Name: Bhairshya Grupta Date: ______Page: ___ Roll no: 220295 ASSIGNMENT- 1 @ Question-1: 1.1. Picture a Scenario where you place a bot of water one a heated stove. As the water starts to boil, discuss the brimary mode of heat transfer responsible for healing the water. Is it conduction, convection, or gradiation? Provide reasons for your choice. Solution: The framery mode of heat transfer responsible for heating the water in this scenario is convection. A Reasons: - Convection involves townsfer of heat

through movement of fluids . Here, as the water heats up, molecules mar bottom of pot gain energy, becomes less dense, and rise This creates a circulation of hot water, and cooler water moves down to replace if Process of hot water rising and cold water sinking sets up a natural convection current, leading to an efficient transfer of heat throughout water in pot.

There conduction would not be effective as it relies on direct contact, but here mater molecules at top are not in direct Contact with heated Stove. 1.2 Gragine you are holding a metal rod over a flame, and after some time, you feel the other end of rod getting hat ruplain heat transfer mechanism involved in this situation and identify whether it is conduction convection or radiation. Turtify your answer. Solution: - The freat transfer mechanism unvolved in this Adustion is Conduction?

Reasons: - & Conductions is transfer of heat through

direct contact b/w particles within the material.

Here, metal rod conducts heat from hot end (done

to flame) to the tooler end (farther from plame).

* As metal rod is held over flame, the molecules at

hot end gain energy and vibrate more rapidly. This

increared kindlic rnergy is then townsferred to the

neighboring molecules through collisions

* Heat travels along metal rod in Step-lay step phous

ruth rach segment of rod passing heat to the next

Segment until it reaches the end that you feel

getting hot.

© Question 2:

Consider heat loss from 200-L cylinderical that water tank in a house to the surrounding medium. Would you consider this to be steady or transient theat transfer problem? Also, would you consider heat transfer problem to be one, two- or three-dimensional? explain.

Solution: I would consider heat loss from hot water tank in a house to be a transient heat transfer problem because water temperature must be changing ruth time. Also I would consider heat transfer problem to be two-dimension runce temperature differences (and thus heat transfer) will exist in radial tind axial directions (lout there will be symmetry about center line and no heat transfer in the azimuthal direction).

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	Atarting much an energy balance on a cylindrical shell volume element, clerus the steady one-dimensional
	chall when an every various the steady one-dimensional
	and and a multi-
	constant thermal conductivity in which heat is general
	at a rate of g and indicate what each variable represent
	i a contact of
Solution	let us consider a thin cylindrical shell blement of
	thickness 'sr' in a long cylinder Taking density of culinder to be 'C' and length
	cylinder to be 'P', specific heat to be 'C' and length' cylinder to be 'P', specific heat to be 'C' and length'
	h = 211/2 winds of heat transfer.
	Li acting normal to direction of heat transfer.
	rnergy balance on cylinderical shell rlement -> Rate of heat going in - Rate of heat coming out + Rate of theat assertation = Accumulation of heat
	heat generation = Accumulation of heat
	Qn - Qn+Δn + Eelement = Δ Eelement
	Where SEclement = Et+St - Et = mC(T++Ar - It)
	NEglement = JCA Dr Clot At - 15)
	Eccement = 9 Velement Volume Gleat generation trate
	Element = g. A & L
	rubstituting, dr-artor + gADr = PCADr (Typat-Tz)
	where A = 21T r L: Qr-Qrtor + 21TgrLDr = PCADr(Tttot-Tb)
	A to
	Dividence by ASh: - (gran - On) + 0 - PC (The - Tr) - (
	Dividing by ASh: - (artar - ar) + g = gc (Tttat-Tt)-& or (2MALA) AAR
	Taking limit Dr - 0 & Dt - 0
	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
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from fourier's faw of freat Conduction $\lim_{\Delta h \to 0} \frac{Q_{r+\Delta k} - Q_{k}}{\Delta r} = \frac{\partial Q}{\partial h} = \frac{\partial}{\partial h} \left(\frac{-K A \partial T}{\partial h} \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} A \partial T \right) \right) - \left(\frac{1}{2} \left(\frac{1}{2} -$ Rukshteiting D& D in 18: $\frac{-1}{A} \frac{\partial}{\partial h} \left(\frac{-kA}{\partial h} \right) + g = g \frac{\partial T}{\partial b}$ A = 217 r L & constant, K: thermal conductivity -> constant (ques) $\frac{1 \cdot k + \lambda}{A} \frac{A \partial T}{\partial \lambda} + g = g c \partial T$ $\frac{1}{2\pi L \cdot x} \frac{K}{\partial x} \left(\frac{2\pi x L \partial T}{\partial x} \right) + g = \frac{\beta c}{\beta L} \frac{\partial L}{\partial x}$ $\frac{2\pi t \, k \, \partial \, \left(\, r \, \partial \, I \, \right) \, + \, g = \, \beta \, c \, \partial \, I \quad \left[\, \, ; \, \, 2\pi \, k \, L \, \rightarrow \, constanl \, \right]}{2\pi t \cdot k \, \partial \, k \, \left(\, \, \partial \, k \, \right) \, + \, g = \, \beta \, c \, \partial \, I \quad \left[\, \, ; \, \, \, \, 2\pi \, k \, L \, \rightarrow \, constanl \, \right]}$ 1 d / rdt) + g = gc dt [duading by k]
rdr (dr) K K dt. i' $\alpha = k$ - thermal diffusurty so $\frac{\beta c}{k} = \frac{1}{\alpha}$ Then, $\frac{1}{r}\frac{\partial}{\partial r}\left(\frac{r}{\partial r}\right) + \frac{q}{k} = \frac{1}{d}\frac{\partial T}{\partial t}$ § generalised regulation § But in question, it is mentioned that 'steady' which means no change with time SO 27 -> 0 Here, Steady one-dimensional heat conduction Equation! $\frac{1}{h} \frac{\partial}{\partial h} \left(\frac{h}{\partial h} \right) + \frac{q}{k} = 0$ @ Question-4: Consider a medium in which heat conduction Equation given in its simplest form: $\frac{\partial^2 T}{\partial x^2} - \frac{1}{2} \frac{\partial T}{\partial t}$ (a) Is heat transfer steady or transient?

Solution: Considering a unit surface area, $A = 1m^2$.

Total rate of heat generation in the plate \rightarrow Egen = Egen V plate = $5 \times 10^6 \times 1 \times 0.03$ [: egen = $5 \times 16^6 \text{ W/m}^3$ given, $5 \times 10^6 \times 10^6 \times 10^6$ Hickness, thickness = $5 \times 10^6 \times 10^6$ Hickness = $5 \times 10^6 \times 10^6 \times 10^6$ Hickness = $5 \times 10^6 \times 10^6 \times 10^6 \times 10^6$ Hickness = $5 \times 10^6 \times 10^6 \times 10^6 \times 10^6$ Hickness = $5 \times 10^6 \times 10^6 \times 10^6 \times 10^6 \times 10^6$ Hickness = $5 \times 10^6 \times 10^$

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Hotoing rince heat is getting lost from both sides of the plate, the neat flux on surface of plate during steady operation: \Rightarrow $9 = \frac{Egen}{Area of plate} = \frac{15 \times 10^4}{2 \times (1)} = \frac{7.5 \times 10^4}{4.5 \times 10^3} = \frac{2 \times (1)}{1.5 \times 10^3} = \frac{2 \times (1)}{1.5 \times 10^3} = \frac{1.5 \times 10^3}{1.5 \times 1$

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