

Bode approximation example

transfer function

Suppose $H(s) = \frac{2000(s/500)}{s + 200}$ ← produce Bode approximation of frequency response $H(j\omega)$

SOL'N

First, we need to write $H(s)$ in proper Bode approximation form:

$$H(s) = \frac{2000(s/500)}{s + 200} = \frac{\cancel{2000}^{10}(s/500)}{\cancel{200}^{200}(s/200 + 1)} = \frac{10(s/500)}{(1 + s/200)}$$

$K, \text{ gain term}$ → 10
 \swarrow zero at DC, with 0dB crossing at 500 rps
 \searrow pole at 200 rps.

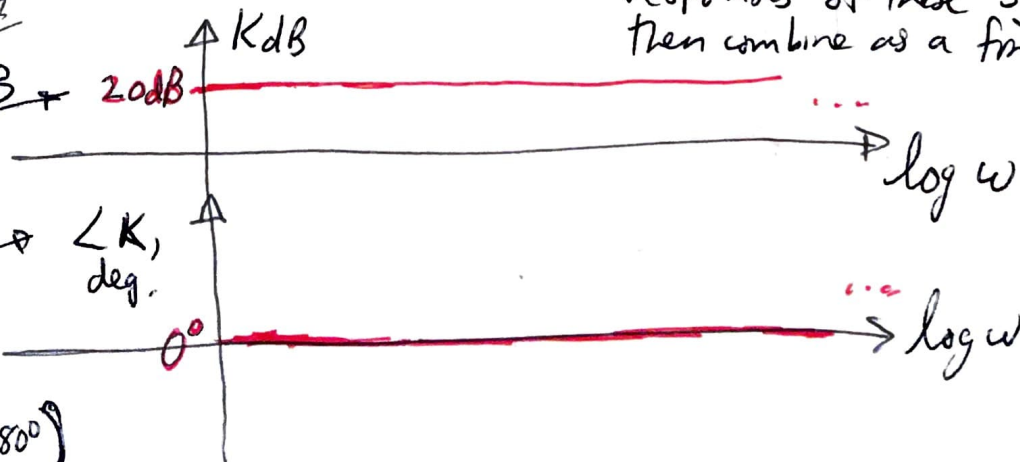
Note that we could also factor the 500 out of the zero at DC term & work with $H(s) = \frac{(1/50)(s/1)}{(1 + s/200)}$, but $K \ll 1$ in this case...

OR, we could "fold" the $K=10$ term into the zero at DC & work with $H(s) = \frac{(s/50)}{(1 + s/200)}$; we have options!

Now, $H(s) = \frac{10(s/500)}{(1 + s/200)}$

3 terms; We will plot out approximations of the Bode responses of these 3 terms first; then combine as a final step

* $K, \text{ gain term}$
 $20 \log_{10}(K) = 20 \log_{10}(10) = 20 \text{ dB}$



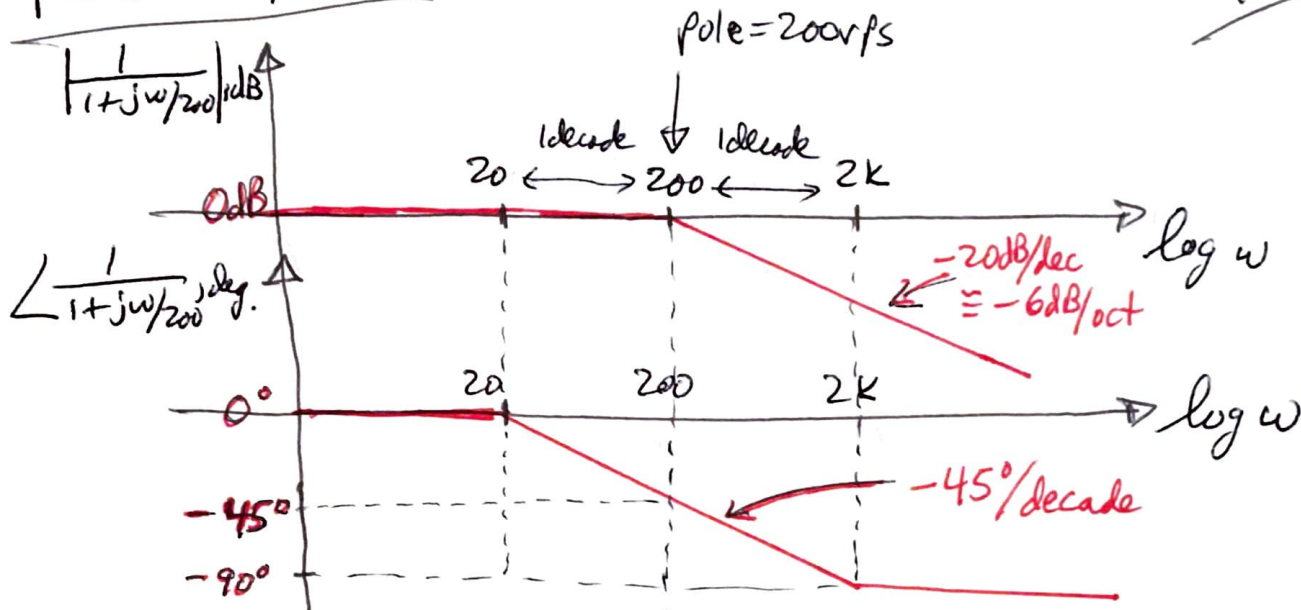
$K > 0$,
So 0° phase shift.
(if $K < 0$, then $\pm 180^\circ$ phase shift)

(cont'd)

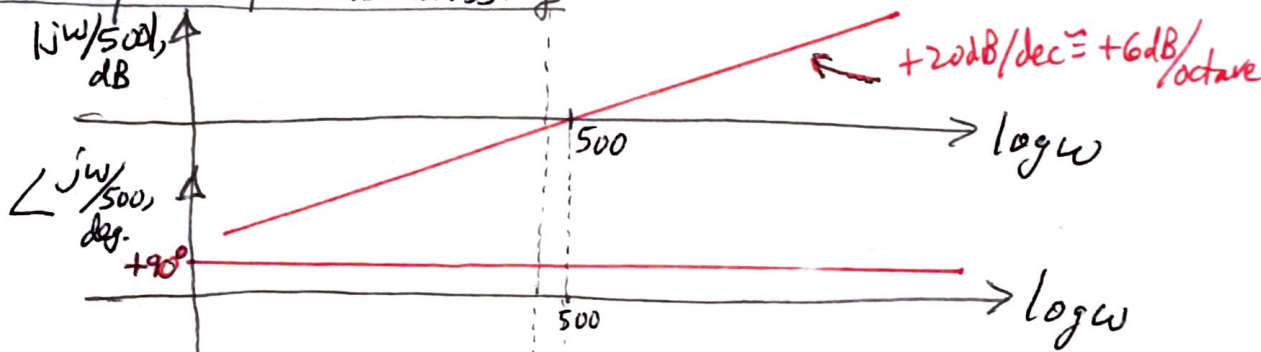
⊗ pole @ 200rps term

<New for sp. 2021>

47



⊕ zero @ DC w/ 500rps 0dB crossing

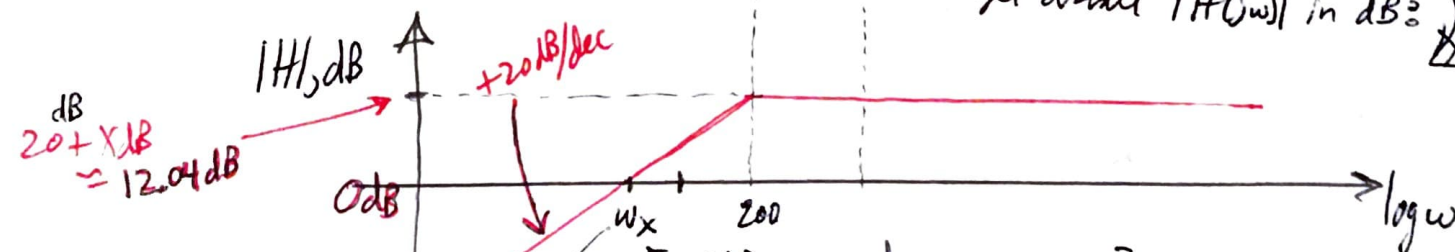


→ Let's combine pole and zero @ DC magnitudes first ⇒ they add in dB, because $\log_{10}(xy) = \log_{10}(x) + \log_{10}(y)$, & $\log_{10}(x/y) = \log_{10}(x) - \log_{10}(y)$

of decades between 200 & 500:
 $\log_{10}(\frac{500}{200}) \approx 0.398 \text{ dec.}$

$$X_{dB} + \frac{20\text{dB}}{\text{dec}}(0.398 \text{ dec.}) = 0\text{dB}$$

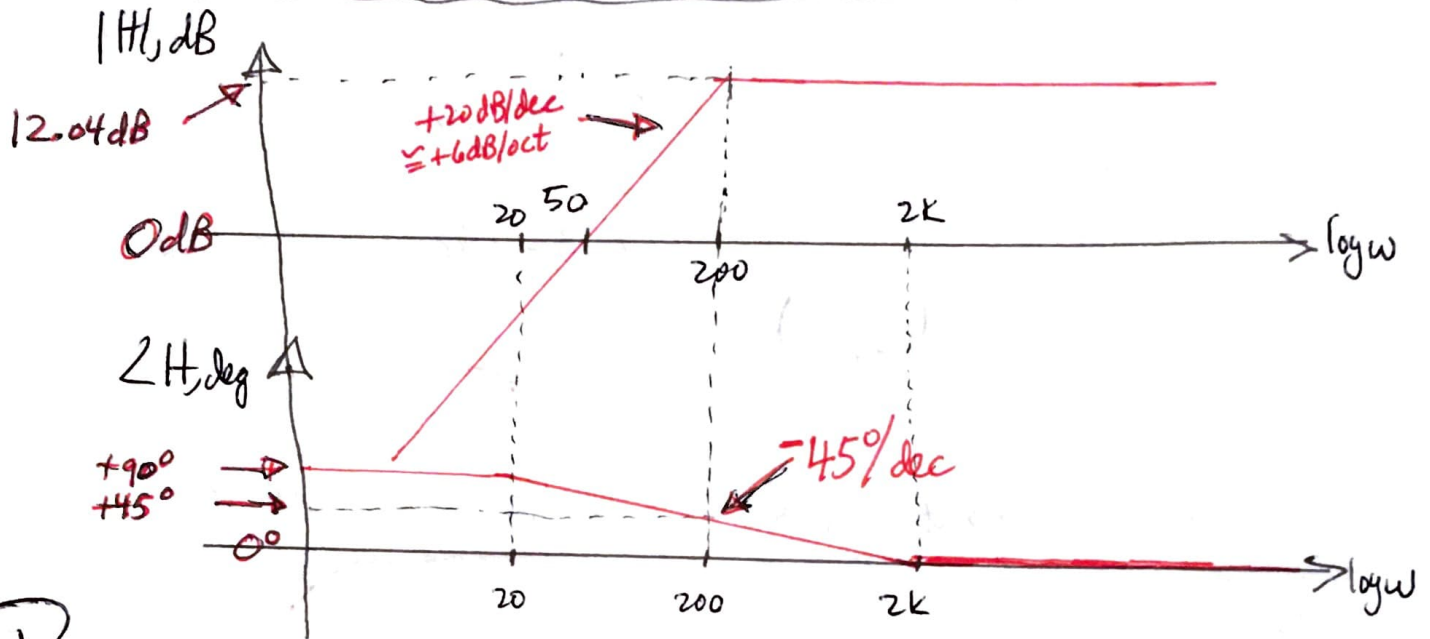
$$\Rightarrow X_{dB} \approx -7.96 \text{ dB}$$



$$\Rightarrow 0\text{dB} + \frac{20\text{dB}}{\text{dec}} (\pm \text{decades}) = 12.04\text{dB} \Rightarrow \# \text{ decades} = \frac{12.04}{20} \approx 0.602 \text{ decades}$$

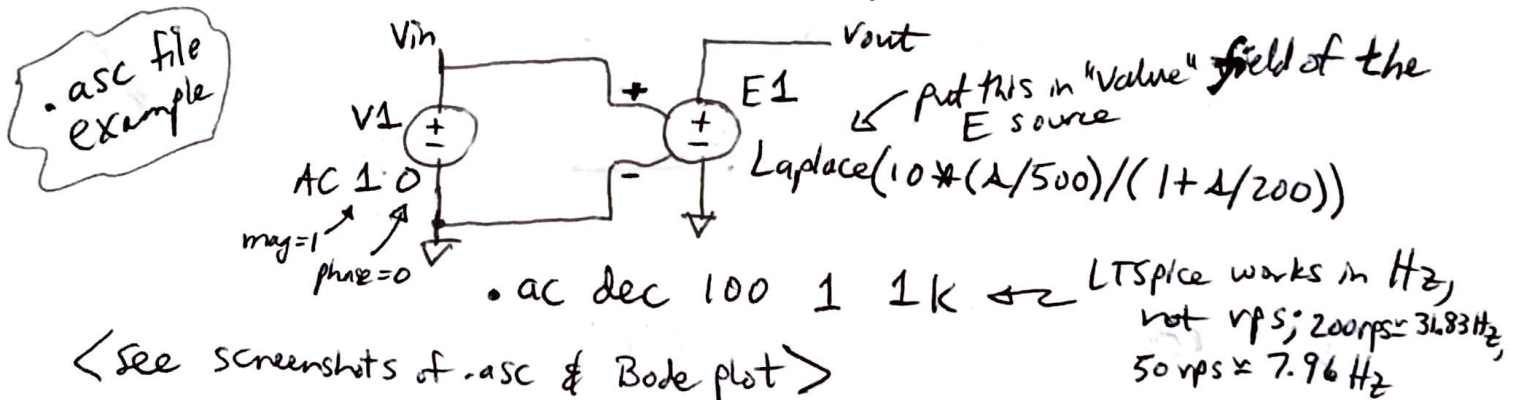
$$\Rightarrow \log_{10}(\frac{200}{w_x}) = 0.602 \Rightarrow w_x = \frac{200}{10^{0.602}} \approx \frac{200}{4} = 50\text{rps} \quad (\text{cont'd})$$

→ the overall ^{approximate} phase response for $H(j\omega)$ is obtained by shifting the pole phase up by 90° (due to the phase of the zero at DC); the K term is positive, so has 0° phase contribution; here is the total Bode approximation of $H(j\omega)$, for completeness:



#1

→ Can confirm approximation w/ high-accuracy LTSpice simulation; if you have the circuit, you can simulate that; if you have $H(s)$, you can use the "Laplace" VCVS (E source); e.g.,



< see screenshots of .asc & Bode plot >

- Errors in the approximation relative to the high-accuracy result:
- ⇒ Actual phase response has more curvature
 - ⇒ The magnitude response has a 3dB error at the pole frequency

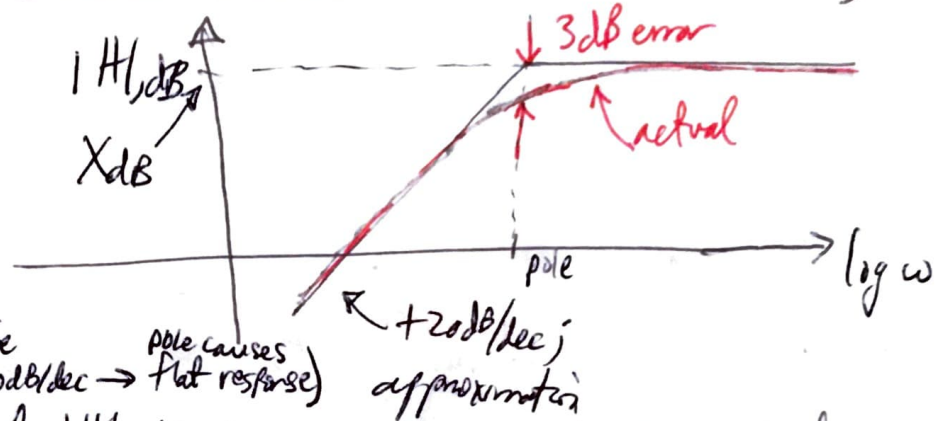
More on "3dB" errors at pole/zero frequencies:

49

⊛ "3dB" errors in the approximation at pole frequencies

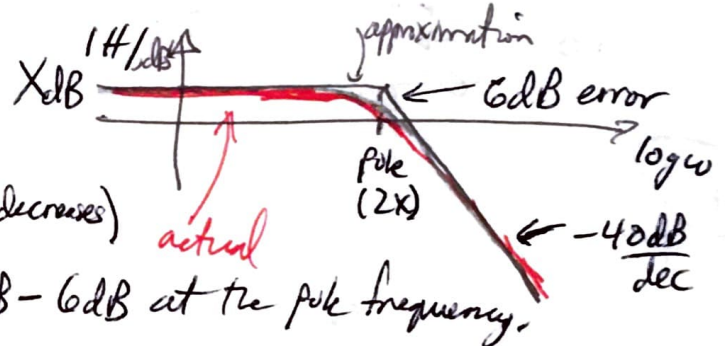
Why is this a pole?

Poles cause magnitude response to decrease after the pole, relative to the preceding trend. i.e., $+20\text{dB/dec} \rightarrow \text{flat response}$



here, the actual $|H|_{\text{dB}}$ is $X_{\text{dB}} - 3\text{dB}$ at the pole frequency

\Rightarrow if the trend (preceding) the pole is $(\pm 20\text{dB/dec})n$, n integer, $n \geq 1$, then the error of the approximation relative to the actual will be $-n 3\text{dB}$ at the pole.

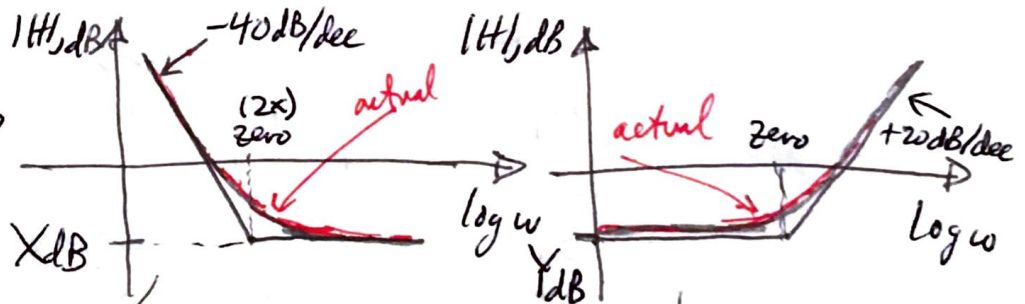


\Rightarrow Another pole scenario \Rightarrow (we know it's a pole because $|H|$ decreases)

Here, the actual $|H|_{\text{dB}}$ is $X_{\text{dB}} - 6\text{dB}$ at the pole frequency.

⊛ "3dB" errors in the approximation at zero frequencies;

two example scenarios



here, the actual $|H|_{\text{dB}}$ is $X_{\text{dB}} + 6\text{dB}$ at the zero frequency

here, the actual $|H|_{\text{dB}}$ is $Y_{\text{dB}} + 3\text{dB}$ at the zero frequency

basic idea: if the trend (preceding) the zero is $(\pm 20\text{dB/dec})n$, n integer, $n \geq 1$,

then the error of the approximation relative to the actual will be $+n 3\text{dB}$ at the zero.

#2

→ Can also confirm Bode approximation w/ high-accuracy Matlab simulation.

option (a)

⇒ can write $H(s)$ in the following form:

$$H(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$$

numerator polynomial in s , order m
denominator polynomial in s , order n

⇒ store coefficients for the two polynomials in two vectors, say num & den:

$$\text{num} = [b_m \ b_{m-1} \ \dots \ b_1 \ b_0];$$

$$\text{den} = [a_n \ a_{n-1} \ \dots \ a_1 \ a_0]; \text{ say } H,$$

⇒ create a transfer function object using tf:

$$H = \text{tf}(\text{num}, \text{den});$$

⇒ have Matlab plot out Bode response:
 $\text{bode}(H)$

⇒ can optionally tell Matlab to plot Bode response over some specific range or rad/sec values; e.g.,

$$w_{\min} = 10; \ w_{\max} = 1e4;$$

$$\text{bode}(H, \{w_{\min}, w_{\max}\})$$

option (b)

⇒ create transfer function object $s = \text{tf}('s')$

⇒ then specify transfer function directly as expression in s ; e.g.,

$$H = (s+1)/(s^2+3*s+1);$$

⇒ then plot Bode response with $\text{bode}(H)$ (or $\text{bode}(H, \{w_{\min}, w_{\max}\})$, as above)

→ For the example we are working on here
(starting on p. 46), we have:

51

$$H(s) = \frac{\left[\frac{10(s/500)}{(1 + s/200)} \right] (500)}{(500)} = \frac{10s}{2.5s + 500} = \frac{10s + 0}{2.5s + 500}$$

⇒ using option (a) on previous page, we have, in Matlab:

$$\text{num} = [10 \ 0]; \text{den} = [2.5 \ 500];$$

$$H = \text{tf}(\text{num}, \text{den});$$

$$\text{bode}(H)$$

⇒ < if ran in class, note the very good agreement between Bode approximation & actual Bode response in Matlab >

⇒ See help bode in Matlab for more details

< Note that help <function> is very useful for your future courses/career, too! >

⇒ Another Matlab bode example: plot Bode response of

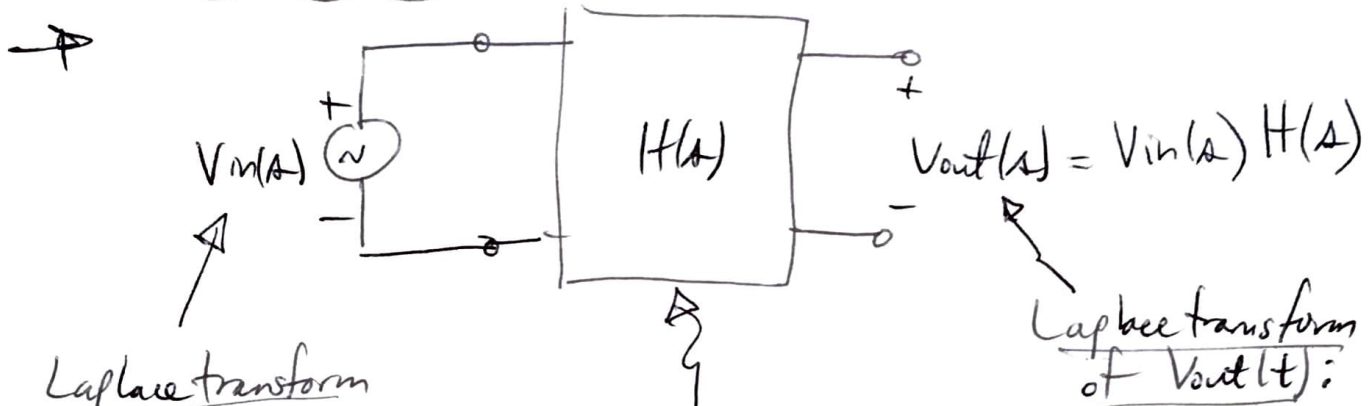
$$H(s) = \frac{s^2 + 0.1s + 7.5}{s^4 + 0.12s^3 + 9s^2}$$

⇒ In Matlab, do:

$$H = \text{tf}([1 \ 0.1 \ 7.5], [1 \ 0.12 \ 9 \ 0 \ 0]);$$

$$\text{bode}(H)$$

λ ?, $j\omega$?, $H(\lambda)$?, phasors? < week 14 discussion > SP, 2021
ELEN2425



Laplace transform
of $v_{in}(t)$:
 $V_{in}(s) = \mathcal{L}\{V_{in}(t)\}$

Laplace transform
of ckt/system
impulse response $h(t)$:
 $H(s) = \mathcal{L}\{h(t)\}$

Laplace transform
of $V_{out}(t)$:
 $V_{out}(s) = \mathcal{L}\{V_{out}(t)\}$

< system poles & zeros
in the complex λ -plane >

more on $h(t)$
in signals & systems

→ Setting $\lambda = j\omega$ yields the Fourier transform of
the signal of interest: ↑ frequency response

$$V_{in}(j\omega) = \mathcal{F}\{V_{in}(t)\}, \quad H(j\omega) = \mathcal{F}\{h(t)\}, \quad V_{out}(j\omega) = \mathcal{F}\{V_{out}(t)\} \\ \text{< system frequency response >} \quad = V_{in}(j\omega) H(j\omega)$$

→ In the specific case of sinusoidal signals, the
Fourier transform of the time-domain signal can be
viewed as a phasor; e.g.,

$$V_{in}(j\omega) = \tilde{V}_{in}, \quad V_{out}(j\omega) = \tilde{V}_{out}, \quad \text{where} \\ \tilde{V}_{out} = \tilde{V}_{in} H(j\omega)$$

✱ Note that the connection between Fourier transforms &
phasors of sinusoidal signals can be somewhat nuanced, this
is essentially the main idea. (For sinusoids, the phasor transform ^{but} & Fourier
transform are essentially two different ways of representing the same information.)