

ME 233 Spring 2012

Solution to Homework #8

1. (a) We want $y(k)$ to be driven to 0 in finite time. Thus, the closed loop transfer function should have all of its poles at the origin. To achieve this, we choose the closed loop characteristic polynomial to be $A_c = 1$. Therefore, the Bezout (Diophantine) equation for this system is given by

$$\begin{aligned} A_c &= A_d AR' + q^{-1} BS \\ 1 &= (1 - q^{-8}) (1 - 1.5q^{-1} + 0.56q^{-2}) (1) + q^{-1} (0.1) S \end{aligned}$$

Thus

$$\begin{aligned} R' &= 1 \\ S &= 10q [1 - (1 - q^{-8}) (1 - 1.5q^{-1} + 0.56q^{-2})] \\ &= 15 - 5.6q^{-1} + 10q^{-7} - 15q^{-8} + 5.6q^{-9} \end{aligned}$$

- (b) See Figure 1 for simulation results.

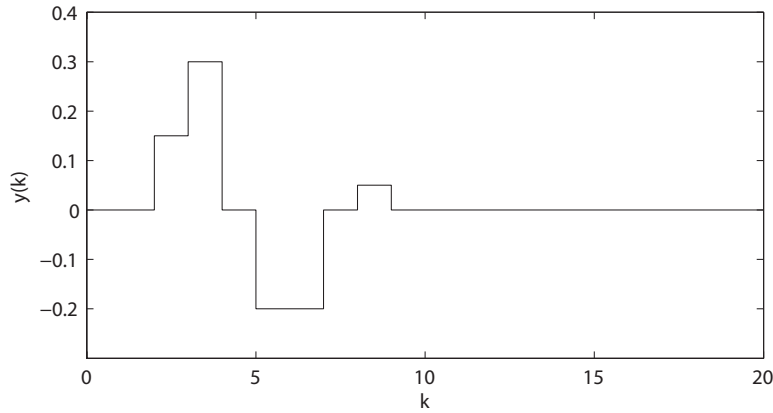


Figure 1: Closed loop simulation results

- (c) See Figure 2 for simulation results.
(d) With this controller, the closed loop system has a pole at z if and only if

$$\begin{aligned} 0 &= 1 + \left[\frac{k_r z^{-(N-1)} \bar{A}(z^{-1})}{0.1 A_d(z^{-1})} \right] \left[\frac{0.1 z^{-2}}{\bar{A}(z^{-1})} \frac{0.8}{(1 - 0.2q^{-1})} \right] \\ &= 1 + \frac{0.8 k_r z^{-N-1}}{(1 - z^{-N})(1 - 0.2z^{-1})} \\ &= 1 + \frac{0.8 k_r}{(z - 0.2)(z^8 - 1)} = 0 \end{aligned}$$

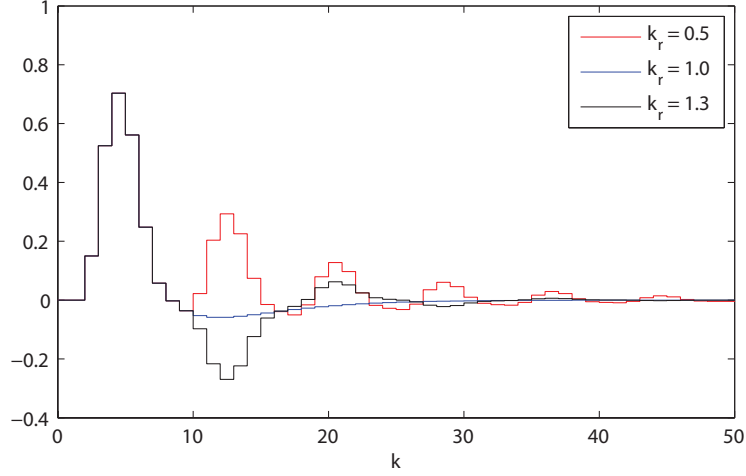


Figure 2: Closed loop simulation results for $k_r = 0.5, 1$, and 1.3

Figure 3 shows the root locus plot of this system. Clearly, the closed loop system is unstable for all $k_r > 0$.

- (e) i. For this system, z is a closed loop pole if and only if

$$\begin{aligned} 0 &= 1 + \frac{0.8k_r}{(z - 0.2)(z^8 - 0.25[z + 2 + z^{-1}])} \\ &= 1 + \frac{0.8k_r z}{(z - 0.2)(z^9 - 0.25[z^2 + 2z + 1])} \end{aligned}$$

Figure 4 shows the root locus plot of the closed loop poles. For $k_r = 0.5$, the system is asymptotically stable.

- ii. See Figure 5 for simulation results.

2. First, we need to design Kalman filter. Solve the following Riccati equation

$$M = \bar{A}M\bar{A}^T + \bar{B}_w W \bar{B}_w^T - \bar{A}M\bar{C}^T [\bar{C}M\bar{C}^T + V]^{-1} \bar{C}M\bar{A}^T$$

where

$$\bar{A} = \begin{bmatrix} 0.8 & 1 \\ 0 & 0 \end{bmatrix}, \quad \bar{B} = \begin{bmatrix} 1 \\ -2 \end{bmatrix}, \quad \bar{B}_w = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad \bar{C} = \begin{bmatrix} 1 & 0 \end{bmatrix}, \quad W = 0.225, \quad V = 0.625.$$

Let

$$M = \begin{bmatrix} m_1 & m_2 \\ m_2 & m_3 \end{bmatrix} \succ 0.$$

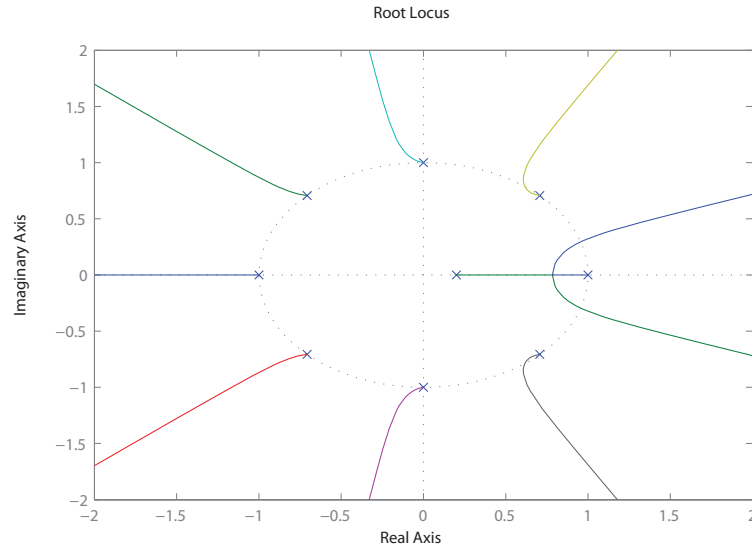


Figure 3: Root locus of repetitive control system with unmodeled plant dynamics

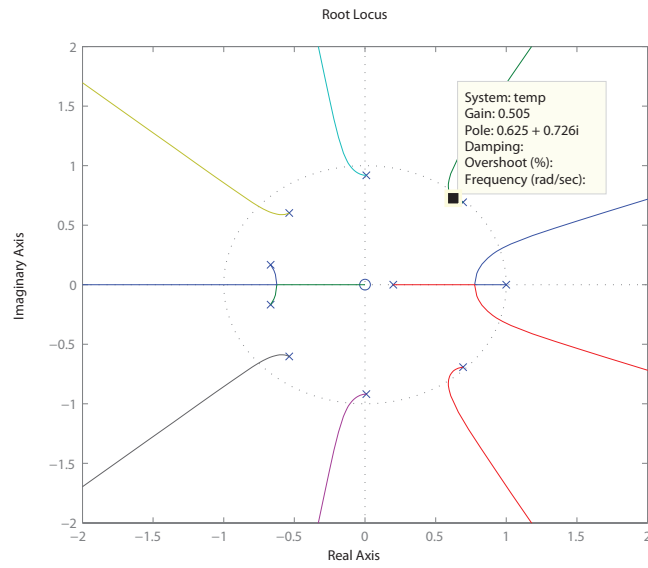


Figure 4: Root locus of Q-filter repetitive control system with unmodelled plant dynamics

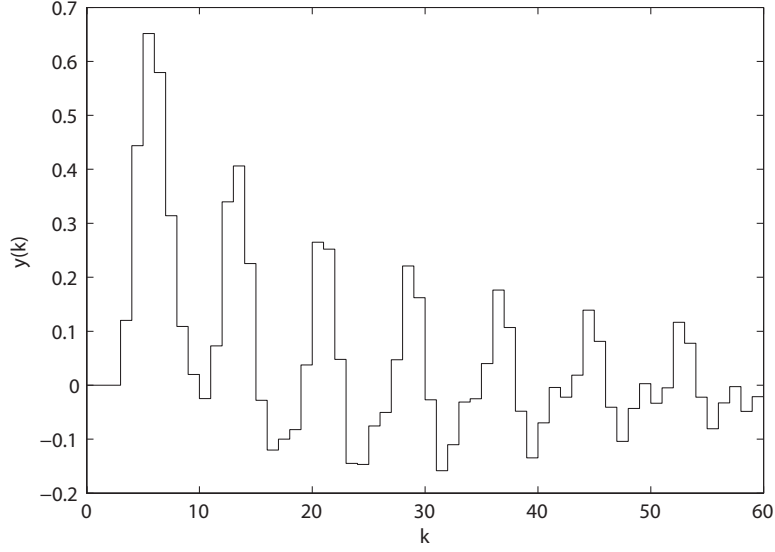


Figure 5: Closed loop simulation results for controller with Q-filter

Then,

$$\begin{aligned}
\begin{bmatrix} m_1 & m_2 \\ m_2 & m_3 \end{bmatrix} &= \begin{bmatrix} 0.8 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} m_1 & m_2 \\ m_2 & m_3 \end{bmatrix} \begin{bmatrix} 0.8 & 0 \\ 1 & 0 \end{bmatrix} + \begin{bmatrix} 0.225 & 0 \\ 0 & 0 \end{bmatrix} - \frac{\begin{bmatrix} 0.8 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} m_1 \\ m_2 \end{bmatrix} \begin{bmatrix} m_1 & m_2 \end{bmatrix} \begin{bmatrix} 0.8 & 0 \\ 1 & 0 \end{bmatrix}}{m_1 + 0.625} \\
&= \begin{bmatrix} 0.8^2 m_1 + 1.6 m_2 + m_3 + 0.225 & 0 \\ 0 & 0 \end{bmatrix} - \frac{1}{m_1 + 0.625} \begin{bmatrix} 0.8^2 m_1^2 + 1.6 m_1 m_2 + m_2^2 & 0 \\ 0 & 0 \end{bmatrix} \\
&\Rightarrow \begin{cases} m_2 = 0 \\ m_3 = 0 \\ m_1 = 0.8^2 m_1 + 0.225 - \frac{0.8^2 m_1^2}{m_1 + 0.625} = 0.225 + \frac{0.4 m_1}{m_1 + 4} \end{cases} \\
&\Rightarrow m_1 = 0.375 \\
&\Rightarrow L = \bar{A} M \bar{C}^T [\bar{C} M \bar{C}^T + V]^{-1} = \begin{bmatrix} 0.3 \\ 0 \end{bmatrix}.
\end{aligned}$$

Then, the output is

$$Y(z) = \bar{C} (zI - \bar{A})^{-1} \bar{B} U(z) + [1 + \bar{C} (zI - \bar{A})^{-1} L] E(z).$$

Thus, we can get the transfer function

$$\begin{aligned}
y(k) &= \bar{C} (qI - \bar{A})^{-1} \bar{B} u(k) + [1 + \bar{C} (qI - \bar{A})^{-1} L] \epsilon(k) \\
&= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} q - 0.8 & -1 \\ 0 & q \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ -2 \end{bmatrix} u(k) + \left\{ 1 + \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} q - 0.8 & -1 \\ 0 & q \end{bmatrix}^{-1} \begin{bmatrix} 0.3 \\ 0 \end{bmatrix} \right\} \epsilon(k) \\
&= \frac{q - 2}{q(q - 0.8)} u(k) + \frac{q - 0.5}{q - 0.8} \epsilon(k) \\
&= \frac{q^{-1}(1 - 2q^{-1})}{1 - 0.8q^{-1}} u(k) + \frac{1 - 0.5q^{-1}}{1 - 0.8q^{-1}} \epsilon(k).
\end{aligned}$$

Thus, we know

$$\begin{aligned}
A(q^{-1}) &= 1 - 0.8q^{-1}, & B^u(q^{-1}) &= q^{-1} - 0.5, & B^s(q^{-1}) &= -2, \\
C(q^{-1}) &= 1 - 0.5q^{-1}, & \bar{B}^u(q^{-1}) &= 1 - 0.5q^{-1}, & d &= 1.
\end{aligned}$$

Solve the Diophantine equation

$$C(q^{-1})\bar{B}^u(q^{-1}) = A(q^{-1})R(q^{-1}) + q^{-1}B^u(q^{-1})S(q^{-1})$$

where

$$R(q^{-1}) = 1 + r_1q^{-1}, \quad S(q^{-1}) = s_0.$$

Then,

$$\begin{aligned} (1 - 0.5q^{-1})(1 - 0.5q^{-1}) &= (1 - 0.8q^{-1})(1 + r_1q^{-1}) + q^{-1}(q^{-1} - 0.5)s_0 \\ \Rightarrow \begin{cases} -1 = r_1 - 0.8 - 0.5s_0 \\ 0.25 = -0.8r_1 + s_0 \end{cases} \\ \Rightarrow \begin{cases} s_0 = 0.15 \\ r_1 = -0.125 \end{cases} \\ \Rightarrow R(q^{-1}) = 1 - 0.125q^{-1}, S(q^{-1}) = 0.15. \end{aligned}$$

Finally, we can get the minimum variance regulator feedback law:

$$u(k) = \frac{-S(q^{-1})}{B^s(q^{-1})R(q^{-1})}y(k) = \frac{0.075}{1 - 0.125q^{-1}}y(k).$$

3. Proof

Applying the signal $y(k)$ to both sides of the Diophantine equation $C(q^{-1})A_m(q^{-1}) = A(q^{-1})R(q^{-1}) + q^{-d}S(q^{-1})$, we see that

$$C(q^{-1})A_m(q^{-1})y(k) = R(q^{-1})A(q^{-1})y(k) + q^{-d}S(q^{-1})y(k).$$

Since $A(q^{-1})y(k) = q^{-d}B(q^{-1})u(k) + C(q^{-1})\epsilon(k)$ by the plant dynamics, we see that

$$\begin{aligned} C(q^{-1})A_m(q^{-1})y(k) &= R(q^{-1})[q^{-d}B(q^{-1})u(k) + C(q^{-1})\epsilon(k)] + q^{-d}S(q^{-1})y(k) \\ &= q^{-d}[R(q^{-1})B(q^{-1})u(k) + S(q^{-1})y(k)] + R(q^{-1})C(q^{-1})\epsilon(k). \end{aligned} \quad (1)$$

Applying the $C(q^{-1})$ polynomial to both sides of the reference model equation, we see that

$$C(q^{-1})A_m(q^{-1})y_m(k) = q^{-d}C(q^{-1})B_m(q^{-1})r_m(k).$$

Subtracting this equation from (1), we see that

$$\begin{aligned} C(q^{-1})A_m(q^{-1})[y(k) - y_m(k)] &= q^{-d}[R(q^{-1})B(q^{-1})u(k) + S(q^{-1})y(k) - C(q^{-1})B_m(q^{-1})r_m(k)] \\ &\quad + R(q^{-1})C(q^{-1})\epsilon(k). \end{aligned}$$

Defining the signals $w(k)$, $z(k)$, and $\epsilon_f(k)$ respectively by

$$\begin{aligned} w(k) &= A_m(q^{-1})[y(k) - y_m(k)] \\ C(q^{-1})z(k) &= R(q^{-1})B(q^{-1})u(k) + S(q^{-1})y(k) - C(q^{-1})B_m(q^{-1})r_m(k) \\ \epsilon_f(k) &= R(q^{-1})\epsilon(k) \end{aligned}$$

we write

$$C(q^{-1})w(k) = q^{-d}C(q^{-1})z(k) + C(q^{-1})\epsilon_f(k).$$

Since the polynomial $C(q^{-1})$ is anti-Schur, we therefore write

$$w(k) = z(k - d) + \epsilon_f(k).$$

By Least Squares property 1, we know that $E\{y(k-j)\epsilon(k)\} = 0$, $\forall j > 0$. Since $u(k)$ is a function of $y(k), y(k-1), y(k-2), \dots$, and $r_m(k), r_m(k-1), r_m(k-2), \dots$, we also see that $E\{u(k-j)\epsilon(k)\} = 0$, $\forall j > 0$. By definition, $z(k)$ is a causal function of $u(k), y(k)$, and $r_m(k)$. Therefore, we see that $E\{z(k-j)\epsilon(k)\} = 0$, $\forall j > 0$. This implies that

$$E\{z(k-d)\epsilon_f(k)\} = E\{z(k-d)\epsilon(k)\} + r_1 E\{z(k-d)\epsilon(k-1)\} \\ + \dots + r_{d-1} E\{z(k-d)\epsilon(k-d+1)\} = 0 .$$

Therefore,

$$J = E\{w^2(k)\} = E\{z^2(k-d)\} + E\{\epsilon_f^2(k)\} + 2E\{z(k-d)\epsilon_f(k)\} \\ = E\{z^2(k-d)\} + E\{\epsilon_f^2(k)\} .$$

Up until this point, we have not used any information involving $u(k)$; the preceding equality holds regardless of how $u(k)$ is chosen, so long as the closed-loop system is stable and $u(k)$ is WSS (i.e. it is a time-invariant function of $y(k)$ and $r_m(k)$). Since the choice of $u(k)$ does not affect the correlation of $\epsilon_f(k)$, we see that minimizing the correlation of $z(k-d)$ also minimizes J . Therefore, choosing

$$u(k) = \frac{1}{R(q^{-1})B(q^{-1})} \left[C(q^{-1})B_m(q^{-1})r_m(k) - S(q^{-1})y(k) \right]$$

makes $C(q^{-1})z(k)$ zero, which in turn makes $z(k)$ zero (because $C(q^{-1})$ is anti-Schur), which obviously minimizes $E\{z(k)\}$. Therefore, this control law minimizes J .