

PROBLEM 3.18 (converted to PMOS)

$$0.18 \mu\text{m}$$

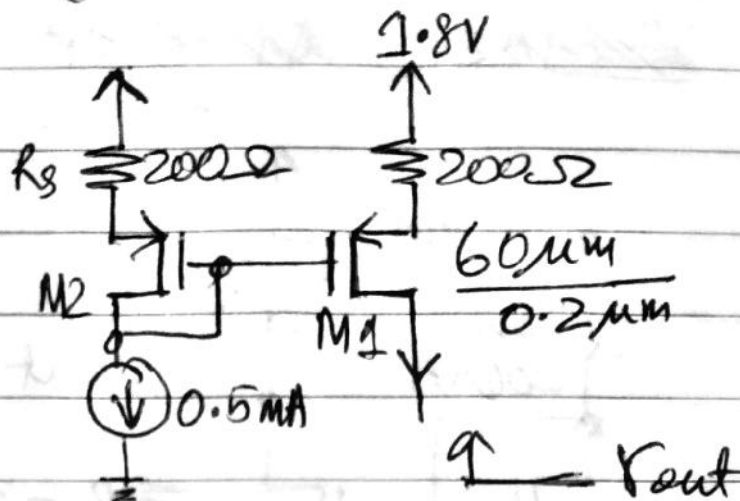
$$\mu_{p\text{cox}} = 70 \mu\text{A/V}^2$$

$$V_p = -0.45$$

$$\lambda \cdot L = 0.08 \mu\text{m/V}$$

(a)

$$V_{\text{out}} = V_{\text{ds1}} (1 + g_{m1} R_s)$$



$$r_{\text{ds1}} = \frac{1}{\lambda \cdot I_{\text{out}}} = \frac{L}{(\lambda \cdot L) I_{\text{out}}} = \frac{0.2 \mu\text{m}}{0.08 \frac{\mu\text{m}}{\text{V}} \cdot 0.5 \text{mA}} = 5 \text{k}\Omega$$

$$g_{m1} = \sqrt{2 I_D \mu_{p\text{cox}} \frac{W}{L}} = \sqrt{2 \times 0.5 \text{mA} \times 70 \frac{\mu\text{A}}{\text{V}^2} \times \frac{60}{0.2}} = 4.5 \text{mS}$$

$$V_{\text{out}} = 5 \text{k}\Omega (1 + 4.5 \times 0.2) = 5 \text{k}\Omega \times 1.9 = \underline{9.5 \text{k}\Omega}$$

(b) For $R_s = 0$, $V_{\text{out}} = r_{\text{ds1}} = \underline{5 \text{k}\Omega}$

(c) $V_o(\text{max}) = ?$ i.e. max voltage M1 is active

$$V_o(\text{max}) = 1.8 \text{V} - I_{\text{out}} R_s - V_{\text{eff1}} \quad g_m = \frac{2 I_D}{V_{\text{eff1}}}$$

$$= 1.8 \text{V} - 0.2 \times 0.5 - \frac{2 \times 0.5 \text{mA}}{4.5 \text{mS}}$$

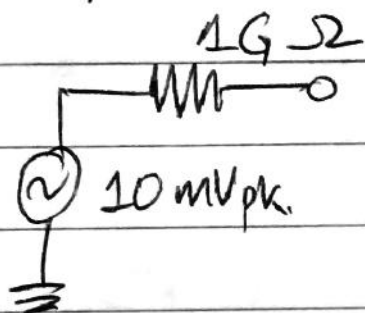
$$= 1.8 - 0.1 - 0.22 = 1.48 \text{V}$$

DESIGN PROBLEM

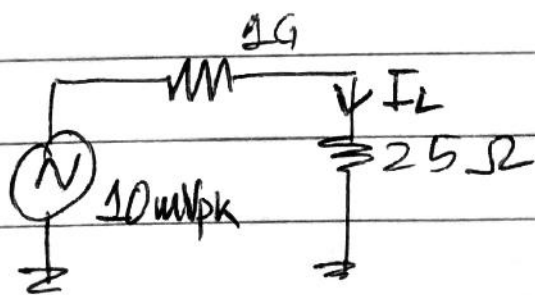
DESIGN A HEADPHONE AMP

.. Deliver 25 mW of peak power to a 25 Ω headphone.

Thevenin model of a MEMS microphone.



Let's see how much power can be delivered directly.

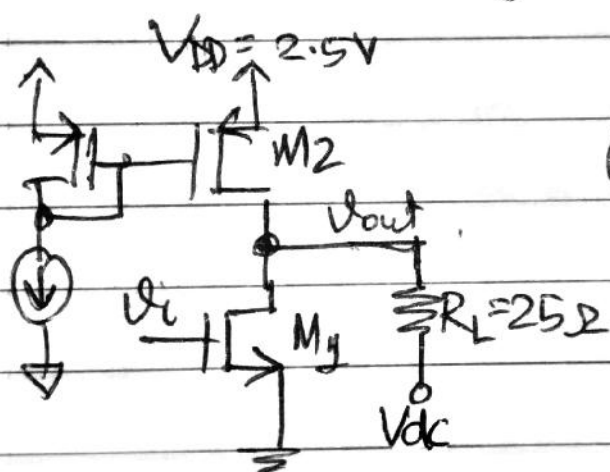


$$P_{out\ pk} = I_L^2 R = \left(\frac{10\ mV_p}{1G + 25\ \Omega} \right)^2 \times 25 \approx 0$$

How about common-source amplifier.
How much gain do we need.

$$P_{out} = \frac{V^2}{R} = 25 \text{ mW} \Rightarrow V \approx 0.8 \text{ V}$$

$$\therefore \text{Voltage gain} = \frac{0.8 \text{ V}}{0.01 \text{ V}} = \underline{\underline{80}}$$



$$\text{Gain} = g_{m1} \cdot (r_{ds1} \parallel r_{ds2} \parallel R_L)$$

$$\therefore R_L \ll r_{ds1,2}$$

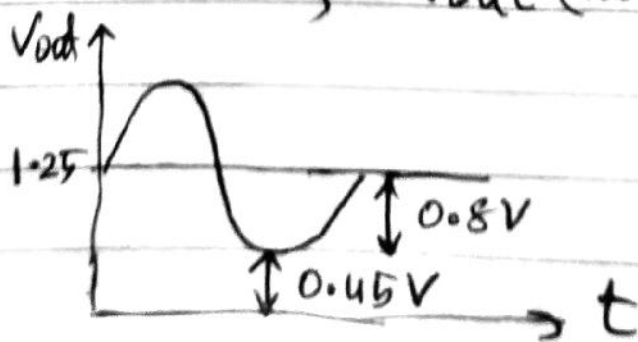
$$\text{Gain} \approx g_{m1} \cdot R_L$$

$$\Rightarrow g_{m1} = \frac{80}{25 \Omega} = \underline{\underline{3.2}}$$

Too high

Let's calculate V_{eff1}

We can assume $V_{out}(DC) = 1.25 \text{ V}$ when there is no signal. Since the output swings $\pm 0.8 \text{ V}$, $V_{out}(min) = 1.25 - 0.8 \text{ V} = 0.45 \text{ V}$



So Let's

$$V_{eff1} = 400 \mu\text{V}$$

$$g_{m1} = \frac{2I_D}{V_{eff1}} \Rightarrow I_D = \frac{g_{m1} \times V_{eff1}}{2}$$

$$= \frac{3.28 \times 0.4V}{2} = \underline{\underline{0.64A!!}}$$

Power consumed in the CS stage

$$= 2.5V \times 0.64 = \underline{\underline{1.6W}}$$

TOO HIGH

Now what if the CS stage is not driving the load directly.

$$A_v = g_{m1} \times (r_{ds1} \parallel r_{ds2}) \approx g_{m1} \cdot \frac{r_{ds}}{2}$$

$$A_v = \frac{2I_D}{V_{eff}} \times \frac{1}{2 \cdot \lambda \cdot I_D} = \frac{L}{V_{eff} \cdot (\lambda \cdot L)}$$

Let's design this $0.18 \mu m$ CMOS (see P3.10)
where $\lambda \cdot L = 0.08 \mu m/V$

$$\Rightarrow L = A_v \cdot V_{eff} \cdot (\lambda \cdot L) = 80 \times 0.4V \times 0.08 \frac{\mu m}{V}$$

$$\boxed{L = 2.56 \mu m.}$$

* we can choose a much smaller current.

* NOTE M1 can be in subthreshold to save more power.

Now we follow the CS stage with source follower.

See Prob 3.15

$$A_v \approx \frac{g_{m1}}{g_{m1} + 1/R_L} = 0.8 \Rightarrow g_{m1} = -\frac{A_v/R_L}{A_v - 1}$$

$$\Rightarrow g_{m1} = \frac{-0.8/25}{0.8 - 1} = 160 \text{ mS}$$

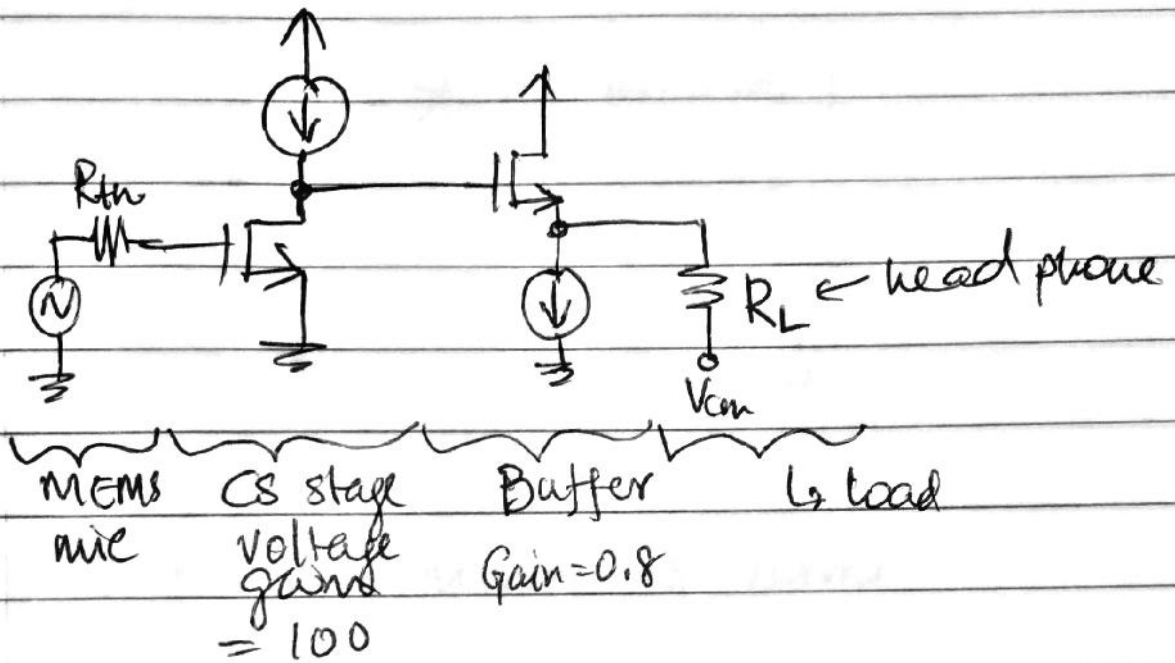
$$\text{or } g_{m1} = \frac{2I_D}{V_{eff}} = 160 \text{ mS}$$

$$\text{For } V_{eff} = 0.4 \text{ V}$$

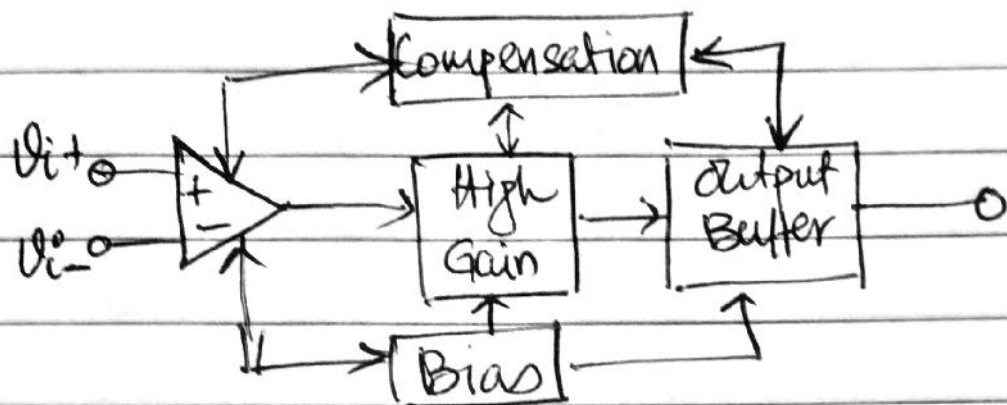
$$I_D = \frac{0.16 \times 0.4}{2} = \underline{\underline{32 \text{ mA}}}$$

$$\begin{aligned} \text{Peak current reqd. thru load} &= \frac{0.8}{25} = 32 \text{ mA} \\ &= \underline{\underline{32 \text{ mA}}} \end{aligned}$$

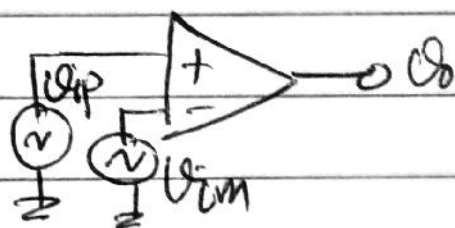
Solution



GENERAL BLOCK DIAGRAM OF A 2-STAGE OP-AMP



Some definition of terms



① Differential Input

$$V_{id} = V_{ip} - V_{im}$$

② Common-mode input

$$V_{cm} = \frac{V_{ip} + V_{im}}{2}$$

③ Differential Gain = $A_d = \frac{V_o}{V_{id}}$

④ Common-mode Gain = $A_{cm} = \frac{V_o}{V_{cm}}$

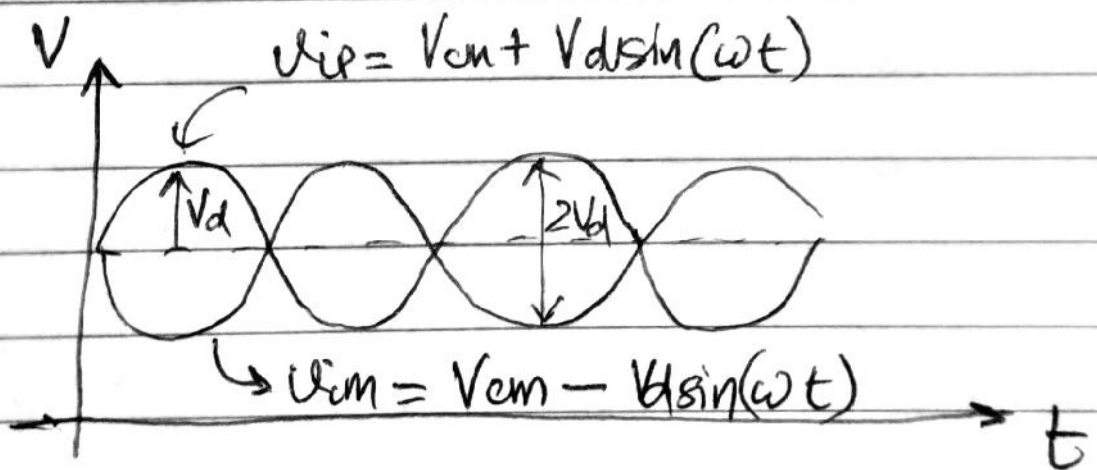
When input has both diff. & common-mode

$$V_o = A_d \cdot (V_{ip} - V_{im}) + A_{cm} \left(\frac{V_{ip} + V_{im}}{2} \right)$$

Ideally you want:

- ① $A_d \rightarrow \text{high} \rightarrow \infty$
- ② $A_{cm} \rightarrow \text{zero} \rightarrow \text{why?}$

Time-domain view of diff & CM signal



$$V_{id} = 2V_d \sin(\omega t)$$

$$V_{icm} = V_{cm}$$

Now let's add a time-varying CM signal say $V_n \sin(\omega t)$

$$V_{ip} = V_{cm} + V_n \sin(\omega t) + V_d \sin(\omega t)$$

$$V_{im} = V_{cm} + V_n \sin(\omega t) - V_d \sin(\omega t)$$

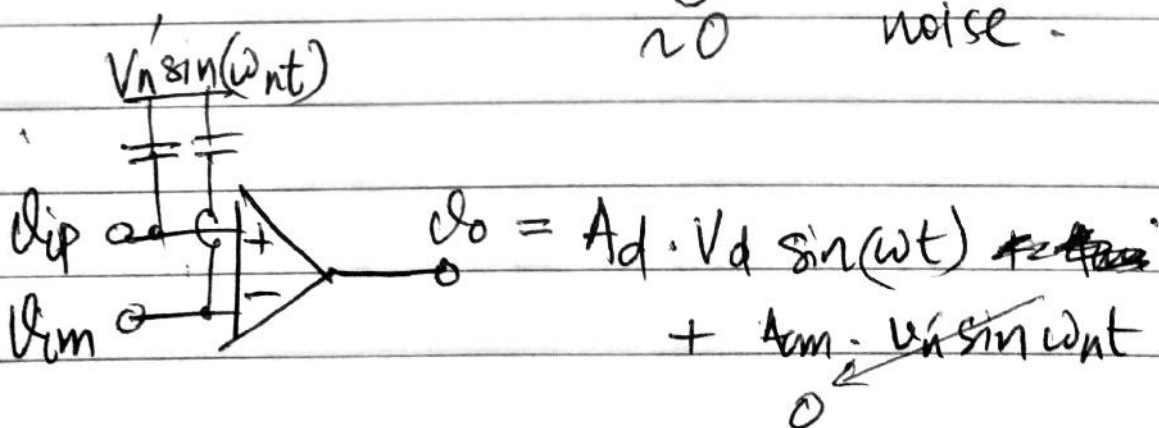
$$V_{id} = 2V_d \sin(\omega t)$$

$$V_{icm} = V_{cm} + \underbrace{V_n \sin(\omega t)}$$

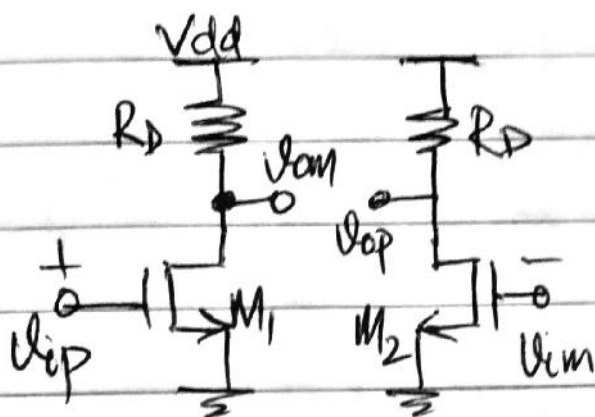
If this noise coupling to inputs then it will be rejected because

$$V_o = A_d \cdot V_d + A_{cm} \cdot V_{icm}$$

\downarrow \downarrow
 ≈ 0 noise



Simple Differential Pair



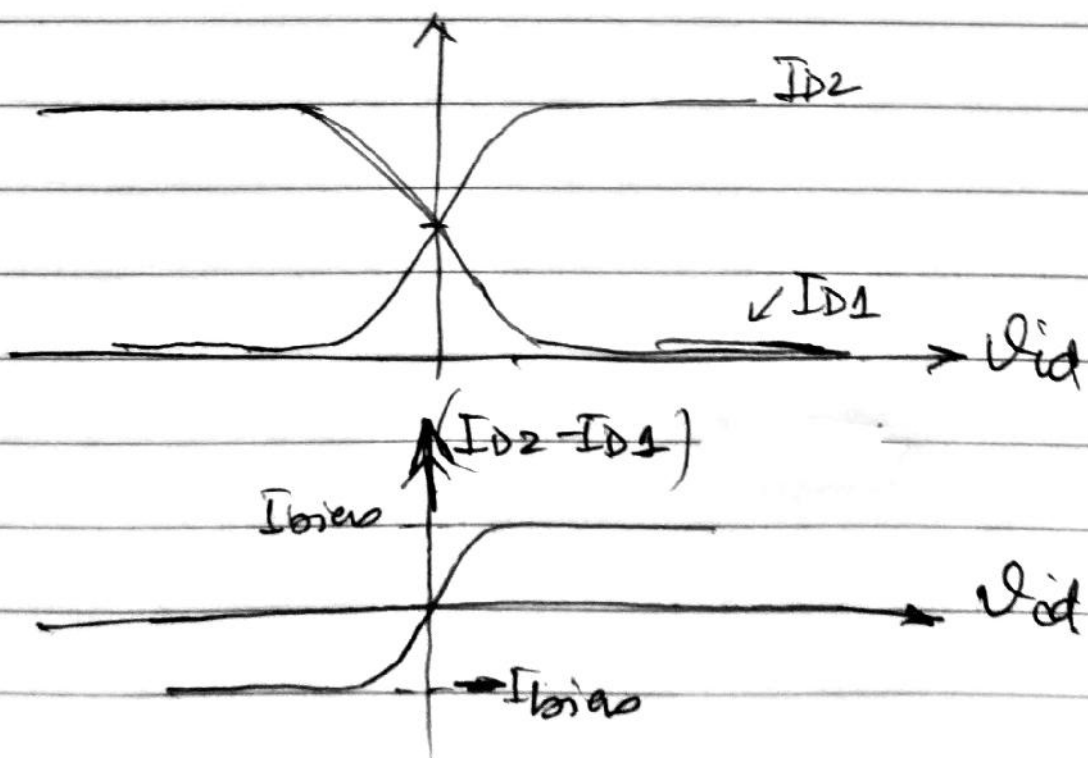
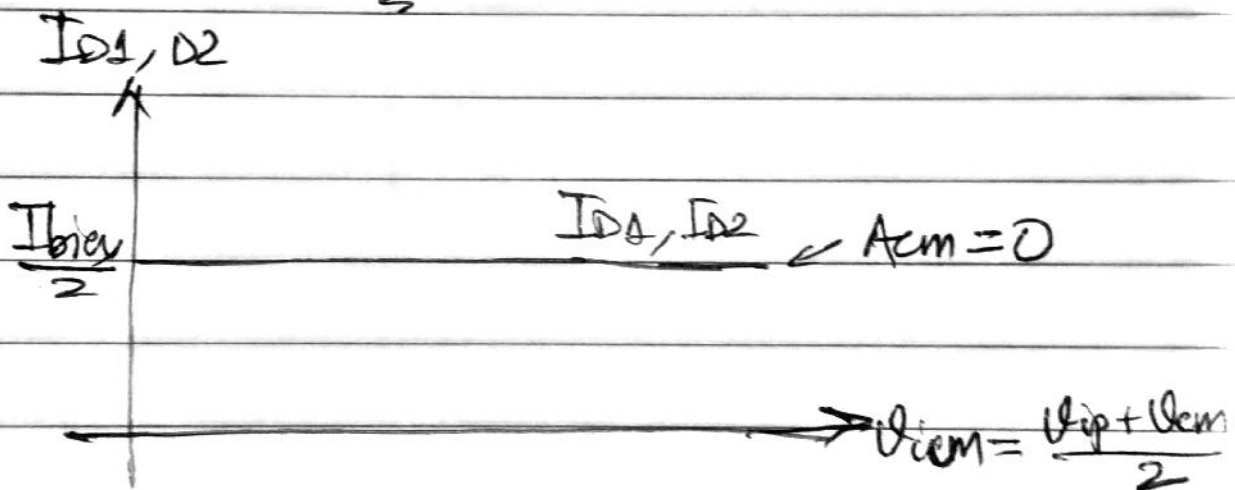
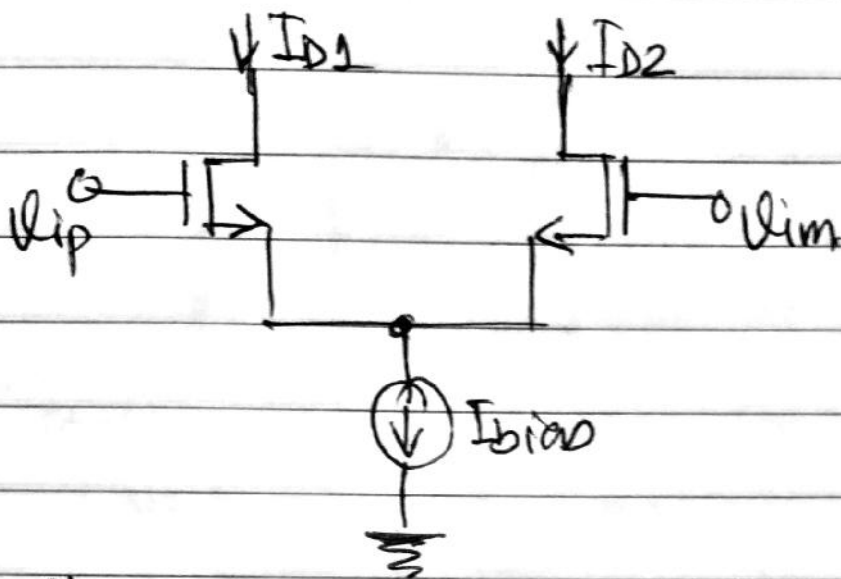
$$v_{op} = -g_m R_D v_{im}$$

$$v_{om} = -g_m R_D v_{ip}$$

$$A_d = \frac{v_{op} - v_{om}}{v_{ip} - v_{im}} = g_m R_L$$

$$A_{cm} = \frac{(v_{op} + v_{om})/2}{(v_{ip} + v_{im})/2} = -g_m R_L \neq 0$$

Basic Differential Pair



Differential Pair with CM Load.

