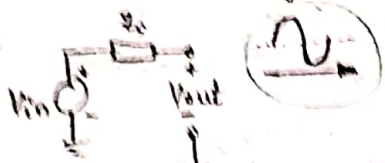


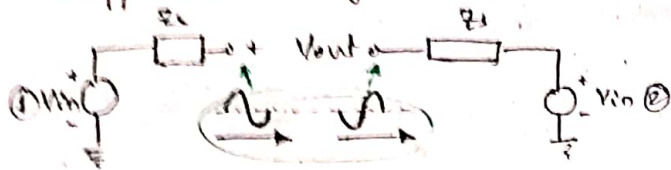
# Differential Amplifiers

## Single-ended and differential operation

- Single-ended signals



- Differential signals.

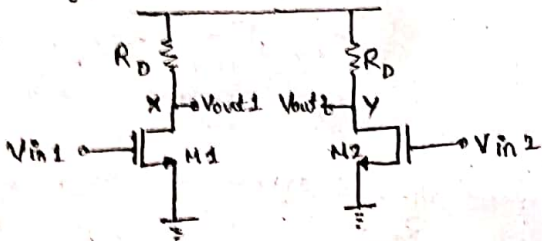


- Advantages of differential

- (i) Reduction of coupling
- (ii) Common mode rejection occurs with noisy supply voltages
- (iii) Reduction of coupled noise by differential operation.
- (iv) Increase in maximum achievable voltage swing!
- (v) Simpler biasing
- (vi) Higher linearity.

## Basic Differential Pair

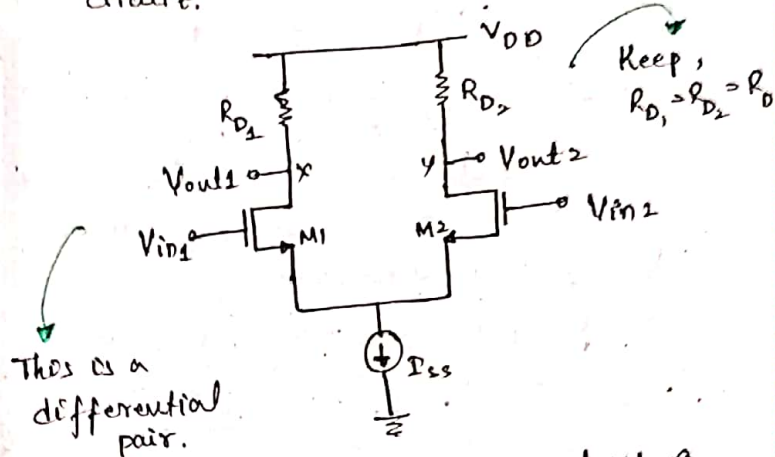
→ Simple differential circuit



This circuit has issues!

- if CM level changes, bias current of M1 & M2 changes, so gm of M1 & M2 changes. When gm of M1 & M2 changes, there is variation in small-signal gain and lowers the maximum allowable output swings.

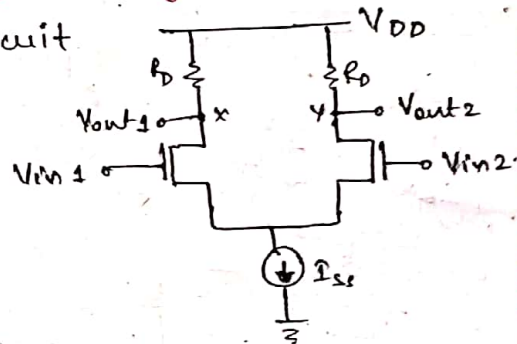
→ To solve this issue, consider the below circuit.



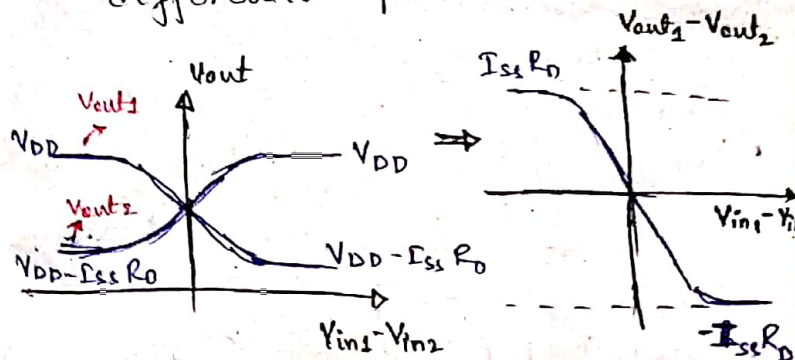
- The differential pair employs a current source  $I_{ss}$  to make  $I_{D1} + I_{D2}$  independent of  $V_{in,CM}$ .
- Thus, if  $V_{in1} = V_{in2}$ , the bias current in each transistor equals to  $\frac{I_{ss}}{2}$  and output common-mode level is  $V_{DD} - \frac{R_D I_{ss}}{2}$ .

## Qualitative Analysis

- For the circuit



⊙ Input-output characteristics of differential pair.



→ Conclusions from I/p-O/p characters.

⊙ For  $\frac{I_{ss}}{2}$  to be current from mosfets then  $V_{in1} = V_{in2}$

⊙ If  $V_{in1} \uparrow$  than  $V_{in2}$ ,  $M_1$  carries greater current than  $M_2$ . Hence  $V_{out1}$  drops below  $V_{out2}$

⊙ If  $V_{in1}$  is very large, then  $M_2$  is off, hence  $V_{out1} = V_{DD} - I_{ss}R_D$  (Min o/p)  
 $V_{out2} = V_{DD}$  (Max o/p)

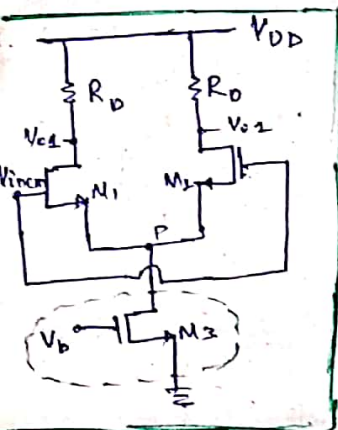
⊙ Small signal gain is maximum for  $V_{in1} = V_{in2}$ .

The small signal gain  $\downarrow$  if  $V_{in1} - V_{in2} \uparrow$

So, have a common mode behaviour, i.e. connect  $V_{in1}$  and  $V_{in2}$  to a single source called  $V_{in,cm}$

case 1:  $V_{in,cm} = 0$ , both  $M_1$  and  $M_2$  are off.  $\therefore I_{D3} = 0$  making  $I_{D1} = I_{D2} = 0$

Hence,  $M_3$  can be replaced with resistor  $R_{on}$ , since  $M_3$  is in deep triode region



case 2:  $V_{in,cm}$  becomes more positive.

• both  $M_1$  and  $M_2$  turns on, if  $V_{in,cm} > V_{th}$ . Then later  $I_{D1}$  and  $I_{D2} \uparrow$

hence  $V_p \uparrow$

• For a significant high  $V_{in,cm}$ , the  $V_{DS}$  of  $M_3$  exceeds  $V_{GS3} - V_{th3}$ , thus allowing it to operate in saturation.

• Hence, for proper operation,

$$V_{in,cm} \geq V_{GS1} + (V_{GS3} - V_{th3})$$

case 3: What if  $V_{in,cm}$  further  $\uparrow$ !

•  $M_1$  &  $M_2$  enters triode region. if

$$V_{in,cm} > V_{out1} + V_{th}$$

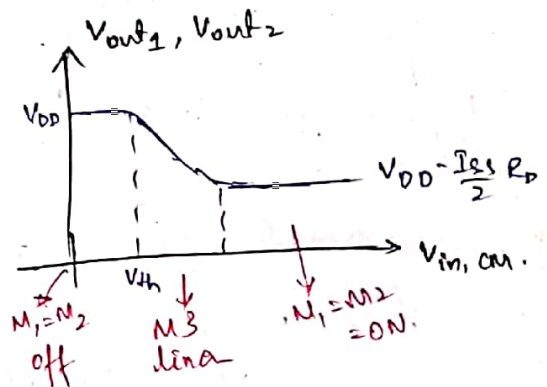
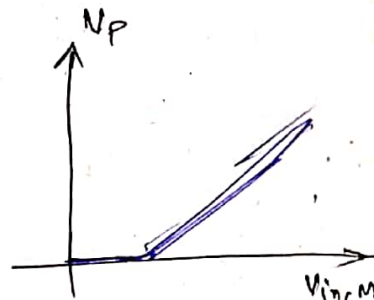
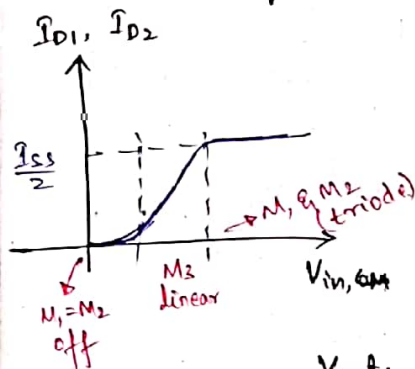
$$V_{in,cm} > V_{DD} - \frac{R_D I_{ss}}{2} + V_{th}$$

• This ~~also~~ restricts the maximum  $V_{in,cm}$  to be minimum value b/w.  $[V_{DD} - \frac{R_D I_{ss}}{2}, V_{DD}]$

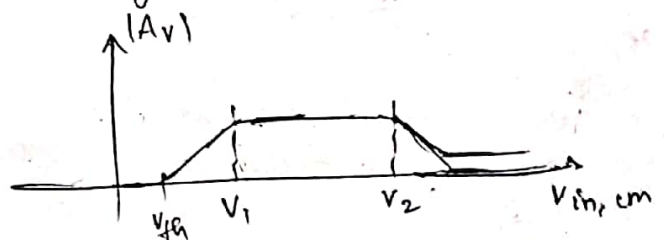
conclusion ⊙ formulae

$$V_{GS1} + (V_{GS3} - V_{th3}) \leq V_{in,cm} \leq \min \left[ V_{DD} - \frac{R_D I_{ss}}{2} + V_{th}, V_{DD} \right]$$

⊙ Graphs:

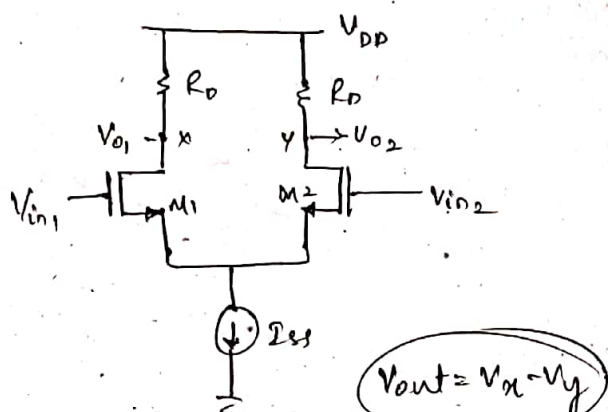


→ Small-signal differential gain of D.P.





→ Small Signal - (half circuit analysis only)



$$A_v = \frac{V_{out}}{V_{in1} - V_{in2}} = -g_m R_0$$

⇒ for half circuit

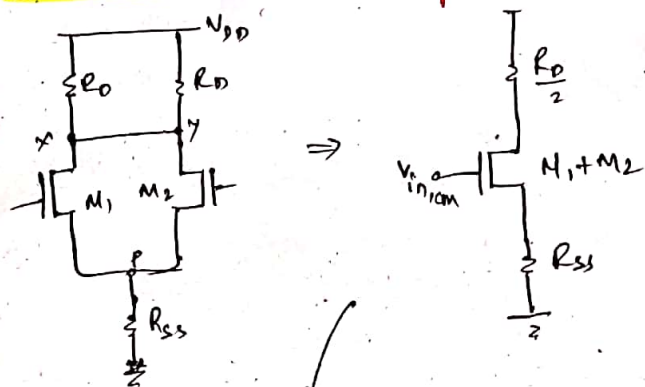
$$A_v = \frac{V_{out}}{V_{in1} - V_{in2}} \times \frac{1}{2} = \frac{-g_m R_0}{2}$$

⊙ Common-mode response due to mismatch in  $R_0$  ( $R_{01} \neq R_{02}$ )

⊙ Common-mode response due to mismatch in transistor ( $M_1 \neq M_2$ )

$$A_v = \frac{-\Delta g_m R_0}{1 + (g_{m1} + g_{m2}) R_{ss}}$$

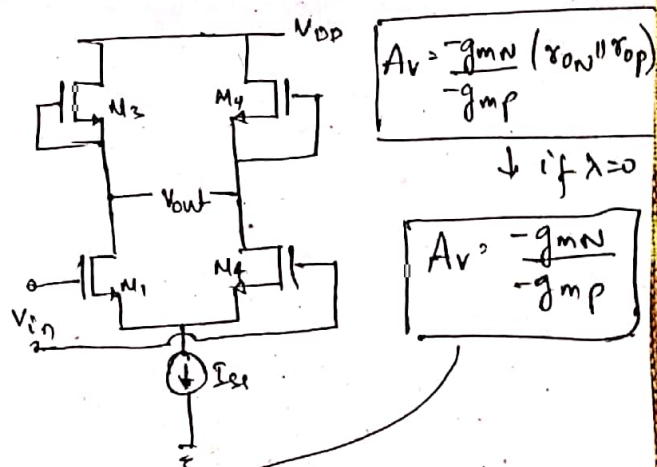
### ⊙ Common-Mode Response



gain

$$A_{v_{cm}} = \frac{V_{out}}{V_{in,cm}} \quad A_v = \frac{R_0/2}{\frac{1}{2g_m} + R_{ss}}$$

### ⊙ Differential Pair with MOS Loads



$$A_v = \frac{-g_{mN} (r_{oN} || r_{oP})}{-g_{mP}}$$

↓ if  $\lambda = 0$

$$A_v = \frac{-g_{mN}}{-g_{mP}}$$

~~$$A_v = \frac{-g_{mN} (r_{oN} || r_{oP})}{-g_{mP}}$$~~

$$A_v = - \sqrt{\frac{\mu_n (\frac{W}{L})_N}{\mu_p (\frac{W}{L})_P}}$$