

Cloud Operations & Innovation (“CO+ I”)

A Feasibility Framework for Waste Heat from Data Centers to a Water Capture System from Uravu Labs

Milestone-2 Report



Date of Submission

04 November 2025

Contents

1. Introduction	1
2. Integration schematic	1
3. Site-specific deep dive.....	3
3.1 Operational threshold for different sites	3
3.2 Reduction in chiller load	5
3.3 Gross and net water production	6
3.4 Specific energy consumption.....	6
3.5 Impact of facility water temperature.....	7
3.5.1 Impact on chiller load.....	7
3.5.2 Impact on water production	8
3.5.3 Impact on specific energy consumption	10
4. Preliminary risk assessment.....	12
5. Concluding remarks.....	12

1. Introduction

The preliminary report findings demonstrate how the Uravu system enables simultaneous cooling and water generation by utilizing waste heat from data centers. This report presents the conceptual layout for integrating the Uravu system with data center operations, provides a detailed analysis of integration across eight priority sites, and highlights key risks and corresponding mitigation strategies.

2. Integration schematic

Integrating the Uravu system with a data center requires a dedicated heat exchanger to enable efficient thermal energy transfer, complemented by engineered piping networks that establish interconnections between the two systems. The integration incorporates instrumentation such as **flow meters, control valves, and actuators** to ensure accurate monitoring and automated control of thermal and hydraulic parameters. The heat exchanger increases the temperature of Uravu's proprietary liquid desiccant to the required desorption temperature. This section outlines the conceptual design, highlighting the configuration of multiple loops tailored for different operating scenarios.

The conceptual CAD and integration schematic is illustrated in **Figure 1** and **Figure 2**. Key components of the Uravu system, including the **absorber, desorber, desiccant-facility water heat exchanger, and condenser**, which all together occupies less than 60 m² of footprint area, along with the associated piping and control infrastructure.

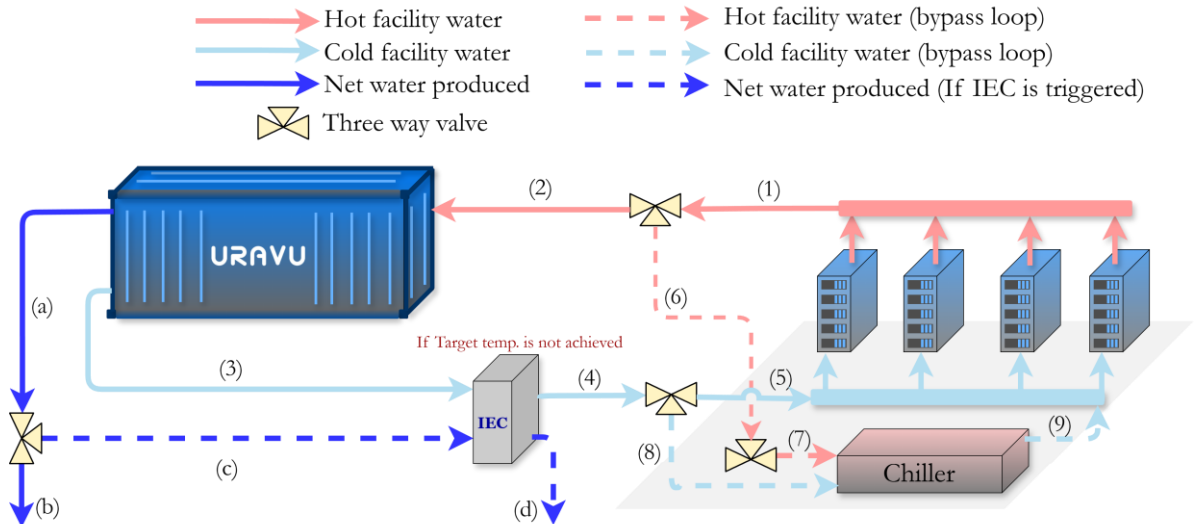


Figure 1: Conceptual schematic layout design of the Uravu system with the data center.

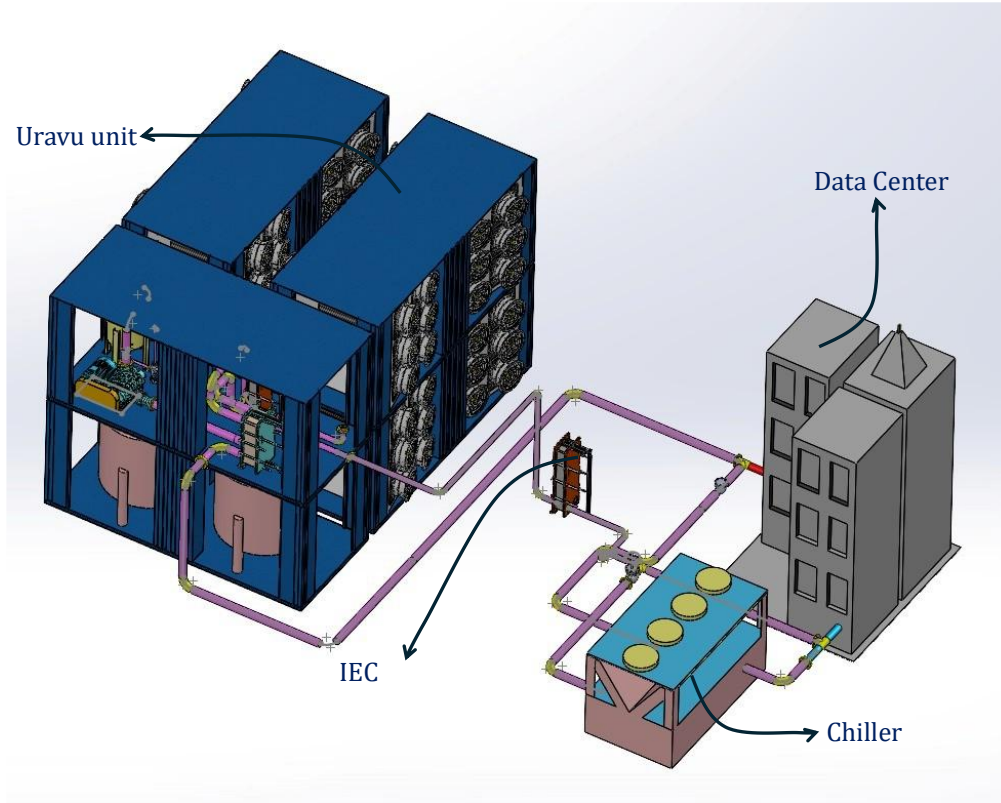


Figure 2: Conceptual CAD layout design of the Uravu system with the data center.

Depending on the operating state of the data center and prevailing ambient conditions, specific fluid loops and components are selectively activated to support cooling requirements. In particular scenarios, **the use of chillers** ensures normal data center operations, regardless of the availability of the **Uravu system**. Various case scenarios are mentioned in **Table 1**.

Table 1: Active loop and component for different scenarios for Uravu integration with the data center.

Scenario	Active loop	Components active
1. The target temperature is achieved with desiccant-facility water HX	$1 \rightarrow 2 \rightarrow 3 \rightarrow 4 \rightarrow 5$ and $(a) \rightarrow (b)$	Uravu unit only
2. The target temperature is not achieved with the desiccant-facility water HX	$1 \rightarrow 2 \rightarrow 3 \rightarrow 4 \rightarrow 5 \rightarrow 8 \rightarrow 9$ and $(a) \rightarrow (c) \rightarrow (d)$	Uravu, IEC, and Chiller
3. Target temperature $>$ WBT, and water consumed in IEC exceeds the generated water	$1 \rightarrow 2 \rightarrow 3 \rightarrow 4 \rightarrow 5 \rightarrow 8 \rightarrow 9$ and $(a) \rightarrow (c) \rightarrow (d)$	Uravu, IEC, and Chiller
4. WBT $>$ downtime trigger temperature	$1 \rightarrow 6 \rightarrow 7 \rightarrow 9$	Chiller only

3. Site-specific deep dive

Eight data center sites have been selected, four from the European Union (EU) and four from the United States (US), for detailed evaluation of the integrated system's performance. The chosen locations are Frankfurt (FRK), Madrid (MRD), London (LON), Stockholm (SHM), Phoenix (PNX), Chicago (CHG), Seattle (STL), and Houston (HSN). Based on operational conditions and local climate, various scenarios may be applicable, as listed in Table 1. For the baseline, the facility water inlet temperature ($T_{\text{fac,in}}$) is maintained at 30°C, with a target outlet temperature (T_{target}) of 18°C. The facility water is maintained at a rate of 1.3 kg/s, and the desiccant flow rate is adjusted based on the available waste heat. Additionally, the Uravu system is programmed with a downtime trigger temperature (T_{trigger}) of 9.5°C, specific to 30°C operating conditions only. Based on the available waste heat temperature, the downtime trigger temperature can also be adjusted. The downtime trigger temperature indicates that Uravu's waste heat-based system is suspended whenever the ambient wet-bulb temperature (WBT) falls below this threshold. Also discussed in the Milestone-1 report, the facility water temperature should follow the given constraint, where, $T_{\text{fac,in}} \geq T_{\text{vap}} + \Delta T_{\text{system}} + BPE$, where ΔT_{system} is approximately 5°C, and the boiling point elevation (BPE) is around 12°C, along with saturation temperature (T_{vap}) which can be adjusted by controlling the vacuum according to the available waste heat temperature.

3.1 Operational threshold for different sites

Figure 3 and **Figure 4** illustrate the annual variation of wet bulb temperature (WBT) across the selected locations. For stable operation of the Uravu system, the downtime trigger temperature must be maintained above the prevailing WBT. Considering the downtime trigger temperature of 9.5°C for facility water temperature of 30°C, the system is programmed to suspend operation whenever WBT surpasses this threshold, in which case the data center cooling shifts to Scenario 4, as described in **Table 1**.

The proportion of time that the complete waste heat-operated integrated system remains active is 57% in Frankfurt, 44% in Madrid, 48% in London, and 67% in Stockholm, when considering the EU cities. For the US, the system is operational for 30% in Phoenix, 54% in Chicago, 16% in Houston, and 51% in Seattle. Due to the low downtime trigger temperature for the Uravu system, the wet bulb temperature remains high for most of the time annually, because of the low-temperature waste heat. However, with change in the waste heat temperature downtime trigger is also adjusted which can lead to a higher uptime for the Uravu system, as observed in **Figure 3** and **Figure 4**.

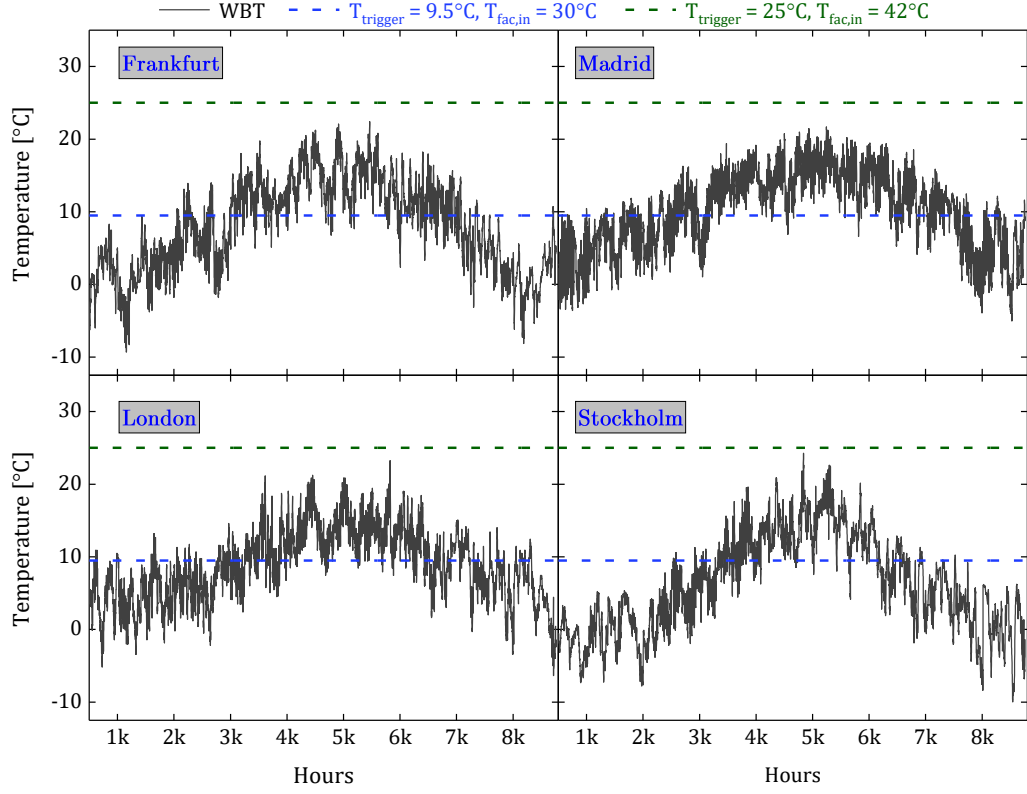


Figure 3: Variation of WBT through the year for the European Union cities against the downtime trigger temperature.

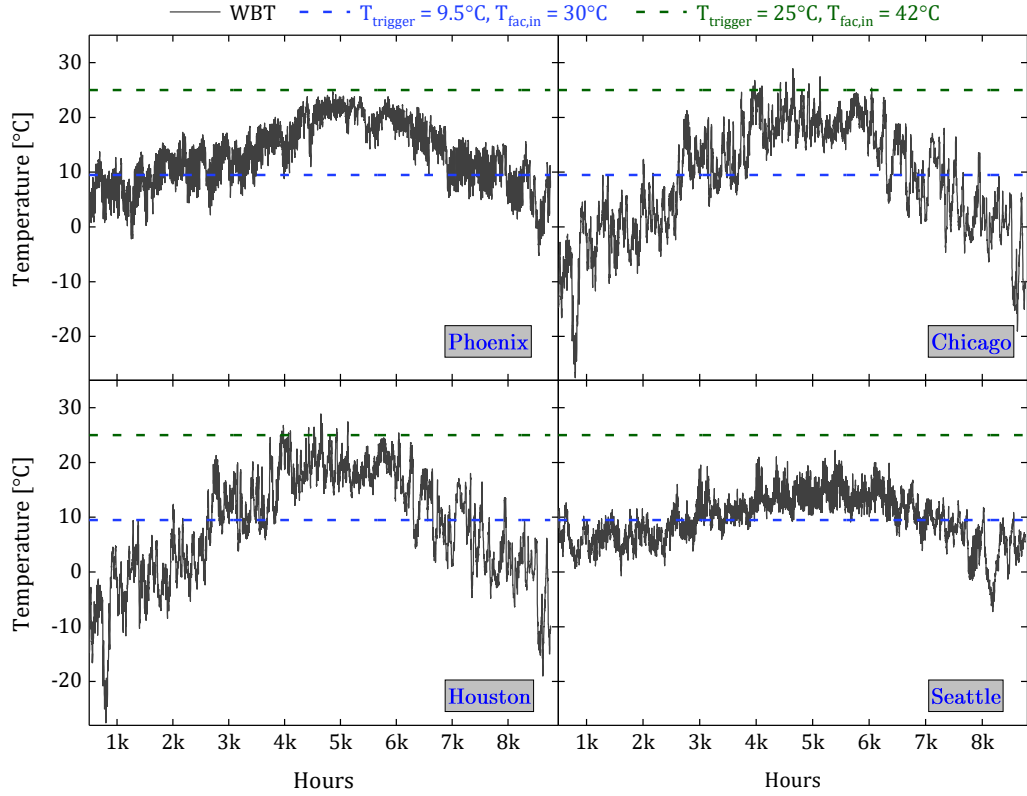


Figure 4: Variation of WBT throughout the year for US-based cities against the downtime trigger temperature.

Based on 30°C waste heat temperature, feasibility rankings based on system uptime for the EU are **Stockholm > London > Frankfurt > Madrid**, and for the US, they are **Chicago > Seattle > Phoenix > Houston**. It is also observed that most downtime events occur during the middle of the year, when WBT levels are typically elevated compared to the rest of the year, thereby limiting the system's operating window.

3.2 Reduction in chiller load

The reduction in annual chiller load for the complete waste heat-based system and the hybrid (electric + waste heat) system has been reported for EU and US cities. For the same available waste heat load at a 30°C facility water temperature and 18°C target temperature, the waste heat system results in a reduction in chiller load of approximately 45-68% for the EU and 16-54% for the US annually, as shown in **Figure 5**. US-based cities experience a lower reduction in chiller load compared to EU-based cities, primarily due to differences in their natural climatic conditions, as explained in Section 3.1. However, in contrast, the hybrid system leads to a reduction in chiller load of approximately 100% in almost every city, except for Houston, due to its hot weather, which results in more chiller utilization. It should also be noted that the reduction in chiller load for a complete waste-heat-based system is directly proportional to Uravu's uptime. However, for the hybrid system, since Uravu's is operational for 100% of the time, the chiller load reduction is proportional to the cooling provided by the hybrid system.

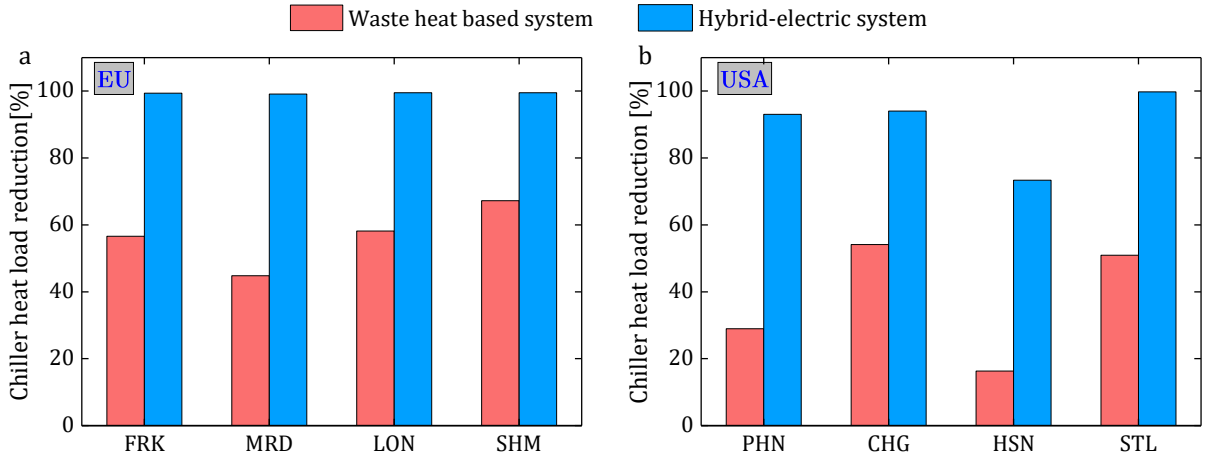


Figure 5: Reduction in chiller load annually for waste heat and hybrid integrated system for data center cooling for (a) the European Union and (b) the US.

3.3 Gross and net water production

Gross and net water production across the selected sites was evaluated for both the waste heat and hybrid configuration, under the same waste heat load. **Figure 6** illustrates that gross water production for a complete waste-heat-driven system varies depending on the total annual uptime at different locations. The net water production of the system will be less than the gross because of the additional water consumption required for desiccant and facility water cooling in the indirect evaporative cooler (IEC). However, with a hybrid system, the gross water production will remain constant throughout the year at $13,369 \text{ m}^3/\text{MW}$ due to 100% uptime of the Uravu system. Similar to a waste-heat system, the net water production will depend on the consumption in IEC for additional cooling load. The net water production is increased by 2 to 8 times for the hybrid system compared to the waste-heat system, ranging from 8000 to $13,300 \text{ m}^3/\text{MW}$.

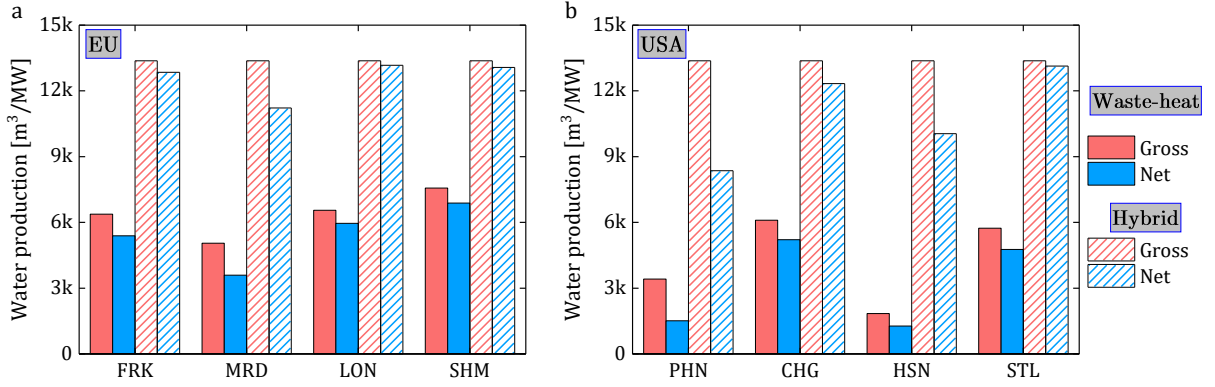


Figure 6: Gross and net water production for waste heat and hybrid integrated system for data center cooling for (a) the European Union and (b) the US.

3.4 Specific energy consumption

Similar to water production, the specific energy consumption (SEC) varies significantly with the different configurations. For the complete waste-heat-based system, the Uravu system's electrical energy consumption will be up to 6 kW, which accounts for pumping and fan power. For a hybrid configuration, the electric energy consumption can reach up to 20 kW, allowing the system to run continuously for 100% of the time.

Figure 7 illustrates that the waste-heat configuration yields SEC values in the range of approximately 69 to $142 \text{ kWh}/\text{m}^3$. The higher value corresponds to Phoenix and Houston due to low net water production. An increase in SEC values of about three times can be observed with the hybrid configuration due to increased electrical power consumption. The SEC value of the hybrid system rises to about $204 \text{ kWh}/\text{m}^3$ and $319 \text{ kWh}/\text{m}^3$ for handling the same amount of waste heat load. This SEC data indicates that while hybrid

configuration integration enables system operation for 100% of the time, it leads to higher energy input. Therefore, it can be concluded that to achieve 100% cooling with low-temperature waste heat reuse using the Uravu hybrid system, there will be an increase in net water production, but with an increase in SEC value. For low-temperature waste heat integration, there always exists a trade-off between the SEC and net water production.

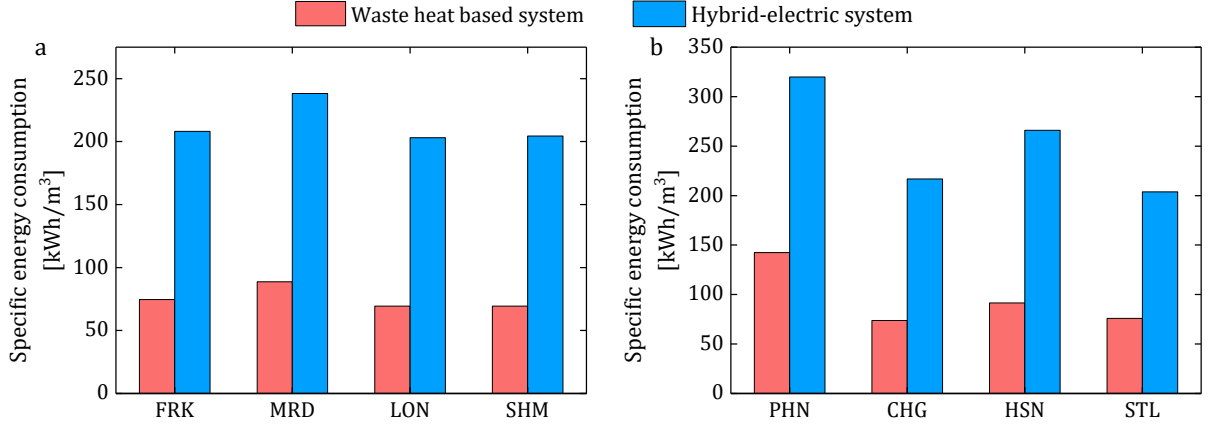


Figure 7: Specific energy consumption for waste heat and hybrid integrated system for data center cooling for (a) the European Union and (b) the US.

3.5 Impact of facility water temperature

The waste heat temperature plays a critical role in the appropriate integration of the Uravu atmospheric water harvesting system with the data center cooling application. The results reported up to Section 3.5 are based on low-temperature waste heat at 30°C. Due to the low temperature, the Uravu's downtime trigger temperature must be kept low, which results in more downtime hours for the Uravu's complete waste heat-driven system. This section illustrates the effect of waste heat temperature on the system's overall performance for both configurations at the same waste heat load.

3.5.1 Impact on chiller load

In EU cities with a minimum waste heat temperature of 40°C, the chiller load can be reduced by up to 100% for Frankfurt, London, and Stockholm. For Madrid, the minimum waste heat temperature requirement is 45°C. As discussed in Section 3.2, with a hybrid system, the reduction in chiller load is consistently close to 100%, regardless of the different waste heat temperatures, as shown in **Figure 8**.

Due to the varying local climatic conditions across the US, there is non-uniformity in the chiller load reduction for both configurations compared to EU cities. As depicted in **Figure 9**, to achieve 100% chiller load reduction with a complete waste heat-driven

system, the minimum waste heat temperature required for Phoenix, Chicago, Houston, and Seattle is 55°C, 45°C, 50°C, and 40°C, respectively. For a hybrid configuration, except for Houston, for which the minimum waste heat temperature required for 100% chiller load reduction is 40°C, while other cities obtain it at 35°C.

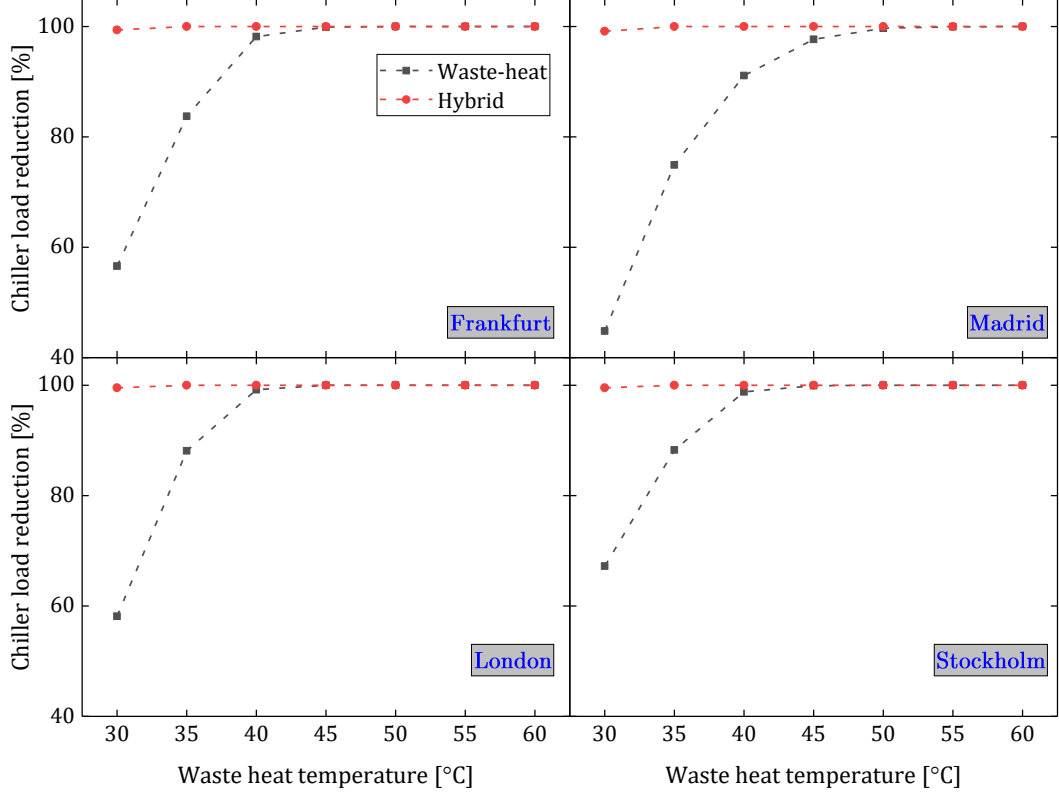


Figure 8: Reduction in chiller load for different European Union cities at varying waste heat temperatures.

3.5.2 Impact on water production

For EU cities utilizing hybrid configurations, the net water production remains almost steady at around 13,400 m³/MW across different waste heat temperatures. In contrast, for systems fully powered by waste heat, the net water output changes with the temperature of the available waste heat. Additionally, depending on the waste heat temperature and local climatic conditions, the water USge in the IEC for Uravu's internal consumption and facility water cooling also fluctuates, thereby influencing the overall net water production, as illustrated in **Figure 10**.

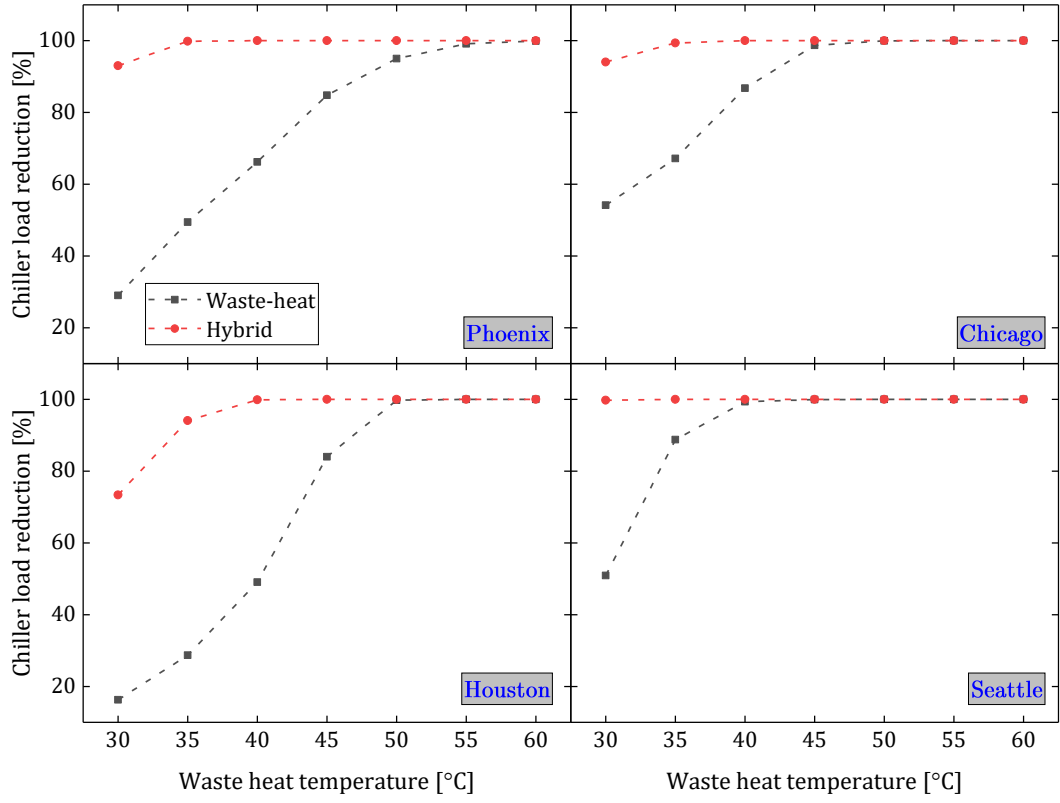


Figure 9: Reduction in chiller load for different US cities at varying waste heat temperatures.

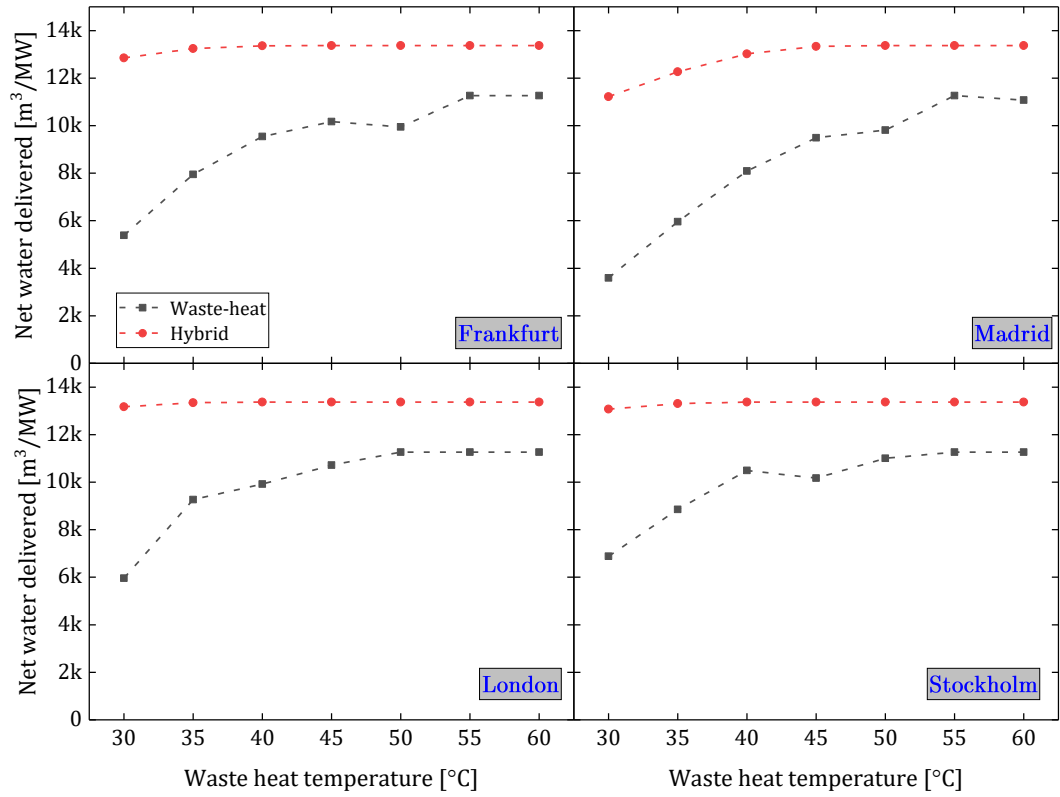


Figure 10: Net water production for different European Union cities at varying waste heat temperatures.

For US cities, variations in net water production are observed with changing waste heat temperatures in a fully waste heat-driven integrated system. These variations primarily result from local climatic conditions, which affect the water demand for supplementary cooling in the IEC. In contrast, for the hybrid configuration, water production tends to stabilize at temperatures above 40°C across different cities, as shown in **Figure 11**. This stabilization occurs because, at higher waste heat temperatures, the ambient temperature is relatively lower, enabling greater free cooling in the air–liquid heat exchanger and consequently reducing the IEC load.

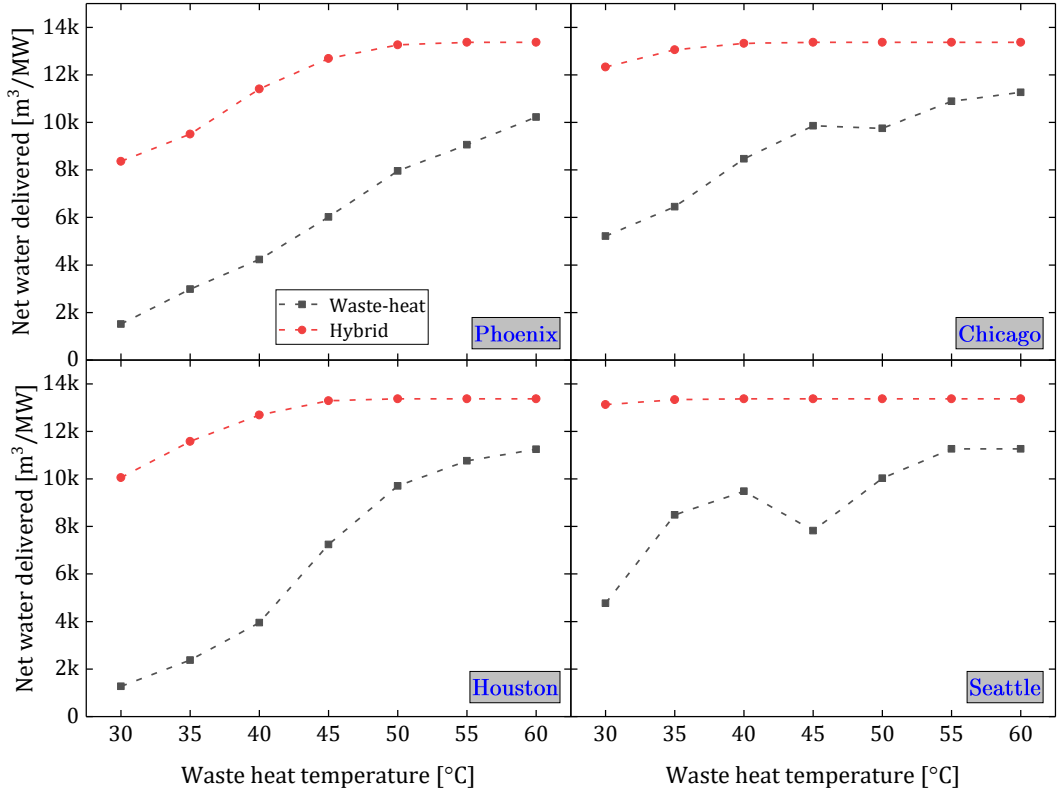


Figure 11: Net water production for different US cities at varying waste heat temperatures.

3.5.3 Impact on specific energy consumption

The specific energy consumption is a strong function of electricity consumption and net water production. Therefore, in the EU, where net water production remains nearly constant, the SEC trends are also constant for both waste heat and hybrid configurations, as shown in **Figure 12**. The hybrid configuration yields a value three times higher than the waste heat configuration, with the maximum value being close to 250 kWh/m³, due to increased electricity consumption, as discussed in Section 3.4.

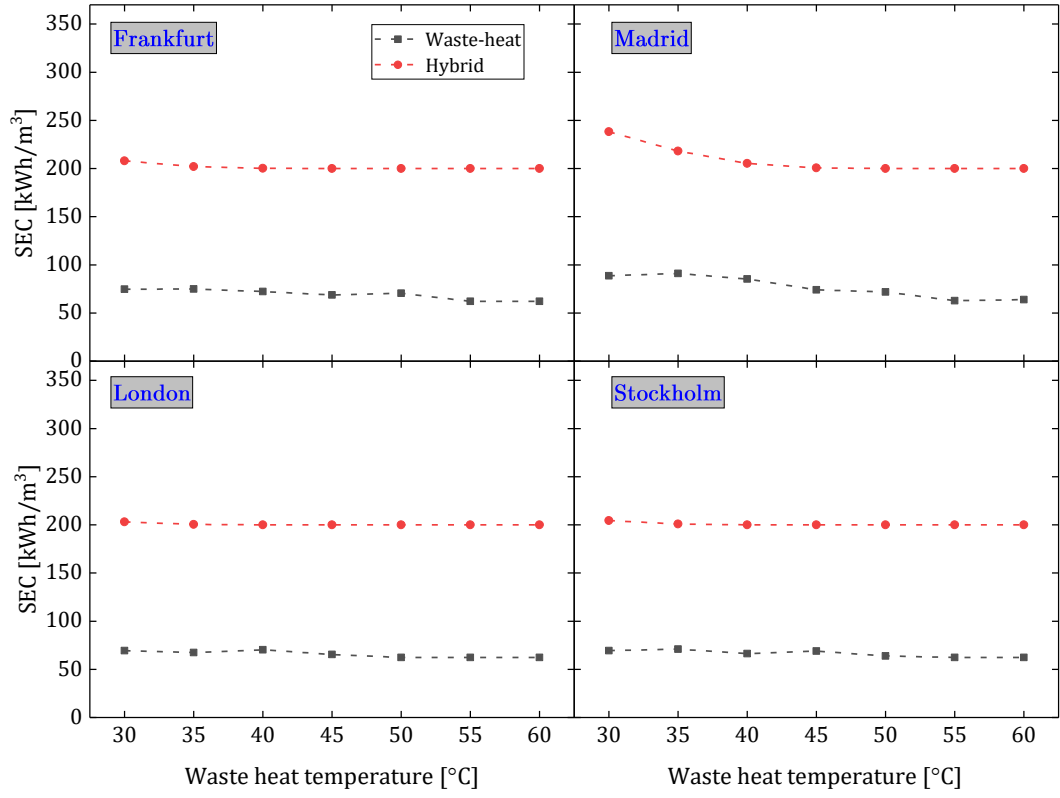


Figure 12: Specific energy consumption for different European Union cities at varying waste heat temperatures.

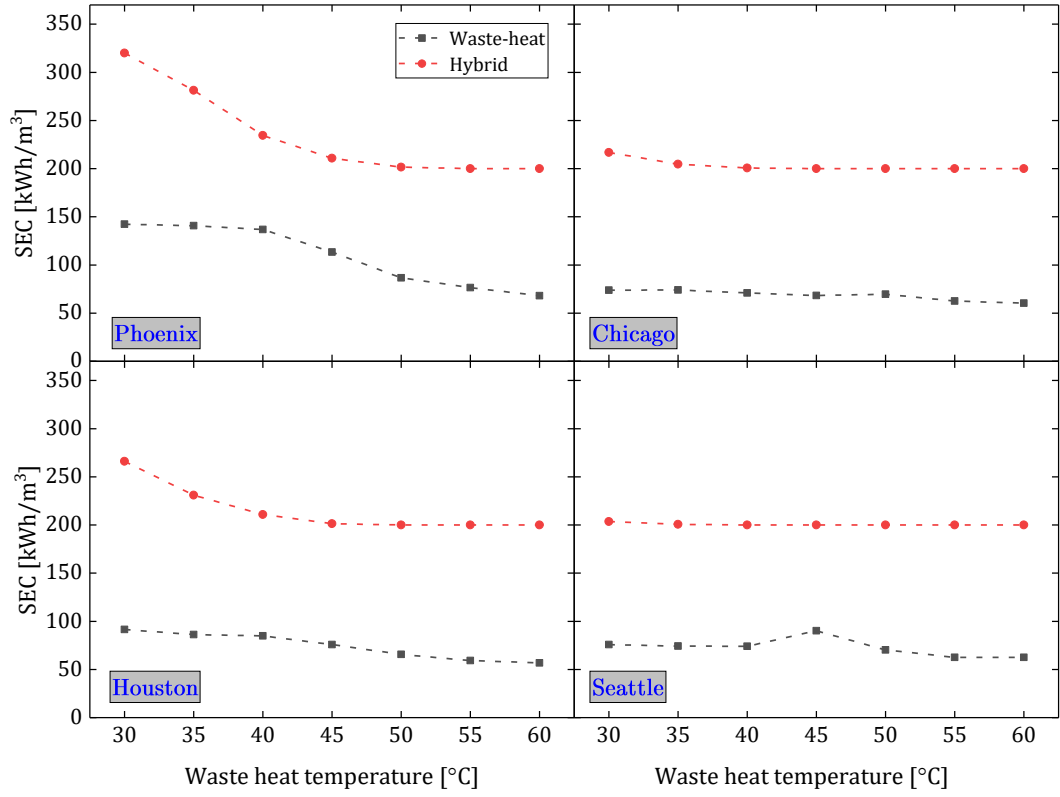


Figure 13: Specific energy consumption for different US cities at varying waste heat temperatures.

Whereas, in the US, the SEC values become constant after 45°C due to variations in uptime and net water production, as reported in Sections 3.5.1 and 3.5.2. For hybrid configurations, due to increased water consumption in IEC at low waste heat temperatures, the SEC values rise to 320 kWh/m³ and 250 kWh/m³ for Phoenix and Houston, respectively, and reduces to 200 kWh/m³ after 45°C. For Chicago and Seattle, it results in a constant SEC value of 200 kWh/m³ at all waste heat temperatures. Similar trends can be observed for the waste heat-driven configuration with a lower SEC value ranging from 150 to 50 kWh/m³, as shown in Figure 13.

4. Preliminary risk assessment

5. Concluding remarks

Considering the varying geographical and climatic conditions, the following insights summarize the performance of the Uravu integrated system for data center cooling:

- **European Union:** Due to relatively uniform weather conditions across the region,
 - The chiller load can be reduced by **40–60%** in a fully waste heat-driven system for **low-temperature waste heat**, and by **100%** in a **hybrid setup** for both low- and high-temperature waste heat.
 - Water production ranges from **4,000 to 10,000 m³/MW** for the **low-temperature waste heat** configuration and reaches **13,000 m³/MW** in the hybrid configuration.
 - Specific energy consumption (SEC) varies between **60 and 100 kWh/m³** for waste heat operation and between **200 and 250 kWh/m³** for the hybrid setup.
- **United States:** Due to diverse climatic conditions across regions, system performance exhibits more variability,
 - Chiller load reduction ranges from **20% to 100%** for waste heat-driven systems and **70% to 100%** for hybrid configurations.
 - Water production ranges from **2,000 to 10,000 m³/MW** for waste heat configurations and from **8,000 to 13,400 m³/MW** for hybrid setups.
 - SEC values range from **60 to 100 kWh/m³** for waste heat operation and **200 to 320 kWh/m³** for hybrid operation.