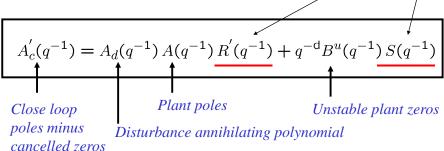
$$A_c(q^{-1}) = A(q^{-1}) R(q^{-1}) + q^{-d} B(q^{-1}) S(q^{-1})$$

$$B^{s}(q^{-1}) A'_{c}(q^{-1}) = B_{s}(q^{-1}) A(q^{-1}) A_{d}(q^{-1}) R'(q^{-1})$$
$$+ q^{-d} B^{s}(q^{-1}) B^{u}(q^{-1}) S(q^{-1})$$

$$A'_{c}(q^{-1}) = A_{d}(q^{-1}) A(q^{-1}) R'(q^{-1}) + q^{-d} B^{u}(q^{-1}) S(q^{-1})$$

Feedback Controller

Diophantine equation: Obtain polynomials $R'(q^{-1})$, $S(q^{-1})$ which satisfy:



$$R(q^{-1}) = R'(q^{-1}) A_d(q^{-1}) B^s(q^{-1})$$
$$A_c(q^{-1}) = B^s(q^{-1}) A'_c(q^{-1})$$

Use previous solution of the Diophantine equation

$$A_c^{'}(q^{-1}) = A_d(q^{-1}) A(q^{-1}) B^{'}(q^{-1}) + q^{-d} B^u(q^{-1}) S(q^{-1})$$

$$\underbrace{A'_{c}(q^{-1})}_{\mathcal{C}(q^{-1})} = \underbrace{\left(A_{d}(q^{-1})A(q^{-1})\right)}_{\mathcal{A}(q^{-1})} \underbrace{R'(q^{-1})}_{\mathcal{R}(q^{-1})} + q^{-1} \underbrace{\left(q^{d-1}B^{u}(q^{-1})\right)}_{\mathcal{B}(q^{-1})} \underbrace{S(q^{-1})}_{\mathcal{S}(q^{-1})}$$

Diophantine equation

$$A'_{c}(q^{-1}) = A_{d}(q^{-1}) A(q^{-1}) B'(q^{-1}) + q^{-d} B^{u}(q^{-1}) S(q^{-1})$$

Solution:

$$R'(q^{-1}) = 1 + r'_1 q^{-1} + \dots + r'_{n'_r} q^{-n'_r}$$

$$S(q^{-1}) = s_o + s_1 q^{-1} + \dots + s_{n_s} q^{-n_s}$$

$$R(q^{-1}) = R'(q^{-1}) A_d(q^{-1}) B^s(q^{-1})$$

$$n'_{r} = d + m_{u} - 1$$
 $n_{s} = \max\{n + n_{d} - 1, n'_{c} - d - m_{u}\}$
 $n_{r} = n'_{r} + n_{d} + m_{s}$

Feedback Controller

$$u(k) = \frac{1}{R(q^{-1})} \left[r(k) - S(q^{-1})y(k) \right]$$

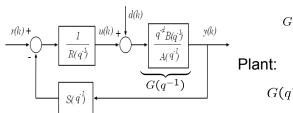
where

$$n'_{r} = d + m_{u} - 1$$
 $n_{s} = \max\{n + n_{d} - 1, n'_{c} - d - m_{u}\}$
 $n_{r} = n'_{r} + n_{d} + m_{s}$

If the degree of the disturbance annihilator polynomial, n_d is large (e.g. N is large), then n_r and n_s are also large

Then, the solution of the Diophantine equation may be ill conditioned.

Example



$$G(q^{-1}) = \frac{q^{-d}B(q^{-1})}{A(q^{-1})}$$

$$G(q^{-1}) = \frac{q^{-2}(2 + 2.4q^{-1})}{(1 - 1.2q^{-1})}$$

Zeros:
$$B(q^{-1}) = (2 + 2.4q^{-1}) \implies \begin{cases} B^s(q^{-1}) = 1 \\ B^u(q^{-1}) = (2 + 2.4q^{-1}) \end{cases}$$

$$d(k) = d(k-1)$$

Disturbance:
$$d(k) = d(k-1) \implies A_d(q^{-1}) = 1 - q^{-1}$$

$$A'_c(q^{-1}) = (1 - 0.5q^{-1})(1 - 0.8q^{-1})$$
$$= (1 - 1.3q^{-1}0.4q^{-2})$$

Diophantine equation

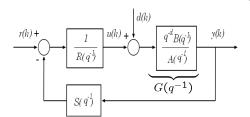
$$A_c^{'}(q^{-1}) = A_d(q^{-1}) A(q^{-1}) R^{'}(q^{-1}) + q^{-\mathsf{d}} B^u(q^{-1}) S(q^{-1})$$

$$(1-1.3q^{-1}0.4q^{-2}) = \underbrace{(1-2.2q^{-1}+1.2q^{-2})}_{A(q^{-1})A_d(q^{-1})} \underbrace{(1+r_1'q^{-1}+r_2'q^{-2})}_{R'(q^{-1})} + q^{-2}\underbrace{(2+2.4q^{-1})}_{B^u(q^{-1})} \underbrace{(s_o+s_1q^{-1})}_{S(q^{-1})}$$
Solution:
$$R'(q^{-1}) = 1 + 0.9q^{-1} + 0.57q^{-2}$$

$$S(q^{-1}) = 0.31 - 0.28q^{-1}$$

$$R(q^{-1}) = A_d(q^{-1})R'(q^{-1}) = (1 - q^{-1})(1 + 0.9q^{-1} + 0.57q^{-2})$$

Example



$$G(q^{-1}) = \frac{q^{-2}(2 + 2.4q^{-1})}{(1 - 1.2q^{-1})}$$

$$d(k) = d(k - 1)$$

Control:
$$u(k) = \frac{1}{R(q^{-1})} [r(k) - S(q^{-1})y(k)]$$

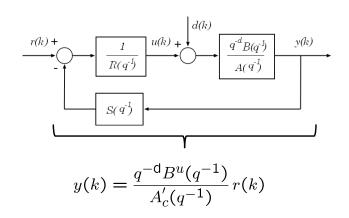
$$R(q^{-1}) = 1 - 0.1q^{-1} - 0.33q^{-2} - 0.57q^{-3}$$

$$S(q^{-1}) = 0.31 - 0.28q^{-1}$$

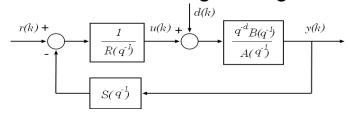
$$r(k) = r(k-1) = 1$$

Feedback Control Law

Feedback control action:



Proof – block diagram algebra



The close loop dynamics is from r(k) and d(k) to y(k)

$$y(k) = \frac{q^{-\mathsf{d}}B(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})} r(k)$$
$$+ \frac{q^{-\mathsf{d}}B(q^{-1})R(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})} d(k)$$

Proof – block diagram algebra

The close loop dynamics is from d(k) to y(k) (r(k) = 0)

$$y(k) = \frac{q^{-\mathsf{d}}B(q^{-1})R(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})}d(k)$$

Substitute:

$$B(q^{-1}) = B^{s}(q^{-1}) B^{u}(q^{-1})$$

$$R(q^{-1}) = R'(q^{-1}) A_{d}(q^{-1}) B^{s}(q^{-1})$$

$$y(k) = \frac{B^{s}(q^{-1})}{B^{s}(q^{-1})} \frac{q^{-\mathsf{d}}B(q^{-1})R'(q^{-1})A_{d}(q^{-1})}{\left[\underbrace{A(q^{-1})A_{d}(q^{-1})R'(q^{-1}) + q^{-\mathsf{d}}B^{u}(q^{-1})S(q^{-1})}_{Cancellation}\right]} d(k)$$
pole-zero
cancellation
$$A'_{c}(q^{-1}) \quad \text{Diophantine equation}$$

Proof – block diagram algebra

The close loop dynamics is from d(k) to y(k) (r(k) = 0)

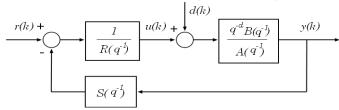
$$y(k) = \left[\frac{q^{-\mathsf{d}}B(q^{-1})R'(q^{-1})}{A'_c(q^{-1})}\right] \underbrace{A_d(q^{-1})d(k)}_{0}$$

$$A_c^{'}(q^{-1})$$
 is Schur $(k) \to 0 \Rightarrow y(k) \to 0$

$$y(k) = \frac{B^{s}(q^{-1})}{B^{s}(q^{-1})} \frac{q^{-\mathsf{d}}B(q^{-1})R'(q^{-1})A_{d}(q^{-1})}{\left[\underbrace{A(q^{-1})A_{d}(q^{-1})R'(q^{-1}) + q^{-\mathsf{d}}B^{u}(q^{-1})S(q^{-1})}_{Cancellation}\right]} d(k)$$

$$A'_{c}(q^{-1}) \quad \textit{Diophantine equation}$$

Proof – block diagram algebra



The close loop dynamics is from r(k) and d(k) to y(k)

$$y(k) = \frac{q^{-\mathsf{d}}B(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})} r(k)$$

$$+ \underbrace{\frac{q^{-\mathsf{d}}B(q^{-1})R(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-\mathsf{d}}B(q^{-1})S(q^{-1})} d(k)}_{Q}$$

Proof – block diagram algebra

$$y(k) = \frac{q^{-d}B(q^{-1})}{A(q^{-1})R(q^{-1}) + q^{-d}B(q^{-1})S(q^{-1})} r(k)$$

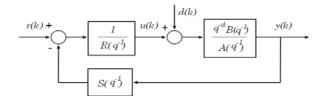
Substitute:

$$B(q^{-1}) = B^{s}(q^{-1}) B^{u}(q^{-1})$$

$$R(q^{-1}) = R'(q^{-1}) A_d(q^{-1}) B^s(q^{-1})$$

$$y(k) = \frac{B^{s}(q^{-1})}{B^{s}(q^{-1})} \frac{q^{-d}B^{u}(q^{-1})}{\left[\underbrace{A(q^{-1})A_{d}(q^{-1})R'(q^{-1}) + q^{-d}B^{u}(q^{-1})S(q^{-1})}_{Diophontine\ equation}\right]} r(k)$$
pole-zero
cancellation
$$A'_{c}(q^{-1}) \quad \text{Diophontine\ equation}$$

Proof – block diagram algebra

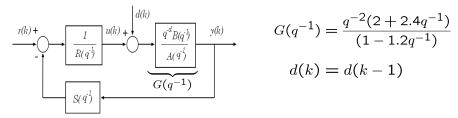


$$y(k) = \frac{q^{-d}B^{u}(q^{-1})}{A'_{c}(q^{-1})} r(k)$$

$$y(k) = \frac{B^s(q^{-1})}{B^s(q^{-1})} \underbrace{\frac{q^{-\mathsf{d}}B^u(q^{-1})}{\left[A(q^{-1})A_d(q^{-1})R'(q^{-1}) + q^{-\mathsf{d}}B^u(q^{-1})S(q^{-1})\right]}}_{pole-zero} r(k)$$

$$A'_C(q^{-1}) \quad \textit{Diophantine equation}$$

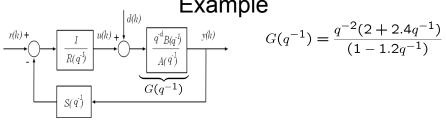
Example



Control:
$$u(k) = \frac{1}{R(q^{-1})} [r(k) - S(q^{-1})y(k)]$$

$$R(q^{-1}) = 1 - 0.1q^{-1} - 0.33q^{-2} - 0.57q^{-3}$$
$$S(q^{-1}) = 0.31 - 0.28q^{-1}$$

Example



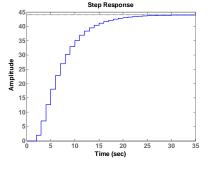
Close loop dynamics:

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$$y(k) = \frac{q^{-d}B^{u}(q^{-1})}{A'_{c}(q^{-1})}r(k)$$

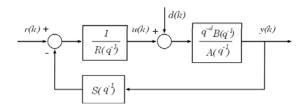
$$y(k) = \frac{q - 2(2 + 2.4q^{-1})}{(1 - 0.8q^{-1})(1 - 0.5q^{-1})} r(k)$$

Unit step response



Feedback Control Law

The feedback control action:



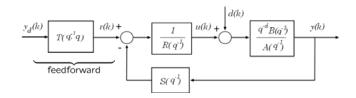
Results in the following close loop input/output dynamics:

$$u(k) = \frac{A(q^{-1})}{B^{s}(q^{-1})A'_{c}(q^{-1})} r(k)$$

$$well-damped zeros + \frac{q^{-d}B^{u}(q^{-1})S(q^{-1})}{A'_{c}(q^{-1})} d(k)$$

Feedforward Control

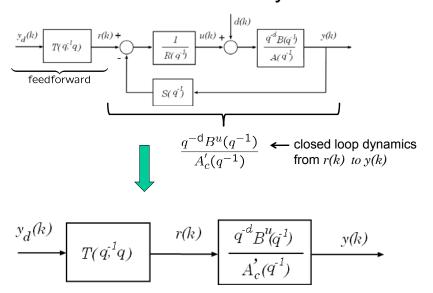
Feedforward control objective is to make y(k) follow $y_d(k)$ as closely as possible.



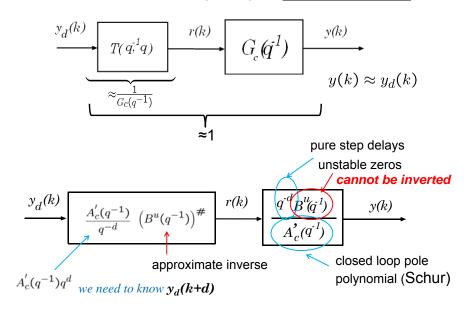
Goal: $y(k) = y_d(k)$ or $y(k) \approx y_d(k)$

how well the objective met depends on whether the plant has unstable zeros or not

Feedforward Control Synthesis



Feedforward control principle: plant inversion

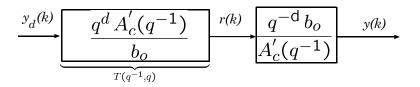


Perfect Tracking Feedforward Control

Perfect tracking can be achieved if all plant zeros are cancelable, i.e.

$$B^u(q^{-1}) = b_o$$

in this case



$$r(k) = \frac{1}{b_0} A'_c(q^{-1}) y_d(k+d)$$

Tracking with unstable zeros

• When the plant has unstable zeros, i.e.

$$B^u(q^{-1}) \neq b_o$$

• We need to find an approximate inverse $\left(B^u(q^{-1})\right)^\#$

$$B^{u}(q^{-1}) \left(B^{u}(q^{-1})\right)^{\#} \approx 1$$

$$\begin{array}{c|c}
 y_d(k) & q^d A'_c(q^{-1}) \left(B^u(q^{-1})\right)^{\#} \\
\hline
 & T(q^{-1},q)
\end{array}$$

$$r(k) \qquad q^{-d} B^u(q^{-1}) \qquad y(k) \qquad y(k)$$

A-causal Bounded-Input Bounded-Output (BIBO) realization of a purely unstable operator

Let
$$B^{u}(p^{-1}) = 0 \iff |p| > 1$$

i.e. all roots of $B^{u*}(q) = q^{m_u}B^u(q^{-1})$ are outside the unite circle

Then we can interpret $\frac{1}{B^u(q^{-1})}$ in two ways:

- $\frac{1}{B^u(q^{-1})}$ is **causal** but unstable
- $\frac{1}{B^u(q^{-1})}$ is **a-causal** but BIBO

A-causal Bounded-Input Bounded-Output (BIBO) realization of a purely unstable operator

Example:
$$B^{u}(q^{-1}) = (2 + 2.4q^{-1}) = 2.4(0.8\overline{3} + q^{-1})$$

$$\frac{1}{B^{u}(q^{-1})} = \frac{0.41\overline{6}}{0.8\overline{3} + q^{-1}} \quad \longleftarrow \quad unstable \ causal \ operator$$

Using an infinite series expansion,

$$\frac{0.41\overline{6}}{(0.8\overline{3} + q^{-1})} = \frac{0.41\overline{6}q}{0.8\overline{3}q + 1}$$

$$= 0.41\overline{6}q \left[1 - 0.8\overline{3}q + (0.8\overline{3}q)^2 - (0.8\overline{3}8q)^3 \cdots + \cdots (-1)^n (0.8\overline{3}q)^n \right]$$
infinite dimensional a-causal operator

A-causal BIBO realization of a purely unstable operator

Thus,
$$y(k) = \frac{1}{2 + 2.4a^{-1}} u(k)$$

Can be realized either as:

$$y(k) = -1.2 y(k-1) + 0.5 u(k)$$
 (unstable)

or

$$y(k) = 0.41\overline{6} \left[u(k+1) - 0.8\overline{3} u(k+2) + (0.8\overline{3})^2 u(k+3) - (0.8\overline{3})^3 u(k+4) + \dots + (-0.8\overline{3})^n u(k+n+1) + \dots \right]$$
(a-causal BIBO)

Example: realizing $\left(B^u(q^{-1})\right)^\#$

Let,
$$B^{u}(q^{-1}) = (2 + 2.4q^{-1})$$

1) Truncated a-casual series expansion:

$$(B^{u}(q^{-1}))^{\#} = 0.41\overline{6} [q - 0.8\overline{3}q^{2} + (0.8\overline{3}q)^{3} - (0.8\overline{3}8q)^{4}]$$

2) Zero-phase error feedforward operator:

$$(B^{u}(q^{-1}))^{\#} = \frac{1}{[4.4]^{2}}(2 + 2.4q)$$

A-causal BIBO approximation of a purely unstable operator

We will now describe two methods of approximating a purely unstable operator:

1) Truncated a-casual series expansion:

$$(B^{u}(q^{-1}))^{\#} = \beta_1 q + \beta_2 q^2 + \dots + \beta_3 q^M$$

2) Zero-phase error feedforward operator: (develop by Prof. Tomizuka)

$$(B^{u}(q^{-1}))^{\#} = \frac{1}{[B^{u}(1)]^{2}} B^{u}(q)$$

Zero-phase error tracking

One of the most popular feedforward techniques for systems with unstable zeros.

$$(B^{u}(q^{-1}))^{\#} = \frac{1}{|B^{u}(0)|^{2}} B^{u}(q)$$

Define the zero-phase operator

$$G_{zp}(q^{-1}, q) = B^{u}(q^{-1}) \left(B^{u}(q^{-1}) \right)^{\#}$$
$$= \frac{B^{u}(q^{-1}) B^{u}(q)}{[B^{u}(1)]^{2}}$$

Zero-phase error transfer function

A-causal zero-phase transfer function:

$$G_{zp}(z^{-1}, z) = \frac{B^u(z^{-1}) B^u(z)}{[B^u(1)]^2}$$

Properties:

- It has zero-phase, i.e. $\operatorname{Im}\left\{G_{zp}(e^{-j\omega},e^{j\omega})\right\}=0$
- It has unity dc gain, i.e.

$$G_{zp}(e^{-0}, e^{0}) = 1$$

Let,
$$B^{u}(q^{-1}) = (2 + 2.4q^{-1})$$

- Zero-phase feedforward: $(B^u(q^{-1}))^\# = \frac{1}{[4.4]^2}(2 + 2.4q)$
 - Zero-phase transfer function:

$$G_{zp}(z^{-1},z) = \frac{(2+2.4z^{-1})(2z+2.4)}{[4.4]^2}$$

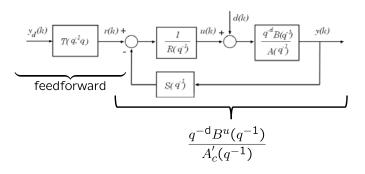
Sinusoidal zero-phase error tracking

If $y_d(k)$ is a sinusoidal, there will be no phase shift between $y_d(k)$ and y(k)

$$y(k) = \frac{B^{u}(q^{-1}) B^{u}(q)}{[B^{u}(1)]^{2}} y_{d}(k)$$
o.5
o
-o.5

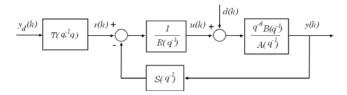
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Zero-phase error feedforward



$$T(q^{-1},q) = A'_{c}(q^{-1}) q^{d} \frac{B^{u}(q)}{[B^{u}(1)]^{2}}$$

Zero-phase error feedforward



$$y(k) = \frac{B^{u}(q^{-1}) B^{u}(q)}{[B^{u}(1)]^{2}} y_{d}(k)$$