

Network Analysis & Systems

Koshy George



Dept. of Elect. & Comm. Engineering,
PES University;
PES Centre for Intelligent Systems

UE18EC201: Network Analysis & Systems



Disclaimer (1)

- **Errors and Omissions:** The author assumes no responsibility or liability for any errors or omissions in the contents of this file. The information is provided on an “as is” basis with no guarantees of completeness, accuracy, usefulness or timeliness and without any warranties of any kind whatsoever, express or implied.
- **Breach of Confidentiality:** The information in this file are confidential and intended solely for the non-commercial use of the individual or entity to whom this file has been given, who accepts full responsibility for its use. You are not permitted to disseminate, distribute, or copy this file. If you are not the intended recipient you are notified that disclosing, copying, distributing or taking any action in reliance on the contents of this information is strictly prohibited.



Disclaimer (2)

- **Fair Use:** This file contains copyrighted material the use of which has not always been specifically authorised by the copyright owner.
- **Copyright:** No part of this file may be reproduced, stored in a retrieval system or transmitted in any form or by any means, mechanical, electronic, photocopying, recording or otherwise without the written permission of the author. Copyright ©2019 K. George. All rights reserved.



Network Analysis and Synthesis

Part V: Network Synthesis



Overview of Syllabus

Unit V (8+2 hours) **Network Synthesis:**

- Hurwitz polynomials.
- Positive real functions.
- Elementary synthesis procedures.
- Properties of R-C impedance, R-L admittance, L-C immittance functions.
- Foster forms I and II.
- Cauer forms I and II.

Ref. C: Chapters 10 & 11.



Reference Books

C: F. F. Kuo, *Network Analysis and Synthesis*, 2nd edn.,
John Wiley, 1966.



Reference Books

- C: F. F. Kuo, *Network Analysis and Synthesis*, 2nd edn., John Wiley, 1966.
- I W. Cauer, *Synthesis of Linear Communication Networks, Vol I & II*, 2nd edn., McGraw-Hill, 1958 (Original German edition, 1941).
- II M. A. Van Valkenburg, *Introduction to Modern Network Synthesis*, John Wiley, 1960.
- III L. Weinberg, *Network Analysis and Synthesis*, McGraw-Hill, 1962.

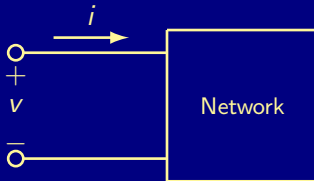


Introduction

- Realisability Conditions.
- Mathematics of Synthesis.
- Our discussion is limited to certain aspects of synthesis of LC , RL , RL and RLC networks.



Network Functions — One-Ports (1)



- The transform impedance at a port is defined as follows:

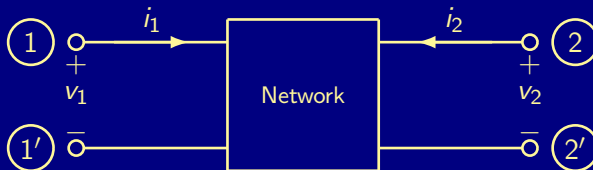
$$Z(s) = \frac{V(s)}{I(s)}$$

- The transform admittance at a port is defined as follows:

$$Y(s) = \frac{I(s)}{V(s)}$$

- These are called driving-point impedance or admittance, or together referred to as driving-point immittance.

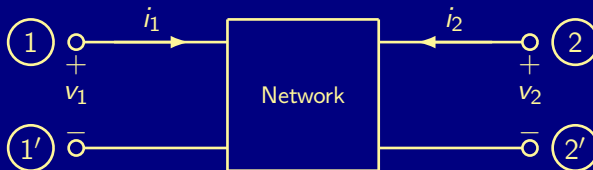
Network Functions — Two-Ports (2)



- A transfer function is used to describe the relationship between the Laplace transform of a quantity at one port to the Laplace transform of a quantity at another port.
- There are three possible forms:
 - The ratio of one voltage to another voltage: voltage transfer ratio.
 - The ratio of one current to another current: current transfer ratio.
 - The ratio of one voltage to another current or one current to another voltage.



Network Functions — Two-Ports (3)

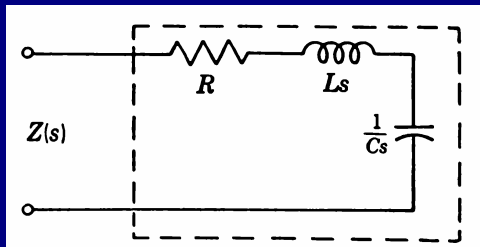


- It is a convention to define a transfer function as the ratio of an output quantity to an input quantity.
- Accordingly, only the following transfer functions are defined:

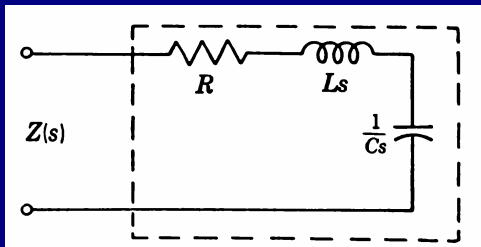
$$\frac{V_2(s)}{V_1(s)}, \quad \frac{I_2(s)}{I_1(s)}, \quad \frac{V_2(s)}{I_1(s)}, \quad \frac{I_2(s)}{V_1(s)}$$



Examples (1)



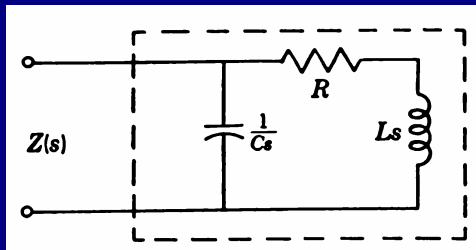
Examples (1)



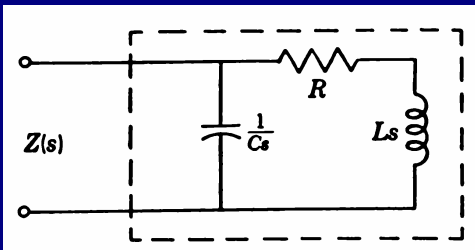
$$Z(s) = L \frac{s^2 + (R/L)s + 1/LC}{s}$$



Examples (2)



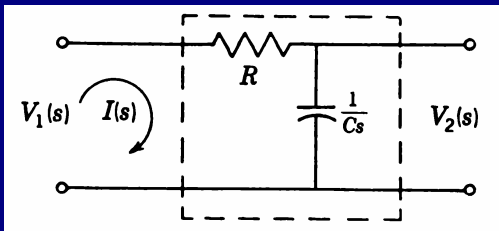
Examples (2)



$$Z(s) = \frac{1}{C} \frac{s + R/L}{s^2 + (R/L)s + 1/LC}$$



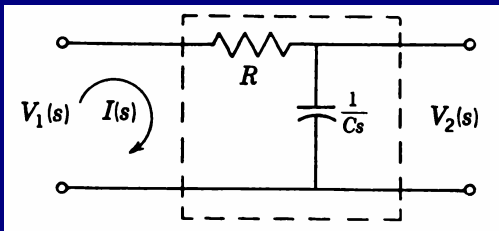
Examples (3)



$$\frac{V_2(s)}{V_1(s)} =$$



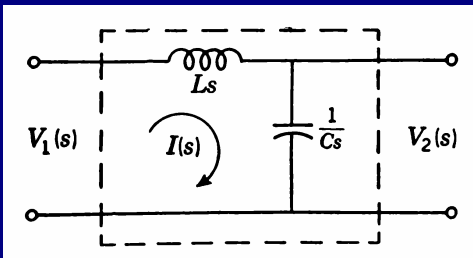
Examples (3)



$$\frac{V_2(s)}{V_1(s)} = \frac{1/RC}{s + 1/RC}$$



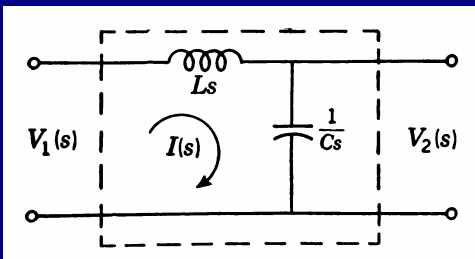
Examples (4)



$$\frac{V_2(s)}{V_1(s)} =$$



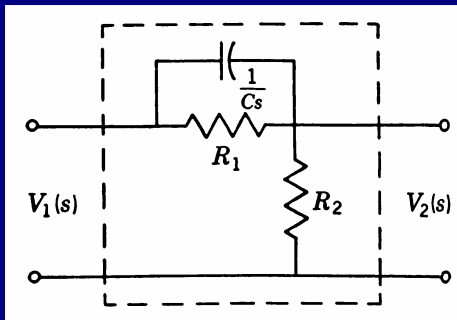
Examples (4)



$$\frac{V_2(s)}{V_1(s)} = \frac{1/LC}{s^2 + 1/LC}$$



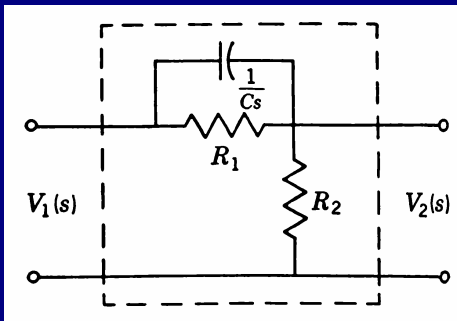
Examples (5)



$$\frac{V_2(s)}{V_1(s)} =$$



Examples (5)



$$\frac{V_2(s)}{V_1(s)} = \frac{s + 1/R_1 C}{s + (R_1 + R_2)/R_1 R_2 C}$$



Network Functions (4)

All network functions can be written in the following form:

$$\begin{aligned} H(s) &= \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)} \\ &= k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \end{aligned}$$

- $A(s) = 0$ has n roots; these are called poles.
- $B(s) = 0$ has m roots; these are called zeros.
- k is called the scale factor.
- A network function is completely specified by its poles, zeros, and the scale factor.



Network Functions (5)

$$\begin{aligned} H(s) &= \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)} \\ &= k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \end{aligned}$$

- When $n > m$, there are $n - m$ zeros at infinity.
- When $n < m$, there are $m - n$ poles at infinity.



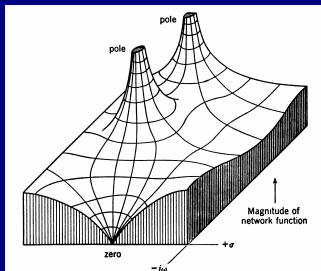
Network Functions (5)

$$\begin{aligned} H(s) &= \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)} \\ &= k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \end{aligned}$$

- When $n > m$, there are $n - m$ zeros at infinity.
- When $n < m$, there are $m - n$ poles at infinity.
- Thus, counting the number of poles and zeros at infinity, the total number of poles is equal to the total number of zeros.
- The poles or zeros may be simple (or distinct) or multiple. For example, a pole-factor $(s - p_j)^{r_j}$ is said to have multiplicity r_j .



Network Functions (6)



- The poles and zeros are called critical frequencies.
- At the poles the network function becomes infinite, and at the zeros the network function becomes zero.
- The network function has a finite non-zero value at other complex frequencies.
- Without poles and zeros, the network function is an expanse of mathematical desert.



Network Functions (7)

$$\begin{aligned} H(s) &= \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)} \\ &= k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \end{aligned}$$

- The coefficients a_i and b_j are real for network functions.
- Accordingly, such functions are called real-rational functions.



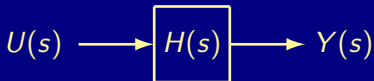
Network Functions (7)

$$\begin{aligned} H(s) &= \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)} \\ &= k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \end{aligned}$$

- The coefficients a_i and b_j are real for network functions.
- Accordingly, such functions are called real-rational functions.
- When $n \geq m$, $H(s)$ is said to be proper rational function.
- When $n > m$, $H(s)$ is said to be strictly proper rational function.
- When $n < m$, $H(s)$ is said to be improper rational function.



Network Functions (8)



- Suppose that $H(s)$ is a transfer function. Then, $Y(s)$ is the transform of the output variable of interest and $U(s)$ is the input variable of interest.
- Clearly,

$$Y(s) = H(s)U(s)$$

- Thus, if $u(t)$ is specified, the transfer function enables the determination of the response $y(t)$ of the network.



Network Functions (9)

- Suppose that the partial fraction expansion¹ is as follows:

$$H(s)U(s) = \sum_{i=1}^n \frac{c_i}{s - p_i} + \sum_{j=1}^{n'} \frac{c'_j}{s - p'_j}$$

assuming

- all the poles are simple,
 - no pole of $H(s)$ cancels a zero of $U(s)$, no pole of $U(s)$ cancels a zero of $H(s)$,
 - and that p_i corresponds to the poles of $H(s)$ and p'_j corresponds to the poles of $U(s)$.
- Then,

$$y(t) = \sum_{i=1}^n c_i e^{p_i t} + \sum_{j=1}^{n'} c'_j e^{p'_j t}$$

¹To be considered in some detail later.



Network Functions (10)

$$y(t) = \sum_{i=1}^n c_i e^{p_i t} + \sum_{j=1}^{n'} c'_j e^{p'_j t}$$

- The frequencies corresponding to p_j are called natural oscillations or free oscillations.
- The frequencies corresponding to p'_j are called forced oscillations.



Network Functions (10)

$$y(t) = \sum_{i=1}^n c_i e^{p_i t} + \sum_{j=1}^{n'} c'_j e^{p'_j t}$$

- The frequencies corresponding to p_j are called natural oscillations or free oscillations.
- The frequencies corresponding to p'_j are called forced oscillations.
- The poles determine the nature of the waveform of the output.
- The zeros determine the strength (i.e., c_i and c'_j) of each part of the response.



Network Functions — One-port (11)

- Consider the driving-point impedance $1/Cs$. There is a pole at $s = 0$ and a zero at $s = \infty$.



Network Functions — One-port (11)

- Consider the driving-point impedance $1/Cs$. There is a pole at $s = 0$ and a zero at $s = \infty$.
- At the pole frequency ($s = 0$) it behaves as an open circuit, and at the zero frequency ($s = \infty$) it behaves as a short circuit.



Network Functions — One-port (11)

- Consider the driving-point impedance $1/Cs$. There is a pole at $s = 0$ and a zero at $s = \infty$.
- At the pole frequency ($s = 0$) it behaves as an open circuit, and at the zero frequency ($s = \infty$) it behaves as a short circuit.
- Similarly, for the driving-point impedance Ls , it behaves as an open circuit at the pole frequency ($s = \infty$) and a short circuit at the zero frequency ($s = 0$).



Network Functions — One-port (11)

- Consider the driving-point impedance $1/Cs$. There is a pole at $s = 0$ and a zero at $s = \infty$.
- At the pole frequency ($s = 0$) it behaves as an open circuit, and at the zero frequency ($s = \infty$) it behaves as a short circuit.
- Similarly, for the driving-point impedance Ls , it behaves as an open circuit at the pole frequency ($s = \infty$) and a short circuit at the zero frequency ($s = 0$).
- More generally, a driving-point impedance $H(s)$ behaves as an open-circuit at a pole frequency and it behaves as a short-circuit at a zero frequency.



Network Functions — One-port (12)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .



Network Functions — One-port (12)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .
- Further, the roots are either real or complex; if the latter, they must occur as conjugate pairs.



Network Functions — One-port (12)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .
- Further, the roots are either real or complex; if the latter, they must occur as conjugate pairs.
- In a one-port network consisting of only passive elements, the response is bounded if the input is bounded.
- That is, the voltage is always bounded when a current source is applied, and the current is always bounded when a voltage source is applied.



Network Functions — One-port (13)

- Therefore, in the partial fraction expansion,

$$y(t) = \sum_{i=1}^n c_i e^{p_i t} + \sum_{j=1}^{n'} c'_j e^{p'_j t}$$

the real part of p_i , $\text{Re } p_i \leq 0$.



Network Functions — One-port (13)

- Therefore, in the partial fraction expansion,

$$y(t) = \sum_{i=1}^n c_i e^{p_i t} + \sum_{j=1}^{n'} c'_j e^{p'_j t}$$

the real part of p_i , $\text{Re } p_i \leq 0$.

- Hence, the poles and zeros of a driving-point immittance cannot lie in the right-half of s -plane.
- Those poles that lie on the imaginary axis must be simple.
- This implies that all coefficients of $B(s)$ or $A(s)$ are non-zero except if they are even (contains only even powers) or odd (contains only odd powers).



Network Functions — One-port (14)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- In a one-port the driving-point immittance Ls or Cs dominates at high-frequencies.
- Otherwise, it may act as a short-circuit in the case of $1/Ls$ or $1/Cs$, or, in their absence, the resistor dominates.



Network Functions — One-port (14)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- In a one-port the driving-point immittance Ls or Cs dominates at high-frequencies.
- Otherwise, it may act as a short-circuit in the case of $1/Ls$ or $1/Cs$, or, in their absence, the resistor dominates.
- More generally,

$$\lim_{s \rightarrow \infty} H(s) = \lim_{s \rightarrow \infty} s^{m-n}$$

- Therefore, for a passive one-port network, $n - m$ is either -1 , 0 , or 1 .
- The term $n - m$ is called relative degree. Thus, for a passive one-port the relative degree is -1 , 0 , or 1 .



Network Functions — One-port (15)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- At low frequencies $s \rightarrow 0$. Thus,

$$H(s) \approx \frac{b_{m-1} s + b_m}{a_{n-1} s + a_n}, \quad b_{m-1} \neq 0, \quad a_{n-1} \neq 0$$

and this should approach the behaviour of s , $1/s$, or a constant.



Network Functions — One-port (15)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- At low frequencies $s \rightarrow 0$. Thus,

$$H(s) \approx \frac{b_{m-1} s + b_m}{a_{n-1} s + a_n}, \quad b_{m-1} \neq 0, \quad a_{n-1} \neq 0$$

and this should approach the behaviour of s , $1/s$, or a constant.

- For an impedance, $b_m = 0$ and $a_n \neq 0$ implies an inductor, and $b_m \neq 0$ and $a_n = 0$ implies a capacitor.



Network Functions — One-port (15)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- At low frequencies $s \rightarrow 0$. Thus,

$$H(s) \approx \frac{b_{m-1} s + b_m}{a_{n-1} s + a_n}, \quad b_{m-1} \neq 0, \quad a_{n-1} \neq 0$$

and this should approach the behaviour of s , $1/s$, or a constant.

- For an impedance, $b_m = 0$ and $a_n \neq 0$ implies an inductor, and $b_m \neq 0$ and $a_n = 0$ implies a capacitor.
- The opposite holds for an admittance.



Network Functions — One-port (15)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \dots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- At low frequencies $s \rightarrow 0$. Thus,

$$H(s) \approx \frac{b_{m-1} s + b_m}{a_{n-1} s + a_n}, \quad b_{m-1} \neq 0, \quad a_{n-1} \neq 0$$

and this should approach the behaviour of s , $1/s$, or a constant.

- For an impedance, $b_m = 0$ and $a_n \neq 0$ implies an inductor, and $b_m \neq 0$ and $a_n = 0$ implies a capacitor.
- The opposite holds for an admittance.
- If $b_m \neq 0$ and $a_n \neq 0$, the behaviour is that of a resistor.



Network Functions — One-port (15)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- At low frequencies $s \rightarrow 0$. Thus,

$$H(s) \approx \frac{b_{m-1} s + b_m}{a_{n-1} s + a_n}, \quad b_{m-1} \neq 0, \quad a_{n-1} \neq 0$$

and this should approach the behaviour of s , $1/s$, or a constant.

- For an impedance, $b_m = 0$ and $a_n \neq 0$ implies an inductor, and $b_m \neq 0$ and $a_n = 0$ implies a capacitor.
- The opposite holds for an admittance.
- If $b_m \neq 0$ and $a_n \neq 0$, the behaviour is that of a resistor.
- To summarise, the terms of the lowest degree may differ at most by one.



Network Functions: Necessary Conditions (One-port) (15)

The necessary conditions for $H(s)$ to be a driving-point function:

- All coefficients must be real and positive.
- There cannot be missing terms, unless all even or all odd terms are missing.
- The real part of all poles and zeros must be negative or zero; if the real part is zero, then that pole or zero must be simple.
- The relative degree may be -1 , 0 , or 1 .
- The terms of lowest degree may differ at most by one.



Network Functions — Two-port (16)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Recall: These are transfer functions.
- Note: $1/H(s)$ does not make sense!



Network Functions — Two-port (16)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Recall: These are transfer functions.
- Note: $1/H(s)$ does not make sense!
- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .



Network Functions — Two-port (16)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Recall: These are transfer functions.
- Note: $1/H(s)$ does not make sense!
- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .
- Further, the roots are either real or complex; if the latter, they must occur as conjugate pairs.



Network Functions — Two-port (16)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- Recall: These are transfer functions.
- Note: $1/H(s)$ does not make sense!
- Since the coefficients are all real, both $B(s)$ and $A(s)$ are real for real s .
- Further, the roots are either real or complex; if the latter, they must occur as conjugate pairs.
- In a two-port consisting of only passive elements, the response is bounded if the input is bounded.



Network Functions — Two-port (17)

- Therefore, the poles of a transfer function cannot lie in the right-half of s -plane.
- Those poles that lie on the imaginary axis must be simple.
- This implies that all coefficients of $A(s)$ are non-zero except if they are even (contains only even powers) or odd (contains only odd powers).



Network Functions — Two-port (17)

- Therefore, the poles of a transfer function cannot lie in the right-half of s -plane.
- Those poles that lie on the imaginary axis must be simple.
- This implies that all coefficients of $A(s)$ are non-zero except if they are even (contains only even powers) or odd (contains only odd powers).
- There are no restrictions on the zero-locations.
- If the zeros lie in the left-half of s -plane, the network function is called minimum-phase; otherwise, they are called non-minimum-phase.



Network Functions — Two-port (18)

$$H(s) = \frac{b_0 s^m + b_1 s^{m-1} + \cdots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \cdots + a_{n-1} s + a_n} = \frac{B(s)}{A(s)}$$

- For voltage-to-voltage and current-to-current transfer functions,

$$H(s) = \frac{Z_2(s)}{Z_1(s) + Z_2(s)} \text{ or } H(s) = \frac{-Y_2(s)}{Y_1(s) + Y_2(s)}$$

and hence,

$$\deg B(s) \leq \deg A(s)$$

- For a transfer function that is an immittance at high frequencies, $H(s) = Ls$ or $H(s) = Cs$, and hence,

$$\deg B(s) \leq \deg A(s) + 1$$



Network Functions: Necessary Conditions (Two-port) (19)

The necessary conditions for $H(s)$ to be a transfer function:

- All coefficients must be real and positive.
- For the denominator polynomial, there cannot be missing terms, unless all even or all odd terms are missing.
- The real part of all poles must be negative or zero; if the real part is zero, then that pole or zero must be simple.
- There are no restrictions on the zero locations.
- For an immittance transfer function, the maximum degree of $B(s)$ is the degree of $A(s)$ plus one.
- For voltage or current ratios, the maximum degree of $B(s)$ is the degree of $A(s)$.

