

UNIVERSITY OF CALIFORNIA AT BERKELEY
 Department of Mechanical Engineering
 ME233 Advanced Control Systems II
 Spring 2012

Homework #8

Assigned: Apr. 12 (Th)
 Due: Apr. 19 (Th)

1. A discrete-time plant is given by

$$A(q^{-1})y(k) = q^{-d} B(q^{-1}) \{u(k) + d(k)\} \quad (1)$$

where $A(q^{-1}) = (1 - 0.8q^{-1})(1 - 0.7q^{-1})$, $d = 1$ and $B(q^{-1}) = 0.1$. Here, $u(k)$ is the control input, $y(k)$ is the output, and $d(k)$ represent the disturbance. The disturbance is known to be periodic and the period is $N = 8$ (i.e. $d(k + 8) = d(k)$).

- (a) Use the fact that $A_d(q^{-1})d(k) = 0$, where $A_d(q^{-1}) = 1 - q^{-8}$ and design the regulator of the form

$$u(k) = -\frac{S(q^{-1})}{A_d(q^{-1})R'(q^{-1})}y(k)$$

which drives $y(k)$ to zero in finite time. (i.e. the closed-loop polynomial should be $A_c(q^{-1}) = 1$. Find the polynomials $R'(q^{-1})$ and $S(q^{-1})$ as the solution of the Diophantine equation

$$A_c(q^{-1}) = A_d(q^{-1})A(q^{-1})R'(q^{-1}) + q^{-d}B(q^{-1})S(q^{-1}).$$

- (b) Simulate the control system designed above when the periodic disturbance is given by

$$(d(0), d(1), \dots, d(7)) = (0, 1.5, 3, 0, -2, -2, 0, 0.5)$$

and $d(k + 8) = d(k)$. Assume that the plant initial condition is zero.

- (c) Now consider a repetitive controller of the form

$$u(k) = -\frac{k_r q^{-(N-d)} A(q^{-1})}{A_d(q^{-1}) B(q^{-1})} y(k).$$

Simulate this repetitive controller under the same conditions described in problem 1b. Try values of 0.5, 1 and 1.3 for k_r .

- (d) Assume now that the plant model form is still described by (1), but the plant dynamics are now given by

$$\begin{aligned} A(q^{-1}) &= (1 - 0.2q^{-1})\bar{A}(q^{-1}) \\ \bar{A}(q^{-1}) &= (1 - 0.8q^{-1})(1 - 0.7q^{-1}) \\ B(q^{-1}) &= 0.08 \\ d &= 2. \end{aligned}$$

Moreover, we use the repetitive controller from the previous part, which is given by

$$u(k) = -\frac{k_r q^{-(N-1)} \bar{A}(q^{-1})}{0.1 A_d(q^{-1})} y(k).$$

In other words, the real plant is

$$G_A(q) = \frac{0.1q^{-1}}{(1 - 0.8q^{-1})(1 - 0.7q^{-1})} \frac{0.8q^{-1}}{(1 - 0.2q^{-1})}$$

but we use the simplified plant

$$G(q) = \frac{0.1q^{-1}}{(1 - 0.8q^{-1})(1 - 0.7q^{-1})}$$

in the control system design process.

Show, using the root locus technique, that the resulting repetitive control system is unstable for any positive k_r .

- (e) Assume again that the plant model form is still described by (1), but the plant dynamics are now given by

$$\begin{aligned} A(q^{-1}) &= (1 - 0.2q^{-1}) \bar{A}(q^{-1}) \\ \bar{A}(q^{-1}) &= (1 - 0.8q^{-1})(1 - 0.7q^{-1}) \\ B(q^{-1}) &= 0.08 \\ d &= 2. \end{aligned}$$

(These are the same dynamics considered in the previous part.) However, we now incorporate the Q-filter modification to the repetitive compensator, in order to make the repetitive controller more robust. Thus,

$$u(k) = -\frac{k_r q^{-(N-1)} \bar{A}(q^{-1})}{0.1 (1 - Q(q, q^{-1})q^{-N})} y(k).$$

where

$$Q(q, q^{-1}) = \frac{q + 2 + q^{-1}}{4}.$$

Do the following:

- i. Plot the root locus of the closed-loop poles of the resulting repetitive control system for $k_r \geq 0$ and determine, a value of k_r for which the resulting repetitive control system is asymptotically stable.
- ii. Simulate this repetitive controller under the same conditions described in problem 1b.

2. Consider the following stationary stochastic system

$$\begin{aligned} \begin{bmatrix} x_1(k+1) \\ x_2(k+1) \end{bmatrix} &= \begin{bmatrix} 0.8 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1(k) \\ x_2(k) \end{bmatrix} + \begin{bmatrix} 1 \\ -2 \end{bmatrix} u(k) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} w(k) \\ y(k) &= x_1(k) + v(k) \end{aligned} \quad (2)$$

where $u(k)$ is a deterministic (known) input, $y(k)$ is the measured output, $w(k)$ and $v(k)$ are zero-mean, jointly Gaussian WSS random sequences with

$$E \left\{ \begin{bmatrix} w(k+j) \\ v(k+j) \end{bmatrix} \begin{bmatrix} w(k) & v(k) \end{bmatrix} \right\} = \begin{bmatrix} 0.225 & 0 \\ 0 & 0.625 \end{bmatrix} \delta(j)$$

Design a minimum variance regulator for this system.

3. In this problem we conduct a minimum variance, model reference stochastic control design exercise. Consider the following ARMAX system

$$A(q^{-1})y(k) = q^{-d} B(q^{-1})u(k) + C(q^{-1})\epsilon(k) \quad (3)$$

where

$$\begin{aligned} A(q^{-1}) &= 1 + a_1 q^{-1} + \cdots + a_n q^{-n} \\ C(q^{-1}) &= 1 + c_1 q^{-1} + \cdots + c_L q^{-L} \\ B(q^{-1}) &= b_o + b_1 q^{-1} + \cdots + b_m q^{-m} \end{aligned}$$

and $\epsilon(k)$ is the steady state Kalman filter residual, which satisfies

$$\begin{aligned} E\{\epsilon(k)\} &= 0, & E\{\epsilon(k+j)\epsilon(k)\} &= \sigma\delta(j), \\ E\{\epsilon(k+j)y(k)\} &= 0, & \forall j > 0. \end{aligned}$$

Assume that $B(q^{-1})$ and $C(q^{-1})$ are anti-Schur polynomials (i.e. the roots of the polynomials $q^m B(q^{-1})$ and $q^L C(q^{-1})$ are all strictly inside the unit circle). Define the model reference

$$A_m(q^{-1})y_m(k) = q^{-d} B_m(q^{-1})r_m(k) \quad (4)$$

where $A_m(q^{-1})$ is an anti-Schur polynomial of the form

$$A_m(q^{-1}) = 1 + a_{m1}q^{-1} + \cdots + a_{mt}q^{-t} \quad (5)$$

$y_m(k)$ is the reference model output, and $r_m(k)$ is the deterministic reference model input. The goal is to obtain the optimal control $u^o(k)$ that minimizes the cost

$$J = E \left\{ \left[A_m(q^{-1}) (y(k) - y_m(k)) \right]^2 \right\}. \quad (6)$$

Show that $u^o(k)$ satisfies

$$\beta(q^{-1})u^o(k) = C(q^{-1})B_m(q^{-1})r_m(k) - S(q^{-1})y(k) \quad (7)$$

where

$$\begin{aligned} C(q^{-1}) A_m(q^{-1}) &= A(q^{-1}) R(q^{-1}) + q^{-d} S(q^{-1}) \\ R(q^{-1}) &= 1 + r_1 q^{-1} + \cdots + r_{d-1} q^{-d+1} \\ \beta(q^{-1}) &= B(q^{-1}) R(q^{-1}) \\ S(q^{-1}) &= s_o + s_1 q^{-1} + \cdots + s_p q^{-p} \end{aligned} \quad p = \max(L + t - d, n - 1).$$