

Bode approximation example

transfer function

$$\text{Suppose } H(s) = \frac{2000(s/500)}{s + 200} \quad \leftarrow \text{produce Bode approximation of frequency response } H(j\omega)$$

SOL'N

First, we need to write $H(s)$ in proper Bode approximation form:

$$H(s) = \frac{2000(s/500)}{s + 200} = \frac{10}{s/200 + 1} = \frac{10(s/500)}{(1 + s/200)} \quad \begin{array}{l} K, \text{ gain term} \\ \downarrow \\ 200 \text{ at DC, with } 0\text{dB crossing of } 500 \text{ rps} \\ \text{pole at } 200 \text{ rps.} \end{array}$$

Note that we could also factor the 500 out of the zero at DC term & work with $H(s) = \frac{1/50}{(s/1)} / (1 + s/200)$, but $K \ll 1$ in this case...

OR, we could "fold" the $K=10$ term into the zero at DC & work with $H(s) = \frac{s/50}{(1 + s/200)}$; we have options!

$$\text{Now, } H(s) = \frac{10(s/500)}{(1 + s/200)}$$

3 terms; We will plot out approximations of the Bode responses of these 3 terms first, then combine as a final step

* K , gain term
 $20\log_{10}(K) = 20\text{dB}$

$K > 0$,
 So 0° phase shift.
 (if $K < 0$, then $\pm 180^\circ$ phase shift)

K_{dB}

$\angle K$, deg.

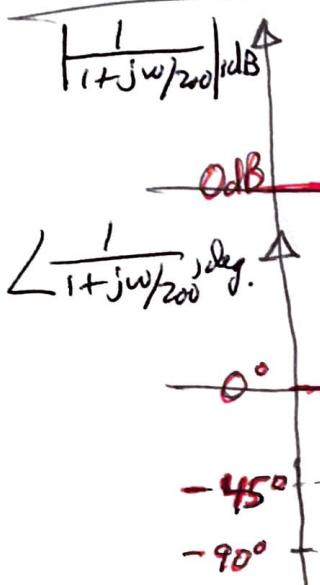
0°

$\log \omega$

$\log \omega$

(cont'd)

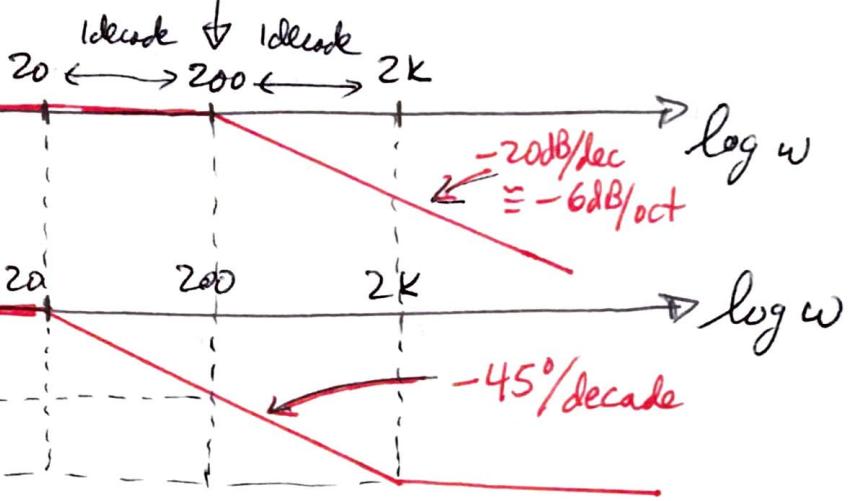
* pole @ 200rps term



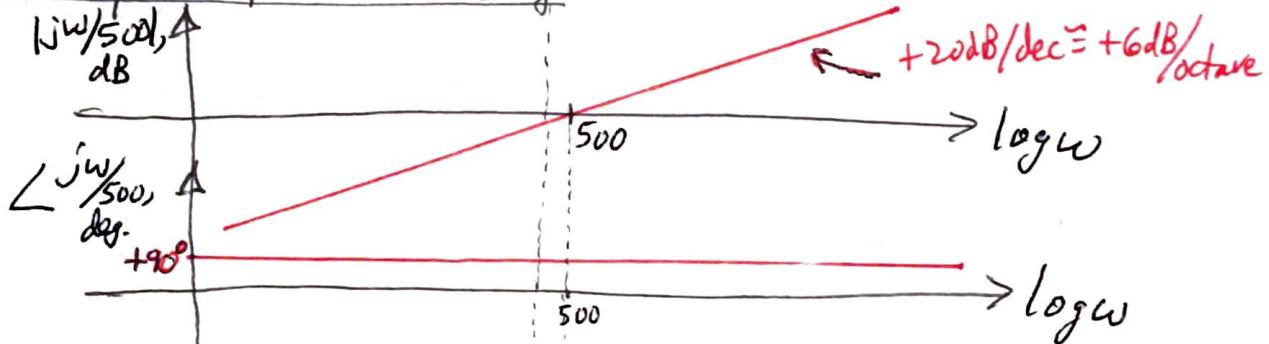
<New for Sp. 2021>

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pole = 200rps



④ zero @ DC w/ 500rps 0dB crossing



→ Let's combine pole and zero @ DC magnitudes first → they add in dB, because $\log_{10}(xy) = \log_{10}(x) + \log_{10}(y)$

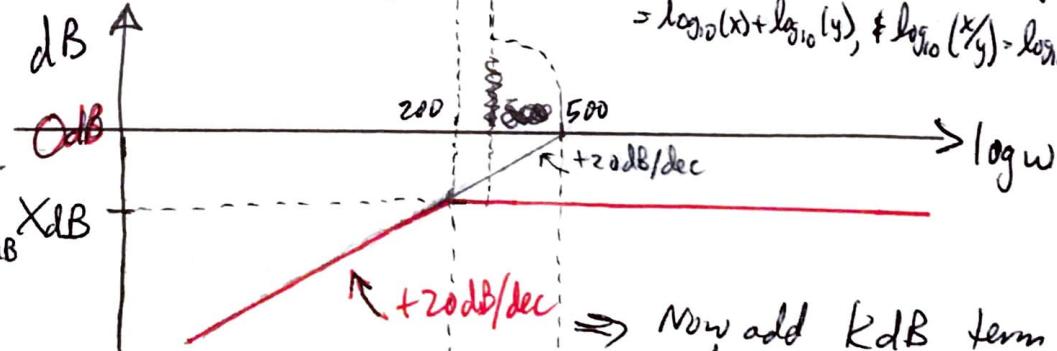
$$\log_{10}\left(\frac{x}{y}\right) = \log_{10}(x) - \log_{10}(y)$$

of decades between 200 & 500: $\log_{10}\left(\frac{500}{200}\right) \approx 0.398 \text{ dec.}$

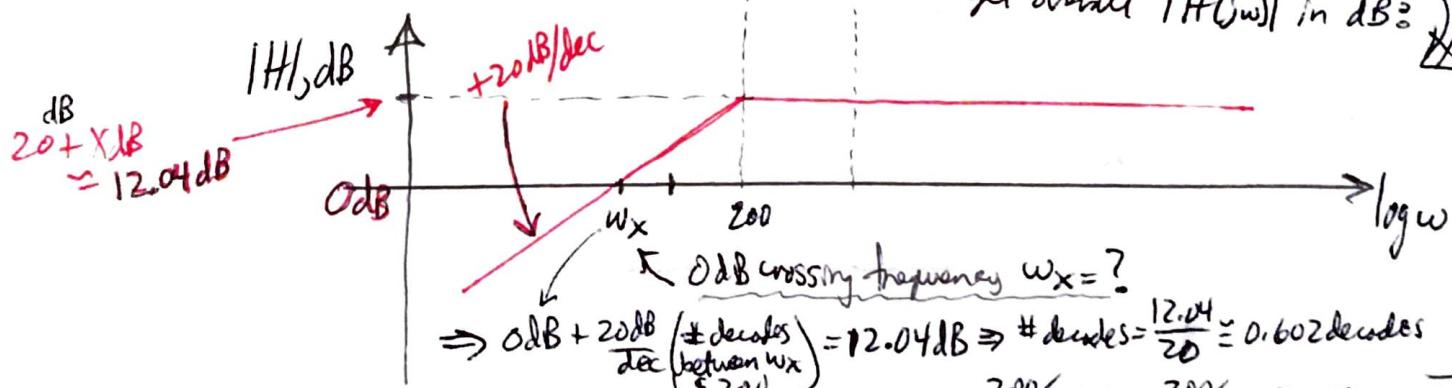
$$\log_{10}\left(\frac{500}{200}\right) \approx 0.398 \text{ dec.}$$

$$X_{dB} + \frac{20 \text{ dB}}{\text{dec}} (0.398 \text{ dec}) = 0 \text{ dB}$$

$$\Rightarrow X_{dB} \approx -7.96 \text{ dB}$$



Now add KdB term to get overall $|H(jw)|$ in dB



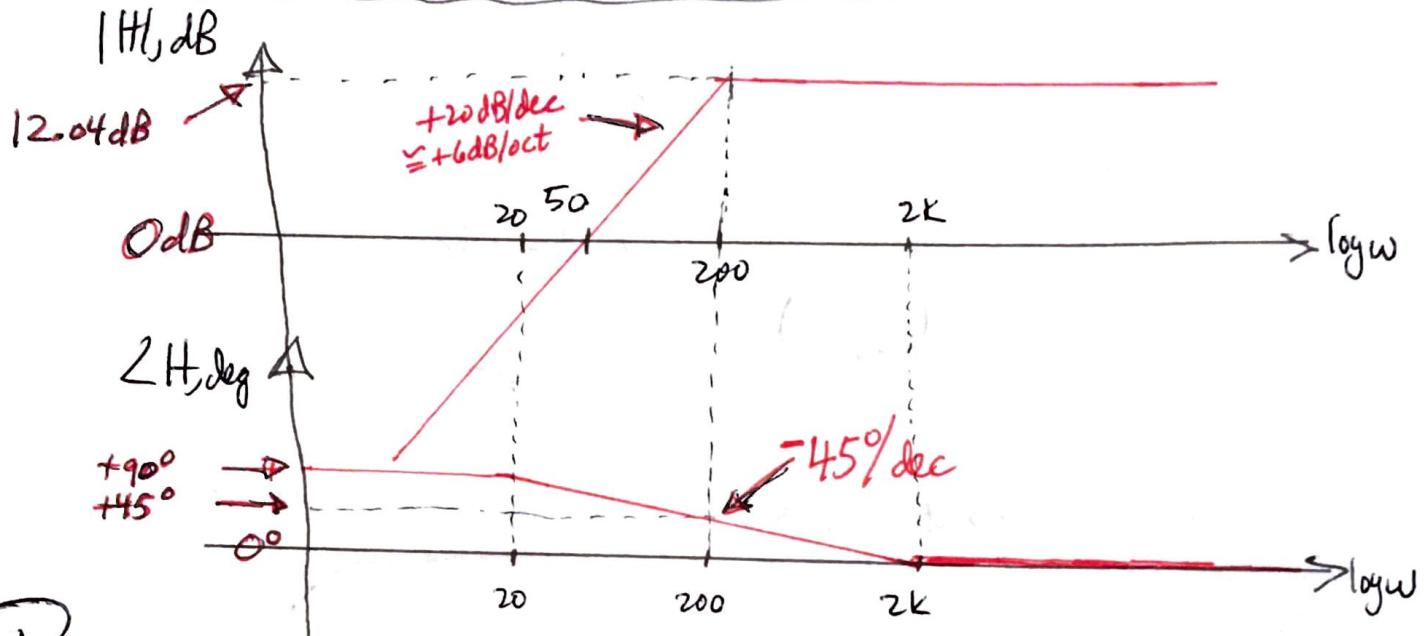
0dB crossing frequency $w_x = ?$

$$\Rightarrow 0 \text{ dB} + \frac{20 \text{ dB}}{\text{dec}} (\# \text{decades between } w_x \text{ and } 200) = 12.04 \text{ dB} \Rightarrow \# \text{decades} = \frac{12.04}{20} \approx 0.602 \text{ decades}$$

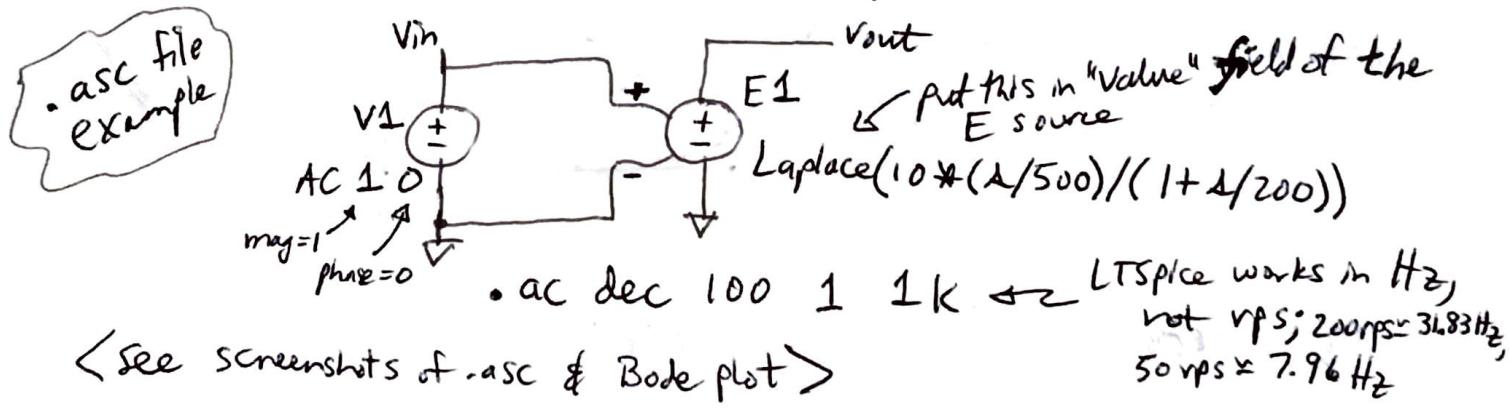
$$\Rightarrow \log_{10}\left(\frac{200}{w_x}\right) = 0.602 \Rightarrow w_x = \frac{200}{10^{0.602}} \approx 200^{\frac{1}{4}} = 50 \text{ rps}$$

(cont'd)

→ The overall approximate phase response for $H(j\omega)$ is obtained by shifting the pole phase up by 90° (due to the phase of the zero at DC); the K term is positive, so has 0° phase contribution; here is the total Bode approximation of $H(j\omega)$, for completeness:



→ Can confirm approximation w/ high-accuracy LTSpice simulation; if you have the circuit, you can simulate that; if you have $H(s)$, you can use the "Laplace" VCVS (E source); e.g.,



- Errors in the approximation relative to the high-accuracy results
- ⇒ Actual phase response has more curvature
- ⇒ The magnitude response has a 3dB error at the pole frequency

More on "3dB" errors at pole/zero frequencies:

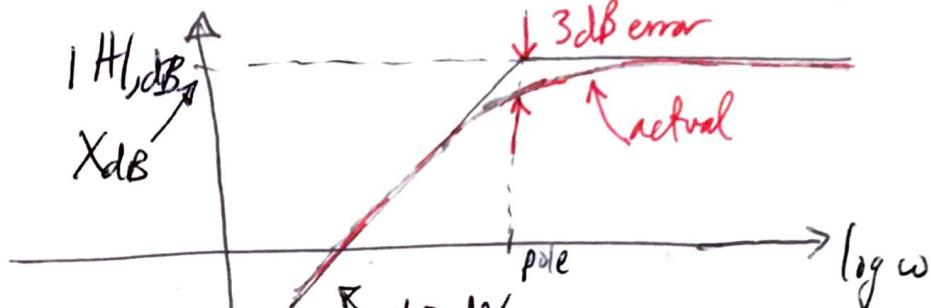
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* "3dB" errors in the approximation at pole frequencies \Rightarrow

Why is this a pole?

Poles cause magnitude response

to decrease after the pole, relative to the preceding trend. (i.e., $+20\text{dB/dec} \rightarrow$ flat response)



pole causes $+20\text{dB/dec}$; approximation

\Rightarrow here, the actual $|H|, \text{dB}$ is $X_{\text{dB}} - 3\text{dB}$ at the pole frequency

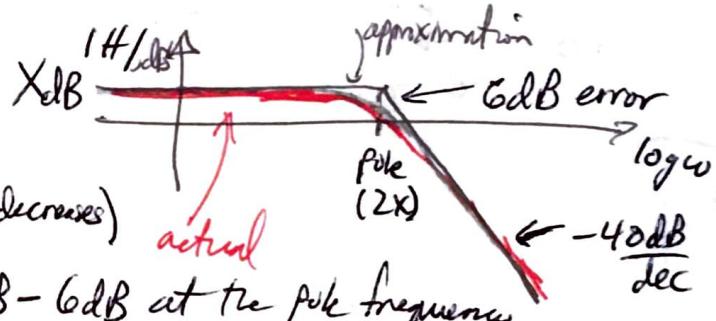
\Rightarrow if the trend (preceding) the pole is $(\frac{+20\text{dB}}{\text{dec}})^n$, n integer, $n \geq 1$,

Then the error of the approximation relative to the actual will be $-n 3\text{dB}$ at the pole.

\Rightarrow Another pole scenario \Rightarrow

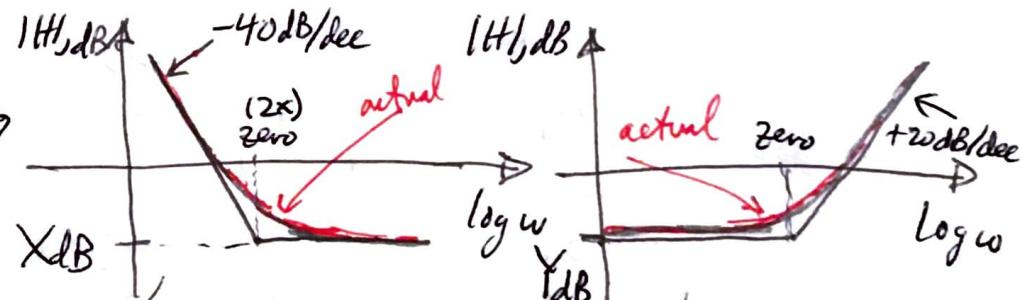
(we know it's a pole because $|H|$ decreases)

Here, the actual $|H|, \text{dB}$ is $X_{\text{dB}} - 6\text{dB}$ at the pole frequency.



* "3dB" errors in the approximation at zero \Rightarrow

two example scenarios



Here, the actual $|H|, \text{dB}$ is $X_{\text{dB}} + 6\text{dB}$ at the zero frequency

here, the actual $|H|, \text{dB}$ is $Y_{\text{dB}} + 3\text{dB}$ at the zero frequency

basic idea: if the trend (preceding) the zero is $(\frac{-20\text{dB}}{\text{dec}})^n$, n integer, $n \geq 1$,

then the error of the approximation relative to the actual will be $+n 3\text{dB}$ at the zero.

#2

→ Can also confirm Bode approximation w/ high-accuracy Matlab simulation.

option
(a) can

⇒ Write $H(s)$ in the following form:

$$H(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$$

numerator polynomial in s ,
order m

denominator polynomial in s ,
order n

⇒ Store coefficients for the two polynomials in two vectors,
say num & den:

$$\text{num} = [b_m \ b_{m-1} \ \dots \ b_1 \ b_0];$$

$$\text{den} = [a_n \ a_{n-1} \ \dots \ a_1 \ a_0], \text{ say } H,$$

⇒ create a transfer function object using tf:

$$H = \text{tf}(\text{num}, \text{den});$$

⇒ have Matlab plot out Bode response:
bode(H)

⇒ can optionally tell Matlab to plot Bode response over some specific range or rad/sec values; e.g.,

$$w_{\min} = 10; \quad w_{\max} = 1e4;$$

$$\text{bode}(H, \{w_{\min}, w_{\max}\})$$

Option
(b)

⇒ create transfer function object $H = \text{tf}'(s')$

⇒ then specify transfer function directly as expression in s ; e.g.,

$$H = (s+1)/(s^2 + 3*s + 1);$$

⇒ then plot Bode response with bode(H) (or bode(H, {wmin, wmax})),
as above

→ For the example we are working on here
 (starting on p. 46), we have:

$$H(s) = \frac{10(\frac{s}{500})(\frac{500}{s})}{(1 + \frac{s}{200})(\frac{500}{s})} = \frac{10s}{2.5s + 500} = \frac{10s + 0}{2.5s + 500}$$

⇒ using option(a) on previous page, we have in Matlab:

$$\text{num} = [10 \ 0]; \quad \text{den} = [2.5 \ 500];$$

$$H = \text{tf}(\text{num}, \text{den});$$

$$\text{bode}(H)$$

⇒ if ran in class, note the very good agreement between Bode approximation & actual Bode response in Matlab

⇒ See help bode in Matlab for more details

⟨ Note that help(function) is very useful for your future courses/career, too! ⟩

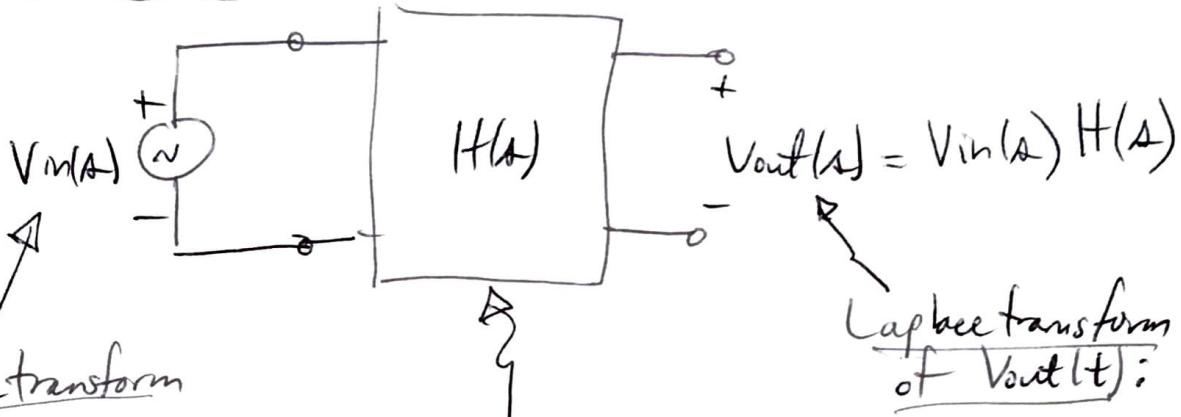
→ Another Matlab bode example: plot Bode response of

$$H(s) = \frac{s^2 + 0.1s + 7.5}{s^4 + 0.12s^3 + 9s^2}$$

⇒ In Matlab, do:

$$H = \text{tf}([1 \ 0.1 \ 7.5], [1 \ 0.12 \ 9 \ 0 \ 0]); \\ \text{bode}(H)$$

A?, $j\omega$?, $H(s)$?, phasors? week 14 discussion SP. 2021
ELEN2425



Laplace transform of $V_{in}(t)$:

$$V_{in}(s) = \mathcal{L}\{V_{in}(t)\}$$

Laplace transform of ckt/system

impulse response $h(t)$:

$$H(s) = \mathcal{L}\{h(t)\}$$

(System poles & zeros in the complex s-plane)

Laplace transform of $V_{out}(t)$:

$$V_{out}(s) = \mathcal{L}\{V_{out}(t)\}$$

(more on $h(t)$ in Signals & Systems)

→ Setting $s=j\omega$ yields the Fourier transform of the signal of interest:
↑ frequency response

$$V_{in}(j\omega) = \mathcal{F}\{V_{in}(t)\}, \quad H(j\omega) = \mathcal{F}\{h(t)\}, \quad V_{out}(j\omega) = \mathcal{F}\{V_{out}(t)\} \\ \text{(System frequency response)} \quad = V_{in}(j\omega) H(j\omega)$$

→ In the specific case of sinusoidal signals, the Fourier transform of the time-domain signal can be viewed as a phasor; e.g.,

$$V_{in}(j\omega) = \tilde{V}_{in}, \quad V_{out}(j\omega) = \tilde{V}_{out}, \quad \text{where} \\ \tilde{V}_{out} = \tilde{V}_{in} H(j\omega)$$

>Note that the connection between Fourier transforms & phasors of sinusoidal signals can be somewhat nuanced; this is essentially the main idea. (For sinusoids, the phasor transform & Fourier transform are essentially two different ways of representing the same information.)