

6th Mid-Semester Examination BE Degree
(MSE-3 Scheme)

Department of Electronics and Communication Engineering

Semester: <u>VI</u>	Course Name: <u>Control Systems</u>
Course code: <u>21ECG62</u>	Faculty Names: <u>Dr. Smitha Perbbur, Dr. Harisha,</u>
Date:	Section A: Section B: Section C: <u>Mr. Divya</u>
	Max. Marks 30

Q.No.	Scheme	Marks	CO;BL
1a)	<p><u>Gain Margin</u>: - Margin in gain allowable by which gain can be increased till system reaches on the verge of instability. $-\frac{1}{2}M-$</p> $GM = \frac{1}{ G(j\omega)H(j\omega) _{\omega=\omega_{gc}}} \quad -\frac{1}{2}M-$ <p>GM should be ≥ 1 for stability $\frac{1}{2}M-$</p> <p><u>Phase Margin</u></p> <p>The amount of additional phase lag which can be introduced in the system till system reaches on the verge of instability is called phase margin P.M. $-\frac{1}{2}M-$</p> <p>OR</p> $PM = 180^\circ + \angle G(j\omega)H(j\omega)_{\omega=\omega_{gc}} \quad -\frac{1}{2}M-$ <p>For stability PM should be ≥ 0. $-\frac{1}{2}M-$</p>	1M	
1b)	<p>$N = -P$ $-\frac{1}{2}M-$</p> <p>It states that for absolute stability of the system, the no. of encirclements of the origin of F-plane by Nyquist plot must be equal to no. of poles of $1 + G(s)H(s)$ i.e. poles of $G(s)H(s)$ which must be in the right half of s plane and in clock wise direction $-\frac{1}{2}M-$</p>	2M	

k) Mapping theorem states that the mapped locus $z'(s)$ encircles the new origin of F-plane as many times as the difference between the no. of zeros and poles of $F(s)$ which are encircled by $z(s)$ path in s-plane mathematically

$$N = Z - P$$

where N = Encirclements of origin of F-plane by $z'(s)$ path

P = no. of poles of $F(s)$ encircled by $z(s)$ path in s-plane. -2M-

Z = no. of zeros of $F(s)$ encircled by $z(s)$ path in s-plane.

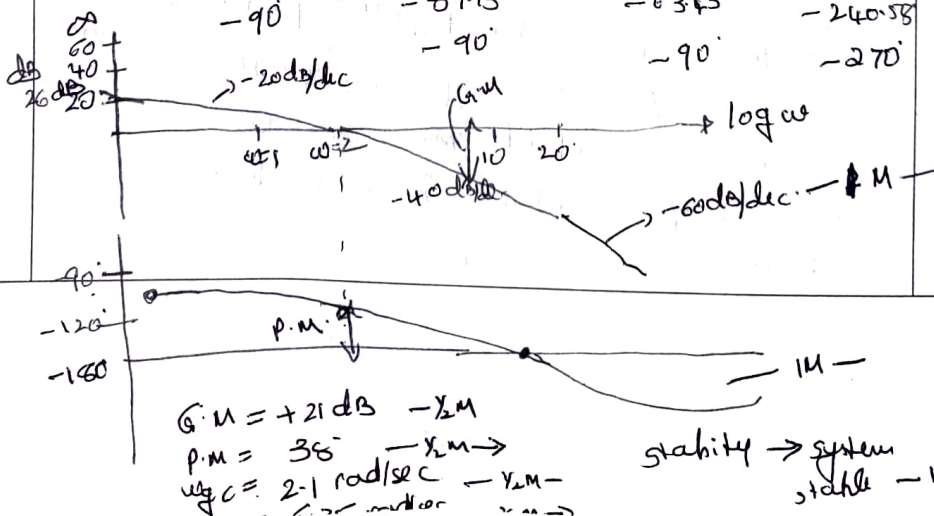
2a) $F(s) = \frac{80}{s(s+2)(s+20)} = \frac{2}{s(1+\frac{s}{2})(1+\frac{s}{20})}$ -1M.
 $20 \log k = 26 \text{ dB}$

i) $k=2$ ii) 1 pole at origin.

iii) simple poles at $\tau_1 = \tau_2$ $\omega_{c1} = 2$ 2M.

iv) simple poles at $\tau_2 = 1/20$ $\omega_{c2} = 20$ 0

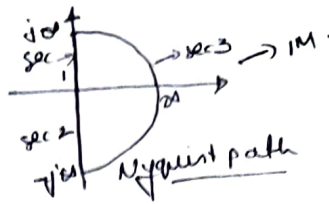
ω	\angle_{pole}	$-\tan^{-1} \omega/2$	$-\tan^{-1} \omega/20$	Φ_R
0.2	-90°	-5.7°	-0.57°	-96.27°
2	-90°	-45°	-5.7°	-140.7°
8	-90°	-75.96°	-21.8°	-187.76°
10	-90°	-78.69°	-26.56°	-195.24°
20	-90°	-84.28°	-45°	-219.28°
40	-90°	-87.13°	-63.43°	-240.58°
∞	-90°	-90°	-90°	-270°



2b) $N = -P = 0$ — 1M

Step

$$G(j\omega)H(j\omega) = \frac{2(1-j\omega)}{(2+j\omega)(3+j\omega)}$$



Sec 1

$$\omega \rightarrow \infty \quad \angle \frac{1-90^\circ}{2+90^\circ} = 0 \angle -270^\circ$$

$$0 - (-270^\circ) = +270^\circ \quad \int 2M$$

$$\omega \rightarrow 0 \quad \frac{1}{3} \frac{0^\circ}{0^\circ} = \frac{1}{3} 0^\circ$$

Sec 2 \rightarrow Mirror image of sec 1.

Intersection with negative real axis

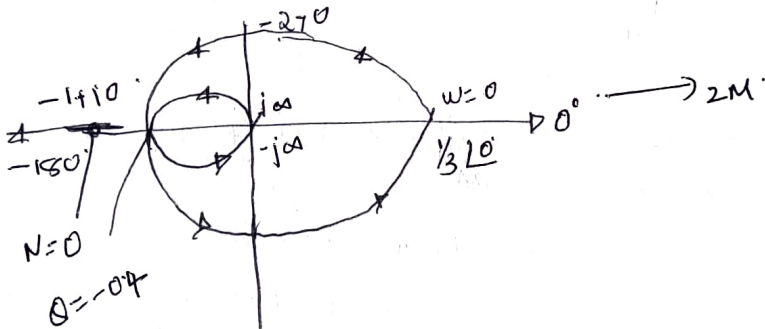
$$G(j\omega)H(j\omega) = \frac{2(1-j\omega)(2+j\omega)(3-j\omega)}{(2+j\omega)(2-j\omega)(3+j\omega)(3-j\omega)}$$

$$= 2 \frac{[(6-6\omega^2) - j\omega(11-\omega^2)]}{(4+\omega^2)(9+\omega^2)}$$

imaginary part to be zero, $\omega = 0$ $\omega = \sqrt{11}$

$\omega = 0$ intersects at $\frac{1}{3}$

$\omega = \sqrt{11}$, it intersects at $Q = -0.4$



3a)

$$G(s)H(s) = \frac{A}{s(1+s/4)(1+s/10)}$$

$$A = \frac{4}{40} \text{ — 1M}$$

1) A is unknown

2) $\frac{1}{3} \rightarrow$ one pole at origin

$$3) \frac{1}{1+s/4} \text{ at } T_1 = \frac{1}{4} \quad \omega_{c1} = \frac{1}{T_1} = 4$$

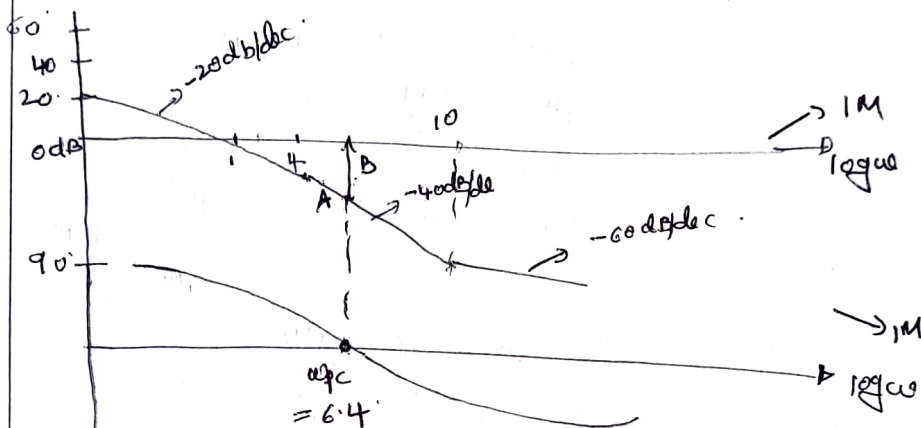
$$4) \frac{1}{1+s/10} \text{ at } T_2 = \frac{1}{10} \quad \omega_{c2} = \frac{1}{T_2} = 10$$

$0 < \omega < 4$ -20 dB/dec
 $4 < \omega < 10$ -40 dB/dec
 $10 < \omega < \infty$ -60 dB/dec

Step 3.

$$G(j\omega)M(j\omega) = \frac{A}{j\omega(1+j\omega/4)(1+j\omega/10)}$$

ω	$\angle M$	$\angle G$	$\angle T$	$\angle \phi$
0.4	-90°	-5.71°	-2.29°	-98°
4	-90°	-45°	-21.8°	-156.8°
10	-90°	-68.2°	-45°	-203.2°
∞	-90°	-60.2°	-35°	-185.2°



$$20 \log A = 22$$

$$A = 12.58 \quad \rightarrow \text{upward shift positive}$$

$$A = \frac{K}{40} \Rightarrow K = 40A = 503.57$$

for marginal stability

Faculty Name (s) & Signature

Section A:

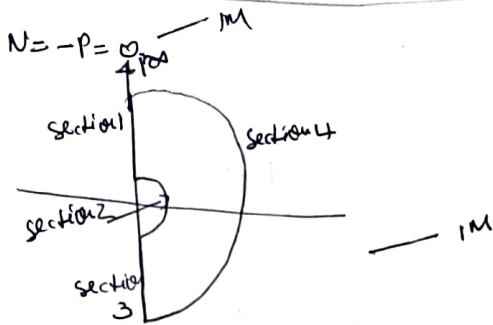
Section B:

Section C:

MSE Coordinators

Dr. B.S. Pavan & Ms. Kushalatha M R

Dr. Parameshachari B D
HoD, ECE, NMIT



For stability $N = -P = 0$.

Section 1: $S = +j\infty$ to $S = +j0$.

starting $\omega \rightarrow +\infty$ $\angle \frac{0}{90 \cdot 180} = 0 \angle -270^\circ$

Terminating $\omega \rightarrow +0$ $\angle \frac{0}{90 \cdot 0} = \infty \angle -90^\circ$

$$\left. \begin{array}{l} -90 - (-270) \\ = +180^\circ \end{array} \right\} 2M$$

Section 2: $S = +j0$ to $S = -j0$

starting $\omega \rightarrow +0$ $\angle -90^\circ$

Terminating $\omega \rightarrow -0$ $\angle 90^\circ$

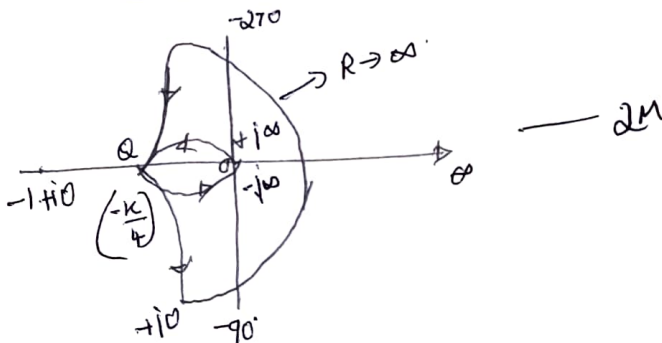
$$90 - (-90) = +180^\circ$$

Step

$$\begin{aligned} G(j\omega)H(j\omega) &= \frac{K(-j\omega)[(2-\omega^2) - 2j\omega]}{(j\omega)(-j\omega)[(2-\omega^2) + 2j\omega][(2-\omega^2) - 2j\omega]} \\ &= \frac{-2K\omega^2 - Kj\omega(2-\omega^2)}{\omega^2[(2-\omega^2)^2 + 4\omega^2]} \end{aligned} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} 2M$$

$$2 - \omega^2 = 0 \quad \omega_{pc} = \sqrt{2}$$

$$Q = \frac{-2K}{(2-2)^2 + 4 \times 2} = \frac{-K}{4} \quad \text{--- } 1M$$



10M

For stability

$$|GQ| < 1 \quad \text{i.e.} \quad \left| \frac{K}{4} \right| < 1 \quad \text{i.e.} \quad K < 4$$

for stability $0 < K < 4$

--- 1M

$$4) \omega_{c1} = 1 \quad \int 1M$$

$$T_1 = 1/\omega_{c1} = 1$$

The shift at $\omega=1$ is 0 dB so $20 \log K = 0 \text{ dB} \therefore K=1$.

$$\omega_{c2} = \omega_2 = 10 \quad T_2 = 1/\omega_{c2} = 0.1$$

$$(1 + T_2 s) = (1 + 0.1s) \text{ as simple zero } \int 1M$$

$$\omega_{c3} = 100 \quad T_3 = 1/\omega_{c3} = 0.01$$

$$T_4 = 1/\omega_{c4} = 0.001 \quad \frac{1}{s + 0.001s} \quad \int 1M$$

$$G(s) H(s) = \frac{(1 + 0.1s)(1 + 0.01s)}{(1 + s)(1 + 0.001s)} \quad \int 1M$$

-4M -