

ME 233 Advanced Control II

Lecture 19

Stability Analysis Using The Hyperstability Theorem

Adaptive Control

Basic Adaptive Control Principle

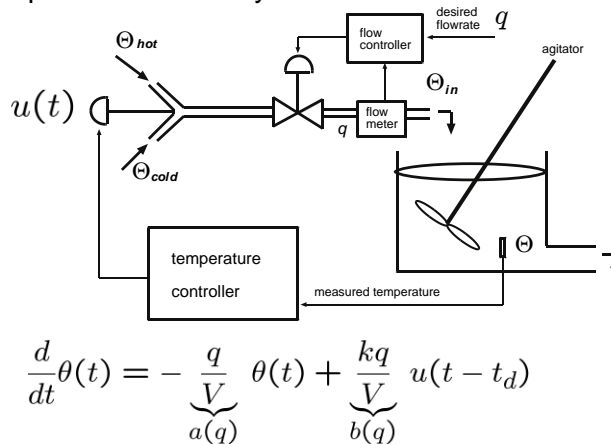
Controller parameters **are not constant**, rather, they are adjusted in an online fashion by a ***Parameter Adaptation Algorithm (PAA)***

When is adaptive control used?

- Plant parameters are unknown
- Plant parameters are time varying

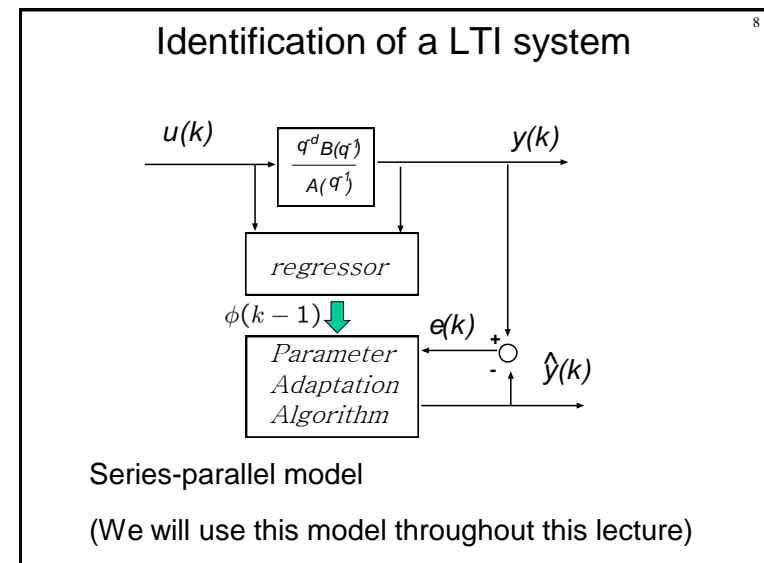
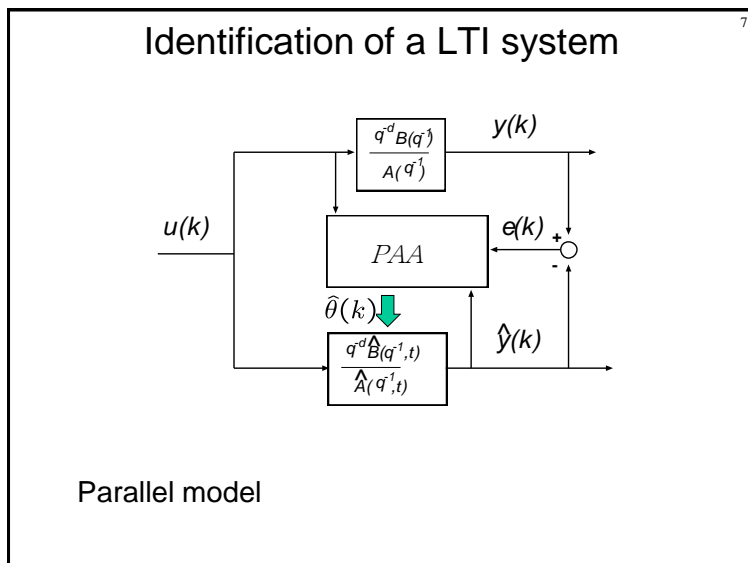
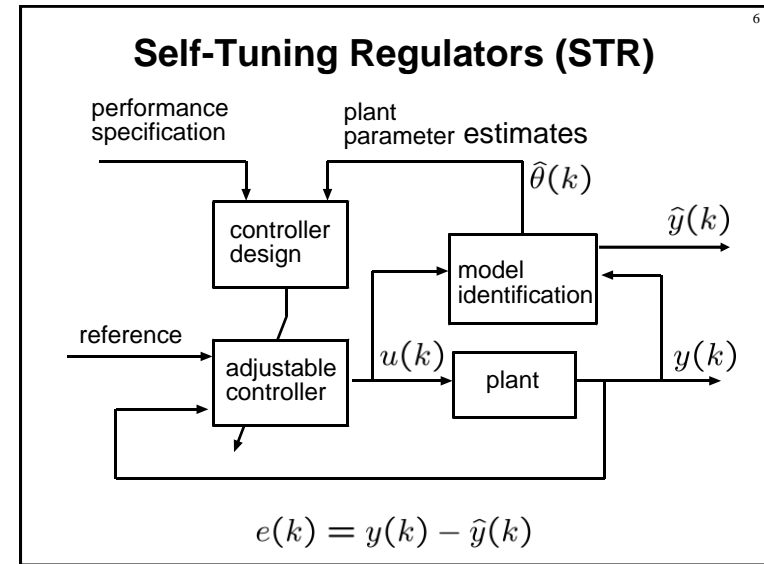
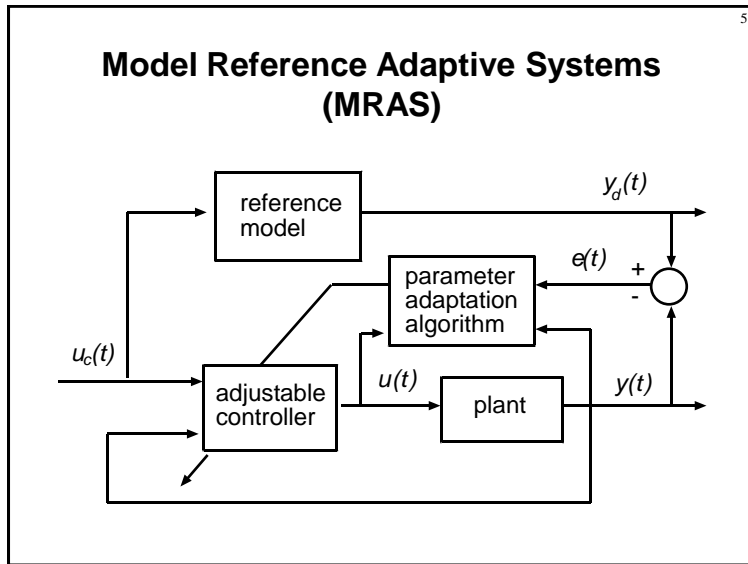
Example of a system with varying parameters

- Temperature control system



Adaptive Control Classification

- Continuous time VS **discrete time**
- Direct VS indirect
- MRAS VS **STR**



Plant ARMA Model

Plant model

$$A(q^{-1})y(k) = q^{-d}B(q^{-1})u(k)$$

where

$$A(q^{-1}) = 1 + a_1q^{-1} + \dots + a_nq^{-n}$$

$$B(q^{-1}) = b_o + b_1q^{-1} + \dots + b_mq^{-m}$$

Unknown plant parameters

Assume ARMA model parameters are unknown

$$y(k) = - \underline{a_1} y(k-1) \dots - \underline{a_n} y(k-n) \\ + \underline{b_o} u(k-d) \dots + \underline{b_m} u(k-d-m)$$

Define:

$$\theta = \left[\underline{a_1} \quad \dots \quad \underline{a_n} \quad \underline{b_o} \quad \dots \quad \underline{b_m} \right]^T$$

As the unknown parameter vector

Regressor vector

Collect all measurable signals in one vector

$$y(k) = - a_1 \underline{y(k-1)} \dots - a_n \underline{y(k-n)} \\ + b_o \underline{u(k-d)} \dots + b_m \underline{u(k-d-m)}$$

We define

$$\phi(k-1) = \left[\underline{-y(k-1)} \quad \dots \quad \underline{-y(k-n)} \right. \\ \left. \underline{u(k-d)} \quad \dots \quad \underline{u(k-d-m)} \right]^T$$

as the known regressor vector

Plant ARMA Model

Plant model

$$y(k) = \phi^T(k-1) \theta$$

where

$$\theta = \left[a_1 \quad \dots \quad a_n \quad b_o \quad \dots \quad b_m \right]^T$$

$$\phi(k-1) = \left[\underline{-y(k-1)} \quad \dots \quad \underline{-y(k-n)} \right. \\ \left. \underline{u(k-d)} \quad \dots \quad \underline{u(k-d-m)} \right]^T$$

Plant ARMA Model

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Plant estimate (series-parallel)

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

where

$$\hat{\theta}(k) = \begin{bmatrix} \hat{a}_1(k) & \cdots & \hat{a}_n(k) & \hat{b}_o(k) & \cdots & \hat{b}_m(k) \end{bmatrix}^T$$

$$\phi(k-1) = \begin{bmatrix} -y(k-1) & \cdots & -y(k-n) \\ u(k-d) & \cdots & u(k-d-m) \end{bmatrix}^T$$

Plant output estimate

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Plant a-posteriori estimate

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

Plant a-priori estimate

$$\hat{y}^o(k) = \phi^T(k-1) \hat{\theta}(k-1)$$

Plant a-posteriori error

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$$y(k) = \phi^T(k-1) \theta$$

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

error: $e(k) = y(k) - \hat{y}(k)$

$$e(k) = \phi^T(k-1) [\theta - \hat{\theta}(k)]$$

$$= \phi^T(k-1) \tilde{\theta}(k)$$

$$\tilde{\theta}(k) = \theta - \hat{\theta}(k)$$

A Parameter Adaptation Algorithm

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PAA $F = F^T \succ 0$

$$\hat{\theta}(k) = \hat{\theta}(k-1) + F \phi(k-1) e(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1) e(k)$$

Adaptation Dynamics

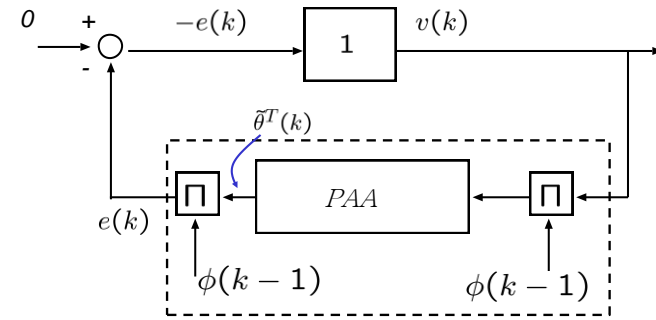
a-posteriori error: $e(k) = y(k) - \hat{y}(k)$

$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Adaptation Dynamics



$$PAA: \quad \tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k-1)v(k)$$

Convergence of Adaptive Systems

Adaptive systems are nonlinear

We need to prove that the algorithms converge:

- **Output error convergence**

$$e(k) \rightarrow 0$$

$$e(k) = y(k) - \hat{y}(k)$$

- **Parameter error convergence**

$$\tilde{\theta}(k) \rightarrow 0$$

$$\tilde{\theta}(k) = \theta - \hat{\theta}(k)$$

Output error Convergence

Our first goal will be to prove the asymptotic convergence of the output error:

$$e(k) \rightarrow 0$$

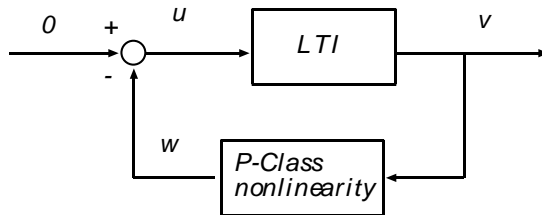
Two frequently used methods of stability analysis are:

- **Stability analysis using Lyapunov's direct method**
 - State space approach
- **Stability analysis using the Passivity or Hyperstability theorems**
 - Input/output approach

Hyperstability

Hyperstability Theory

- Developed by V.M. Popov to analyze the stability of a class of feedback systems (monograph published in 1973)

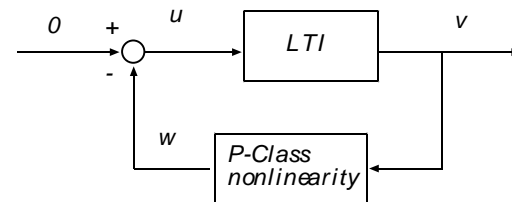


- Popularized by I.D. Landau for the analysis of adaptive systems (first book published in 1979)

Hyperstability Theory

Hyperstability Theory

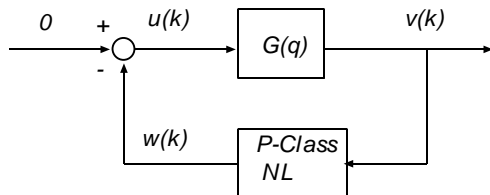
- Applies to both continuous time and discrete time systems



- Abuse of notation:** We will denote the LTI block by its transfer function

DT Hyperstability Theory

$$G(z) = C(zI - A)^{-1}B + D$$

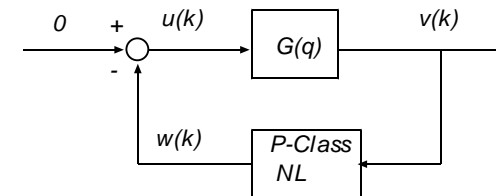


- State space description of the LTI Block:

$$x(k+1) = Ax(k) + Bu(k)$$

$$v(k) = Cx(k) + Du(k)$$

DT Hyperstability Theory

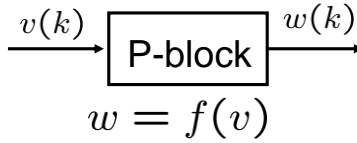


- P-class nonlinearity: (passive nonlinearities)

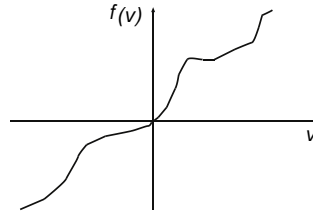
$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_o^2 \quad \forall k \geq 0$$

Where γ_o is a bounded constant.

Example: Static nonlinearity:

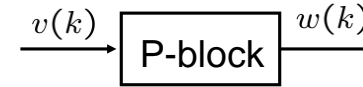


$$v f(v) \geq 0$$



$$\sum_{j=0}^k w^T(j)v(j) = \sum_{j=0}^k \underbrace{f(v(j))v(j)}_{\geq 0} \geq 0 > -\gamma_o^2$$

Example: Dynamic P-class block



$$\begin{cases} \tilde{\theta}(k) = \tilde{\theta}(k-1) + F\phi(k-1)v(k) \\ w(k) = \phi^T(k-1)\tilde{\theta}(k) \end{cases} \quad \begin{aligned} \phi(k) &\in \mathcal{R}^n \\ \tilde{\theta}(-1) &\in \mathcal{R}^n \\ F = F^T &\succ 0 \\ \|\tilde{\theta}(-1)\| &< \infty \\ \|\phi(k)\| &< \infty \end{aligned}$$

Example: Dynamic P-class block

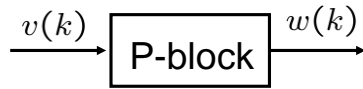
$$w(k) = \phi^T(k-1)\tilde{\theta}(k) \quad \tilde{\theta}(k) = \tilde{\theta}(k-1) + F\phi(k-1)v(k)$$

$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \phi^T(j-1)\tilde{\theta}(j)v(j) \\ &= \sum_{j=0}^k \tilde{\theta}^T(j) \underbrace{[\phi(j-1)v(j)]}_{F^{-1}[\tilde{\theta}(j) - \tilde{\theta}(j-1)]} \\ &= \sum_{j=0}^k \tilde{\theta}^T(j)F^{-1}[\tilde{\theta}(j) - \tilde{\theta}(j-1)] \\ &= \sum_{j=0}^k \{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j-1) \} \end{aligned}$$

Example: Dynamic P-class block

$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j-1) \} \\ &\quad + \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) - \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \\ \sum_{j=0}^k w(j)v(j) &= \frac{1}{2} \sum_{j=0}^k \{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \} \\ &\quad + \underbrace{\frac{1}{2} \sum_{j=0}^k [\tilde{\theta}(j) - \tilde{\theta}(j-1)]^T F^{-1} [\tilde{\theta}(j) - \tilde{\theta}(j-1)]}_{\geq 0} \end{aligned}$$

Example: Dynamic P-class block

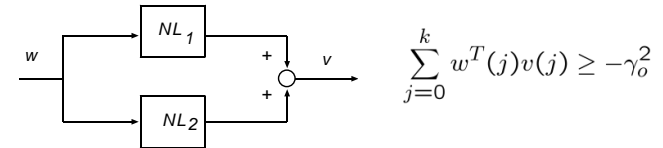


$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &\geq \frac{1}{2} \sum_{j=0}^k \{ \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j) - \tilde{\theta}^T(j-1) F^{-1} \tilde{\theta}(j-1) \} \\ &= \frac{1}{2} \tilde{\theta}^T(k) F^{-1} \tilde{\theta}(k) - \underbrace{\frac{1}{2} \tilde{\theta}^T(-1) F^{-1} \tilde{\theta}(-1)}_{\gamma_o^2} \\ &\geq -\gamma_o^2 \end{aligned}$$

Examples of P-class NL

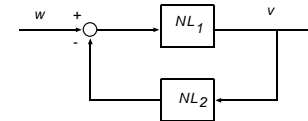
Lemma:

- The parallel combination of two P-class nonlinearities is also a P-class nonlinearity.



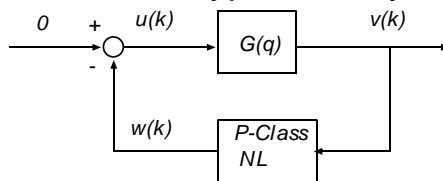
$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_o^2$$

- The feedback combination of two P-class nonlinearities is also a P-class nonlinearity.



$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_o^2$$

DT Hyperstability

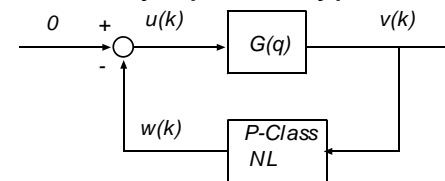


Hyperstability: The above feedback system is hyperstable if there exist positive bounded constants δ_1, δ_2 such that, for any state space realization of $G(q)$,

$$\|x(k)\| < \delta_1 [\|x(0)\| + \delta_2] \quad \forall k \geq 0$$

FOR ALL P-class nonlinearities

DT Asymptotic Hyperstability

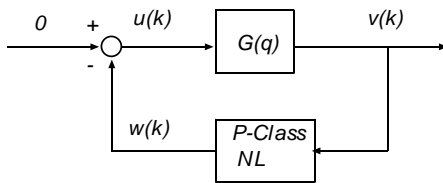


Asymptotic Hyperstability: The above feedback system is asymptotically hyperstable if

- It is hyperstable
- for any state space realization of $G(z)$,

$$\lim_{k \rightarrow \infty} x(k) = 0$$

DT Hyperstability Theorems



Hyperstability Theorem: The above feedback system is hyperstable **iff** the transfer function $G(z)$ of the LTI block is **Positive Real**.

Asymptotical Hyperstability Theorem: The above feedback system is asymptotically hyperstable **iff** the transfer function $G(z)$ of the LTI block is **Strictly Positive Real**.

Strictly Positive Real (SPR) TF

$$G(z) = C(zI - A)^{-1}B + D$$

Is **Strictly Positive Real (SPR)** iff:

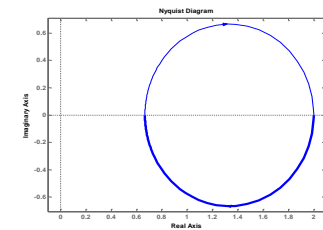
1. All poles of $G(z)$ are asymptotically stable.

2. $G(e^{j\omega}) + G^T(e^{-j\omega}) \succ 0$

for all $0 \leq \omega \leq \pi$

Example:

$$G(z) = \frac{z}{z + 0.5}$$



Strictly Positive Real (SPR) TF

For scalar rational transfer functions

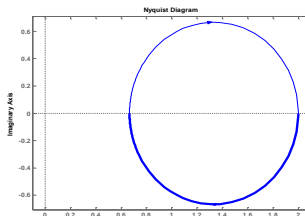
$$G(z) = \frac{B(z)}{A(z)}$$

1. All poles of $G(z)$ are asymptotically stable.

2. $\text{Re}\{G(e^{j\omega})\} > 0$ for all ω , $0 \leq \omega \leq \pi$

Note:

A necessary (but not sufficient) condition for $G(z)$ to be SPR is that its relative degree must be 0.



Matrix Inequality Interpretation of SPR

The transfer function

$$G(z) = C(zI - A)^{-1}B + D$$

is **Strictly Positive Real (SPR)** if and only if

there exists $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

SPR state-space realization fact

Theorem: If $G(z) = C(zI - A)^{-1}B + D$ is SPR, then

$$D + D^T \succ 0$$

Proof: Choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

Note that

$$B^T P B - D - D^T \prec 0$$

$$\Rightarrow D + D^T \succ B^T P B \succeq 0$$



SPR TF is P-class

Let $G(z) = C(zI - A)^{-1}B + D$ be SPR

Then there exist positive definite functions

$$V(x) \succ 0 \quad \lambda_1(x, u) \succ 0$$

Such that any input $u(k)$ output $y(k)$ pair satisfies

$$\begin{aligned} \sum_{j=0}^k y^T(j)u(j) &= V(x(k+1)) - V(x(0)) + \sum_{j=0}^k \lambda_1(x(j), u(j)) \\ &\geq -\gamma_0^2 \quad \gamma_0^2 = V(x(0)) \end{aligned}$$

Shorthand notation

$$x(k) \rightarrow x_k$$

$$u(k) \rightarrow u_k$$

$$y(k) \rightarrow y_k$$

$$v(k) \rightarrow v_k$$

$$w(k) \rightarrow w_k$$

Proof

Let $G(z) = C(zI - A)^{-1}B + D$ be SPR

Choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

Define the Lyapunov function

$$V(x_k) = \frac{1}{2} x_k^T P x_k \succ 0$$

and the function

$$\lambda_1(x, u) = -\frac{1}{2} \begin{bmatrix} x \\ u \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} \succ 0$$

Proof

$$\begin{aligned}
 V(x_{k+1}) - V(x_k) &= \frac{1}{2}(Ax_k + Bu_k)^T P (Ax_k + Bu_k) - \frac{1}{2}x_k^T P x_k \\
 &= \frac{1}{2} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B \\ B^T P A & B^T P B \end{bmatrix} \begin{bmatrix} x_k \\ u_k \end{bmatrix} \\
 &= \frac{1}{2} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x_k \\ u_k \end{bmatrix} \\
 &\quad + \frac{1}{2} [u_k^T C x_k + u_k^T D u_k + u_k^T D^T u_k + x_k^T C^T u_k] \\
 &= -\lambda_1(x_k, u_k) + (Cx_k + Du_k)^T u_k \\
 &= -\lambda_1(x_k, u_k) + y_k^T u_k
 \end{aligned}$$

Proof

From the previous slide

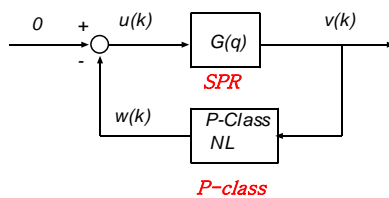
$$\begin{aligned}
 V(x_{k+1}) - V(x_k) &= -\lambda_1(x_k, u_k) + y_k^T u_k \\
 \Rightarrow y_k^T u_k &= V(x_{k+1}) - V(x_k) + \lambda_1(x_k, u_k)
 \end{aligned}$$

Summing both sides of the equation yields

$$\sum_{j=0}^k y_j^T u_j = V(x_{k+1}) - V(x_0) + \sum_{j=0}^k \lambda_1(x_j, u_j)$$

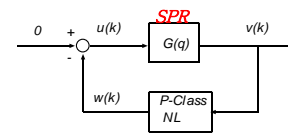
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Proof of the sufficiency part of the Asymptotic Hyperstability Theorem - Discrete Time



- Since the nonlinearity is P-class, $\sum_{j=0}^k w_j^T v_j \geq -\gamma_1^2$
- Since LTI block is SPR, we can use the choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$



Hyperstability

From the previous proof (SPR TF is P-class), we have

$$\sum_{j=0}^k v_j^T u_j = V(x_{k+1}) - V(x_0) + \sum_{j=0}^k \lambda_1(x_j, u_j)$$

where

$$V(x_k) = \frac{1}{2} x_k^T P x_k \succ 0$$

$$\lambda_1(x, u) = -\frac{1}{2} \begin{bmatrix} x \\ u \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} \succ 0$$

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Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

Rearranging terms,

$$V(x_{k+1}) = V(x_0) + \sum_{j=0}^k v_j^T u_j - \sum_{j=0}^k \lambda_1(x_j, u_j)$$

From the P-class nonlinearity:

$$\sum_{j=0}^k w_j^T v_j \geq -\gamma_1^2 \quad \Rightarrow \quad \sum_{j=0}^k v_j^T u_j \leq \gamma_1^2$$

Therefore,

$$V(x_{k+1}) \leq V(x_0) + \gamma_1^2 - \underbrace{\sum_{j=0}^k \lambda_1(x_j, u_j)}_{\geq 0} \leq V(x_0) + \gamma_1^2$$

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Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

From the previous slide

$$V(x_k) \leq V(x_0) + \gamma_1^2$$

$$\Rightarrow \frac{1}{2}x_k^T P x_k \leq \frac{1}{2}x_0^T P x_0 + \gamma_1^2$$

$$\Rightarrow \lambda_{\min}(P)\|x_k\|^2 \leq \lambda_{\max}(P)\|x_0\|^2 + 2\gamma_1^2$$

$$\Rightarrow \|x_k\|^2 \leq \frac{\lambda_{\max}(P)}{\lambda_{\min}(P)} \left(\|x_0\|^2 + \frac{2}{\lambda_{\max}(P)} \gamma_1^2 \right)$$

Therefore, the feedback system is hyperstable

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Asymptotic Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

$$0 \leq V(x_{k+1}) \leq V(x_0) + \gamma_1^2 - \sum_{j=0}^k \lambda_1(x_j, u_j)$$

$$\Rightarrow \underbrace{\sum_{j=0}^k \lambda_1(x_j, u_j)}_{\substack{\bullet \text{ monotonic nondecreasing sequence in } k \\ \bullet \text{ bounded above}}} \leq V(x_0) + \gamma_1^2$$

$$\Rightarrow \lim_{k \rightarrow \infty} \lambda_1(x_k, u_k) = 0 \quad \Rightarrow \quad \lim_{k \rightarrow \infty} x_k = 0, \quad \lim_{k \rightarrow \infty} u_k = 0$$

Therefore, the feedback system is asymptotically hyperstable

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Additional Result

$$G(z) = C(zI - A)^{-1}B + D$$

We have already shown that

$$\lim_{k \rightarrow \infty} x_k = 0, \quad \lim_{k \rightarrow \infty} u_k = 0$$

From this we see that

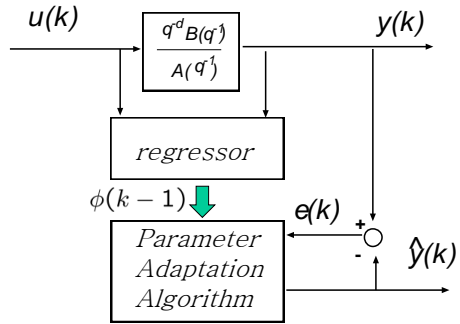
$$\lim_{k \rightarrow \infty} v_k = \lim_{k \rightarrow \infty} (C x_k + D u_k) = 0$$

$$\lim_{k \rightarrow \infty} w_k = \lim_{k \rightarrow \infty} (-u_k) = 0$$

Therefore, $x(k)$, $u(k)$, $v(k)$, and $w(k)$ converge to 0

Stability analysis of Series-parallel ID

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Series-Parallel ID Dynamics (review)

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a-posteriori error: $e(k) = y(k) - \hat{y}(k)$

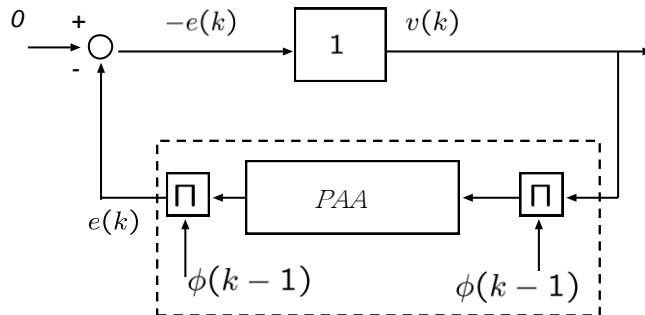
$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Series-Parallel ID Dynamics (review)

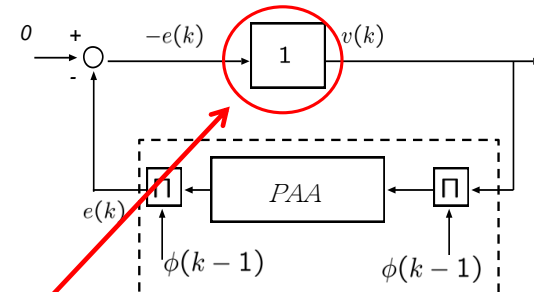
82



PAA: $\tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k-1)v(k)$

Stability analysis of Series-parallel ID

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Strictly Positive Real

How we implement the PAA

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1. $e^o(k) = y(k) - \phi^T(k-1)\hat{\theta}(k-1)$
2.
$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-1)F\phi(k-1)}$$
3. $\hat{\theta}(k) = \hat{\theta}(k-1) + F\phi(k-1)e(k)$

Stability analysis of Series-parallel ID

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We have shown that

$$e(k) \rightarrow 0$$

Now we will show that

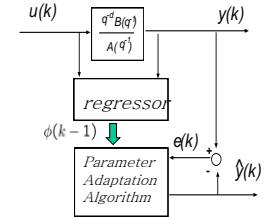
$$e^o(k) \rightarrow 0$$

Under the following assumptions:

$$|u(k)| < \infty \quad A(q^{-1}) \text{ is anti-Schur}$$

Since $y(k) = \frac{q^{-d}B(q^{-1})}{A(q^{-1})}u(k) \Rightarrow |y(k)| < \infty$

Since $\phi(k-1) = \begin{bmatrix} y(k-1) \\ \vdots \\ u(k-d) \\ \vdots \end{bmatrix} \Rightarrow \|\phi(k-1)\| < \infty$



Stability analysis of Series-parallel ID

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Thus, we know that

$$e(k) \rightarrow 0$$

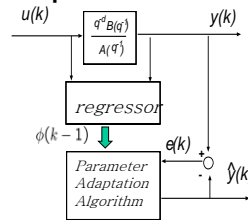
$$\|\phi(k-1)\| < \infty$$

Remember that

$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-1)F\phi(k-1)}$$

$$\Rightarrow e^o(k) = \underbrace{e(k)}_{\rightarrow 0} \underbrace{\{1 + \phi^T(k-1)F\phi(k-1)\}}_{< \infty}$$

$$\Rightarrow e^o(k) \rightarrow 0$$



Stability analysis of Series-parallel ID

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We have shown that

$$e(k) \rightarrow 0 \quad e^o(k) \rightarrow 0$$

$$\|\phi(k-1)\| < \infty$$

What about the parameter error $\tilde{\theta}(k)$?

since

$$\underbrace{e^o(k)}_{\rightarrow 0} = \phi^T(k-1)\tilde{\theta}(k-1) \Rightarrow |\phi^T(k)\tilde{\theta}(k)| \rightarrow 0$$

However, this **does not imply** that the parameter error goes to zero

We need to impose another condition on $u(k)$ to guarantee that the parameter error goes to zero. (**persistence of excitation**)

