1.a)
$$x(k+1) = Ax(k) + Bu(k) + B_w w(k)$$

$$w(k) = C_w x_w(k), x_w(k+1) = A_w x_w(k) + B_n \eta(k)$$

$$E[x(0)] = x_o, E[x(0) - x_o)(x(0) - x_o)^T] = X_o$$

$$E[x_w(0)] = x_o, E[x(w(0) - x_w(0) - x_w(0) - x_w)^T] = X_w$$

$$E[x_w(0)] = 0, E[\eta(k)\eta(k+l)^T] = \Gamma \delta(l)$$

$$J = \frac{1}{2}E\left[x^T(N)Sx(N) + \sum_{k=0}^{N-1} [x^T(k)Qx(k) + u^T(k)Ru(k)]\right]$$
If $x(k)$ and $x_w(k)$ are both measurable for all k , let extended state $x_e(k) = \begin{bmatrix} x(k) \\ x_w(k) \end{bmatrix}$

$$J = \frac{1}{2}E\left[\begin{bmatrix} x(N) \\ x_w(N) \end{bmatrix}^T \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(N) \\ x_w(N) \end{bmatrix} + \sum_{k=0}^{N-1} [x(k) \\ 0 & M_w \end{bmatrix}^T \begin{bmatrix} Q & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(k) \\ x_w(k) \end{bmatrix} + u^T(k)Ru(k) \end{bmatrix}$$

$$x_e(k+1) = \begin{bmatrix} x(k+1) \\ x_w(k+1) \end{bmatrix} = \begin{bmatrix} A & B_w C_w \\ 0 & A_w \end{bmatrix} \begin{bmatrix} x(k) \\ x_w(k) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(k) + \begin{bmatrix} 0 \\ B_n \end{bmatrix} \eta(k)$$
Optimal control solution is as in deterministic LQR, $u^o(k) = -K(k+1)x_e(k) = -K(k+1) \begin{bmatrix} x(k) \\ x_w(k) \end{bmatrix}$

$$K(k+1) = \begin{pmatrix} R + \begin{bmatrix} B \\ 0 \end{bmatrix}^T P(k+1) \begin{bmatrix} B \\ 0 \end{bmatrix}^{-1} \begin{bmatrix} B \\ 0 \end{bmatrix}^T P(k+1) \begin{bmatrix} A & B_w C_w \\ 0 & A_w \end{bmatrix}$$

$$P(k-1) = \begin{bmatrix} Q & 0 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} A & B_w C_w \\ A_w \end{bmatrix}^T P(k) \begin{bmatrix} A & B_w C_w \\ 0 & A_w \end{bmatrix} - \begin{bmatrix} A & B_w C_w \\ 0 & A_w \end{bmatrix}^T P(k) \begin{bmatrix} B \\ 0 \end{bmatrix} K(k)$$

$$P(N) = \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix}, \text{ and assuming initial values } x(0) \text{ and } x_w(0) \text{ are uncorrelated, the optimal cost is:}$$

$$J^o = \frac{1}{2} \begin{bmatrix} x_o \\ x_w \end{bmatrix}^T P(0) \begin{bmatrix} x_o \\ x_w \end{bmatrix} + \frac{1}{2} \operatorname{trace} \left(P(0) \begin{bmatrix} X_o & 0 \\ 0 & X_{xw} \end{bmatrix} + b(0)$$

$$b(k) = b(k+1) + \operatorname{trace} \left(\begin{bmatrix} 0 \\ B_n \end{bmatrix}^T P(k+1) \begin{bmatrix} 0 \\ B_n \end{bmatrix} \Gamma \right), b(N) = 0$$
1.b)
$$y(k) = Cx(k) + v(k), E[v(k)] = 0, E[v(k)v(k+l)^T] = V \delta(l)$$

$$v(k) \text{ independent from } x(0), x_w(0), \text{ and } \eta(k)$$

$$y(k) = \begin{bmatrix} C & 0 \\ x_w(k) \end{bmatrix} + v(k)$$
Construct Kalman filter observer $\hat{x}_e(k) = \begin{bmatrix} \hat{x}(k) \\ \hat{x}_w(k) \end{bmatrix} = \hat{x}_e^o(k) + F(k) \hat{y}^o(k)$

$$\hat{x}_e^o(k) = 0 \begin{pmatrix} x(k) \\ x_w(k) \end{pmatrix} = \begin{bmatrix} A & B_w C_w \\ x_w(k) \end{bmatrix} \hat{x}_e(k) + \begin{bmatrix} B \\ 0 \end{bmatrix} u(k)$$

$$\hat{y}^o(k) = y(k) - (C & 0) \hat{x}^o(k) = 0$$

$$A_w \end{bmatrix} \hat{x}_e(k) + \begin{bmatrix} B \\ 0 \end{bmatrix} u(k)$$

$$\begin{split} E(k) &= \begin{bmatrix} C & 0 \end{bmatrix} M(k) \begin{bmatrix} C & 0 \end{bmatrix}^T + V \\ F(k) &= M(k) \end{bmatrix} C & 0 \end{bmatrix}^T E(k)^{-1} \\ Z(k) &= M(k) - F(k) \begin{bmatrix} C & 0 \end{bmatrix} M(k) \\ M(k+1) &= \begin{bmatrix} A & B_k C_w \\ 0 & A_w \end{bmatrix}^T Z(k) \begin{bmatrix} A & B_k C_w \\ 0 & A_w \end{bmatrix}^T + \begin{bmatrix} 0 \\ B_n \end{bmatrix} \Gamma \begin{bmatrix} 0 \\ B_n \end{bmatrix}^T \\ M(0) &= \begin{bmatrix} X_o & 0 \\ 0 & X_w \end{bmatrix}, \text{ optimal control based on a-posteriori state estimate: } u^o(k) = -K(k+1)\hat{x}_o(k) \\ \text{where } K(k+1) \text{ is defined exactly as in part a.} \\ \text{optimal cost } J^o &= \hat{J}^o + \sum_{j=0}^{N-1} \operatorname{trace} \left[\frac{Q}{0} & 0 \\ 0 & 0 \end{bmatrix} Z(j) \right) + \operatorname{trace} \left[\begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} Z(N) \right) \\ \hat{J}^o &= \frac{1}{2} \begin{bmatrix} x_o \\ x_w \end{bmatrix}^T P(0) \begin{bmatrix} x_o \\ x_w \end{bmatrix} + \frac{1}{2} \operatorname{trace} \left[P(k+1)^T P(k+1) E(k+1) \end{bmatrix}, \hat{b}(N) = 0 \\ \hat{b}(k) &= \hat{b}(k+1) + \operatorname{trace} \left[F(k+1)^T P(k+1) H(k+1) \end{bmatrix} E(k+1) \end{bmatrix}, \hat{b}(N) = 0 \\ \hat{b}(k) &= \hat{b}(k+1) + \operatorname{trace} \left[F(k+1)^T P(k+1) M(k+1) \end{bmatrix} C & 0 \end{bmatrix}^T \end{bmatrix} \\ 1.c) \\ \text{If } x(k) \text{ is measurable for all } k, \text{ we have } x(k) - Ax(k-1) - Bu(k-1) = B_w C_w x_w(k-1) \\ \text{Let } y_w(k-1) = B_w C_w x_w(k-1), \text{ so at step } k \text{ we know } y_w(k-1) \text{ with zero measurement noise } x_w(k) = A_w x_w(k-1) + B_u \eta(k-1) \\ \hat{x}^w_w(k) = A_w x_w(k-1) + B_u \eta(k-1) \\ E_w(k-1) = B_w C_w x_w(k-1) C_y^T B_w^T + 0 \\ E_w(k-1) = B_w C_w M_w(k-1) C_y^T B_w^T + 0 \\ E_w(k-1) = M_w(k-1) C_w^T B_w^T E_w(k-1)^T B_w C_w M_w(k-1) \\ M_w(k) = A_w Z_w(k-1) A_w^T + B_w^T F_w^T, \text{ initial condition } M_w(0) = X_w \\ \text{Let } Y_w(k-1) = M_w(k-1) C_w^T B_w^T E_w(k-1) B_w C_w M_w(k-1) \\ E(x_w(k)) Y_w(k-1) = E\{A_w x_w(k-1) + B_w \eta(k-1) Y_w(k-1)\} \\ E(x_w(k)) Y_w(k-1) = A_w E\{x_w(k-1) + y_w(k-1)\} + B_w E\{\eta(k-1) + y_w(k-1)\} \\ E(x_w(k)) Y_w(k-1) = A_w E\{x_w(k-1) + y_w(k-1) + P_w(k-1) + P_w(k-1)\} \\ x_w(k) = B_w C_w x_w(k-1) = B_w C_w A_w x_w(k-2) + B_w C_w B_v \eta(k-2) \\ \text{Therefore } y(k-1) \text{ and earlier don't contain any information about } \eta(k-1) \\ \text{so } E(\eta(k-1)) Y_w(k-1) = A_w E\{x_w(k-1) + Y_w(k-1)\} = A_w E(x_w(k-1)) Y_w(k-1) + A_w E(x_w(k)) \\ \text{where } again K(k+1) \text{ is defined exactly as in part a. In the special circumstances of this problem with the one-step observation delay, the value used by the controller happens$$

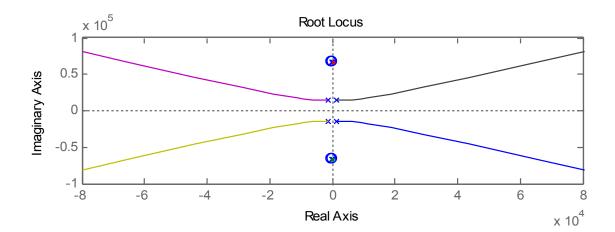
estimate instead of the usual a-posteriori estimate. (I wonder if this also holds in more general cases?)

 $J = \frac{1}{2} E \left\{ \begin{bmatrix} x(N) \\ \hat{x}_{v}^{o}(N) \end{bmatrix}^{T} \begin{bmatrix} S & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(N) \\ \hat{x}_{v}^{o}(N) \end{bmatrix} + \sum_{k=0}^{N-1} \left(\begin{bmatrix} x(k) \\ \hat{x}_{v}^{o}(k) \end{bmatrix}^{T} \begin{bmatrix} Q & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(k) \\ \hat{x}_{v}^{o}(k) \end{bmatrix} + u^{T}(k) R u(k) \right\}$ $\hat{x}_{w}^{o}(k) = A_{w} \hat{x}_{w}(k-1 \mid k) = A_{w} \hat{x}_{w}^{o}(k-1) + A_{w} F_{w}(k-1) \tilde{v}_{w}^{o}(k-1)$

$$\begin{split} \tilde{y}_{w}^{w}(k-1) &= y_{w}(k-1) - B_{w}C_{w}\tilde{x}_{w}^{w}(k-1) + B_{w}C_{w}x_{w}(k-1) - B_{w}C_{w}\tilde{x}_{w}^{w}(k-1) \\ x(k) &= Ax(k-1) + Bu(k-1) + B_{w}C_{w}x_{w}(k-1) = Ax(k-1) + Bu(k-1) + B_{w}C_{w}\tilde{x}_{w}^{w}(k-1) \\ \left[\frac{x(k)}{x_{w}^{w}(k)}\right] &= \begin{bmatrix} A & B_{w}C_{w} \\ 0 & A_{w} \end{bmatrix} \begin{bmatrix} x(k-1) \\ \tilde{x}_{w}^{w}(k) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(k-1) + \begin{bmatrix} I \\ A_{w}F_{w}(k-1) \end{bmatrix} \tilde{y}_{w}^{w}(k-1) \\ \left[\frac{x^{w}}{x_{w}^{w}(k-1)}\right] &= \begin{bmatrix} A & B_{w}C_{w} \\ 0 & A_{w} \end{bmatrix} \begin{bmatrix} x(k) \\ \tilde{x}_{w}^{w}(k) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(k) + \begin{bmatrix} I \\ A_{w}F_{w}(k) \end{bmatrix} \tilde{y}_{w}^{w}(k) \\ E \begin{bmatrix} \tilde{y}_{w}^{w}(k) \tilde{y}_{w}^{w}(k)^{T} \end{bmatrix} &= E_{w}(k) = B_{w}C_{w}M_{w}(k)C_{w}^{T}B_{w}^{T} \\ So using this form, the optimal cost is $J^{o} = \frac{1}{2} \begin{bmatrix} x_{o} \\ x_{wo} \end{bmatrix}^{T} P(0) \begin{bmatrix} x_{o} \\ x_{wo} \end{bmatrix} + \frac{1}{2} \operatorname{trace} \left(P(0) \begin{bmatrix} X_{o} & 0 \\ 0 & X_{wo} \end{bmatrix} \right) + b(0) \\ b(k) &= b(k+1) + \operatorname{trace} \left(\begin{bmatrix} I \\ A_{w}F_{w}(k) \end{bmatrix}^{T} P(k+1) \begin{bmatrix} I \\ A_{w}F_{w}(k) \end{bmatrix} E_{w}(k) \right), b(N) = 0 \end{split}$
2.a)
$$Z_{1}(s) &= \frac{1.367 \cdot 10^{4}}{s^{2} + 134 s + 4.52 \cdot 10^{9}} V_{1}(s) = 1.367 \cdot 10^{4} \cdot W(s) \\ \operatorname{Inverse Laplace transform,} \tilde{z}_{1}(t) + 134 \tilde{z}_{1}(t) + 4.52 \cdot 10^{9} \cdot z_{1}(t) = 1.367 \cdot 10^{4} \cdot w(t) \\ \operatorname{Assuming the given transfer function was for the suspension by itself, since we know $w(t)$ is in units of force we have $m_{1} = 1/(1.367 \cdot 10^{4}) + b_{1} = 134 J/(1.367 \cdot 10^{4})$. $k_{1} = 4.52 \cdot 10^{9} / (1.367 \cdot 10^{4})$ For the actuator, $m_{2} = (t) + b / (z(t) - z_{1}(t)) + b / z(t) - z_{1}(t) = b z_{1}(t) + z_{2}(t) + 4.52 \cdot 10^{9} / (1.367 \cdot 10^{4}) \\ E_{1}(t) = -134 \tilde{z}_{1}(t) + 4.52 \cdot 10^{9} \cdot z_{1}(t) = 1.367 \cdot 10^{4} \cdot w(t) + 5 \cdot 10^{-3} \cdot z_{2}(t) + 400 \cdot z_{2}(t) - 2.5 \cdot 10^{-5} u(t) \\ \tilde{z}_{1}(t) = -134 \tilde{z}_{1}(t) + 4.52 \cdot 10^{9} \cdot z_{1}(t) + 1.367 \cdot 10^{4} \cdot w(t) + 5 \cdot 10^{-3} \cdot z_{2}(t) + 400 \cdot z_{2}(t) - 2.5 \cdot 10^{-5} u(t) \\ \tilde{z}_{2}(t) = -z_{1}(t) - 2.50468 \cdot 10^{8} \cdot z_{1}(t) + 1.367 \cdot 10^{4} \cdot w(t) + 68.35 \tilde{z}_{2}(t) + 2.5468 \cdot 10^{8} \cdot z_{2}(t) + 12.84175 u(t) \\ \tilde{z}_{2}(t) = -2.104 + 2.10^{9} \cdot z_{1}(4s + 1) + 1.86 \cdot 10^{9} \cdot z_{1}(t) + 1.86 \cdot 10^{9} \cdot z_{2}(t) + 1.86 \cdot 10^{9} \cdot z_{2}(t)$$$$$

TF from u to x is $G(s) = C(sI - A)^{-1}B = \frac{12.5 s^2 + 1675 s + 5.65 \cdot 10^{10}}{s^4 + 2702 s^3 + 4.726 \cdot 10^9 s^2 + 1.133 \cdot 10^{13} s + 9.04 \cdot 10^{17}}$ Symmetric root locus of G(-s)G(s) shown on next page 2.c)

stationary LQG regulator minimizing cost $J = E\{z^2(t) + Ru^2(t)\}/2 = E\{x^T(t)C^TCx(t) + Ru^2(t)\}/2$ optimal controller $u^o(t) = -K\hat{x}(t)$, $K = R^{-1}B^TP$, $A^TP + PA + C^TC - PBR^{-1}B^TP = 0$ KF estimator $\dot{\hat{x}}(t) = A\hat{x}(t) + Bu(t) + L(v(t) - C\hat{x}(t))$, $L = MC^TV^{-1}$



$$\text{Matlab says } M = \begin{bmatrix} 9.9388 \cdot 10^{-12} & -1.0381 \cdot 10^{-11} & 5.895 \cdot 10^{-12} & 2.7248 \cdot 10^{-8} \\ -1.0381 \cdot 10^{-11} & 1.0902 \cdot 10^{-11} & -2.7262 \cdot 10^{-8} & 8.1553 \cdot 10^{-12} \\ 5.895 \cdot 10^{-12} & -2.7262 \cdot 10^{-8} & 4.4979 \cdot 10^{-2} & -4.6987 \cdot 10^{-2} \\ 2.7248 \cdot 10^{-8} & 8.1553 \cdot 10^{-12} & -4.6987 \cdot 10^{-2} & 4.9168 \cdot 10^{-2} \end{bmatrix}, \ L = \begin{bmatrix} -26.65 \\ 31.346 \\ -1.642 \cdot 10^{6} \\ 1.642 \cdot 10^{6} \end{bmatrix}$$

from care $(A^T, C^T, B_w W B_w^T, V)$

For
$$R=1$$
, Matlab gives $P=\begin{bmatrix} 2.288\cdot10^{-4} & 2.098\cdot10^{-4} & 6.7825\cdot10^{-12} & -1.0384\cdot10^{-10} \\ 2.098\cdot10^{-4} & 2.0674\cdot10^{-4} & 2.7321\cdot10^{-9} & 2.5062\cdot10^{-9} \\ 6.7825\cdot10^{-12} & 2.7321\cdot10^{-9} & 1.1008\cdot10^{-12} & 1.0502\cdot10^{-12} \\ -1.0384\cdot10^{-10} & 2.5062\cdot10^{-9} & 1.0502\cdot10^{-12} & 1.0037\cdot10^{-12} \end{bmatrix}$

and $K = [-1.3358 \cdot 10^{-9} \quad 3.125 \cdot 10^{-8} \quad 1.311 \cdot 10^{-11} \quad 1.2531 \cdot 10^{-11}]$, both from care $(A, B, C^T C, R)$ optimal cost $J^o = \text{trace}\{P[BKM + B_w W B_w^T]\}$, for R = 1 we have $J^o = 7.8156 \cdot 10^{-14}$

For
$$R = 10^{-10}$$
, LQR result is $P = \begin{bmatrix} 2.2873 \cdot 10^{-4} & 2.0973 \cdot 10^{-4} & 7.6393 \cdot 10^{-12} & -1.0298 \cdot 10^{-10} \\ 2.0973 \cdot 10^{-4} & 2.0668 \cdot 10^{-4} & 2.7321 \cdot 10^{-9} & 2.5062 \cdot 10^{-9} \\ 7.6393 \cdot 10^{-12} & 2.7321 \cdot 10^{-9} & 1.1005 \cdot 10^{-12} & 1.0499 \cdot 10^{-12} \\ -1.0298 \cdot 10^{-10} & 2.5062 \cdot 10^{-9} & 1.0499 \cdot 10^{-12} & 1.0034 \cdot 10^{-12} \end{bmatrix}$

and $K = [-13.251 \ 312.5 \ 0.13106 \ 0.12527]$, with optimal cost $J^o = 7.8156 \cdot 10^{-14}$

$$J^{o} = \operatorname{trace} \{ C_{\mathcal{O}}^{T} C_{\mathcal{O}} M + L^{T} P L V \}$$

First let $Q = C_Q^T C_Q$. Next, note that the matrices Q, M, and V are positive semidefinite.

 $Q \ge 0$ by construction from C_Q , $M \ge 0$ since it is the solution of a Kalman filter Riccati equation, and $V \ge 0$ since it is a covariance matrix. These positive semidefinite matrices are symmetric and real-valued so they are each diagonalizable. Let $M = T_M \Lambda_M T_M^{-1}$ and $V = T_V \Lambda_V T_V^{-1}$

The transformations T_M and T_V of the symmetric real matrices are orthogonal: $T_M^{-1} = T_M^T$, $T_V^{-1} = T_V^T$ $C_O^T C_O M = Q T_M \Lambda_M T_M^T$

The trace of a matrix is the sum of its eigenvalues, so the trace is invariant to a similarity transform. trace $\{C_Q^T C_Q M\} = \text{trace}\{T_M^T Q T_M \Lambda_M\}$ Since Λ_M is diagonal, the columns with zero eigenvalues will result in columns of all zeros in the

Since Λ_M is diagonal, the columns with zero eigenvalues will result in columns of all zeros in the product matrix $T_M^T Q T_M \Lambda_M$, and those columns will not contribute to the trace.

So defining $\Lambda_M^{1/2}$ as the matrix with positive square roots of the eigenvalues of M on its diagonal, and $(\Lambda_M^{1/2})^{\#}$ as the pseudoinverse matrix with reciprocal values at the nonzero diagonals of $\Lambda_M^{1/2}$, but zeros everywhere else, we can take a pseudo-similarity transform without altering the trace.

$$\operatorname{trace} \{ C_{\mathcal{Q}}^{T} C_{\mathcal{Q}} M \} = \operatorname{trace} \{ \Lambda_{M}^{1/2} T_{M}^{T} Q T_{M} \Lambda_{M} (\Lambda_{M}^{1/2})^{\#} \} = \operatorname{trace} \{ \Lambda_{M}^{1/2} T_{M}^{T} Q T_{M} \Lambda_{M}^{1/2} \}$$

For any vector x, let $z = T_M \Lambda_M^{1/2} x$. Then $x^T \Lambda_M^{1/2} T_M^T Q T_M \Lambda_M^{1/2} x = z^T Q z$

By positive semidefiniteness $z^T Q z \ge 0$, so that implies $\Lambda_M^{1/2} T_M^T Q T_M \Lambda_M^{1/2}$ is positive semidefinite, and therefore has nonnegative eigenvalues and a nonnegative trace.

trace
$$\{C_O^T C_O M\}$$
 = trace $\{\Lambda_M^{1/2} T_M^T Q T_M \Lambda_M^{1/2}\} \ge 0$

Likewise trace $\{L^T P L V\}$ = trace $\{L^T P L T_V \Lambda_V T_V^T\}$ = trace $\{T_V^T L^T P L T_V \Lambda_V\}$

Using corresponding definitions of $\Lambda_V^{1/2}$ and $(\Lambda_V^{1/2})^{\#}$ and the same zero-eigenvalue argument,

trace
$$\{L^T P L V\}$$
 = trace $\{\Lambda_V^{1/2} T_V^T L^T P L T_V \Lambda_V (\Lambda_V^{1/2})^\#\}$ = trace $\{\Lambda_V^{1/2} T_V^T L^T P L T_V \Lambda_V^{1/2}\}$

For any vector x, let $z = LT_V \Lambda_V^{1/2} x$. Then $x^T \Lambda_V^{1/2} T_V^T L^T P LT_V \Lambda_V^{1/2} x = z^T P z$

 $z^T P z \ge 0$ by positive semidefiniteness of P, so $\Lambda_V^{1/2} T_V^T L^T P L T_V \Lambda_V^{1/2}$ is positive semidefinite trace $\{L^T P L V\}$ = trace $\{\Lambda_V^{1/2} T_V^T L^T P L T_V \Lambda_V^{1/2}\} \ge 0$

For this example trace $\{C_O^T C_O M\} = 7.7945 \cdot 10^{-14}$

With
$$R=1$$
, trace $\{L^T P L V\} = 2.1091 \cdot 10^{-16}$

With
$$R = 10^{-10}$$
, trace $\{L^T P L V\} = 2.1090 \cdot 10^{-16}$

This is essentially at roundoff error, definitely two orders of magnitude smaller than the other term.

Difficult to tell for sure with only this data, but it appears as $R \to 0$, $J^o \to \operatorname{trace}\{C_Q^T C_Q M\}$ 2.e)

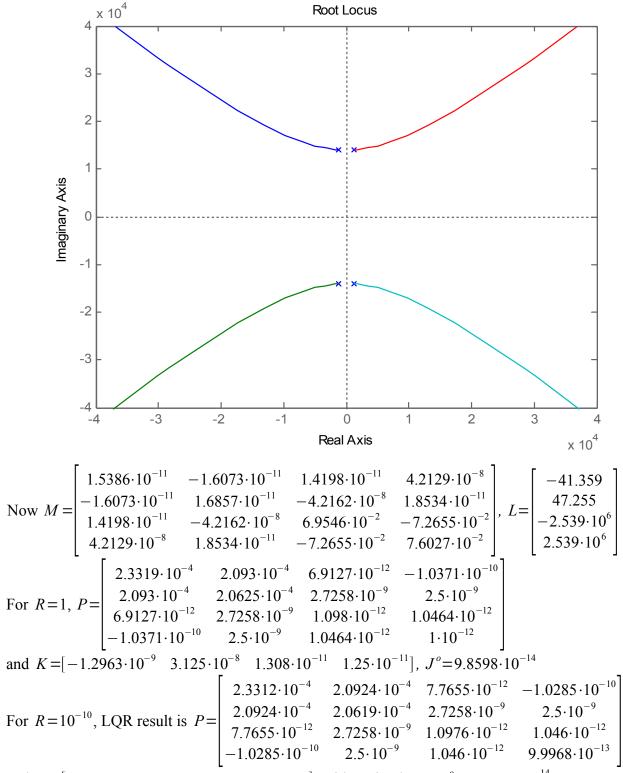
Now z_1 does not depend on z_2 or u(t), so $\ddot{z}_1(t) + 134 \dot{z}_1(t) + 4.52 \cdot 10^9 \cdot z_1(t) = 1.367 \cdot 10^4 \cdot w(t)$ As before, $\ddot{z}_2(t) = -\ddot{z}_1(t) - 2500 \dot{z}_2(t) - 2 \cdot 10^8 z_2(t) + 12.5 u(t)$

$$\ddot{z}_{2}(t) = 134 \, \dot{z}_{1}(t) + 4.52 \cdot 10^{9} \, z_{1}(t) - 1.367 \cdot 10^{4} \, w(t) - 2500 \, \dot{z}_{2}(t) - 2 \cdot 10^{8} \, z_{2}(t) + 12.5 \, u(t)$$

$$\dot{x}(t) = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -4.52 \cdot 10^9 & 0 & -134 & 0 \\ 4.52 \cdot 10^9 & -2 \cdot 10^8 & 134 & -2500 \end{bmatrix} \begin{bmatrix} z_1(t) \\ z_2(t) \\ \dot{z}_1(t) \\ \dot{z}_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 12.5 \end{bmatrix} u(t) + \begin{bmatrix} 0 \\ 0 \\ 1.367 \cdot 10^4 \\ -1.367 \cdot 10^4 \end{bmatrix} w(t)$$

TF from u to x is
$$G(s) = C(sI - A)^{-1}B = \frac{12.5}{s^2 + 2500 s + 2.10^8}$$

Symmetric root locus of G(-s)G(s) shown on next page



and $K = [-12.857 \ 312.5 \ 0.13075 \ 0.12496]$, with optimal cost $J^o = 9.8598 \cdot 10^{-14}$ LQG results quite similar between the two models. Biggest difference was in the transfer function and therefore root locus as well. There was a pole/zero cancellation and a reduction of order.

3.a)
$$\frac{d}{dt} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ m \end{bmatrix} u(t) + \begin{bmatrix} 1 \\ 1 \end{bmatrix} w(t), \ y(t) = \begin{bmatrix} 1 & 0 \\ x_2(t) \end{bmatrix} + v(t)$$

$$J = E\{x^T(\tau)Qx(\tau) + u^2(\tau)\} = \lim_{t \to \infty} E\left[\frac{1}{T}\int_0^\tau [x^T(\tau)Qx(\tau) + u^2(\tau)]d\tau\right]$$

$$Q = \rho\begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \end{bmatrix} = \rho\begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}. \quad R = 1, \text{ nominal } m_0 = 1$$
optimal controller $u(t) = -K_{LQ}x(t), \quad K_{LQ} = R^{-1}B^TP, \quad A^TP + PA + Q - PBR^{-1}B^TP = 0$

$$0 = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} \begin{bmatrix} 1 & 1 \\ p_{12} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} + \rho\begin{bmatrix} 1 & 1 \\ p_{12} & p_{11} + p_{12} \\ p_{12} & p_{12} + p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{11} + p_{12} \\ p_{12} & p_{12} + p_{22} \end{bmatrix} \begin{bmatrix} 0 & 1 \\ p_{11} & p_{11} & p_{12} \\ p_{12} & p_{12} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{11} + p_{12} \\ p_{12} & p_{12} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{11} & p_{12} \\ p_{12} & p_{12} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} \\ p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{22} & p_{12} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{11} & p_{12} & p_{12} \\ p_{12} & p_{12} & p_{12} \\ p_{12} & p_{12} & p_{22} \end{bmatrix} + \begin{bmatrix} p_{11} & p_{11} + p_{12} \\ p_{12} & p_{12} & p_{22} \\ p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} \\ p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{12} & p_{12} & p_{12} \\ p_{12} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{12} & p_{12} & p_{22} \\ p_{12} & p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{12} & p_{12} & p_{22} \\ p_{12} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{12} & p_{12} & p_{22} \\ p_{12} & p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{12} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{12} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_{22} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ p_{22} & p_{22} & p_{22} \\ p_{22} & p_{22} & p_$$

$$s^2 + (-2 + 2m + m\sqrt{4 + \rho})s + 1 = 0$$

 $\sqrt{4+\rho} \ge 2$ so for m > 0.5 the middle coefficient is positive, and the real parts of the eigenvalues will be negative, giving a stable closed-loop system

For
$$\rho = 5$$
 and $m = 1$, $s^2 + \sqrt{9}s + 1 = 0$
 $\lambda = (-3 \pm \sqrt{9} - 4)/2 = (-3 \pm \sqrt{5})/2 < 0$

3.c)

$$\frac{d}{dt} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ m \end{bmatrix} u(t) + \begin{bmatrix} L_1 \\ L_2 \end{bmatrix} \tilde{y}(t), \quad \tilde{y}(t) = y(t) - \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix}$$

$$AM + MA^{T} = -B_{w}WB_{w}^{T} + MC^{T}V^{-1}CM, W = 1, V = \sigma$$

Note that
$$B_w W B_w^T = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$$
, and let $M = \begin{bmatrix} M_{11} & M_{12} \\ M_{12}^T & M_{22} \end{bmatrix}$

$$\frac{d}{dt} \begin{bmatrix} \hat{x}_2(t) \\ \hat{x}_1(t) \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_2(t) \\ \hat{x}_1(t) \end{bmatrix} + \begin{bmatrix} m \\ 0 \end{bmatrix} u(t) + \begin{bmatrix} L_2 \\ L_1 \end{bmatrix} \tilde{y}(t), \quad \tilde{y}(t) = y(t) - \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_2(t) \\ \hat{x}_1(t) \end{bmatrix}$$

Let
$$M_{\text{flip}} = \begin{bmatrix} M_{22} & M_{12}^T \\ M_{12} & M_{11} \end{bmatrix}$$
, $C_{\text{flip}} = \begin{bmatrix} 0 & 1 \end{bmatrix}$

$$A^{T} M_{\text{flip}} + M_{\text{flip}} A = -B_{w} W B_{w}^{T} + M_{\text{flip}} C_{\text{flip}}^{T} V^{-1} C_{\text{flip}} M_{\text{flip}}$$

recall the LQR Riccati equation from part a was: $A^T P + P A + Q - P B R^{-1} B^T P = 0$

 $B = C_{\text{flip}}^T$ for m = 1, so if we multiply every term by σ^{-1} we get the same Riccati equation:

$$A^{T}(\sigma^{-1}M_{\text{flip}}) + (\sigma^{-1}M_{\text{flip}})A + B_{w}\sigma^{-1}B_{w}^{T} - (\sigma^{-1}M_{\text{flip}})C_{\text{flip}}^{T}C_{\text{flip}}(\sigma^{-1}M_{\text{flip}}) = 0$$

Where $Q = B_w \sigma^{-1} B_w^T$ for $\rho = \sigma^{-1}$

$$\sigma^{-1} M_{\text{flip}} = \sigma^{-1} \begin{bmatrix} M_{22} & M_{12}^T \\ M_{12} & M_{11} \end{bmatrix} = P = \begin{bmatrix} 4 + 2\sqrt{4 + \sigma^{-1}} & 2 + \sqrt{4 + \sigma^{-1}} \\ 2 + \sqrt{4 + \sigma^{-1}} & 2 + \sqrt{4 + \sigma^{-1}} \end{bmatrix}$$

$$M = \begin{bmatrix} M_{11} & M_{12} \\ M_{12}^T & M_{11} \end{bmatrix} = \sigma \begin{bmatrix} 2 + \sqrt{4 + \sigma^{-1}} & 2 + \sqrt{4 + \sigma^{-1}} \\ 2 + \sqrt{4 + \sigma^{-1}} & 4 + 2\sqrt{4 + \sigma^{-1}} \end{bmatrix}$$

$$K_{KF} = M C^{T} V^{-1} = \sigma \begin{bmatrix} 2 + \sqrt{4 + \sigma^{-1}} & 2 + \sqrt{4 + \sigma^{-1}} \\ 2 + \sqrt{4 + \sigma^{-1}} & 4 + 2\sqrt{4 + \sigma^{-1}} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \sigma^{-1} = \begin{bmatrix} 2 + \sqrt{4 + \sigma^{-1}} \\ 2 + \sqrt{4 + \sigma^{-1}} \end{bmatrix} = \beta \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

3.d)

Assuming expectations over all noise variables in the following:

$$\begin{split} \frac{d}{dt} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} &= \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ m \end{bmatrix} u(t) = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} - \begin{bmatrix} 0 \\ m \end{bmatrix} \alpha \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} \\ \frac{d}{dt} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} &= \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ m_o \end{bmatrix} u(t) + \begin{bmatrix} L_1 \\ L_2 \end{bmatrix} \tilde{y}(t), \ \tilde{y}(t) &= y(t) - \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} \\ \frac{d}{dt} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} &= \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} - \begin{bmatrix} 0 \\ m_o \end{bmatrix} \alpha \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} + \beta \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} - \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} \\ \frac{d}{dt} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} &= \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & -m\alpha & -m\alpha \\ \beta & 0 & 1-\beta & 1 \\ \beta & 0 & -\beta-m_o\alpha & 1-m_o\alpha \end{bmatrix} \begin{bmatrix} x_1(t) \\ \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & -m\alpha & -m\alpha \\ \beta & 0 & 1-\beta & 1 \\ \beta & 0 & -\beta-\alpha & 1-\alpha \end{bmatrix} \begin{bmatrix} x_1(t) \\ \hat{x}_1(t) \\ \hat{x}_2(t) \end{bmatrix} \end{aligned}$$

3.e)

For $\rho = \sigma = 5$, m = 1, $\alpha = 2 + \sqrt{4 + 5} = 5$, $\beta = 2 + \sqrt{4 + 5^{-1}} = 4.0494$ the eigenvalues of the part d matrix in this case are -2.618, -1.2483, -0.80109, and -0.38197. the eigenvalues of full-state LQR from part b were -2.618 and -0.38197 so the separation principle holds in this m = 1 example

3.f

With m=1.1, the eigenvalues of the above matrix are -3.4846, -0.83368 ± 1.4736 , and 0.10258. The eigenvalues are not where we expected them to be from the LQR and KF results, especially since we now have a complex pair, and even worse one of the closed-loop eigenvalues is unstable.