

1. 推导“多刚体”模型的ZMP计算公式

$$p_x = \frac{Mgx + p_z \dot{p}_x - \dot{L}_y}{Mg + \dot{p}_z} \quad p_y = \frac{Mgy + p_z \dot{p}_y + \dot{L}_x}{Mg + \dot{p}_z}$$

I'll do some review first.

recall the 10 parameters to describe a robot

Mass : M

Center of Mass (C.M) : $C \equiv [c_x \ c_y \ c_z]^T$ } about world reference frame

Momentum : $P \equiv [p_x \ p_y \ p_z]^T$

Angular momentum : $L \equiv [L_x \ L_y \ L_z]^T$ } about origin

$$\textcircled{1} \quad \dot{C} = v = P/M \rightarrow \dot{C} = P/M$$

$$\textcircled{2} \quad P = \dot{C}M, \dot{P} = \ddot{C}M = f_{all} \rightarrow \dot{P} = f_{all}$$

$$\textcircled{3} \quad L = C \times P,$$

$$\begin{aligned} \dot{L} &= \dot{C} \times P + C \times \dot{P} \\ &= \dot{C} \times \dot{C}M + C \times f_{all} \\ &= \tau \end{aligned}$$

$$\rightarrow \dot{L} = \tau_{all}$$

denote f as all forces but gravity.

$$\text{then } \dot{P} = Mg + f$$

denote τ as the momentum without the gravity effect

$$\text{then } \dot{L} = C \times Mg + \tau$$

Now we derive ZMP

$$\tau = p \times f + \tau_p$$

\uparrow world 处 torque \uparrow ZMP 点 \uparrow ZMP 点 处 力 \uparrow ZMP 处 torque, where $\tau_{px} = \tau_{py} = 0$

we will need to transfer the τ to origin of zw frame

$$\text{as } \begin{cases} \dot{P} = Mg + f \\ \dot{L} = C \times Mg + \tau \end{cases} \text{ are all expressed in zw frame.}$$

apply $\tau_p = \tau - p \times f$ to above.

$$\begin{aligned} \tau_p &= \dot{L} - c \times M g - p \times (\dot{p} - M g) \\ \tau_p &= \dot{L} - c \times M g + \dot{p} \times p - M g \times p \end{aligned} \quad \left\{ \begin{array}{l} a \equiv [a_x \ a_y \ a_z]^T \\ b \equiv [b_x \ b_y \ b_z]^T \\ a \times b = \begin{pmatrix} a_y b_z - a_z b_y \\ a_z b_x - a_x b_z \\ a_x b_y - a_y b_x \end{pmatrix} \end{array} \right.$$

scalar \downarrow vector

$$\tau_{px} = \dot{L}_x - M(c_y g_z - c_z g_y) + \dot{p}_z p_y - \dot{p}_y p_z - M(g_y p_z - g_z p_y) = 0$$

$$\tau_{py} = \dot{L}_y - M(c_z g_x - c_x g_z) + \dot{p}_z p_x - \dot{p}_x p_z - M(g_z p_x - g_x p_z) = 0$$

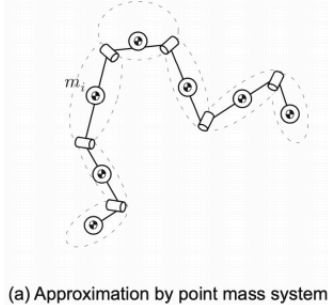
$$\begin{aligned} \text{denote } [c_x \ c_y \ c_z]^T &\equiv [x \ y \ z]^T \\ [g_x \ g_y \ g_z]^T &\equiv [0 \ 0 \ -g]^T \end{aligned}$$

$$\text{then } \begin{cases} \dot{L}_x - M g y + \dot{p}_z p_y - \dot{p}_y p_z + M g p_y = 0 \\ \dot{L}_y + M g x + \dot{p}_z p_x - \dot{p}_x p_z - M g p_x = 0 \end{cases}$$

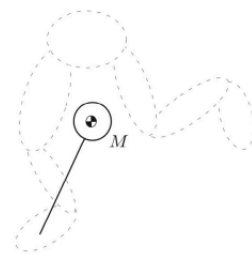
$$\text{solve for } p_x \text{ and } p_y: \quad p_x = \frac{M g x + p_z \dot{p}_y - \dot{L}_y}{M g + \dot{p}_z}$$

$$p_y = \frac{M g y + p_z \dot{p}_x + \dot{L}_x}{M g + \dot{p}_z} \quad \square$$

2. 推导“质点系”模型和“单质点”模型的ZMP计算公式



(a) Approximation by point mass system



(b) Approximation by a single point mass

(c)

$$P = \sum_{i=1}^N p_i = \sum_{i=1}^N \dot{c}_i m_i$$

$$L = \sum_{i=1}^N c_i \times p_i = \sum_{i=1}^N m_i (c_i \times \dot{c}_i)$$

$$\text{we denote } C \equiv [c_x \ c_y \ c_z]^T \equiv [x \ y \ z]^T$$

$$\text{then } \begin{cases} P_x = \sum_{i=1}^N m_i \dot{x}_i \\ P_y = \sum_{i=1}^N m_i \dot{y}_i \\ P_z = \sum_{i=1}^N m_i \dot{z}_i \end{cases} \quad \begin{cases} L_x = \sum_{i=1}^N m_i (y_i \dot{z}_i - z_i \dot{y}_i) \\ L_y = \sum_{i=1}^N m_i (z_i \dot{x}_i - x_i \dot{z}_i) \\ L_z = \sum_{i=1}^N m_i (x_i \dot{y}_i - y_i \dot{x}_i) \end{cases}$$

By last problem:

$$P_x = \frac{Mg_x + P_z \dot{P}_x - \dot{L}_y}{Mg + \dot{P}_z} = \frac{P_x g + P_z \dot{P}_x - \dot{L}_y}{Mg + \dot{P}_z}$$

$$P_y = \frac{Mg_y + P_z \dot{P}_y + \dot{L}_x}{Mg + \dot{P}_z} = \frac{P_y g + P_z \dot{P}_y + \dot{L}_x}{Mg + \dot{P}_z}$$

$$\begin{cases} \dot{P}_x = \sum_{i=1}^N m_i \ddot{x}_i \\ \dot{P}_y = \sum_{i=1}^N m_i \ddot{y}_i \\ \dot{P}_z = \sum_{i=1}^N m_i \ddot{z}_i \end{cases} \quad \begin{cases} \dot{L}_x = \sum_{i=1}^N m_i (\dot{y}_i \dot{z}_i + y_i \ddot{z}_i - \dot{z}_i \dot{y}_i - z_i \ddot{y}_i) = \sum_{i=1}^N m_i (y_i \ddot{z}_i - z_i \ddot{y}_i) \\ \dot{L}_y = \sum_{i=1}^N m_i (\dot{z}_i \dot{x}_i + x_i \ddot{z}_i - \dot{x}_i \dot{z}_i - z_i \ddot{x}_i) = \sum_{i=1}^N m_i (x_i \ddot{z}_i - z_i \ddot{x}_i) \end{cases}$$

$$P_x = \frac{\sum_{i=1}^N m_i x_i g + P_z m_i \ddot{x}_i - m_i (x_i \ddot{z}_i - z_i \ddot{x}_i)}{\sum_{i=1}^N m_i g + m_i \ddot{z}_i}$$

$$P_y = \frac{\sum_{i=1}^N m_i y_i g + P_z m_i \ddot{y}_i + m_i (y_i \ddot{z}_i - z_i \ddot{y}_i)}{\sum_{i=1}^N m_i g + m_i \ddot{z}_i}$$

simplify we'll have :

$$P_x = \frac{\sum_{i=1}^N m_i [x_i (g + \ddot{z}_i) - (z_i - P_z) \ddot{x}_i]}{\sum_{i=1}^N m_i (g + \ddot{z}_i)}$$

$$P_y = \frac{\sum_{i=1}^N m_i [y_i (g + \ddot{z}_i) - (z_i - P_z) \ddot{y}_i]}{\sum_{i=1}^N m_i (g + \ddot{z}_i)}$$

(b)

$$P = M\dot{c} \quad L = c \times M\dot{c}$$

$$\begin{cases} \dot{P}_x = M\ddot{x} \\ \dot{P}_y = M\ddot{y} \\ \dot{P}_z = M\ddot{z} \end{cases} \quad \begin{cases} \dot{L}_x = M(y\ddot{z} - z\ddot{y}) \\ \dot{L}_y = M(z\ddot{x} - x\ddot{z}) \\ \dot{L}_z = M(x\ddot{y} - y\ddot{x}) \end{cases}$$

$$P_x = \frac{p_x g + p_z \dot{p}_x - \dot{L}_y}{M_g + \dot{p}_z} = \frac{M \dot{x} g + p_z M \ddot{x} - M_3 \ddot{x} + M \ddot{x}}{M_g + M \ddot{z}} = x - \frac{(z - p_z) \ddot{x}}{\ddot{z} + g}$$

$$P_y = \frac{p_y g + p_z \dot{p}_y + \dot{L}_x}{M_g + \dot{p}_z} = \frac{M \dot{y} g + p_z M \ddot{y} + M \ddot{y} - M_y \ddot{x}}{M_g + M \ddot{z}} = y - \frac{(z - p_z) \ddot{y}}{\ddot{z} + g}$$

3. 阅读论文，总结满足ZMP稳定条件的双足步规划方法

Q. Huang *et al.*, "Planning walking patterns for a biped robot," *IEEE Transactions on Robotics and Automation*, vol. 17, no. 3, pp. 280-289, 2001.

<https://ieeexplore.ieee.org/document/938385>

(可在Sakai “课程资料” / “作业附件” 中下载)

34

Overview: 还是用中文说比较清楚，该方法在给定环境和行走机器人的运动的情况下，首先将行走机器人的hip ankle关节的平面轨迹x z theta约束到仅包含2个变量参数（x_ed x_sd）的曲线族，然后遍历这两个变量参数的取值范围，选择ZMP宽裕度最高、速度最快的一组解，然后利用hip ankle曲线进行逆运动学求解关节角度，控制机器人关节从而实现行走。

机器人的模型固定参数和变量参数如下

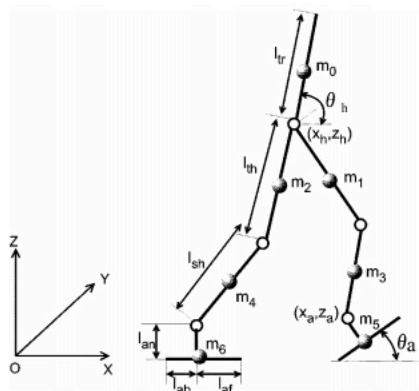


Fig. 1. Model of the biped robot.

fig1所有参数都是机器人结构决定的，fig2的qf qb参数是事先确定不变的，fig2的xed xsd是针对每一步需要搜索确定的。

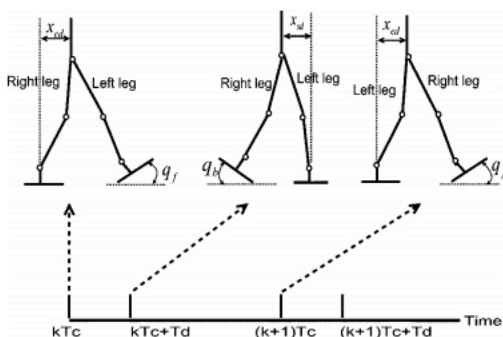


Fig. 2. Walking cycle.

整个算法的流程如下，我们先 claim 如下的 hip 和 ankle 轨迹：

$$x_h(t) = \begin{cases} kD_s + x_{ed}, & t = kT_c \\ (k+1)D_s - x_{sd}, & t = kT_c + T_d \\ (k+1)D_s + x_{ed}, & t = (k+1)T_c. \end{cases} \quad z_h(t) = \begin{cases} H_{hmin}, & t = kT_c + 0.5T_d \\ H_{hmax}, & t = kT_c + 0.5(T_c - T_d) \\ H_{hmin}, & t = (k+1)T_c + 0.5T_d. \end{cases}$$

theta hip 即躯干的倾斜角度，一直为 0 即躯干保持竖直。

$$\theta_a(t) = \begin{cases} q_{gs}(k), & t = kT_c \\ q_b, & t = kT_c + T_d \\ -q_f, & t = (k+1)T_c \\ -q_{ge}(k), & t = (k+1)T_c + T_d \end{cases}$$

$$x_a(t) = \begin{cases} kD_s, & t = kT_c \\ kD_s + l_{an} \sin q_b + l_{af}(1 - \cos q_b), & t = kT_c + T_d \\ kD_s + L_{ao}, & t = kT_c + T_m \\ (k+2)D_s - l_{an} \sin q_f - l_{ab}(1 - \cos q_f), & t = (k+1)T_c \\ (k+2)D_s, & t = (k+1)T_c + T_d \end{cases}$$

$$z_a(t) = \begin{cases} h_{gs}(k) + l_{an}, & t = kT_c \\ h_{gs}(k) + l_{af} \sin q_b + l_{an} \cos q_b, & t = kT_c + T_d \\ H_{ao}, & t = kT_c + T_m \\ h_{ge}(k) + l_{ab} \sin q_f + l_{an} \cos q_f, & t = (k+1)T_c \\ h_{ge}(k) + l_{an}, & t = (k+1)T_c + T_d \end{cases}$$

可以看到，上述的轨迹中，除了 $q_{gs}(k)$ $q_{ge}(k)$ $h_{gs}(k)$ $h_{ge}(k)$ x_{sd} x_{ed} 外，都是机器人结构的固有参数或实现设定的常数参数。而 these 与 k 相关的参数是由环境确定的，机器人在行走的过程中利用传感器确定。

利用这些关键点，结合速度与位置的关系，可以使用多项式插值，获得运动轨迹。具体的边界条件如下：

$$\begin{cases} \dot{\theta}_a(kT_c) = 0 \\ \dot{\theta}_a((k+1)T_c + T_d) = 0 \\ \dot{x}_a(kT_c) = 0 \\ \dot{x}_a((k+1)T_c + T_d) = 0 \\ \dot{z}_a(kT_c) = 0 \\ \dot{z}_a((k+1)T_c + T_d) = 0. \end{cases} \quad \begin{cases} \dot{x}_h(kT_c) = \dot{x}_h(kT_c + T_c) \\ \ddot{x}_h(kT_c) = \ddot{x}_h(kT_c + T_c). \end{cases}$$

利用上述 claim 的轨迹我们可以算出给定 x_{sd} x_{ed} 的 ZMP，并与支撑多边形比较，算出的宽裕度。 x_{sd} 和 x_{ed} 从 0 开始依次增加直到宽裕度满足要求。整体算法的流程如右图所示：

