

ME233 Advance Control II Lecture 2

Review of ME 232 Lectures 25 & 26

Linear Quadratic Regulators (LQR) PART II

(ME232 Class Notes pp. 135-137)

Outline

Previous lecture :

- Dynamic programming
- Solution of finite-horizon LQR

This Lecture: Review ME232 results on

- Infinite horizon LQR (steady state)
 - Stability margins
 - Reciprocal root locus

Infinite Horizon LQ regulator

LTI system:

$$x(k+1) = Ax(k) + Bu(k) \quad x(0) = x_o$$

LQR that minimizes the cost:

$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{x^T(k) Q x(k) + u^T(k) R u(k)\}$$

$$Q = C^T C \succeq 0$$

$$R \succ 0$$

Infinite Horizon (IH) LQ regulator

Assume that $[A, B]$ stabilizable and $[A, C]$ detectable,

- Optimal, asymptotically stable, close loop system

$$x(k+1) = [A - BK] x(k) \quad x(0) = x_o$$

$$K = [R + B^T P B]^{-1} B^T P A$$

Algebraic Riccati Equation (ARE)

$$P = Q + A^T P A - A^T P B [R + B^T P B]^{-1} B^T P A$$

Infinite Horizon LQ Regulator

Lets analyze the stability and robustness properties of the closed loop system:

$$x(k+1) = Ax(k) + Bu(k)$$

$$u(k) = -Kx(k) + v(k)$$

With fictitious reference input $v(k)$

$$v(k) = v_o = 0$$

Infinite Horizon LQ Regulator

Use the Z-transform:

$$X(z) = (zI - A)^{-1}BU(z)$$

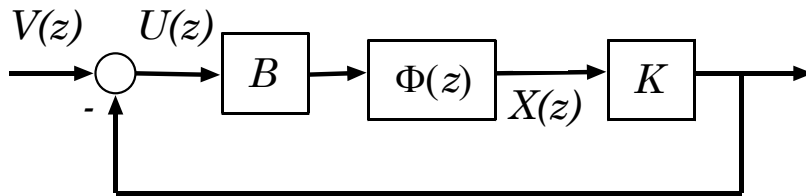
$$U(z) = -KU(z) + V(z)$$

Define

$$\Phi(z) = (zI - A)^{-1}$$

Infinite Horizon LQ Regulator

Close loop system block diagram:



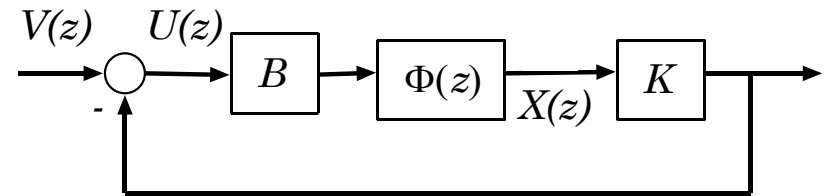
$$\Phi(z) = (zI - A)^{-1}$$

$$X(z) = \Phi(z)BU(z)$$

$$U(z) = V(z) - KX(z)$$

Infinite Horizon LQ Regulator

Close loop system block diagram:

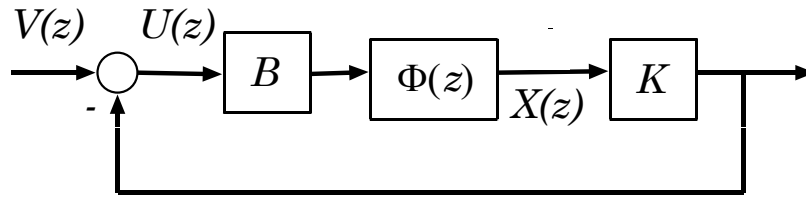


Open loop transfer function:

$$G_o(z) = K\Phi(z)B$$

Infinite Horizon LQ Regulator

Close loop system block diagram:

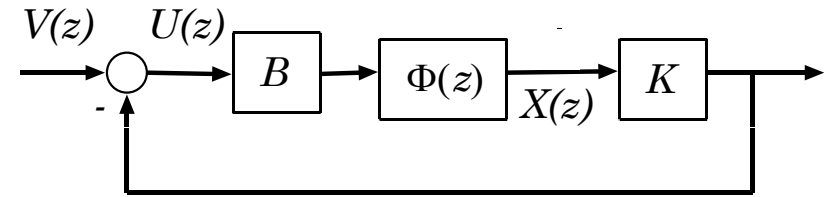


Close loop sensitivity transfer function
(from $V(z)$ to $U(z)$):

$$S(z) = [I + K\Phi(z)B]^{-1}$$

Infinite Horizon LQ Regulator

Close loop system block diagram:

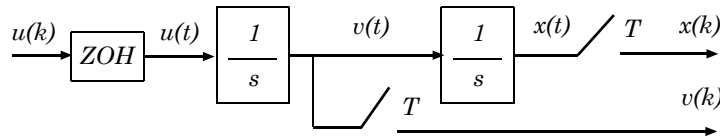


For Single Input Systems $u(k) \in \mathcal{R}$

$$S(z) = \frac{1}{1 + K\Phi(z)B}$$

Example – Double Integrator

Double integrator with ZOH and sampling time $T=1$:

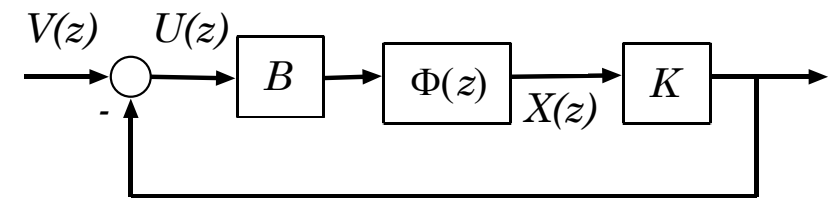


$$\begin{bmatrix} x_1(k+1) \\ x_2(k+1) \end{bmatrix} = \begin{bmatrix} 1 & T \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(k) \\ x_2(k) \end{bmatrix} + \begin{bmatrix} \frac{T^2}{2} \\ \frac{T}{1} \end{bmatrix} u(k)$$

$$\begin{bmatrix} x_1(k+1) \\ x_2(k+1) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(k) \\ x_2(k) \end{bmatrix} + \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} u(k)$$

Example – Double Integrator

Close loop system block diagram:

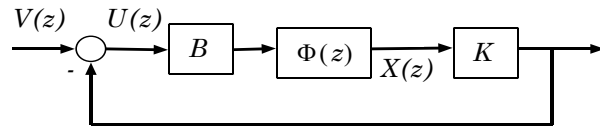


$$\begin{bmatrix} x_1(k+1) \\ x_2(k+1) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(k) \\ x_2(k) \end{bmatrix} + \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} u(k)$$

$$y(k) = \begin{bmatrix} 1 & 0 \end{bmatrix} x(k) \quad J = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + Ru^2(k)\}$$

Example – Double Integrator

Close loop system block diagram:



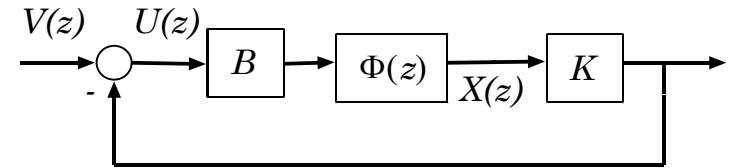
For $R = 10$ we obtained $K = \begin{bmatrix} 0.21 & 0.65 \end{bmatrix}$

Open loop transfer function:

$$G_o(z) = K\Phi(z)B = \begin{bmatrix} 0.21 & 0.61 \end{bmatrix} \begin{bmatrix} (z-1) & -1 \\ 0 & (z-1) \end{bmatrix}^{-1} \begin{bmatrix} 0.5 \\ 1 \end{bmatrix}$$

$$= \frac{0.76z - 0.55}{(z-1)^2}$$

Example – Double Integrator

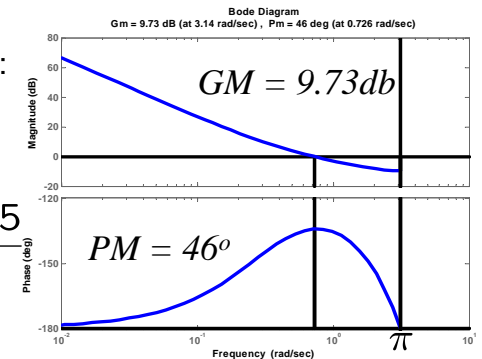


$R = 10$

Open loop transfer function:

$$G_o(j\omega) = K\Phi(j\omega)B$$

$$= \frac{0.76 e^{j\omega} - 0.55}{(e^{j\omega} - 1)^2}$$

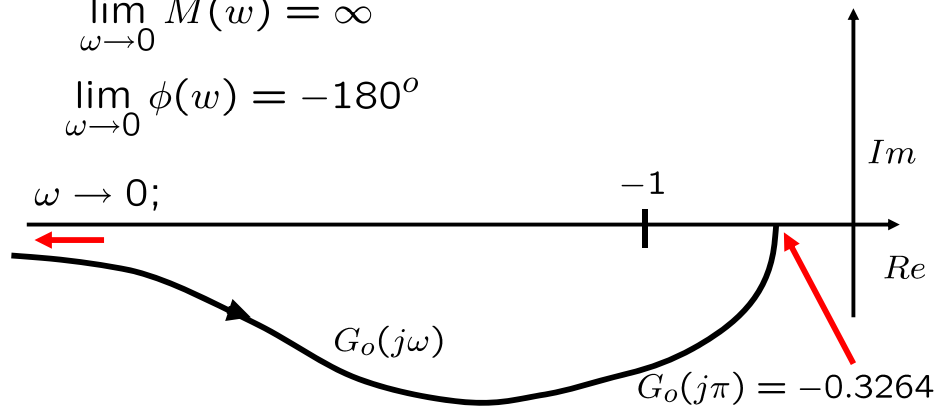


Example – Nyquist plot

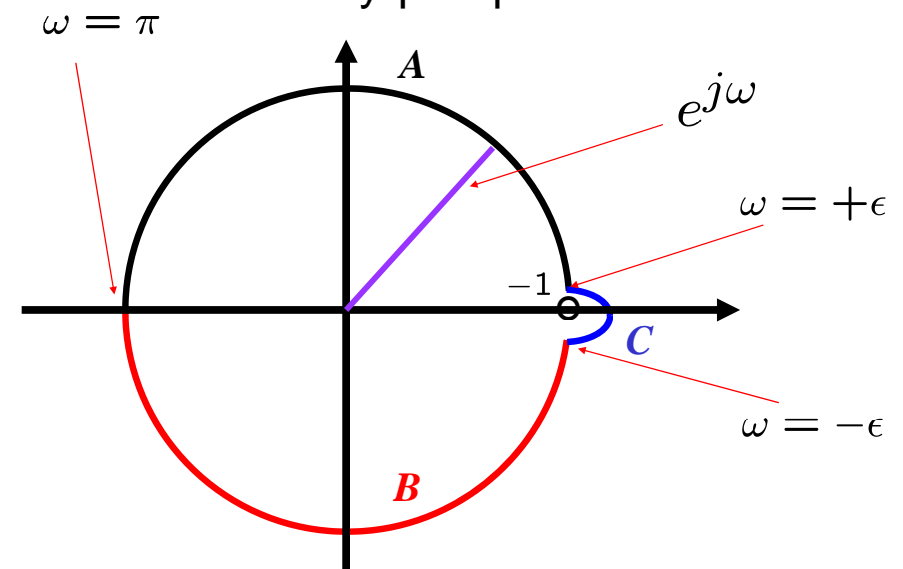
$$G_o(j\omega) = \frac{0.76 e^{j\omega} - 0.55}{(e^{j\omega} - 1)^2} = M(\omega) e^{j\phi(\omega)}$$

$$\lim_{\omega \rightarrow 0} M(\omega) = \infty$$

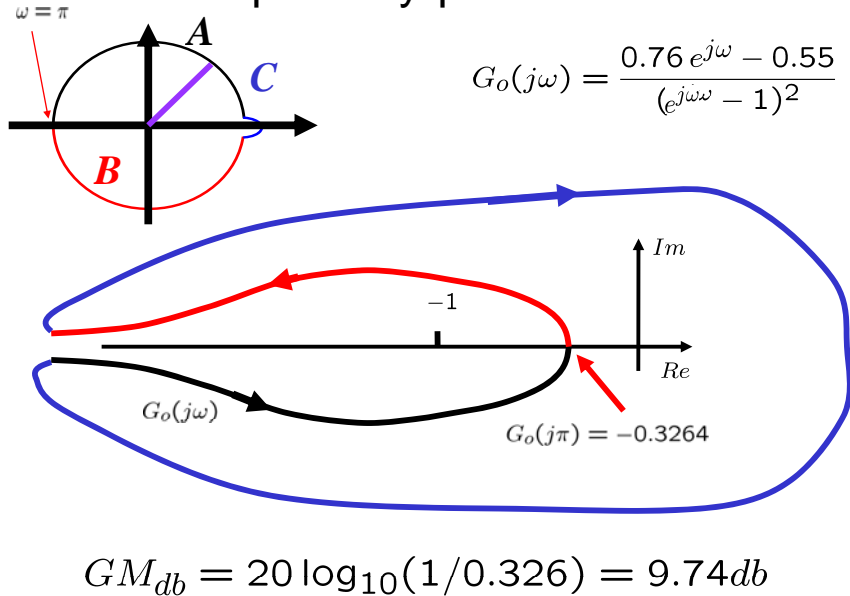
$$\lim_{\omega \rightarrow 0} \phi(\omega) = -180^\circ$$



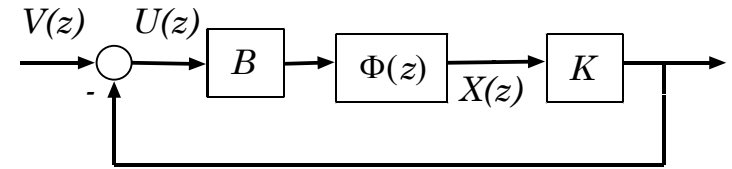
Nyquist path



Example – Nyquist Theorem



Example – Double Integrator

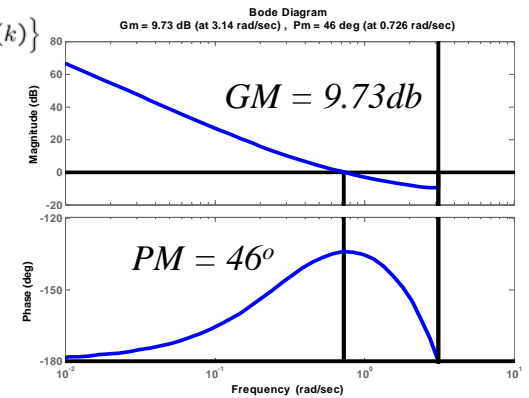


$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + u^T(k) R u(k)\}$$

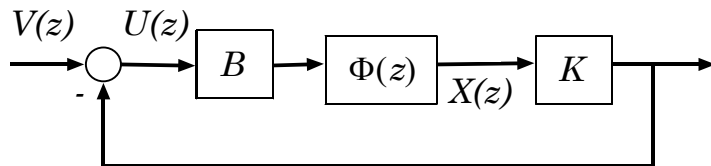
$$R = 10$$

Bode Plot

$$G_o(j\omega) = \frac{0.76 e^{j\omega} - 0.55}{(e^{j\omega} - 1)^2}$$



Example – Double Integrator

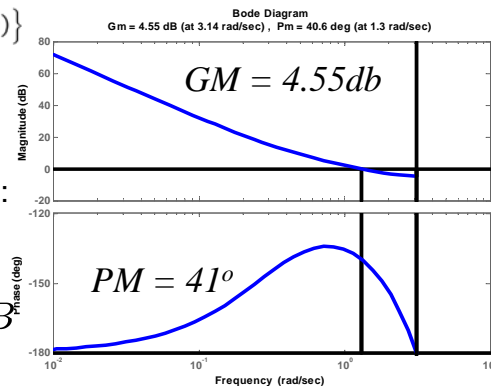


$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + u^T(k) R u(k)\}$$

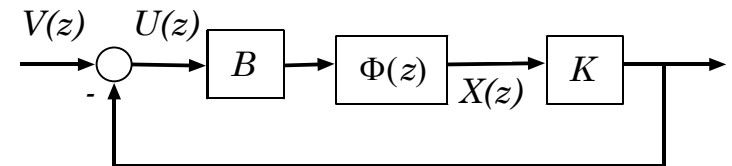
$$R = 0.1$$

Open loop transfer function:

$$G_o(j\omega) = K\Phi(j\omega)B$$



Example – Double Integrator

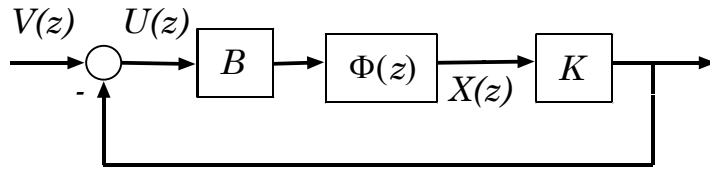


$$R = 10$$

Sensitivity transfer function:

$$S(z) = \frac{1}{1 + K\Phi(z)B} = \frac{z^2 - 2z + 1}{z^2 - 1.24z + 0.45}$$

Example – Double Integrator

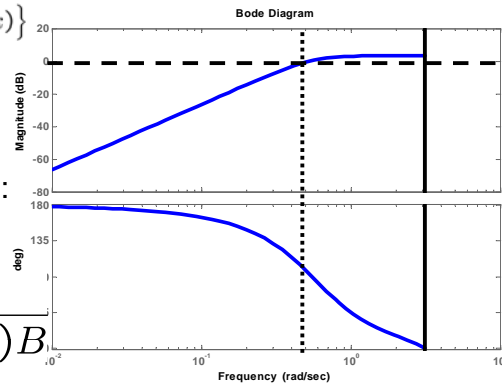


$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + u^T(k) R u(k)\}$$

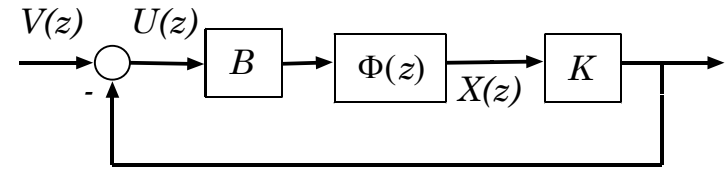
$$R = 10$$

Sensitivity transfer function:

$$S(j\omega) = \frac{1}{1 + K\Phi(j\omega)B}$$



Example – Double Integrator

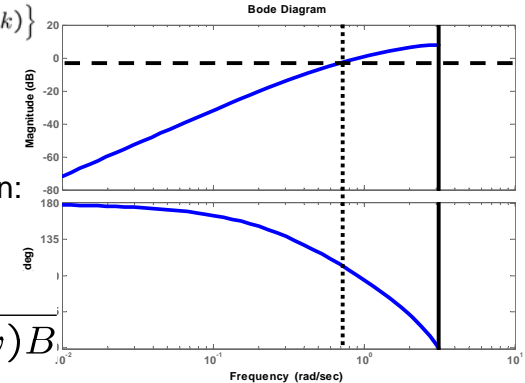


$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + u^T(k) R u(k)\}$$

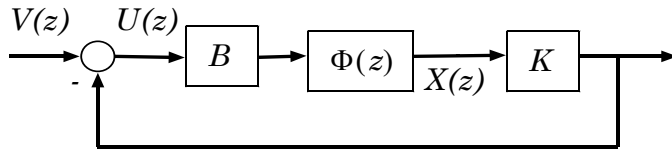
$$R = 0.1$$

Open loop transfer function:

$$S(j\omega) = \frac{1}{1 + K\Phi(j\omega)B}$$



Example – Double Integrator

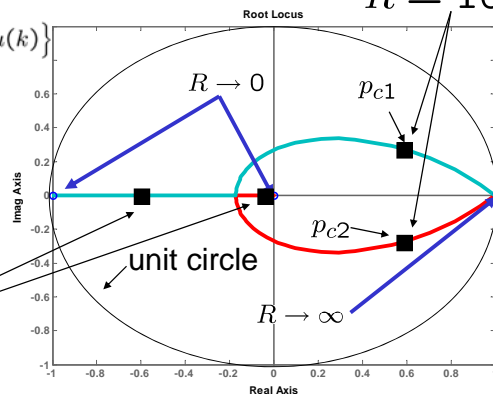


$$J[x_o] = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + u^T(k) R u(k)\}$$

$$R = 10$$

Close loop poles for
varying values of
 $R \in (\infty, 0)$

$$R = 0.1$$

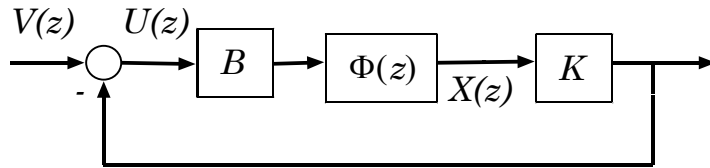


Stability and Robustness of LQR

- For Single Input LQR systems, $(u(k) \in \mathcal{R})$
- Guaranteed open loop frequency response gain and phase margins can be determined in close form.
- Locus of the LQR close loop poles as a function of varying $R \in (\infty, 0)$ can be easily plotted

LQR Return difference equality

Return difference for LQR



Open loop transfer function:

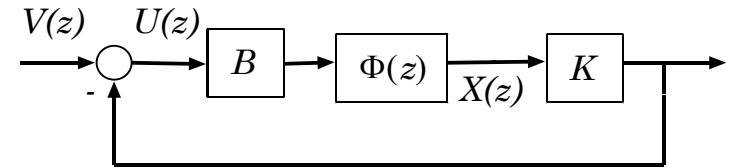
$$G_o(z) = K\Phi(z)B$$

Close loop sensitivity transfer function ($V(z)$ to $U(z)$)

$$S(z) = [I + K\Phi(z)B]^{-1} = [I + G_o(z)]^{-1}$$

$$S(z) = [\text{return difference}]^{-1}$$

Return difference for LQR



Open loop transfer function:

$$G_o(z) = K\Phi(z)B$$

$$\text{Return difference: } [I + K\Phi(z)B] = [I + G_o(z)]$$

Return difference for LQR

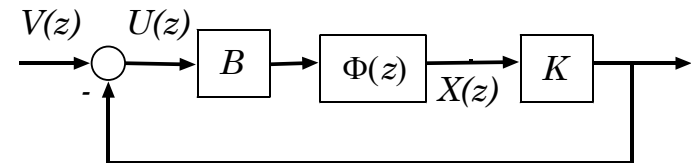
Close loop poles are the zeros of the return difference

Open loop poles are the poles of the return difference

$$\begin{aligned} \text{Det}[I + G_o(z)] &= \text{Det}[I + K\Phi(z)B] \\ &= \text{Det}[I + BK\Phi(z)] \\ &= \text{Det}[\Phi^{-1}(z) + BK]\text{Det}\Phi(z) \\ &= \text{Det}[zI - A + BK]\text{Det}[zI - A]^{-1} \end{aligned}$$

$$\text{Det}[I + G_o(z)] = \frac{\text{Det}[zI - A + BK]}{\text{Det}[zI - A]}$$

Output weighting in LQ cost



Open loop transfer function

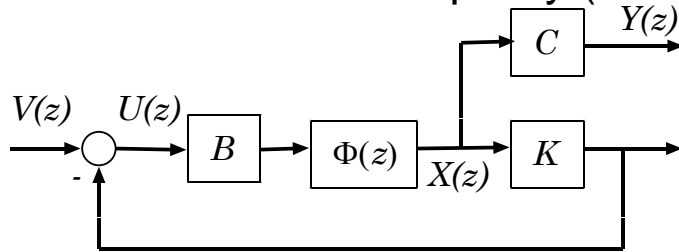
LQ cost:

$$G_o(z) = K\Phi(z)B \quad J = \frac{1}{2} \sum_{k=0}^{\infty} \{ \underline{y^2(k)} + Ru^2(k) \}$$

Open loop transfer function from $U(z)$ to $Y(z)$:

$$G(z) = C\Phi(z)B$$

LQ Return Difference Equality (RDE)



Return difference equality (see ME232 class notes):

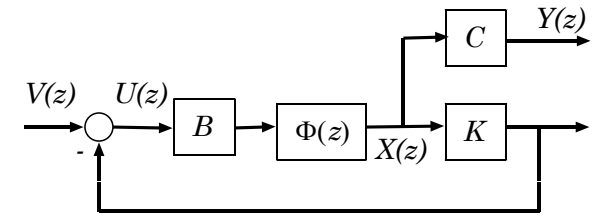
$$[I + G_o(z^{-1})]^T [R + B^T P B] [I + G_o(z)] = R + G^T(z^{-1}) G(z)$$

Open loop transfer function: TF from $U(z)$ to $Y(z)$:
 $G_o(z) = K \Phi(z) B$ $G(z) = C \Phi(z) B$

RDE for Single Input Systems

When:

$$u(k) \in \mathcal{R}$$



$$(1 + G_o(z^{-1}))(1 + G_o(z)) = \frac{R}{R + B^T P B} \left[1 + \frac{1}{R} G(z^{-1})^T G(z) \right]$$

Open loop transfer function: TF from $U(z)$ to $Y(z)$:
 $G_o(z) = K \Phi(z) B$ $G(z) = C \Phi(z) B$

Return Difference Frequency Response

$$(1 + G_o(z^{-1}))(1 + G_o(z)) = \frac{R}{R + B^T P B} \left[1 + \frac{1}{R} G(z^{-1})^T G(z) \right]$$

Set $z = e^{j\omega}$:

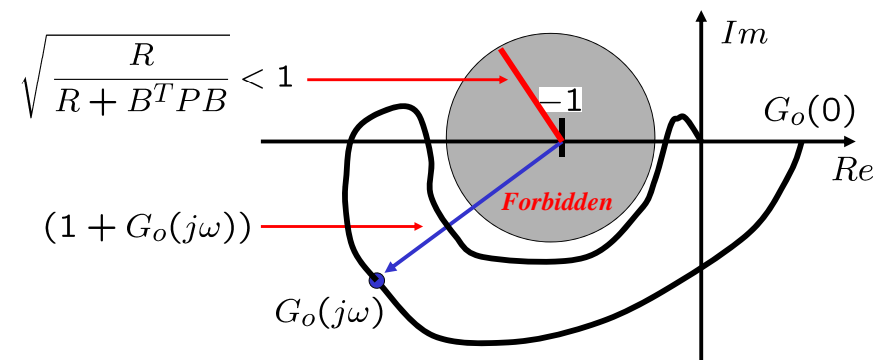
$$\underbrace{(1 + G_o(e^{-j\omega}))(1 + G_o(e^{j\omega}))}_{|(1 + G_o(e^{j\omega}))|^2} = \frac{R}{R + B^T P B} \underbrace{\left[1 + \frac{1}{R} G(e^{-j\omega})^T G(e^{j\omega}) \right]}_{|G(e^{j\omega})|^2} \geq 1$$

$$|(1 + G_o(e^{j\omega}))|^2 \geq \frac{R}{R + B^T P B}$$

Stability Margins of Single Input LQR

$$|(1 + G_o(e^{j\omega}))| \geq \sqrt{\frac{R}{R + B^T P B}}$$

Nyquist plot of $G_o(j\omega)$

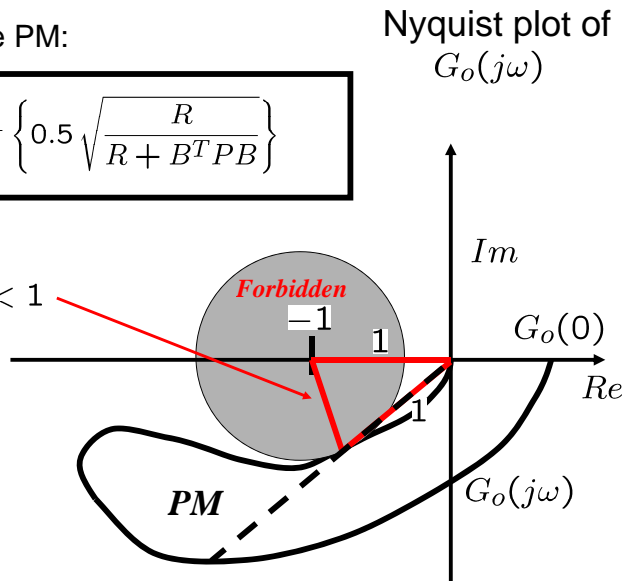


Phase Margin of Single Input LQR

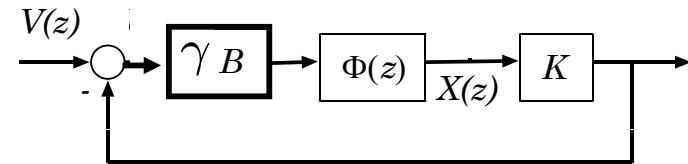
Worst possible PM:

$$PM \geq 2 \sin^{-1} \left\{ 0.5 \sqrt{\frac{R}{R + B^T P B}} \right\}$$

$$\sqrt{\frac{R}{R + B^T P B}} < 1$$



Loop Gain γ Margins

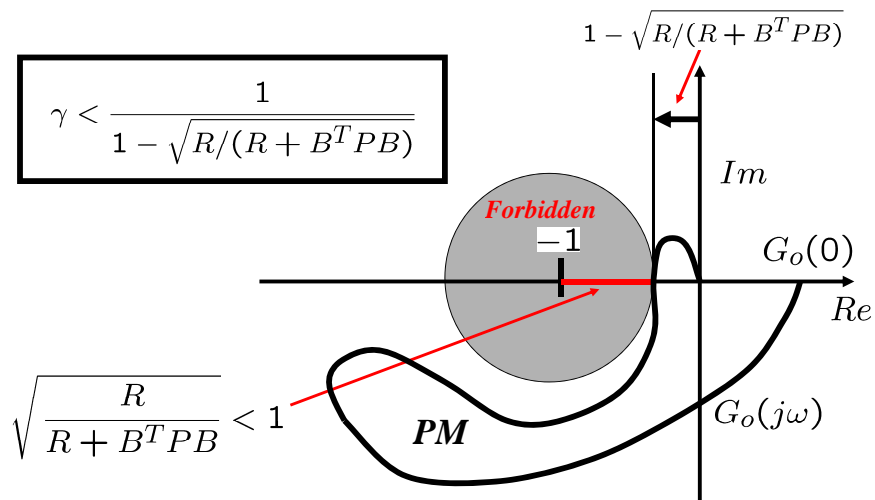


- Control system is designed for $\gamma = 1$
- How big (or small) can γ be before the system becomes unstable?

Gain Margin – one possibility

System is guaranteed to be asymptotically stable when

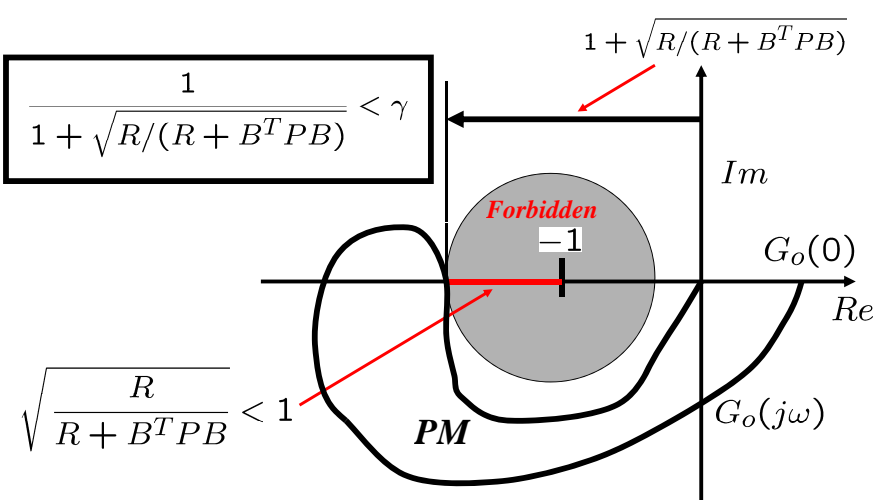
$$\gamma < \frac{1}{1 - \sqrt{R/(R + B^T P B)}}$$



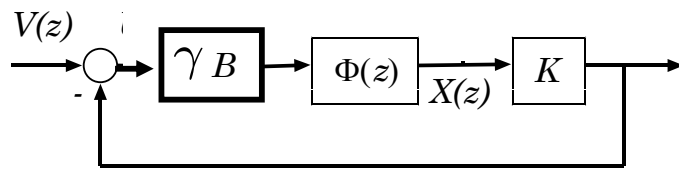
Gain Margin – another possibility

System is guaranteed to be asymptotically stable when

$$\frac{1}{1 + \sqrt{R/(R + B^T P B)}} < \gamma$$



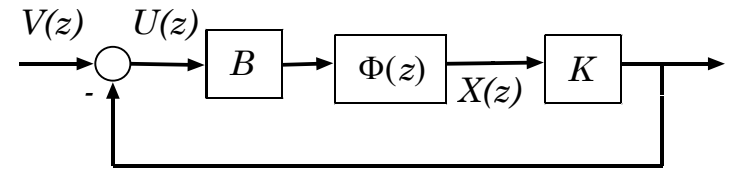
Loop Gain γ Margins



- Control system is designed for $\gamma = 1$
- System is **guaranteed** to remain asymptotically stable for

$$\frac{1}{1 + \sqrt{R/(R + B^T P B)}} < \gamma < \frac{1}{1 - \sqrt{R/(R + B^T P B)}}$$

Example – Double Integrator



For $R = 10$ we obtained $K = \begin{bmatrix} 0.21 & 0.65 \end{bmatrix}$

$$P = \begin{bmatrix} 3 & 3.16 \\ 3.16 & 8.1 \end{bmatrix}$$

Open loop transfer function:

$$G_o(z) = K\Phi(z)B = \frac{0.76z - 0.55}{(z - 1)^2}$$

Example – Double Integrator

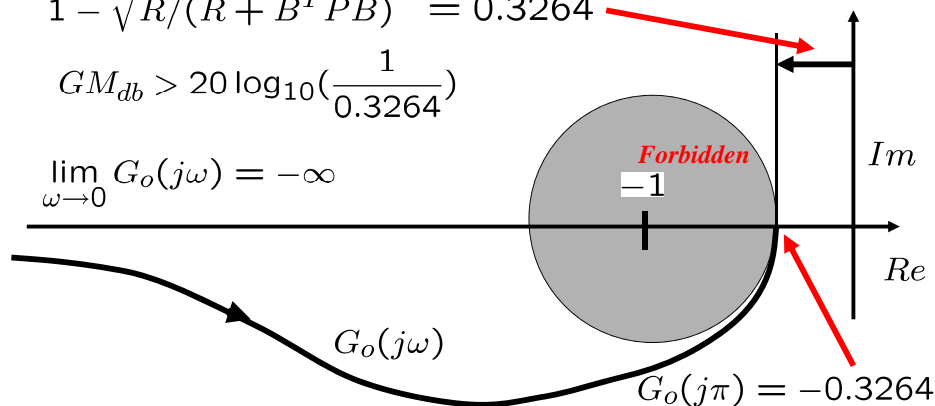
$$G_o(j\omega) = \frac{0.76 e^{j\omega} - 0.55}{(e^{j\omega} - 1)^2}$$

$$GM_{db} > 9.726 \text{ db}$$

$$1 - \sqrt{R/(R + B^T P B)} = 0.3264$$

$$GM_{db} > 20 \log_{10}\left(\frac{1}{0.3264}\right)$$

$$\lim_{\omega \rightarrow 0} G_o(j\omega) = -\infty$$



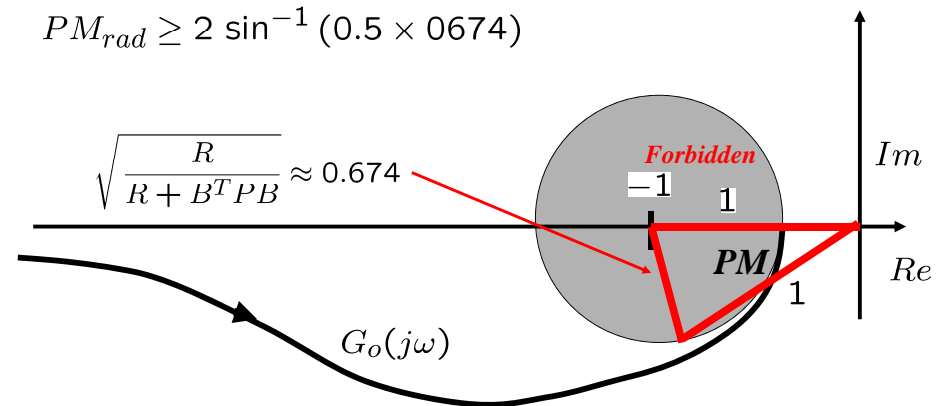
Example – Double Integrator

$$G_o(j\omega) = \frac{0.76 e^{j\omega} - 0.55}{(e^{j\omega} - 1)^2}$$

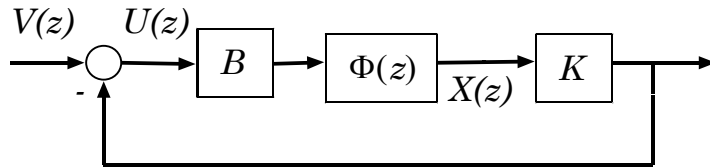
$$PM_{deg} > 39.3^\circ$$

$$PM_{rad} \geq 2 \sin^{-1}(0.5 \times 0.674)$$

$$\sqrt{\frac{R}{R + B^T P B}} \approx 0.674$$



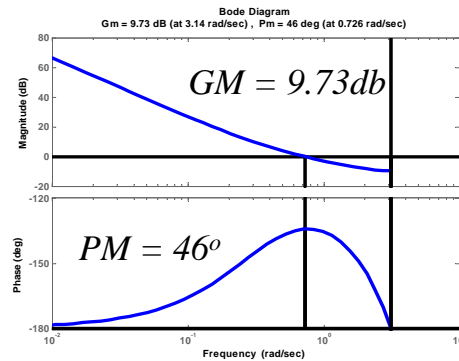
Example – Double Integrator



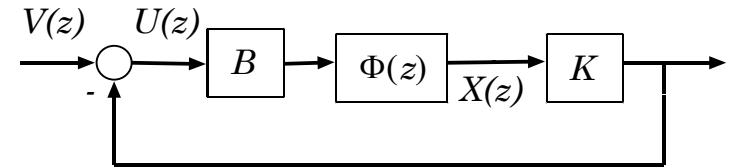
$$G_o(z) = \frac{0.76z - 0.55}{(z - 1)^2}$$

Open loop transfer function:

$$R = 10$$



Poles of an LQR

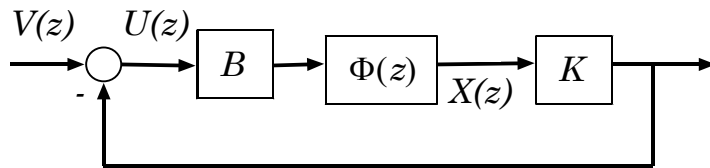


Close loop poles are the zeros of the return difference

Open loop poles are the poles of the return difference

$$\text{Det}[I + G_o(z)] = \frac{\text{Det}[zI - A + BK]}{\text{Det}[zI - A]}$$

Poles of an LQR

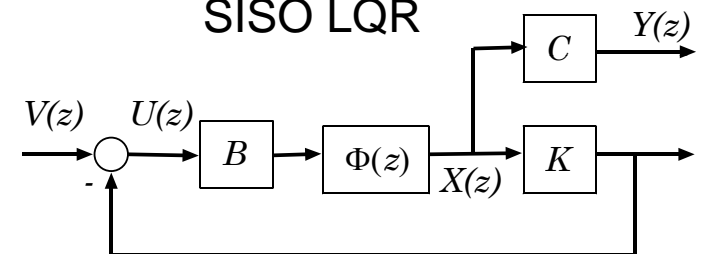


Open loop polynomial: $A(z) = \text{Det}[zI - A]$

Close loop polynomial: $A_c(z) = \text{Det}[zI - A + BK]$

$$\text{Det}[I + G_o(z)] = \frac{\text{Det}[zI - A + BK]}{\text{Det}[zI - A]}$$

SISO LQR



Open loop transfer function from $U(z)$ to $Y(z)$:

$$G(z) = C\Phi(z)B$$

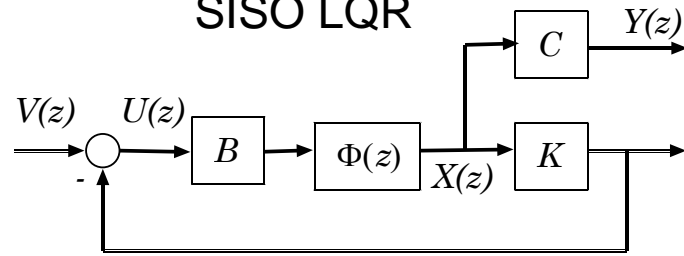
when

$$u(k) \in \mathcal{R}$$

$$y(k) \in \mathcal{R}$$

$$G(z) = \frac{\bar{B}(z)}{A(z)}$$

SISO LQR



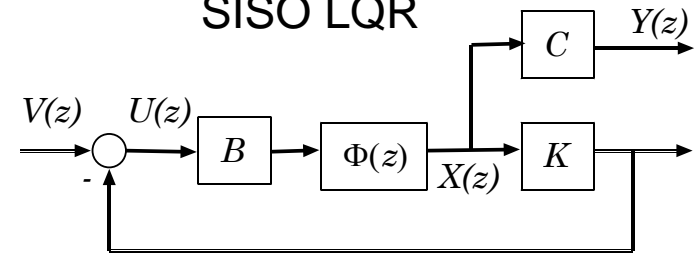
Open loop poles: $A(z) = 0$

Close loop poles: $A_c(z) = 0$

Open loop plant zeros: $\bar{B}(z) = 0$

$$\text{TF from } U \rightarrow Y \quad G(z) = C\Phi(z)B = \frac{\bar{B}(z)}{A(z)}$$

SISO LQR



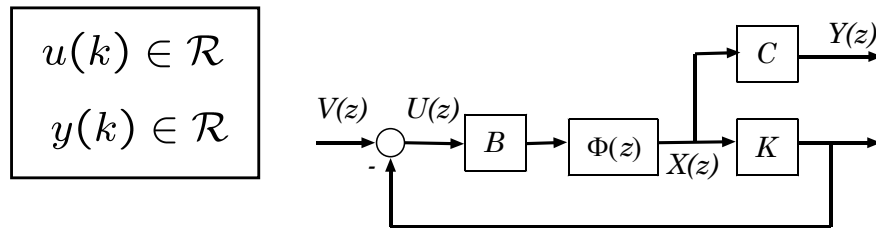
Open loop polynomial: $A(z) = z^n + a_1 z^{n-1} + \dots + a_0$

Close loop polynomial: $A_c(z) = z^n + a_{c1} z^{n-1} + \dots + a_{c0}$

Open loop plant zero polynomial: $\bar{B}(z) = \bar{b}_m(z^m + b_1 z^{m-1} + \dots + b_0)$

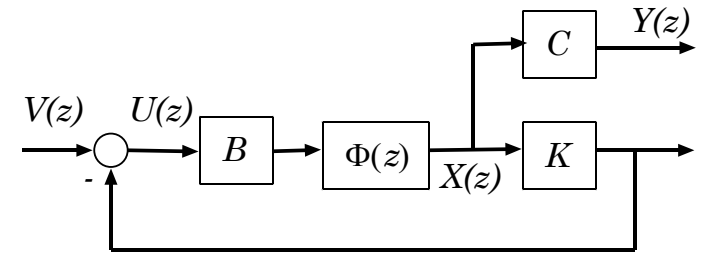
$$\text{TF from } U \rightarrow Y \quad G(z) = C\Phi(z)B = \frac{\bar{B}(z)}{A(z)}$$

SISO Return Difference Equality (RDE)



$$\underbrace{(1 + G_o(z^{-1}))}_{\frac{A_c(z^{-1})}{A(z^{-1})}} \underbrace{(1 + G_o(z))}_{\frac{A_c(z)}{A(z)}} = \underbrace{\frac{R}{R + B^T P B}}_{\gamma > 0 \text{ for } R \in (0, \infty)} \left[1 + \frac{1}{R} \underbrace{G(z^{-1})}_{\frac{\bar{B}(z^{-1})}{A(z^{-1})}} \underbrace{G(z)}_{\frac{\bar{B}(z)}{A(z)}} \right]$$

SISO Return Difference Equality (RDE)



$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = \gamma \left[1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} \right]$$

Basis for the Reciprocal root locus technique

RDE Left hand side:

$2n$ zeros of the transfer function:

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = 0$$

n close loop poles: $A_c(z) = (z - p_{c1}) \cdots (z - p_{cn})$

n zeros of: $A_c(z^{-1}) = (z - \frac{1}{p_{c1}}) \cdots (z - \frac{1}{p_{cn}}) \frac{a_{co}}{z^n}$

n reciprocals of close loop poles

$$a_{co} = (-1)^n p_{c1} p_{c1} \cdots p_{cn}$$

RDE Left hand side:

$2n$ zeros of the transfer function:

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = 0$$

n close loop poles: $p_{c1}, p_{c2}, \cdots p_{cn}$

n reciprocals of close loop poles: $\frac{1}{p_{c1}}, \frac{1}{p_{c2}}, \cdots \frac{1}{p_{cn}}$

$$|p_{ci}| < 1 \quad \left| \frac{1}{p_{ci}} \right| > 1 \quad R \in (0, \infty)$$

LQ Reciprocal Root Locus

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = \gamma \left[1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} \right]$$



$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\beta = \left(\frac{a_o}{a_{co}} \right) \frac{R}{R + B^T P B}$$

Is a constant, which does not affect the Reciprocal root locus

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$\left| \frac{1}{p_{ci}} \right| < 1$ inverses of close loop eigenvalues (**always unstable**)

$|p_{ci}| < 1$ closed loop eigenvalues (**always asymptotically stable**)

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

open loop eigenvalues

Inverses of open loop eigenvalues

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

n-m zeros at the origin

zeros of $\bar{B}(z)$

Inverses of zeros of $\bar{B}(z)$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\bar{B}(z) = \bar{b}_m (z^n + \dots + b_o)$$

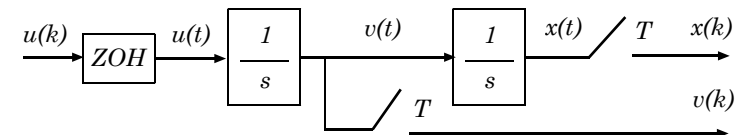
$$A(z) = z^n + \dots + a_o,$$

$$\frac{b_o}{a_o} > 0 \Rightarrow \text{negative feedback}$$

$$\frac{b_o}{a_o} < 0 \Rightarrow \text{positive feedback}$$

Example – Double Integrator

Double integrator with ZOH and sampling time $T=1$:

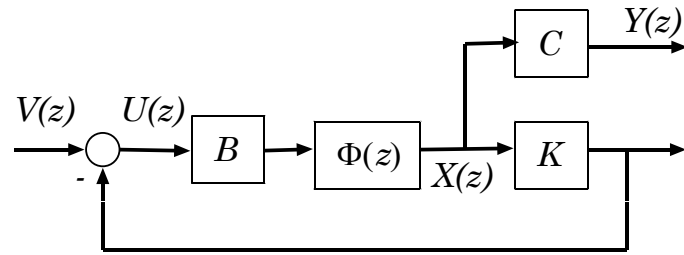


$$\begin{bmatrix} x_1(k+1) \\ x_2(k+1) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(k) \\ x_2(k) \end{bmatrix} + \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} u(k)$$

$$y(k) = \begin{bmatrix} 1 & 0 \end{bmatrix} x(k)$$

$$J = \frac{1}{2} \sum_{k=0}^{\infty} \{y^2(k) + R u^2(k)\} \quad R > 0$$

Example – Double Integrator



$$G(z) = C\Phi(z)B$$

$$G(z) = \frac{\bar{B}(z)}{A(z)} = \frac{\frac{1}{2}(z+1)}{(z-1)^2} = \frac{\frac{1}{2}(z+1)}{(z^2 - 2z + 1)}$$

$$\frac{b_o}{a_o} = \frac{1}{1}$$

Example – Double Integrator

$$\frac{\bar{B}(z)}{A(z)} = \frac{\frac{1}{2}(z+1)}{(z^2 - 2z + 1)} \quad \left\{ \begin{array}{l} \bar{b}_m = \frac{1}{2} \\ a_o = 1 \\ n = 2 \end{array} \right. \quad \begin{array}{l} b_o = 1 \\ m = 1 \end{array}$$

$$\left\{ \begin{array}{l} n - m = 1 \\ \frac{a_o}{b_o} = 1 \end{array} \right.$$

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

$$1 + \frac{(1/2)^2}{R} \left(\frac{1}{1} \right) \frac{z(z+1)(z+1)}{(z-1)(z-1)(z-1)(z-1)} = 0$$

Example – Double Integrator

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

$$1 + \frac{1}{R} \frac{\overbrace{\frac{1}{2}(z^{-1}+1)}^{\bar{B}(z^{-1})}}{\underbrace{(z^{-1}-1)^2}_{A(z^{-1})}} \frac{\overbrace{\frac{1}{2}(z+1)}^{\bar{B}(z)}}{\underbrace{(z-1)^2}_{A(z)}} = 0$$

Example – Double Integrator

$$1 + \frac{1}{R} \frac{\frac{1}{2}(z^{-1}+1)}{(z^{-1}-1)^2} \frac{\frac{1}{2}(z+1)}{(z-1)^2} = 0$$

$$1 + \frac{1}{R} \frac{\frac{1}{4}z^{-1}(z+1)}{(z^{-1}-1)^2} \frac{(z+1)}{(z-1)^2} = 0$$

$$1 + \frac{1}{R} \frac{\frac{1}{4}z^{-1}(z+1)}{z^{-2}(z-1)^2} \frac{(z+1)}{(z-1)^2} = 0$$

Example – Double Integrator

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

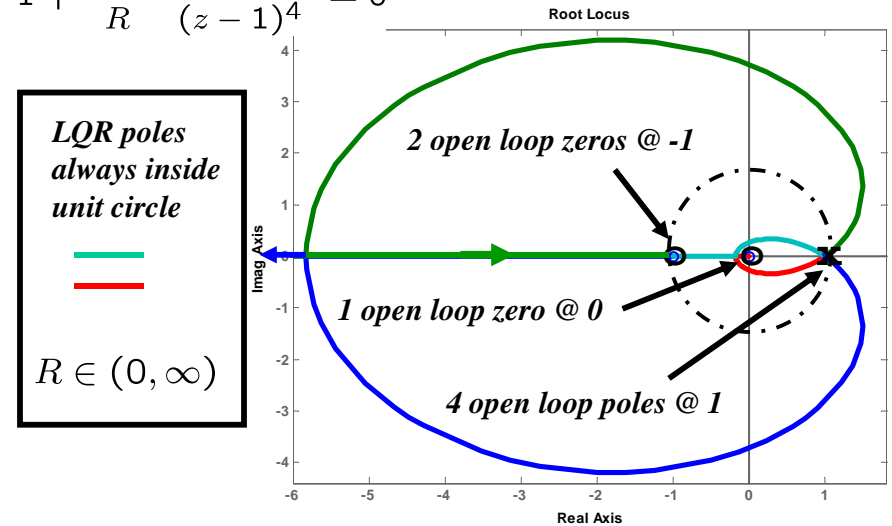
1 open loop zero @ 0 2 open loop zeros @ -1

$$1 + \frac{0.25}{R} \frac{z(z+1)^2}{(z-1)^4} = 0$$

4 open loop poles @ 1

Example – Double Integrator

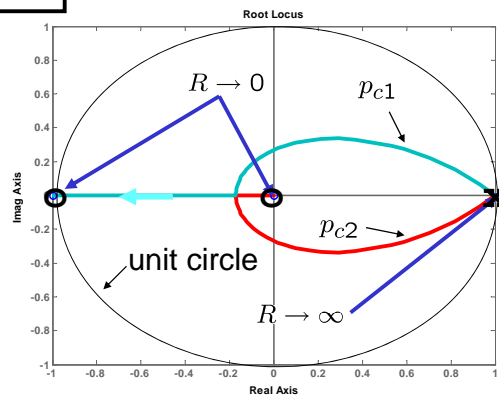
$$1 + \frac{0.25}{R} \frac{z(z+1)^2}{(z-1)^4} = 0$$



LQR Close Loop poles

$$1 + \frac{0.25}{R} \frac{z(z+1)^2}{(z-1)^4} = 0 \quad R \rightarrow \infty \Rightarrow \begin{cases} p_{c1} \rightarrow 1 \\ p_{c2} \rightarrow 1 \end{cases}$$

$$R \rightarrow 0 \Rightarrow \begin{cases} p_{c1} \rightarrow -1 \\ p_{c2} \rightarrow 0 \end{cases}$$

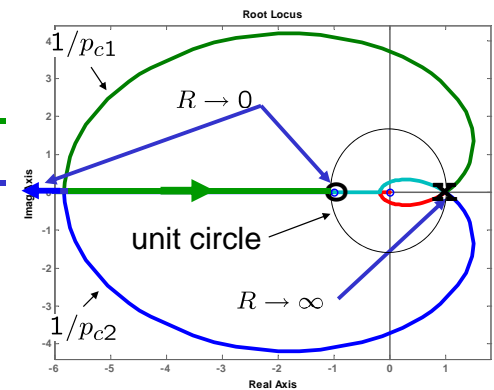


LQR Close Loop poles reciprocals

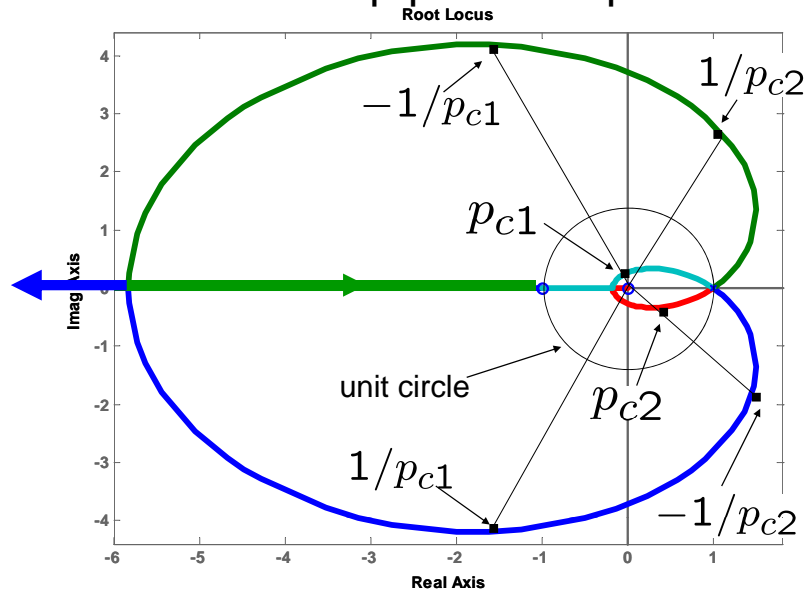
$$1 + \frac{0.25}{R} \frac{z(z+1)^2}{(z-1)^4} = 0 \quad R \rightarrow \infty \Rightarrow \begin{cases} 1/p_{c1} \rightarrow 1 \\ 1/p_{c2} \rightarrow 1 \end{cases}$$

$$R \rightarrow 0 \Rightarrow \begin{cases} 1/p_{c1} \rightarrow -1 \\ 1/p_{c2} \rightarrow -\infty \end{cases}$$

always unstable



LQR Close Loop poles reciprocals



Summary

- Convergence of LQR as horizon $N \rightarrow \infty$
 - $[A \ B]$ stabilizable
 - $[A \ C]$ detectable
- Infinite horizon LQR
- Solution of algebraic Riccati equation
- Close loop system is asymptotically stable
- Return difference equality
 - Guaranteed gain and phase margins of LQR
 - Reciprocal root locus (LQR close loop poles)

Additional Material

- More details on plotting the LQR Reciprocal root locus
- LQR Reciprocal Root Locus with open loop eigenvalues and zeros at the origin

Roots and their reciprocals

Consider the polynomial:

$$A(z) = z^n + a_1 z^{n-1} + \dots + a_0$$

$$= (z - p_1)(z - p_2) \cdots (z - p_n)$$

$$A(z) = z^n - \left(\sum_{i=1}^n p_i \right) z^{n-1} + \dots + (-1)^n \prod_{i=1}^n p_i$$

$$a_o = (-1)^n \prod_{i=1}^n p_i$$

Roots and their reciprocals

Consider now the transfer function:

$$\begin{aligned}
 A(z) &= z^{-n} + a_1 z^{-(n-1)} + \dots + a_0 \\
 &= (z^{-1} - p_1)(z^{-1} - p_2) \dots (z^{-1} - p_n) \\
 &= \frac{a_0}{z^n} \left(z - \frac{1}{p_1}\right) \left(z - \frac{1}{p_2}\right) \dots \left(z - \frac{1}{p_n}\right) \\
 a_0 &= (-1)^n \prod_{i=1}^n p_i
 \end{aligned}$$

Zeros of $A(z^{-1})$ are reciprocals of roots of $A(z)$

RDE Left hand side:

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = 0$$

$$\begin{aligned}
 \frac{A_c(z)}{A(z)} &= \frac{z^n + a_{cn-1}z^{n-1} + \dots + a_{co}}{z^n + a_{n-1}z^{n-1} + \dots + a_o} \\
 &= \frac{(z - p_{c1})(z - p_{c2}) \dots (z - p_{cn})}{(z - p_{o1})(z - p_{o2}) \dots (z - p_{on})}
 \end{aligned}$$

RDE Right hand side:

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = 0$$

$$\begin{aligned}
 \frac{A_c(z^{-1})}{A(z^{-1})} &= \frac{z^{-n} + a_{cn-1}z^{-n+1} + \dots + a_c}{z^{-n} + a_{n-1}z^{-n+1} + \dots + a_o} \\
 &= \frac{a_{co} z^{-n} (z - \frac{1}{p_{c1}}) (z - \frac{1}{p_{c2}}) \dots (z - \frac{1}{p_{cn}})}{a_o z^{-n} (z - \frac{1}{p_{o1}}) (z - \frac{1}{p_{o2}}) \dots (z - \frac{1}{p_{on}})}
 \end{aligned}$$

RDE Right hand side:

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

$$\begin{aligned}
 \frac{\bar{B}(z)}{A(z)} &= \frac{\bar{b}_m z^m + \bar{b}_{m-1} z^{m-1} + \dots + \bar{b}_o}{z^n + a_{n-1} z^{n-1} + \dots + a_o} \\
 &= \frac{\bar{b}_m (z - z_{o1})(z - z_{o2}) \dots (z - z_{om})}{(z - p_{o1})(z - p_{o2}) \dots (z - p_{on})}
 \end{aligned}$$

RDE Right hand side:

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

$$\frac{\bar{B}(z^{-1})}{A(z^{-1})} = \frac{\bar{b}_m z^{-m} + \bar{b}_{m-1} z^{-m+1} + \dots + \bar{b}_0}{z^{-n} + a_{n-1} z^{-n+1} + \dots + a_0}$$

$$= \frac{\bar{b}_m b_0 z^{-m} (z - \frac{1}{z_{o1}}) (z - \frac{1}{z_{o2}}) \cdot (z - \frac{1}{z_{om}})}{a_0 z^{-n} (z - \frac{1}{p_{o1}}) (z - \frac{1}{p_{o2}}) \cdot (z - \frac{1}{p_{on}})}$$

RDE Right hand side:

$$1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} = 0$$

$$1 + \frac{\bar{b}_m^2 b_0}{R a_0} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = 0$$

LQ Reciprocal Root Locus

$$\frac{A_c(z^{-1})A_c(z)}{A(z^{-1})A(z)} = \gamma \left[1 + \frac{1}{R} \frac{\bar{B}(z^{-1})\bar{B}(z)}{A(z^{-1})A(z)} \right]$$



$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_0 \bar{b}_m^2}{a_0 R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\beta = \left(\frac{a_0}{a_{co}} \right) \frac{R}{R + B^T P B}$$

Is a constant, which does not affect the Reciprocal root locus

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_0 \bar{b}_m^2}{a_0 R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$\left| \frac{1}{p_{ci}} \right| < 1$ inverses of close loop eigenvalues (**always unstable**)

$|p_{ci}| < 1$ closed loop eigenvalues (**always asymptotically stable**)

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

open loop eigenvalues

Inverses of open loop eigenvalues

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

n-m zeros at the origin

zeros of $\bar{B}(z)$

Inverses of zeros of $\bar{B}(z)$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\bar{B}(z) = \bar{b}_m (z^n + \dots + b_o)$$

$$A(z) = z^n + \dots + a_o,$$

$$\frac{b_o}{a_o} > 0 \Rightarrow \text{negative feedback}$$

$$\frac{b_o}{a_o} < 0 \Rightarrow \text{positive feedback}$$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} \frac{z^{n-m} \prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$R \rightarrow \infty \Rightarrow p_{ci} \rightarrow \text{Stable} \begin{cases} p_{oi} \\ \text{or} \\ 1/p_{oi} \end{cases}$$

$$R \rightarrow \infty \Rightarrow 1/p_{ci} \rightarrow \text{Unstable} \begin{cases} p_{oi} \\ \text{or} \\ 1/p_{oi} \end{cases}$$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$R \rightarrow 0 \Rightarrow p_{ci} \rightarrow \text{Stable} \begin{cases} z_{oi} & \boxed{i = 1, \dots, m} \\ \text{or} \\ 1/z_{oi} \end{cases}$$

$$R \rightarrow 0 \Rightarrow p_{ci} \rightarrow 0 \quad \boxed{i = m + 1, \dots, n}$$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$R \rightarrow 0 \Rightarrow 1/p_{ci} \rightarrow \text{Unstable} \begin{cases} z_{oi} & \boxed{i = 1, \dots, m} \\ \text{or} \\ 1/z_{oi} \end{cases}$$

$$R \rightarrow 0 \Rightarrow |1/p_{ci}| \rightarrow \infty \quad \boxed{i = m + 1, \dots, n}$$

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\bar{B}(z) = \bar{b}_m (z^n + \dots + b_o) \quad A(z) = z^n + \dots + a_o,$$

$$R \rightarrow 0 \Rightarrow |1/p_{ci}| \rightarrow \infty \quad \boxed{\frac{b_o}{a_o} > 0}$$

$$\frac{(2q+1)\pi}{n-m} \quad q = 0, 1, \dots, (n-m) - 1$$

(negative feedback RL rules)

LQ Reciprocal Root Locus

$$\frac{\prod_{i=1}^n (z - p_{ci}) \prod_{i=1}^n (z - \frac{1}{p_{ci}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} = \beta \left[1 + \frac{b_o \bar{b}_m^2}{a_o R} z^{n-m} \frac{\prod_{i=1}^m (z - z_{oi}) \prod_{i=1}^m (z - \frac{1}{z_{oi}})}{\prod_{i=1}^n (z - p_{oi}) \prod_{i=1}^n (z - \frac{1}{p_{oi}})} \right]$$

$$\bar{B}(z) = \bar{b}_m (z^n + \dots + b_o) \quad A(z) = z^n + \dots + a_o,$$

$$R \rightarrow 0 \Rightarrow |1/p_{ci}| \rightarrow \infty \quad \boxed{\frac{b_o}{a_o} < 0}$$

$$\frac{(2q)\pi}{n-m} \quad q = 0, 1, \dots, (n-m) - 1$$

(positive feedback RL rules)

LQR Reciprocal Root Locus with open loop eigenvalues and zeros at the origin

Consider a nth order LTI system:

$$x(k+1) = Ax(k) + Bu(k) \quad x(0) = x_o$$

Under the optimal control which minimizes

$$J = \frac{1}{2} \sum_{k=0}^{\infty} \{y^T(k)y(k) + u^T(k)Ru(k)\}$$

$$y(k) = Cx(k)$$

Assume that

$\det(A) = 0$

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Notice that optimal control law is given by:

$$u(k) = -Kx(k)$$

where:

$$K = [R + B^T P B]^{-1} B^T P A$$

$$= K' A$$

As a consequence, the close loop matrix A_c will also be singular:

$$A_c = A - BK = (I - BK') A$$

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Therefore if,

$$A(z) = \det(zI - A) = z^r A'(z)$$

then:

$$A'(z) = z^{n-r} + \dots + a'_o, \quad a'_o \neq 0$$

$$A_c(z) = \det(zI - A + BK) = z^{r_c} A'_c(z)$$

$$A'_c(z) = z^{n-r_c} + \dots + a'_{co},$$

$$r_c \geq 1$$

This implies that at least one open loop eigenvalue at the origin is invariant under LQR control.

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Lets also assume that there can be zeros at the origin. Thus,

$$\bar{B}(z) = z^p \bar{B}'(z)$$

$$\bar{B}'(z) = \bar{b}_m (z^{m-p} + \dots + b_o),$$

$$= \bar{b}_m \prod_{i=1}^{m-p} (z - z_{oi})$$

$$b_o = \prod_{i=1}^{m-p} z_{oi} \neq 0$$

Reciprocal Root Locus with open loop eigenvalues and zeros at the origin

To determine r_c and to plot the remaining $n-r_c$ close loop eigenvalues, we utilize:

$$A_c(z^{-1}) A_c(z) = \gamma \left[A(z^{-1}) A(z) + \frac{1}{R} \bar{B}(z^{-1}) \bar{B}(z) \right]$$

where:

$$A(z) = z^{-r} A'(z), \quad A'(z) = \prod_{i=1}^{n-r} (z - p_{oi}), \quad a_o = \prod_{i=1}^{n-r} (-p_{oi})$$

$$A_c(z) = z^{-r_c} A'_c(z), \quad A'_c(z) = \prod_{i=1}^{n-r_c} (z - p_{ci}), \quad a_{co} = \prod_{i=1}^{n-r_c} (-p_{ci})$$

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Thus, from

$$A_c(z^{-1}) A_c(z) = \gamma \left[A(z^{-1}) A(z) + \frac{1}{R} \bar{B}(z^{-1}) \bar{B}(z) \right]$$

we obtain

$$z^{-(n-r_c)} \prod_{i=1}^{n-r_c} (z - p_{ci}) \left(z - \frac{1}{p_{ci}} \right) = \beta \left[z^{-(n-r)} \prod_{i=1}^{n-r} (z - p_{oi}) \left(z - \frac{1}{p_{oi}} \right) + \frac{\bar{b}_m^2 b_o}{R a_o} z^{-(m-p)} \prod_{i=1}^{m-p} (z - z_{oi}) \left(z - \frac{1}{z_{oi}} \right) \right]$$

where

$$r_c = n - \max [(n - r), (m - p)]$$

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Case 1: $(n - r) \geq (m - p) \Rightarrow r_c = r$

There are r close loop eigenvalues at the origin and

The remaining $n-r$ close loop eigenvalues are plotted using:

$$\frac{\prod_{i=1}^{n-r} (z - p_{ci}) \left(z - \frac{1}{p_{ci}} \right)}{\prod_{i=1}^{n-r} (z - p_{oi}) \left(z - \frac{1}{p_{oi}} \right)} =$$

$$\beta \left[1 + \frac{\bar{b}_m^2 b_o}{R a_o} \frac{z^{[(n-r)-(m-p)]} \prod_{i=1}^{m-p} (z - z_{oi}) \left(z - \frac{1}{z_{oi}} \right)}{\prod_{i=1}^{n-r} (z - p_{oi}) \left(z - \frac{1}{p_{oi}} \right)} \right]$$

$$\beta = \left(\frac{a_o}{a_{co}} \right) \frac{R}{R + B^T P B}$$

LQR Reciprocal Root Locus with open loop eigenvalues and zeros at the origin

Case 2: $(m - p) > (n - r) \Rightarrow r_c = n - (m - p)$

There are $r_c < r$ close loop eigenvalues at the origin and

the remaining $m - p$ close loop eigenvalues are plotted using:

$$\frac{\prod_{i=1}^{m-p} (z - p_{ci}) \left(z - \frac{1}{p_{ci}} \right)}{\prod_{i=1}^{m-p} (z - z_{oi}) \left(z - \frac{1}{z_{oi}} \right)} =$$

$$\alpha \left[1 + \frac{R a_o}{\bar{b}_m^2 b_o} \frac{z^{[(m-p)-(n-r)]} \prod_{i=1}^{n-r} (z - p_{oi}) \left(z - \frac{1}{p_{oi}} \right)}{\prod_{i=1}^{m-p} (z - z_{oi}) \left(z - \frac{1}{z_{oi}} \right)} \right]$$

$$\alpha = \left(\frac{b_o \bar{b}_m^2}{a_{co} R} \right) \frac{R}{R + B^T P B}$$

Notice that R is in the numerator and the zeros are in the denominator