

ME 233 Advance Control II

Lecture 23

Stability Analysis of a Direct Adaptive Control System

Deterministic SISO ARMA models

SISO ARMA model

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) u(k)$$

Where all inputs and outputs are scalars:

- $u(k)$ control input
- $y(k)$ output

d is the **known** pure time delay

Deterministic SISO ARMA models

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) u(k)$$

Where polynomials:

$$A(q^{-1}) = 1 + a_1 q^{-1} + \dots + a_n q^{-n}$$

$$B(q^{-1}) = b_o + b_1 q^{-1} + \dots + b_m q^{-m}$$

are co-prime

and $B(q^{-1})$ is Hurwitz

Control Objectives

1. Pole Placement: The poles of the closed loop system must be placed at specific locations in the complex plane.

- **Closed loop pole polynomial:**

$$A_c(q^{-1}) = B(q^{-1}) A'_c(q^{-1})$$

Where:

- $B(q^{-1})$ cancelable plant zeros
- $A'_c(q^{-1})$ monic Hurwitz polynomial chosen by the designer

$$A'_c(q^{-1}) = 1 + a'_{c1} q^{-1} + \dots + a'_{c n'_c} q^{-n'_c}$$

Control Objectives

2. Tracking: The output sequence $y(k)$ must follow a **reference** sequence $y_d(k)$ which is known

- Reference model:**

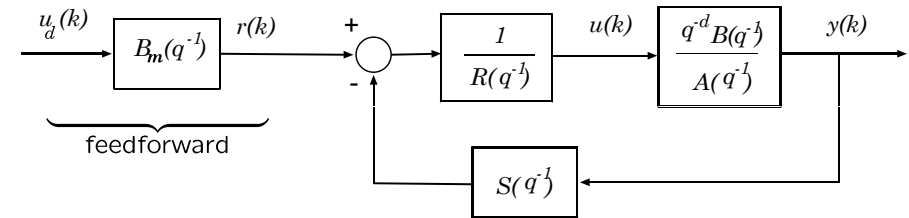
$$A'_c(q^{-1})y_d(k) = q^{-d} B_m(q^{-1}) u_d(k)$$

Where:

- $u_d(k)$ **known** reference input control input sequence
- $A'_c(q^{-1})$ monic Hurwitz polynomial chosen by the designer
- $B_m(q^{-1})$ zero polynomial, chosen by the designer

Control Law

- Feedback and feedforward actions:



$$u(k) = \frac{1}{R(q^{-1})} [r(k) - S(q^{-1})y(k)]$$

$$r(k) = B_m(q^{-1}) u_d(k) \quad \text{Feedforward (causal)}$$

Feedback Controller

Diophantine equation: Obtain polynomials $\underline{R'(q^{-1})}$, $\underline{S(q^{-1})}$ which satisfy:

$$A'_c(q^{-1}) = A(q^{-1}) \underline{R'(q^{-1})} + q^{-d} \underline{S(q^{-1})}$$

Close loop poles

Plant poles

Plant pure delays

$$\begin{aligned} R(q^{-1}) &= R'(q^{-1}) B(q^{-1}) \\ A_c(q^{-1}) &= B(q^{-1}) A'_c(q^{-1}) \end{aligned}$$

Controller parameters

Start with the Diophantine equation

$$A'_c(q^{-1}) = A(q^{-1}) R'(q^{-1}) + q^{-d} S(q^{-1})$$

Multiply both sides by $y(k)$

$$A'_c(q^{-1}) y(k) = R'(q^{-1}) A(q^{-1}) y(k) + q^{-d} S(q^{-1}) y(k)$$

Controller parameters

$$A'_c(q^{-1}) y(k) = R'(q^{-1}) \underbrace{A(q^{-1}) y(k)} + q^{-d} S(q^{-1}) y(k)$$

Insert plant dynamics

$$A(q^{-1}) y(k) = q^{-d} B(q^{-1}) u(k)$$

$$A'_c(q^{-1}) y(k) = q^{-d} [R'(q^{-1}) \underbrace{B(q^{-1}) u(k)} + S(q^{-1}) y(k)]$$

$$A'_c(q^{-1}) y(k) = q^{-d} [R(q^{-1}) u(k) + S(q^{-1}) y(k)]$$

Pole placement

Key Idea: Parameterize plant close-loop dynamics in terms of the controller parameters

$$\underbrace{A'_c(q^{-1}) y(k)} = q^{-d} [R(q^{-1}) u(k) + S(q^{-1}) y(k)]$$

Desired close loop polynomial (not including zeros)

- Plant must have minimum phase zeros

$B(q^{-1})$ must be **Hurwitz**

Controller parameters and regressor

$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = q^{-d} [\underbrace{R(q^{-1}) u(k) + S(q^{-1}) y(k)}]$$



$$\underbrace{r_o u(k) + \dots + r_{n_r} u(k - n_r) + s_o y(k) + \dots + s_{n_s} y(k - n_s)}$$

$$\begin{bmatrix} s_o & \dots & s_{n_s} & r_o & \dots & r_{n_r} \end{bmatrix}^T \begin{bmatrix} y(k) \\ \dots \\ y(k - n_s) \\ u(k) \\ \dots \\ u(k - n_r) \end{bmatrix}$$

Controller parameters and regressor

$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = q^{-d} [\underbrace{R(q^{-1}) u(k) + S(q^{-1}) y(k)}]$$



$$\begin{bmatrix} s_o & \dots & s_{n_s} & r_o & \dots & r_{n_r} \end{bmatrix}^T \underbrace{\begin{bmatrix} y(k) \\ \dots \\ y(k - n_s) \\ u(k) \\ \dots \\ u(k - n_r) \end{bmatrix}}_{\phi(k)} = \theta_c^T \phi(k)$$

$$\eta(k) = \phi^T(k - d) \theta_c$$

Control Objective

$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = q^{-d} \underbrace{\left[R(q^{-1}) u(k) + S(q^{-1}) y(k) \right]}_{\underbrace{A'_c(q^{-1}) y_d(k)}_{\eta_d(k)}}$$

Such that

$$\eta(k) = \eta_d(k)$$

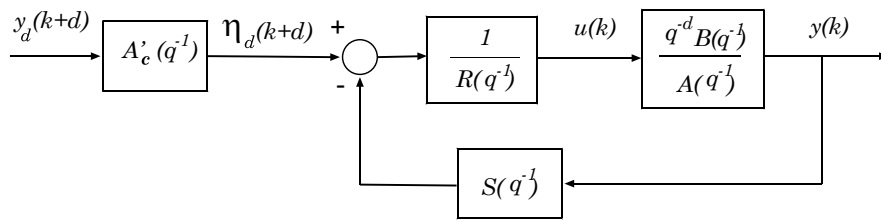
Control Law

$$A'_c(q^{-1}) y(k) = q^{-d} \underbrace{\left[R(q^{-1}) u(k) + S(q^{-1}) y(k) \right]}_{\underbrace{A'_c(q^{-1}) y_d(k)}_{\eta_d(k)}}$$

Control law:

$$\left[R(q^{-1}) u(k-d) + S(q^{-1}) y(k-d) \right] = \eta_d(k)$$

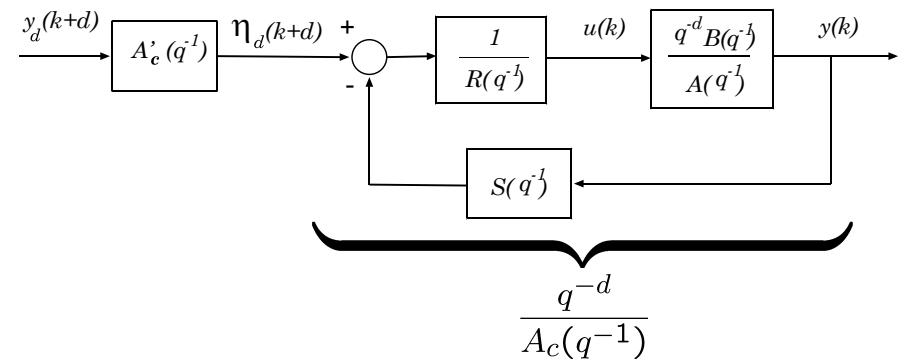
Control Law



$$\underbrace{\left[R(q^{-1}) u(k-d) + S(q^{-1}) y(k-d) \right]}_{A'_c(q^{-1}) y(k) = \eta(k)} = \eta_d(k)$$

$$A'_c(q^{-1}) y(k) = \eta(k)$$

Close loop dynamics



$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = \underbrace{A'_c(q^{-1}) y_d(k)}_{\eta_d(k)}$$

Control Law Implementation

$$A'_c(q^{-1}) y(k) = q^{-d} \underbrace{[R(q^{-1}) u(k) + S(q^{-1}) y(k)]}_{A'_c(q^{-1}) y_d(k)}$$

Control law:

$$R(q^{-1}) u(k) = \underbrace{A'_c(q^{-1}) y_d(k + d)}_{B_m(q^{-1}) u_d(k)} - S(q^{-1}) y(k)$$

$$B_m(q^{-1}) u_d(k) = r(k)$$

$$R(q^{-1}) u(k) = r(k) - S(q^{-1}) y(k)$$

PAA

$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = q^{-d} \underbrace{[R(q^{-1}) u(k) + S(q^{-1}) y(k)]}_{r_o u(k) + \dots + r_{n_r} u(k - n_r) + s_o y(k) + \dots + s_{n_s} y(k - n_s)}$$



$$\begin{bmatrix} s_o & \dots & s_{n_s} & r_o & \dots & r_{n_r} \end{bmatrix}^T \begin{bmatrix} y(k) \\ \dots \\ y(k - n_s) \\ u(k) \\ \dots \\ u(k - n_r) \end{bmatrix}$$

PAA

$$\underbrace{A'_c(q^{-1}) y(k)}_{\eta(k)} = q^{-d} \underbrace{[R(q^{-1}) u(k) + S(q^{-1}) y(k)]}_{\underbrace{\begin{bmatrix} s_o & \dots & s_{n_s} & r_o & \dots & r_{n_r} \end{bmatrix}^T}_{\theta_c^T} \underbrace{\begin{bmatrix} y(k) \\ \dots \\ y(k - n_s) \\ u(k) \\ \dots \\ u(k - n_r) \end{bmatrix}}_{\phi(k)}}$$

$$\eta(k) = \phi^T(k - d) \theta_c$$

PAA

Plant dynamics:

$$\eta(k) = \phi^T(k - d) \theta_c$$

RLS PAA:

$$e^o(k) = \eta(k) - \phi^T(k - d) \hat{\theta}_c(k - 1)$$

$$e(k + 1) = \frac{e^o(k + 1)}{1 + \phi^T(k - d + 1) F(k) \phi(k - d + 1)}$$

$$\hat{\theta}_c^o(k + 1) = \hat{\theta}_c(k) + F(k) \phi(k - d + 1) e(k + 1)$$

$$F(k + 1) = \frac{1}{\lambda_1(k)} \left[F(k) - \frac{F(k) \phi(k - d + 1) \phi^T(k - d + 1) F(k)}{\frac{\lambda_1(k)}{\lambda_2(k)} + \phi^T(k - d + 1) F(k) \phi(k - d + 1)} \right]$$

PAA projection

PAA: Projection

$$\hat{\theta}_c(k) = \begin{cases} \hat{\theta}_c^o(k) & \text{if } \hat{r}_o^o(k) \geq b_{\min o} \\ \left[\hat{s}_o^o(k) \cdots \hat{s}_{n_s}^o(k) \underset{\substack{\uparrow \\ \text{Replace } \hat{r}_o^o(k) \text{ by } b_{\min o} \text{ if it becomes too small.}}}{b_{\min o}} \cdots \hat{r}_{n_r}^o(k) \right]^T & \text{if } \hat{r}_o^o(k) < b_{\min o} \end{cases}$$

Control law will divide by $\hat{r}_o(k)$. Thus, the projection algorithm prevents the control action from becoming too large.

PAA Gain matrix

Gain matrix:

$$F(k+1) = \frac{1}{\lambda_1(k)} \left[F(k) - \frac{F(k)\phi_f(k-d+1)\phi_f^T(k-d+1)F(k)}{\frac{\lambda_1(k)}{\lambda_2(k)} + \phi_f^T(k-d+1)F(k)\phi_f(k-d+1)} \right]$$

$$0 < \lambda_1(k) \leq 1$$

$$0 \leq \lambda_2(k) < 2$$

are adjusted so that the maximum singular value of $F(k)$ is uniformly bounded, and

$$0 < K_{\min} \leq \lambda_{\min} \{F(k)\} \leq \lambda_{\max} \{F(k)\} < K_{\max} < \infty.$$

A-priori and a-posteriori errors

Plant dynamics:

$$\eta(k) = \phi^T(k-d)\theta_c$$

A-priori estimation error

$$e^o(k) = \underbrace{\eta(k)}_{\phi^T(k-d)\theta_c} - \phi^T(k-d)\hat{\theta}_c(k-1)$$

$$e^o(k) = \phi^T(k-d)\tilde{\theta}_c(k-1)$$

A-priori and a-posteriori errors

Plant dynamics:

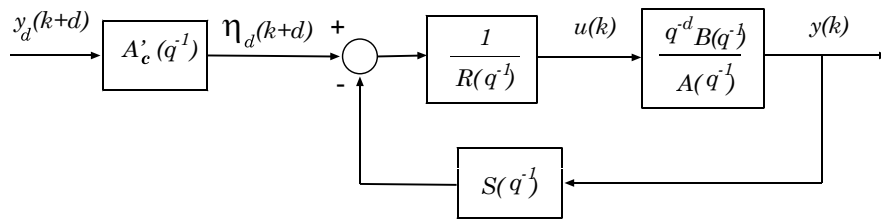
$$\eta(k) = \phi^T(k-d)\theta_c$$

A-posteriori estimation error

$$e(k) = \underbrace{\eta(k)}_{\phi^T(k-d)\theta_c} - \phi^T(k-d)\hat{\theta}_c(k)$$

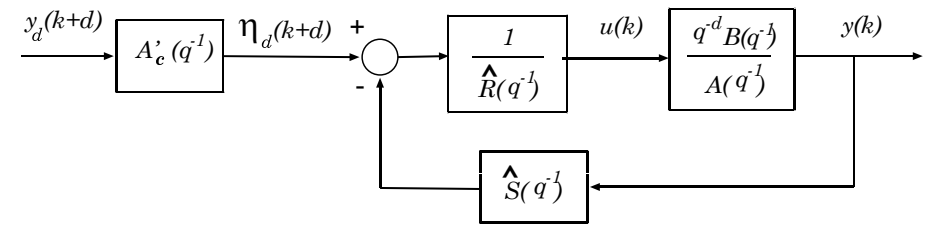
$$e(k) = \phi^T(k-d)\tilde{\theta}_c(k)$$

Control Law – Known Parameters



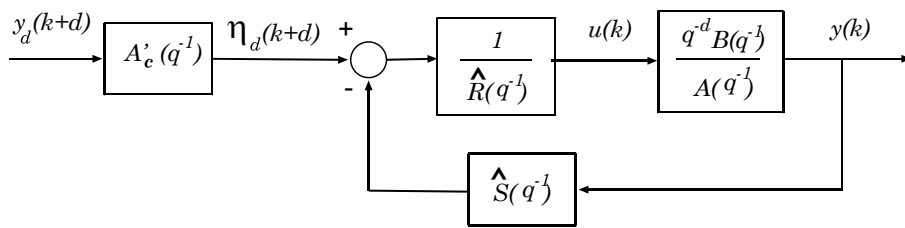
$$\eta_d(k+d) = \underbrace{\left[R(q^{-1}) u(k) + S(q^{-1}) y(k) \right]}_{\phi^T(k) \theta_c = \eta(k+d)}$$

Adaptive Control Law



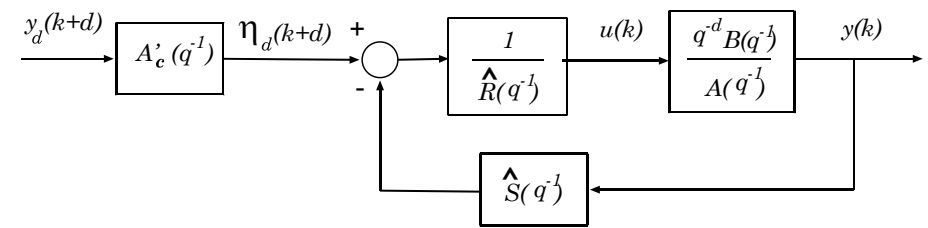
$$\eta_d(k+d) = \underbrace{\left[\hat{R}(q^{-1}, k) u(k) + \hat{S}(q^{-1}, k) y(k) \right]}_{\phi^T(k) \hat{\theta}_c(k)}$$

Adaptive Control Law



$$\eta_d(k+d) = \underbrace{\phi^T(k) \hat{\theta}_c(k)}_{\text{not necessarily } = \eta(k+d) \text{ why?}} = \underbrace{\phi^T(k) \theta_c}_{\text{not necessarily } = \eta(k+d) \text{ why?}}$$

Adaptive Control Objective



Filter tracking error:

$$\epsilon(k) = \eta(k) - \eta_d(k)$$

$$\boxed{\lim_{k \rightarrow \infty} \epsilon(k) = 0}$$

Filter error Dynamics

$$\epsilon(k) = \underbrace{\eta(k)}_{\phi^T(k-d)\theta_c} - \underbrace{\eta_d(k)}_{-\phi^T(k-d)\hat{\theta}_c(k-d)}$$

$$\underbrace{\phi^T(k-d) [\theta_c - \hat{\theta}_c(k-d)]}_{\tilde{\theta}_c(k-d)}$$

$$\epsilon(k) = \phi^T(k-d)\tilde{\theta}_c(k-d)$$

Adaptive Control with **Constant Gain**

Adaptive control algorithm:

1. $\eta(k) = A_c'(q^{-1}) y(k)$ **filtered output signal**
2. $e^o(k) = \eta(k) - \phi^T(k-d)\hat{\theta}_c(k-1)$ **a-priori error**
3.
$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-d)F\phi(k-d)}$$

$$\hat{\theta}_c(k) = \hat{\theta}_c(k-1) + F\phi(k-d) e(k)$$
} **PAA**
4. $\phi^T(k)\hat{\theta}_c(k) = \eta_d(k+d)$ **control action**

Notes on error terms

- **Parameter** error vector: $\tilde{\theta}_c(k) = \theta_c - \hat{\theta}_c(k)$

- **A-posteriori** output error:

$$e(k) = \phi(k-d)^T \tilde{\theta}_c(k)$$

- **A-priori** output error:

$$e^o(k) = \phi(k-d)^T \tilde{\theta}_c(k-1)$$

- **Tracking** filter error:

$$\epsilon(k) = \phi(k-d)^T \tilde{\theta}_c(k-d)$$

Adaptive Control with **RLS**

Adaptive control algorithm:

1. $\eta(k) = A_c'(q^{-1}) y(k)$ **filtered output signal**
2. $e^o(k) = \eta(k) - \phi^T(k-d)\hat{\theta}_c(k-1)$ **a-priori error**
3.
$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-d)F(k-1)\phi(k-d)}$$

$$\hat{\theta}_c(k) = \hat{\theta}_c(k-1) + F(k-1)\phi(k-d) e(k)$$
} **PAA**

$$F(k+1) = \frac{1}{\lambda_1(k)} \left[F(k) - \frac{F(k)\phi(k-d+1)\phi^T(k-d+1)F(k)}{\frac{\lambda_1(k)}{\lambda_2(k)} + \phi^T(k-d+1)F(k)\phi(k-d+1)} \right]$$
4. $\phi^T(k)\hat{\theta}_c(k) = \eta_d(k+d)$ **control action**

Stability Theorem

Under the conditions:

1. Model orders and delay: n , m and d are known
2. $B(q^{-1})$ is Hurwitz
3. Projections are used: $\hat{r}_o(k) \geq b_{\min o}$

$$0 < K_{\min} \leq \lambda_{\min} \{F(k)\} \leq \lambda_{\max} \{F(k)\} < K_{\max} < \infty.$$

The tracking error converges to zero.

$$\lim_{k \rightarrow \infty} \epsilon(k) = 0$$

Stability Theorem

Notice that the theorem **does not require**:

- control input be a-priori bounded

$$|u(k)| < \infty$$

- $A(q^{-1})$ be Hurwitz
- Persistence of excitation or parameter convergence
 $\tilde{\theta}_c(k) \rightarrow 0$

Stability Analysis Step 1

Prove that the a-posteriori error converges to zero using Hyperstability theory.

$$\lim_{k \rightarrow \infty} e(k) = 0$$

where,

$$e(k) = \phi^T(k-d) \tilde{\theta}_c(k)$$

$$e(k) = \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)}$$

Stability Analysis Step 2

Prove that the parameter error stops changing:

$$\lim_{k \rightarrow \infty} |\Delta \tilde{\theta}_c(k)| = \lim_{k \rightarrow \infty} |\tilde{\theta}_c(k) - \tilde{\theta}_c(k-1)| = 0$$

Note: $\Delta \tilde{\theta}_c(k) \rightarrow 0 \not\Rightarrow \tilde{\theta}_c(k) \rightarrow 0$

Stability Analysis Step 3

Prove that:

$$\lim_{k \rightarrow \infty} \frac{(e^o(k))^2}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

and

$$\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

Stability Analysis Step 3

- Note that the result in step 3:

$$\lim_{k \rightarrow \infty} \frac{(e^o(k))^2}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

is different (**stronger**) than the one in step 1:

$$\lim_{k \rightarrow \infty} e(k) = \lim_{k \rightarrow \infty} \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

Stability Analysis Step 4

Prove that the regressor vector is an **affine function** of the truncated infinity norm of the filtered tracking error

$$|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|.$$

For some finite **non-negative** constants C_1 and C_2

$$0 \leq C_1 < \infty$$

$$0 \leq C_2 < \infty$$

Goodwin's Key technical Lemma

We will use **Goodwin's Lemma** to prove that the filtered tracking error converges to zero

$$\lim_{k \rightarrow \infty} \epsilon(k) = 0$$

Therefore, since $A'_c(q^{-1})$ is Hurwitz

$$\lim_{k \rightarrow \infty} y(k) = y_d(k)$$

Goodwin's technical lemma

Given sequences $\epsilon(k) \in \mathcal{R}$ and $\phi(k) \in \mathcal{R}^n$

Under the conditions:

1. $\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k) |\phi(k-d)|^2} = 0 \quad 0 \leq b(k) < B < \infty$
2. $|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|. \quad \begin{matrix} 0 \leq C_1 < \infty \\ 0 \leq C_2 < \infty \end{matrix}$

Then:

$$\lim_{k \rightarrow \infty} \epsilon(k) = 0 \quad \text{and} \quad |\phi(k)| < \infty$$

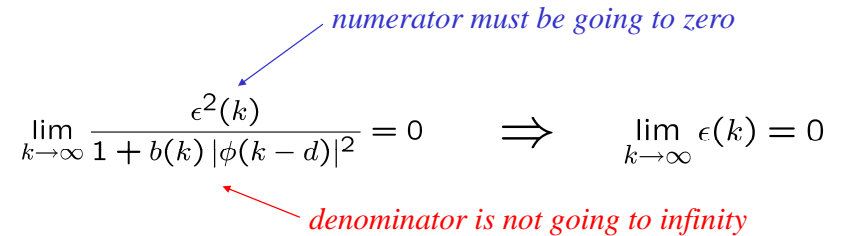
Goodwin's technical lemma

Proof:

Assume first that $|\epsilon(k)| < \infty \quad |\phi(k)| < \infty$

Then, $1 + b(k) |\phi(k-d)|^2 < \infty$

$$\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k) |\phi(k-d)|^2} = 0 \quad \Rightarrow \quad \lim_{k \rightarrow \infty} \epsilon(k) = 0$$



Goodwin's technical lemma

We will now that

$$\lim_{k \rightarrow \infty} |\epsilon(k)| = \infty \quad \Rightarrow \quad \lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k) |\phi(k-d)|^2} > 0$$

Goodwin's technical lemma

Assume that $\lim_{k \rightarrow \infty} |\epsilon(k)| = \infty$

there exists a subsequence $\{k_n\}$ of the sampling sequence $\{k\}$ such that

$$|\epsilon(k)| \leq |\epsilon(k_n)| \quad \text{for } k \leq k_n$$

Goodwin's technical lemma

Assume: $\lim_{k \rightarrow \infty} |\epsilon(k)| = \infty$

Then, since $|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|$.

along $\{k_n\}$

$$|\phi(k_n - d)| \leq C_1 + C_2 |\epsilon(k_n)|.$$

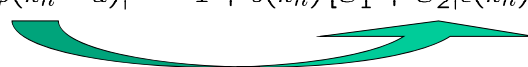
Goodwin's technical lemma

Assume: $\lim_{k \rightarrow \infty} |\epsilon(k)| = \infty$

Then, since $|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|$.

along $\{k_n\}$

$$\frac{\epsilon^2(k_n)}{1 + b(k_n) |\phi(k_n - d)|^2} \geq \frac{\epsilon^2(k_n)}{1 + b(k_n) [C_1 + C_2 |\epsilon(k_n)|]^2}$$

 smaller

Goodwin's technical lemma

$$\frac{\epsilon^2(k_n)}{1 + b(k_n) |\phi(k_n - d)|^2} \geq \frac{\epsilon^2(k_n)}{1 + b(k_n) [C_1 + C_2 |\epsilon(k_n)|]^2}$$

since $\lim_{k_n \rightarrow \infty} |\epsilon(k_n)| = \infty$ $0 \leq b(k) < B < \infty$

$$\begin{aligned} \lim_{k_n \rightarrow \infty} \frac{\epsilon^2(k_n)}{1 + b(k_n) |\phi(k_n - d)|^2} &\geq \lim_{k_n \rightarrow \infty} \frac{\epsilon^2(k_n)}{1 + b(k_n) [C_1 + C_2 |\epsilon(k_n)|]^2} \\ &\geq \lim_{\epsilon \rightarrow \infty} \frac{\epsilon^2}{1 + B [C_1 + C_2 |\epsilon|]^2} \end{aligned}$$

$$\begin{aligned} 0 &\leq C_1 < \infty \\ 0 &\leq C_2 < \infty \end{aligned}$$

$$\geq \frac{1}{BC_2^2} > 0$$

Goodwin's technical lemma

Thus, if $\lim_{k \rightarrow \infty} |\epsilon(k)| = \infty$

Then, $\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k) |\phi(k-d)|^2} > 0$

Therefore,

$$\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k) |\phi(k-d)|^2} = 0 \Rightarrow \begin{aligned} |\epsilon(k)| &< \infty \\ |\phi(k)| &< \infty \end{aligned}$$

\Rightarrow

$$\boxed{\lim_{k \rightarrow \infty} \epsilon(k) = 0}$$

Q.E.D

Stability Analysis

I will do the stability analysis using the constant gain PAA.

$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-d)F\phi(k-d)}$$

$$\tilde{\theta}_c(k) = \tilde{\theta}_c(k-1) + F\phi(k-d)e(k)$$

$$F = F^T \quad \text{and} \quad F > 0$$

The proof for the RLS PAA can be found in pages 52-65 of the ME233 part II class notes.

Stability Analysis Step 1

Prove that the a-posteriori error converges to zero using Hyperstability theory.

$$\lim_{k \rightarrow \infty} e(k) = 0$$

where,

$$e(k) = \phi^T(k-d)\tilde{\theta}_c(k)$$

$$e(k) = \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)}$$

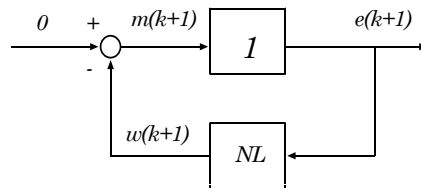
Stability Analysis Step 1

Proof: The proof is similar to the one that we did for the parallel identification system with constant gain:

- **Linear block 1:**

$$e(k) = \phi(k-d)\tilde{\theta}_c(k)$$

$$= m(k)$$



- **Nonlinear block NL:**

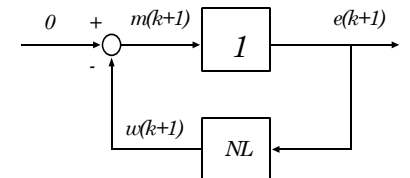
$$\tilde{\theta}_c(k) = \tilde{\theta}_c(k-1) - F\phi(k-d)e(k)$$

$$w(k) = -m(k) = -\tilde{\theta}_c(k)^T \phi(k-d)$$

Stability Analysis Step 1

We need to show that NL is a P-class

$$\sum_{j=1}^k w(j)e(j) \geq -\gamma_o^2$$



where

$$\tilde{\theta}_c(k) = \tilde{\theta}_c(k-1) - F\phi(k-d)e(k)$$

$$w(k) = -\tilde{\theta}_c(k)^T \phi(k-d)$$

Stability Analysis Step 1

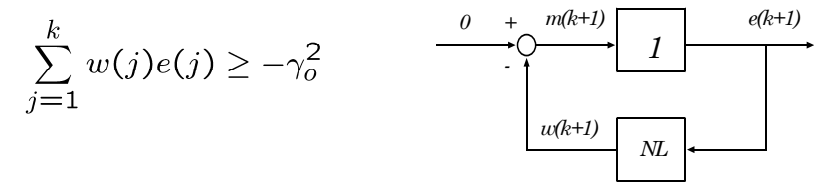
- Doing a bit of algebra we obtain:

$$w(k)e(k) = \tilde{\theta}_c(k)^T F^{-1} \underbrace{[\tilde{\theta}_c(k) - \tilde{\theta}_c(k-1)]}_{\Delta \tilde{\theta}_c(k)}$$

- Completing the squares,
(see the class notes on Lecture 20 for details)

$$\begin{aligned} w(k)e(k) &= \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \frac{1}{2} \tilde{\theta}_c(k-1)^T F^{-1} \tilde{\theta}_c(k-1) \\ &\quad + \frac{1}{2} \Delta \tilde{\theta}_c(k)^T F^{-1} \Delta \tilde{\theta}_c(k) \end{aligned}$$

Stability Analysis Step 1



Using the expression in the previous slide,

$$\begin{aligned} 2 \sum_{j=1}^k w(j)e(j) &= \sum_{j=1}^k \underbrace{\{\tilde{\theta}_c(j)^T F^{-1} \tilde{\theta}_c(j) - \tilde{\theta}_c(j-1)^T F^{-1} \tilde{\theta}_c(j-1)\}}_{\tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0)} \\ &\quad + \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) \end{aligned}$$

Stability Analysis Step 1

Therefore,

$$\begin{aligned} \sum_{j=1}^k w(j)e(j) &= \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \frac{1}{2} \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0) \\ &\quad + \frac{1}{2} \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) \end{aligned}$$

Since every term is a positive definite function,

$$\sum_{j=1}^k w(j)e(j) \geq -\gamma_o^2 \quad \gamma_o^2 = \frac{1}{2} \tilde{\theta}_c^T(0) F^{-1} \tilde{\theta}_c(0)$$

Stability Analysis Step 1

By the asymptotic Hyperstability theorem,

$$\lim_{k \rightarrow \infty} e(k) = 0$$

where

$$e(k) = \phi^T(k-d) \tilde{\theta}_c(k)$$

$$e(k) = \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)}$$

Q.E.D

Stability Analysis Step 2

Prove that the parameter error stops changing:

$$\lim_{k \rightarrow \infty} |\Delta \tilde{\theta}_c(k)| = \lim_{k \rightarrow \infty} |\tilde{\theta}_c(k) - \tilde{\theta}_c(k-1)| = 0$$

Note: $\Delta \tilde{\theta}_c(k) \rightarrow 0 \not\Rightarrow \tilde{\theta}_c(k) \rightarrow 0$

Stability Analysis Step 2

Prove that the parameter error stops changing.

Lets remember, from the analysis done to show that NL is P-class,

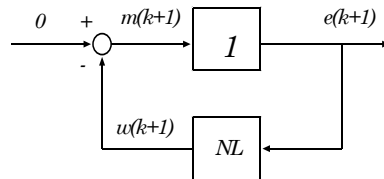
$$\begin{aligned} \sum_{j=1}^k w(j)e(j) &= \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \frac{1}{2} \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0) \\ &\quad + \frac{1}{2} \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) \end{aligned}$$

Stability Analysis Step 2

On the other hand, from the feedback loop and the linear block, we have

$$e(k) = -w(k)$$

and



$$\sum_{j=1}^k w(j)e(j) = - \sum_{j=1}^k e(j)e(j)$$

Stability Analysis Step 2

Therefore,

$$\begin{aligned} \underbrace{\sum_{j=1}^k w(j)e(j)}_{\downarrow} &= \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \frac{1}{2} \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0) \\ &\quad + \frac{1}{2} \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) \\ &= - \sum_{j=1}^k e(j)e(j) \end{aligned}$$

Stability Analysis Step 2

Combining,

$$\begin{aligned}
 -\sum_{j=1}^k e^2(j) &= \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) - \frac{1}{2} \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0) \\
 &\quad + \frac{1}{2} \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j)
 \end{aligned}$$

Rearranging terms,

$$\begin{aligned}
 \frac{1}{2} \sum_{j=1}^k \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) + \sum_{j=1}^k e^2(j) + \frac{1}{2} \tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k) &= \gamma_o^2 \\
 \gamma_o^2 &= \frac{1}{2} \tilde{\theta}_c(0)^T F^{-1} \tilde{\theta}_c(0)
 \end{aligned}$$

Stability Analysis Step 2

Notice that the expression below applies for all k

$$\frac{1}{2} \sum_{j=1}^k \underbrace{\Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j)}_{\geq 0} + \underbrace{\sum_{j=1}^k e^2(j)}_{\geq 0} + \frac{1}{2} \underbrace{\tilde{\theta}_c(k)^T F^{-1} \tilde{\theta}_c(k)}_{\geq 0} = \gamma_o^2$$

↑
bounded

Therefore, since all terms are non-negative,

$$\begin{aligned}
 \sum_{j=1}^{\infty} \Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j) &\leq \gamma_o^2 < \infty \\
 \sum_{j=1}^{\infty} e^2(j) &\leq \gamma_o^2 < \infty
 \end{aligned}$$

Stability Analysis Step 2

$$\sum_{j=1}^{\infty} \underbrace{\Delta \tilde{\theta}_c(j)^T F^{-1} \Delta \tilde{\theta}_c(j)}_{\geq 0} \leq \gamma_o^2 < \infty$$

$$\Rightarrow \lim_{k \rightarrow \infty} \Delta \tilde{\theta}_c(k)^T F^{-1} \Delta \tilde{\theta}_c(k) = 0$$

Since, $F = F^T$, $F > 0$ and $F^{-1} > 0$

$$\Rightarrow \boxed{\lim_{k \rightarrow \infty} |\Delta \tilde{\theta}_c(k)| = 0}$$

Q.E.D

Stability Analysis Step 2

Similarly, since

$$\sum_{j=1}^{\infty} e^2(j) \leq \gamma_o^2 < \infty$$

$$\Rightarrow \boxed{\lim_{k \rightarrow \infty} e(k) = 0}$$

We have proven the **sufficiency** portion of the **Asymptotic Hyperstability Theorem**, when the linear block is an identity.

So far we have:

$$1. \quad e(k) \rightarrow 0 \quad \not\Rightarrow \begin{cases} e^o(k) \rightarrow 0 \\ \epsilon(k) \rightarrow 0 \end{cases}$$



$$\frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} \rightarrow 0$$

$$2. \quad |\Delta \tilde{\theta}_c(k)| \rightarrow 0$$

Stability Analysis Step 3

Prove that:

$$\lim_{k \rightarrow \infty} \frac{(e^o(k))^2}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

and

$$\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

Stability Analysis Step 3

- Note that this result:

$$\lim_{k \rightarrow \infty} \frac{(e^o(k))^2}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

is stronger than the one in step 1:

$$\lim_{k \rightarrow \infty} e(k) = \lim_{k \rightarrow \infty} \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1) \phi(k-d)} = 0$$

Stability Analysis Step 3

From the PAA we have

$$\hat{\theta}_c(k) = \hat{\theta}_c(k-1) + F\phi(k-d) e(k)$$

Which implies

$$\hat{\theta}_c(k) - \hat{\theta}_c(k-1) = F\phi(k-d) e(k)$$

$$\Delta \hat{\theta}_c(k) = F\phi(k-d) e(k)$$

$$\Delta \tilde{\theta}_c(k) = -F\phi(k-d) e(k)$$

Stability Analysis Step 3

Inserting $\Delta\tilde{\theta}_c(k) = -F\phi(k-d)e(k)$

Into $\lim_{k \rightarrow \infty} \Delta\tilde{\theta}_c(k)^T F^{-1} \Delta\tilde{\theta}_c(k) = 0$

We obtain

$$\lim_{k \rightarrow \infty} \phi^T(k-d)F(k-1)\phi(k-d)e^2(k) = 0$$

Adding $\lim_{k \rightarrow \infty} e(k) = 0$ we obtain

$$\lim_{k \rightarrow \infty} [1 + \phi^T(k-d)F(k-1)\phi(k-d)]e^2(k) = 0$$

Stability Analysis Step 3

From

$$\lim_{k \rightarrow \infty} [1 + \phi^T(k-d)F(k-1)\phi(k-d)]e^2(k) = 0$$

And the fact that

$$e(k) = \frac{e^o(k)}{1 + \phi(k-d)^T F(k-1)\phi(k-d)}$$

we obtain our first result

$$\lim_{k \rightarrow \infty} \frac{(e^o(k))^2}{1 + \phi(k-d)^T F(k-1)\phi(k-d)} = 0$$

Stability Analysis Step 3

To prove the second result

$$\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + \phi(k-d)^T F(k-1)\phi(k-d)} = 0$$

We use $\epsilon(k) = \phi(k-d)^T \tilde{\theta}_c(k-d)$

and add and subtract: $e^o(k) = \phi(k-d)^T \tilde{\theta}_c(k-1)$

$$\epsilon(k) = e^o(k) - \phi(k-d)^T [\tilde{\theta}_c(k-1) - \tilde{\theta}_c(k-d)]$$

Stability Analysis Step 3

Notice that,

$$|\tilde{\theta}_c(k-1) - \tilde{\theta}_c(k-d)| = |\Delta\tilde{\theta}_c(k-1) + \dots + \Delta\tilde{\theta}_c(k-d+1)|$$

$$\leq |\Delta\tilde{\theta}_c(k-1)| + \dots + |\Delta\tilde{\theta}_c(k-d+1)|$$

Thus, for a finite d, since

$$\lim_{k \rightarrow \infty} |\Delta\tilde{\theta}_c(k)| = 0$$

$$\Rightarrow \lim_{k \rightarrow \infty} |\tilde{\theta}_c(k-1) - \tilde{\theta}_c(k-d)| = 0$$

Stability Analysis Step 3

From

$$\epsilon(k) = e^o(k) - \phi(k-d)^T [\tilde{\theta}_c(k-1) - \tilde{\theta}_c(k-d)]$$

we obtain

$$\begin{aligned} \frac{\epsilon(k)}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}} &= \frac{e^o(k)}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}} \\ &\quad - \underbrace{\frac{\phi(k-d)^T [\hat{\theta}_c(k-1) - \hat{\theta}_c(k-d)]}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}}}_{\rightarrow 0} \end{aligned}$$

Stability Analysis Step 3

Also, using Schwartz inequality

$$\begin{aligned} \left| \frac{\phi(k-d)^T [\hat{\theta}_c(k-1) - \hat{\theta}_c(k-d)]}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}} \right| &\leq \underbrace{\frac{|\phi(k-d)|}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}}}_{\leq \frac{1}{\lambda_{\min}^{1/2}(F)} < \infty} \underbrace{|\hat{\theta}_c(k-1) - \hat{\theta}_c(k-d)|}_{\rightarrow 0} \\ &\leq \frac{1}{\lambda_{\min}^{1/2}(F)} < \infty \quad \rightarrow 0 \end{aligned}$$

therefore

$$\lim_{k \rightarrow \infty} \left| \frac{\phi(k-d)^T [\hat{\theta}_c(k-1) - \hat{\theta}_c(k-d)]}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}} \right| = 0$$

Stability Analysis Step 3

Since,

$$\begin{aligned} \frac{\epsilon(k)}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}} &= \underbrace{\frac{e^o(k)}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}}}_{\rightarrow 0} \\ &\quad - \underbrace{\frac{\phi(k-d)^T [\hat{\theta}_c(k-1) - \hat{\theta}_c(k-d)]}{(1 + \phi^T(k-d)F\phi(k-d))^{\frac{1}{2}}}}_{\rightarrow 0} \end{aligned}$$

Thus

$$\boxed{\lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + \phi^T(k-d)F\phi(k-d)} = 0}$$

Q.E.D

Stability Analysis Step 4

Prove that the regressor vector is an **affine function** of the truncated infinity norm of the filtered tracking error

$$|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|.$$

For some finite **non-negative** constants C_1 and C_2

$$0 \leq C_1 < \infty$$

$$0 \leq C_2 < \infty$$

Stability Analysis Step 4

The full proof is in pages 61-65 of ME233 class notes part II.

The proof utilizes:

1) Triangle inequality:

$$a = b + c \Rightarrow |a| \leq |b| + |c|$$

Stability Analysis Step 4

The full proof is in pages 61-65 of ME233 class notes part II.

The proof utilizes:

2) BIBO stability of linear asymptotically stable systems

$$u(k-d) = \frac{A(q^{-1})}{B(q^{-1})} y(k) \quad \text{Where } B(q^{-1}) \text{ is Hurwitz}$$

$$|u(k-d)| \leq K_1 + K_2 \max_{j \in [0, k]} |y(j)|$$

For some bounded non-negative constants

$$0 \leq K_1 < \infty$$

$$0 \leq K_2 < \infty$$

Stability Analysis Step 4

We want to show that: $|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|$.

For simplicity, let's assume that

$$\phi(k-d) = \begin{bmatrix} y(k-d) & u(k-d) \end{bmatrix}^T$$

Then, using the Euclidean norm,

$$|\phi(k-d)|^2 = |y(k-d)|^2 + |u(k-d)|^2$$

$$|\phi(k-d)| \leq |y(k-d)| + |u(k-d)|$$

Stability Analysis Step 4

We have $|\phi(k-d)| \leq |y(k-d)| + |u(k-d)|$

- Now we use the fact that $B(q^{-1})$ is **Hurwitz**

$$|u(k-d)| \leq K_1 + K_2 \max_{j \in [0, k]} |y(j)|$$

Therefore

$$|\phi(k-d)| \leq |y(k-d)| + K_1 + K_2 \max_{j \in [0, k]} |y(j)|$$

Notice that $|y(k-d)| \leq \max_{j \in [0, k]} |y(j)|$

Stability Analysis Step 4

Therefore, setting $K_3 = K_2 + 1$

$$|\phi(k-d)| \leq K_1 + K_3 \max_{j \in [0, k]} |y(j)|$$

- Now we use the fact that $A'_c(q^{-1})$ is **Hurwitz**

$$y(k) = \frac{1}{A'_c(q^{-1})} \eta(k)$$

Therefore,

$$|y(k)| \leq L_1 + L_2 \max_{j \in [0, k]} |\eta(j)|$$

For some bounded
non-negative constants

$$L_1 \quad L_2$$

Stability Analysis Step 4

Therefore, setting $J_1 = K_1 + K_3 L_1$ and $J_2 = K_3 L_2$

$$|\phi(k-d)| \leq J_1 + J_2 \max_{j \in [0, k]} |\eta(j)|$$

- Now we use the triangle inequality.

$$\epsilon(k) = \eta(k) - \eta_d(k) \implies |\eta(k)| \leq |\epsilon(k)| + |\eta_d(k)|$$

Since the desired filter trajectory, $\eta_d(k)$, is bounded,

Define: $J_4 = \max_{j \in [0, \infty)} |\eta_d(k)|$

Stability Analysis Step 4

Therefore,

$$|\phi(k-d)| \leq J_1 + J_2 \max_{j \in [0, k]} |\eta(j)|$$

$$\max_{j \in [0, k]} |\eta(j)| \leq \max_{j \in [0, k]} |\epsilon(j)| + J_4$$

Setting, $C_1 = J_1 + J_2 J_4$ and $C_2 = J_2$ we obtain:

$$|\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|.$$

Q.E.D

What do we have so far?

$$1. \quad \frac{\epsilon^2(k)}{1 + \phi^T(k-d)F(k-1)\phi(k-d)} \rightarrow 0$$

$$\epsilon(k) = \eta(k) - \eta_d(k) = A'_c(q^{-1})(y(k) - y_d(k))$$

$$2. \quad |\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|.$$

$$0 \leq C_1 < \infty$$

$$0 \leq C_2 < \infty$$

Notice that

$$\phi^T(k-d)F(k-1)\phi(k-d) \leq \lambda_{\max}(F) |\phi(k-d)|^2$$

Therefore, defining $b = \lambda_{\max}(F) < \infty$

$$\underbrace{\frac{\epsilon^2(k)}{1 + \phi^T(k-d)F(k-1)\phi(k-d)}}_{\rightarrow 0} \geq \underbrace{\frac{\epsilon^2(k)}{1 + b|\phi(k-d)|^2}}_{\rightarrow 0}$$

Thus we have shown

$$1. \quad \frac{\epsilon^2(k)}{1 + b|\phi(k-d)|^2} \rightarrow 0 \quad 0 < b < \infty$$

$$2. \quad |\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|.$$

$$0 \leq C_1 < \infty$$

$$0 \leq C_2 < \infty$$

Stability Analysis **Step 5**

Finally, we will use **Goodwin's Lemma**

$$\lim_{k \rightarrow \infty} \epsilon(k) = 0$$

Therefore, since $A'_c(q^{-1})$ is Hurwitz

$$\lim_{k \rightarrow \infty} y(k) = y_d(k)$$

Goodwin's technical lemma

Given sequences $\epsilon(k) \in \mathcal{R}$ and $\phi(k) \in \mathcal{R}^n$

Under the conditions:

$$1. \quad \lim_{k \rightarrow \infty} \frac{\epsilon^2(k)}{1 + b(k)|\phi(k-d)|^2} = 0 \quad 0 \leq b(k) < B < \infty$$

$$2. \quad |\phi(k-d)| \leq C_1 + C_2 \max_{j \in [0, k]} |\epsilon(j)|. \quad \begin{array}{l} 0 \leq C_1 < \infty \\ 0 \leq C_2 < \infty \end{array}$$

Then:

$$\lim_{k \rightarrow \infty} \epsilon(k) = 0 \quad \text{and} \quad |\phi(k)| < \infty$$