UNIVERSITÀ DEGLI STUDI DI TRENTO

DEPARTMENT OF MATHEMATICS
MASTER DEGREE IN MATHEMATICS

THESIS

Modeling and simulation of craniovertebral decompression

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3.1 The Navier-Stokes equations

3.1.1 The Navier-Stokes equations on a fixed domain

The flow in the SAS and in the spinal cord can be described by the incompressible Navier-Stokes equations for Newtonian fluids. They describe the motion of a fluid with constant density ρ in a domain $\Omega \subset \mathbb{R}^d$ (where $d = 2, 3$). They read

$$\rho\dot{\mathbf{u}} + \rho(\mathbf{u} \cdot \nabla)\mathbf{u} - \nabla \cdot \sigma(\mathbf{u}, p) = \mathbf{f}, \qquad \mathbf{x} \in \Omega,\ t > 0 \tag{3.1}$$

$$\nabla \cdot \mathbf{u} = 0, \qquad \mathbf{x} \in \Omega,\ t > 0 \tag{3.2}$$

We are going to solve the problem for the velocity field $\mathbf{u}(\mathbf{x}, t)$, and the pressure field $p(\mathbf{x}, t)$, where $\mathbf{x} = (x, y)$. The quantity $\sigma(\mathbf{u}, p)$, is the Cauchy stress tensor for a Newtonian fluid, given by

$$\sigma(\mathbf{u}, p) = 2\mu\epsilon(\mathbf{u}) - p\mathbb{I},$$

where $\epsilon(\mathbf{u})$ is the symmetric strain rate tensor

$$\epsilon(\mathbf{u}) = \frac{1}{2}(\nabla\mathbf{u} + (\nabla\mathbf{u})^T).$$

The constant μ represents the fluid viscosity, while $\mathbf{f}$ denotes a forcing term per unit of mass. Substituting σ in (**??**) we obtain

$$\rho\dot{\mathbf{u}} + \rho(\mathbf{u} \cdot \nabla)\mathbf{u} - \nabla \cdot [\nu(\nabla\mathbf{u} + (\nabla\mathbf{u})^T)] + \nabla p = \mathbf{f}, \tag{3.3}$$

$$\nabla \cdot \mathbf{u} = 0, \tag{3.4}$$

The term $(\mathbf{u} \cdot \nabla)\mathbf{u}$ describes the process of convective transport, while $-\nabla \cdot [\mu(\nabla\mathbf{u} + (\nabla\mathbf{u})^T)]$ describes the process of molecular diffusion [].
Since μ is constant, from the continuity equation we obtain

$$\nabla \cdot [\mu(\nabla \mathbf{u} + (\nabla \mathbf{u})^T)] = \mu[\Delta \mathbf{u} + \nabla(\nabla \cdot \mathbf{u})] = \mu \Delta \mathbf{u},$$

hence the system can be written in the equivalent form

$$\rho \dot{\mathbf{u}} + \rho(\mathbf{u} \cdot \nabla)\mathbf{u} - \mu \Delta \mathbf{u} + \nabla p = \mathbf{f}, \tag{3.5}$$

$$\nabla \cdot \mathbf{u} = 0. \tag{3.6}$$

In order for the problem to be well posed, it is necessary to assign an initial condition

$$\mathbf{u}(\mathbf{x}, 0) = \mathbf{u}_0(\mathbf{x}) \quad \forall \mathbf{x} \in \Omega,$$

where $\mathbf{u}_0$ is a given divergence-free vector field, together with suitable boundary conditions, such as

$$\begin{cases} \mathbf{u}(\mathbf{x}, t) = \phi(\mathbf{x}, t) & \forall \mathbf{x} \in \Gamma_D \\ \left(\mu \dfrac{\partial \mathbf{u}}{\partial \mathbf{n}} - p\mathbf{n}\right)(\mathbf{x}, t) = \psi(\mathbf{x}, t) & \forall \mathbf{x} \in \Gamma_N \end{cases}$$

where ϕ and ψ are given vector functions, while Γ_D and Γ_N give a partition of the domain boundary $\partial\Omega$, that is $\Gamma_D \cup \Gamma_N = \partial\Omega, \mathring{\Gamma}_D \cap \mathring{\Gamma}_N = \emptyset$. Moreover, $\mathbf{n}$ is the outward unit normal vector to $\partial\Omega$. The second equation in [PUT REFERENCE TO THE PREVIOUS SYSTEM] can also be written in another form

$$[\nu(\nabla \mathbf{u} + \nabla \mathbf{u}^T) - p\mathbf{n}] = \psi(\mathbf{x}, t) \quad \forall \mathbf{x} \in \Gamma_N.$$

Remark. In our notation, if $\mathbf{u} = (u_x, u_y)^T$ and $\mathbf{x} = (x, y)^T$, then $\nabla \mathbf{u}$ is defined as

$$\nabla \mathbf{u} = \begin{pmatrix} \frac{\partial u_x}{\partial x} & \frac{\partial u_x}{\partial y} \\ \frac{\partial u_y}{\partial x} & \frac{\partial u_y}{\partial y} \end{pmatrix}$$

3.1.2 Navier-Stokes on a moving domain

Our next step is to allow the domain and its boundary to move, and solve the Navier-Stokes equations on this deforming domain. Let Ω_t denote the fluid domain which depends on time t. Let Ω_0 denote the fixed fluid domain at $t = 0$. In fluid-structure interaction, the fluid domain Ω_t consists of the same material particles at all times, and moves with the material points within the structure. Also assume that we have a mesh $\mathcal{T}_t$ of the domain Ω_t. Let $\mathbf{w}$ denote the *mesh velocity*, and $\mathbf{y}$ the *mesh displacement* with respect to the reference domain Ω_0, and thus by definition $\dot{\mathbf{y}} = \mathbf{w}$ where the superposed dot denotes the time derivative. The mesh velocity can be

Figure 3.1: Left: spinal cord in the SAS. Right: Schematic illustration of computational domain

chosen arbitrarily in principle, but this choice could effect the accuracy of the solution [].

The movement of the domain Ω_t is governed by the mesh displacement, i.e. for all $x(t) \in \Omega_t$, each corresponding to a point $x_0 \in \Omega_0$, we have that

$$x(t) = x_0 + \mathbf{y}(t)(x_0). \tag{3.7}$$

Check the precise formulation carefully in Donea reference e.g.

An ALE formulation of the Navier-Stokes equations on the deforming domain Ω_t reads: find the velocity $\mathbf{u}$ and the pressure p such that

$$\rho\dot{\mathbf{u}} + \rho[(\mathbf{u} - \mathbf{w}) \cdot \nabla]\mathbf{u} - \mu\Delta\mathbf{u} + \nabla p = \mathbf{f}, \qquad \text{in } \Omega_t, \tag{3.8}$$

$$\nabla \cdot \mathbf{u} = 0, \qquad \text{in } \Omega_t, \tag{3.9}$$

for $t \in (0, T]$ where $\mathbf{f}$ is a given body force, ρ is the fluid density, μ is the fluid viscosity. The system (3.8)–(3.9) must be closed by appropriate boundary and initial conditions.

We will let the fluid domain boundary follow the changes on the fluid-structure interface. Moreover, to move the entire domain, we will use a *Laplacian smoothing* algorithm [**?**]. More precisely, our mesh smoothing equation reads: given a boundary velocity $\mathbf{u}_0$, find $\mathbf{w}$ that satisfies

$$\begin{aligned} -\Delta\mathbf{w} &= 0 \quad \text{in } \Omega_t, \\ \mathbf{w} &= \mathbf{u}_0 \quad \text{on } \partial\Omega_t. \end{aligned} \tag{3.10}$$

for each $t \in [0, T]$

3.2 Modelling the SAS with elastic surroundings

We will consider a fluid domain Ω_t representing a section of the subarachnoid space between the spinal cord and the surrounding tissue.

Assuming axial symmetry along the spinal cord length axes, we consider a two-dimensional rectangular reference domain $\Omega_0 = [0, L_x] \times [0, L_y]$. We define the

- top boundary: $\partial\Omega^0_{\text{top}} = \{(x_0, x_1) | x_1 = L_y\}$;
- bottom boundary: $\partial\Omega^0_{\text{bottom}} = \{(x_0, x_1) | x_1 = 0\}$;
- tissue boundary: $\partial\Omega^0_{\text{tissue}} = \{(x_0, x_1) | x_0 = L_x\}$;

- cord boundary: $\partial\Omega^0_{\mathrm{cord}} = \{(x_0, x_1) | x_0 = 0\}$;

and thus $\partial\Omega^0 = \partial\Omega^0_{\mathrm{top}} \cup \partial\Omega^0_{\mathrm{bottom}} \cup \partial\Omega^0_{\mathrm{cord}} \cup \partial\Omega^0_{\mathrm{tissue}}$. Further,

$$\partial\Omega^t_{\mathrm{i}} = \partial\Omega^0_{\mathrm{i}} + \mathbf{y}(t)(\partial\Omega^0_{\mathrm{i}}), \tag{3.11}$$

for each i.

We are interested in studying the effect of craniovertebral decompression on the fluid flow and pressure dynamics in the subarachnoid space. In particular, we assume that craniovertebral decompression induces a change in the compliance of the tissue surrounding the spinal canal []. For simplicity, we aim to model the compliance of the surrounding tissue via a boundary condition for the fluid flow. We will assume that the tissue boundary $\partial\Omega_{\mathrm{tissue}}$ is elastic with stiffness $k > 0$ and in particular allowed to move. To this end, we introduce the boundary conditions

$$\mu \frac{\partial \mathbf{u}^n}{\partial \mathbf{n}} - p\mathbf{n} = -k\mathbf{y} \cdot \mathbf{n} \qquad \text{on } \partial\Omega_{\mathrm{tissue}}, \tag{3.12}$$

$$\mathbf{u}^t = \mathbf{0} \qquad \text{on } \partial\Omega_{\mathrm{tissue}}, \tag{3.13}$$

where $\mathbf{n}$ is the outward pointing boundary normal and $\mathbf{y}$ still denotes the mesh displacement. For simplicity, on the spinal cord side, we assume that the cord is rigid and fixed, i.e.:

$$\mathbf{u} = \mathbf{0} \quad \text{on } \partial\Omega_{\mathrm{cord}}. \tag{3.14}$$

To induce a fluid flow in the subarachnoid space, we prescribe an inlet velocity $\tilde{u}$ on the top boundary, while on the bottom boundary we assume that $(\mu\nabla\mathbf{u} - pI) \cdot \mathbf{n} = 0$.

For the mesh equation, we let the mesh velocity follow the fluid velocity on the tissue boundary, while the mesh velocity is assumed to be zero (i.e. the mesh boundary is fixed) on the remaining boundary:

$$\mathbf{w} = \mathbf{u} \qquad \text{on } \partial\Omega_{\mathrm{tissue}}, \tag{3.15}$$

$$\mathbf{w} = \mathbf{0} \qquad \text{on } \partial\Omega^t \setminus \partial\Omega_{\mathrm{tissue}} \tag{3.16}$$

Note that $\partial\Omega_{\mathrm{cord}}$ and $\partial\Omega_{\mathrm{tissue}}$ are *physical* boundaries, i.e. they model portions of the spinal cord and surrounding tissue. This means that $\mathbf{u}$ and $\mathbf{w}$ should have the same value on these boundaries, since the fluid follows the movement (if any) of the walls.

Chapter 4

Numerical methods

4.1 Finite element formulation

4.2 Weak formulation of Navier-Stokes with ALE term

I don't think I really need this section, I can say everything in the entire model with the elastic constant

From [PUT REFERENCE TO EQUATION WITH w], we multiply by a test function v the first equation and by the test function q the second equation, and integrate over Ω. We hence obtain:

$$\int_\Omega \rho \dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx - \int_\Omega \nabla\cdot(\mu\nabla\mathbf{u}-pI)\mathbf{v}\,dx = \int_\Omega \mathbf{f}\,dx,$$
$$\int_\Omega (\nabla\cdot\mathbf{u})q\,dx = 0.$$

As before, the term $-\int_\Omega \nabla\cdot(\mu\nabla\mathbf{u}-pI)\mathbf{v}\,dx$ can be integrated by parts:

$$-\int_\Omega \nabla\cdot(\mu\nabla\mathbf{u}-pI)\mathbf{v}\,dx = \int_\Omega (\mu\nabla\mathbf{u}-pI)\cdot\nabla\mathbf{v}\,dx - \int_{\partial\Omega}(\mu\nabla\mathbf{u}-pI)\cdot\mathbf{n}\,\mathbf{v}\,ds.$$

The boundary $\partial\Omega$ can be divided in two boundaries $\partial\Omega = \partial\Omega_D \cup \partial\Omega_N$, where $\partial\Omega_D$ and $\partial\Omega_N$ are respectively the Dirichlet boundary and the Neumann boundary. Since we chose $\mathbf{v} \in \hat{V}$, the term on $\partial\Omega_D$ is zero. The term on $\partial\Omega_D$ is also zero: since $\sigma = \mu\nabla\mathbf{u} - pI$ and $\sigma\cdot\vec{\mathbf{n}} = 0$ on $\partial\Omega_D$, the remaining term on the boundary is also zero. Hence,

$$-\int_{\partial\Omega}(\mu\nabla\mathbf{u}-pI)\cdot\mathbf{n}\,\mathbf{v}\,dx = 0.$$

The variational formulation reads:

$$\int_\Omega \rho\dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx + \int_\Omega (\mu\nabla\mathbf{u} - pI)\cdot\nabla\mathbf{v}\,dx = \int_\Omega \mathbf{f}\,dx,$$
$$\int_\Omega (\nabla\cdot\mathbf{u})q\,dx = 0.$$

We now want to write the variational formulation for the Poisson problem: let $\mathbf{z}$ be a test function in [SPECIFY THE SPACE]. Integrating by parts equation [PUT REFERENCE], we obtain

$$\int_\Omega \nabla^2\mathbf{w}\,\mathbf{z}\,dx = -\int_\Omega \nabla\mathbf{w}\cdot\nabla\mathbf{z}\,dx + \int_{\partial\Omega}\frac{\partial\mathbf{w}}{\partial\mathbf{n}}\mathbf{z}\,ds.$$

Since we are assuming Dirichlet boundary conditions on the entire boundary, we choose $\mathbf{z} = \mathbf{0}$ everywhere, hence the term $\int_{\partial\Omega}\frac{\partial\mathbf{w}}{\partial\mathbf{n}}\,\mathbf{z}\,dx = 0$. Typically, the boundary $\partial\Omega_t$ will be divided into a physical and a fictitious boundary. We note as well that on the physical boundary, the values of $\mathbf{w}$ and $\mathbf{u}$ should be the same. Finally, we obtain

$$\int_\Omega \nabla^2\mathbf{w}\,\mathbf{z}\,dx = -\int_\Omega \nabla\mathbf{w}\cdot\nabla\mathbf{z}\,dx = 0.$$

The problem reads: find $\mathbf{w} \in$ [SOME SPACE TO SPECIFY] such that

$$\begin{aligned} -\int_{\Omega_t} \nabla\mathbf{w}\cdot\nabla\mathbf{z}\,dx = 0, &\quad \text{in } \Omega_t, \\ \mathbf{w} = \mathbf{u}, &\quad \text{on } \partial\Omega_t \end{aligned}$$

$\forall\mathbf{z} \in$ [SPECIFY SPACE].
Reminder: in our case, we choose

$$\begin{aligned} \mathbf{w} &= \mathbf{u} \ \text{ on } \partial\Omega_{Tissue}, \\ \mathbf{w} &= \mathbf{0} \ \text{ on } \partial\Omega_t \setminus \partial\Omega_{Tissue}. \end{aligned}$$

so we are allowing just the part of the boundary $\partial\Omega_{Tissue}$ to move.

4.3 Weak formulation of N-S on moving domain

We now want to give a brief introduction of a tool that allows us to impose boundary conditions in a weak way. This formulation of the problem seems necessary as we want to allow a movement of the mesh just in the normal direction, and assume zero tangential velocity. This can be done using the following method.

4.3.1 The Nitsche's method

Nitsche's method was proposed as a way for treating boundary conditions in finite element method. In particular, it is used to weakly impose boundary and interface conditions, and it is applicable to a wide class of problems. Let us use Poisson's equation as a model problem. Given a domain Ω with boundary $\Gamma = \partial\Omega$, the problem is to find $\mathbf{u}$ such that

$$-\Delta \mathbf{u} = \mathbf{f} \qquad \text{in } \Omega, \tag{4.1}$$

subject to the boundary condition

$$\mathbf{u} = \mathbf{g} \qquad \text{on } \Gamma. \tag{4.2}$$

Generally, Dirichlet boundary conditions as (4.2) are strongly imposed by seeking the solution $\mathbf{u}$ in some function space V_g, consisting of functions that already satisfy (4.2). The idea of Nitsche's method [**?**] is to introduce a function space V that does not satisfy that requirement, while 'weakly' enforcing the boundary condition. In order to derive the weak formulation, let us multiply equation (4.1) by a test function $\mathbf{v}$ and integrate by parts. We obtain

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} \, dx - \int_\Gamma \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \mathbf{v} \, ds = \int_\Omega \mathbf{f} \mathbf{v} \, dx. \tag{4.3}$$

We now want to enforce the boundary condition (4.2) by adding a new term

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} \, dx - \int_\Gamma \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \mathbf{v} \, dx + \gamma \int_\Gamma \mu(\mathbf{u} - \mathbf{g}) \mathbf{v} \, ds = \int_\Omega \mathbf{f} \mathbf{v} \, dx, \tag{4.4}$$

where $\gamma > 0$ is a penalty parameter and μ is a weight to adjust the penalty of the jump. Nitsche in [**?**] proved that the choice $\mu = \gamma h^{-1}$, with h being the local mesh size, gives an optimally convergent method. In order to make the variational form symmetric, we can add the term $\int_\Gamma \nabla \mathbf{u} \cdot \mathbf{n}(\mathbf{u} - \mathbf{g}) \, ds$ to recover symmetry. Hence, the final Nitsche method reads:

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} \, dx - \int_\Gamma \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \mathbf{v} \, ds - \int_\Gamma \frac{\partial \mathbf{v}}{\partial \mathbf{n}} \mathbf{u} \, ds + \gamma \int_\Gamma h^{-1} \mathbf{u} \mathbf{v} \, ds = \tag{4.5}$$

$$\int_\Omega \mathbf{f} \mathbf{v} \, dx - \int_\Gamma \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \mathbf{g} \, ds + \gamma \int_\Gamma h^{-1} \mathbf{g} \mathbf{v} \, ds. \tag{4.6}$$

What we would like to do now is using the previous method to weakly set boundary conditions on the normal and the tangential components of the velocity field $\mathbf{u}$. The problem is to find $\mathbf{u}$ such that

$$-\Delta \mathbf{u} = \mathbf{f} \quad \text{in } \Omega, \tag{4.7}$$

$$\frac{\partial \mathbf{u}^n}{\partial \mathbf{n}} = \mathbf{l} \quad \text{on } \Gamma, \tag{4.8}$$

$$\mathbf{u}^t = \mathbf{g} \quad \text{on } \Gamma. \tag{4.9}$$

where $\mathbf{u}^n$ and $\mathbf{u}^t$ are respectively the normal and tangential components of the velocity $\mathbf{u}$, and $\mathbf{u} = \mathbf{u}^n + \mathbf{u}^t$. We multiply by a test function $\mathbf{v}$, and substitute $\mathbf{u} = \mathbf{u}^n + \mathbf{u}^t$ and $\mathbf{v} = \mathbf{v}^n + \mathbf{v}^t$ in (4.3). Integrating over the domain Ω, we obtain

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} dx - \int_\Gamma \frac{\partial \mathbf{u}^n}{\partial \mathbf{n}} \mathbf{v}^n \, ds - \int_\Gamma \frac{\partial \mathbf{u}^t}{\partial \mathbf{n}} \mathbf{v}^t \, ds = \int_\Omega \mathbf{f} \mathbf{v} \, dx. \tag{4.10}$$

From the boundary condition (4.8), we have

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} dx - \int_\Gamma \frac{\partial \mathbf{u}^t}{\partial \mathbf{n}} \mathbf{v}^t \, ds = \int_\Gamma \mathbf{l} \mathbf{v}^n \, ds + \int_\Omega \mathbf{f} \mathbf{v} \, dx \tag{4.11}$$

Applying the Nitsche method on the boundary term in the left hand side, we get

$$\int_\Omega \nabla \mathbf{u} \cdot \nabla \mathbf{v} dx - \int_\Gamma \frac{\partial \mathbf{u}^t}{\partial \mathbf{n}} \mathbf{v}^t \, ds - \int_\Gamma \frac{\partial \mathbf{v}^t}{\partial \mathbf{n}} \mathbf{u}^t \, ds + \gamma \int_\Gamma h^{-1} \mathbf{u}^t \mathbf{v}^t \, ds = \tag{4.12}$$

$$\int_\Gamma \mathbf{l} \mathbf{v}^n \, ds + \int_\Omega \mathbf{f} \mathbf{v} \, dx - \int_\Gamma \frac{\partial \mathbf{v}^t}{\partial \mathbf{n}} \mathbf{g} \, ds + \gamma \int_\Gamma h^{-1} \mathbf{g} \mathbf{v}^t \, ds \tag{4.13}$$

4.3.2 Applying Nitsche's method to Navier-Stokes

We start from equations (3.8)– (3.9), and multiply the first one by a test function $\mathbf{v}$, and by a test function q the second equation, and integrate over Ω. We obtain:

$$\int_\Omega \rho \dot{\mathbf{u}} \, \mathbf{v} \, dx + \int_\Omega \rho [(\mathbf{u} - \mathbf{w}) \cdot \nabla] \mathbf{u} \, \mathbf{v} \, dx - \int_\Omega \nabla \cdot (\mu \nabla \mathbf{u} - pI) \mathbf{v} \, dx = \int_\Omega \mathbf{f} \mathbf{v} \, dx,$$

$$\int_\Omega (\nabla \cdot \mathbf{u}) q \, dx = 0.$$

Integrating by parts the term $-\int_\Omega \nabla \cdot (\mu \nabla \mathbf{u} - pI) \mathbf{v} \, dx$, and applying Green formula, we have

$$-\int_\Omega \nabla \cdot (\mu \nabla \mathbf{u} - pI) \mathbf{v} \, dx = \int_\Omega (\mu \nabla \mathbf{u} - pI) \cdot \nabla \mathbf{v} \, dx - \int_{\partial\Omega} (\mu \nabla \mathbf{u} - pI) \cdot \mathbf{n} \, \mathbf{v} \, ds.$$

The boundary $\partial\Omega_t$ can be divided in the four boundaries:

$$\partial\Omega_t = \partial\Omega_{Top} \cup \partial\Omega_{Bottom} \cup \partial\Omega_{Cord} \cup \partial\Omega_{Tissue}.$$

On $\partial\Omega_{Top}$ and $\partial\Omega_{Cord}$ we assume Dirichlet boundary conditions for the velocity $\mathbf{u}$, hence the test function $\mathbf{v}$ will be zero on these two boundaries. Moreover, I assumed $\sigma \cdot \mathbf{n} = 0$ on $\partial\Omega_{Bottom}$, while $\sigma \cdot \mathbf{n} = \pm k\mathbf{y}$ on $\partial\Omega_{Tissue}$, where $\mathbf{y}$ is the mesh displacement vector. The boundary term becomes

$$-\int_{\partial\Omega_t} (\mu\nabla\mathbf{u} - pI) \cdot \mathbf{n}\,\mathbf{v}\,dx = -\int_{\partial\Omega_{Tissue}} (\pm k\mathbf{y})\,\mathbf{v}\,dx.$$

The variational formulation reads:

$$\int_\Omega \rho\dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx + \int_\Omega (\nu\nabla\mathbf{u} - pI)\cdot\nabla\mathbf{v}\,dx \\ - \int_{\partial\Omega_{tissue}} (\pm k\mathbf{y})\,\mathbf{v}\,dx = \int_\Omega \mathbf{f}\mathbf{v}\,dx.$$

We now would like to set the tangential component of the velocity to 0, in order to allow the mesh to move just in the normal direction of the $\partial\Omega_{tissue}$ boundary.

We also need another condition for the normal direction, WHICH ONE? TO WRITE PRECISELY

We start from

$$\int_\Omega \rho\dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx - \int_\Omega \nabla\cdot(\mu\nabla\mathbf{u} - pI)\mathbf{v}\,dx = \int_\Omega \mathbf{f}\mathbf{v}\,dx$$

I integrate by parts and obtain

$$\int_\Omega \rho\dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx + \int_\Omega (\mu\nabla\mathbf{u} - pI)\cdot\nabla\mathbf{v}\,dx \\ - \int_{\partial\Omega} (\mu\nabla\mathbf{u} - pI)\cdot\mathbf{n}\,\mathbf{v}\,ds = \int_\Omega \mathbf{f}\mathbf{v}\,dx$$

According to the boundary conditions, the boundary term $\partial\Omega_{tissue}$ is the only one that survives, hence

$$\int_\Omega \rho\dot{\mathbf{u}}\,\mathbf{v}\,dx + \int_\Omega \rho[(\mathbf{u}-\mathbf{w})\cdot\nabla]\mathbf{u}\,\mathbf{v}\,dx + \int_\Omega (\mu\nabla\mathbf{u} - pI)\cdot\nabla\mathbf{v}\,dx \\ - \int_{\partial\Omega_{tissue}} (\mu\nabla\mathbf{u} - pI)\cdot\mathbf{n}\,\mathbf{v}\,ds = \int_\Omega \mathbf{f}\mathbf{v}\,dx$$

Since $\nabla \mathbf{u} \cdot \mathbf{n} = \frac{\partial \mathbf{u}}{\partial \mathbf{n}}$, I can rewrite the boundary term:

$$
\begin{aligned}
\int_{\partial\Omega_{tissue}} (\mu \nabla \mathbf{u} - pI) \cdot \mathbf{n}\, \mathbf{v}\, ds &= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} - p\mathbf{n})\, \mathbf{v}\, ds && (4.14)\\
&= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{v} - p\mathbf{n} \cdot \mathbf{v})\, ds && (4.15)\\
&= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot (v_n \mathbf{n} + v_t \mathbf{t}) - p\, v_n)\, ds && (4.16)\\
&= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{n} v_n - p\, v_n)\, ds && (4.17)\\
&+ \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{t}\, v_t)\, ds && (4.18)\\
&= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{n} - p) v_n\, ds && (4.19)\\
&+ \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{t}\, v_t)\, ds && (4.20)\\
&= \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} - p\mathbf{n}) \cdot \mathbf{n} v_n\, ds && (4.21)\\
&+ \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{t}\, v_t)\, ds && (4.22)\\
&= \int_{\partial\Omega_{tissue}} (k\mathbf{y}) \cdot \mathbf{n} v_n\, ds && (4.23)\\
&+ \int_{\partial\Omega_{tissue}} (\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} \cdot \mathbf{t}\, v_t)\, ds && (4.24)\\
& && (4.25)
\end{aligned}
$$

The vector $\mathbf{v}$ can be split in its normal and tangential components, as follows: $\mathbf{v} = v_n \mathbf{n} + v_t \mathbf{t}$. Substituting the $\mathbf{v}$ in (4.14) and simplifying we have

4.4 FEniCS

Something about FEniCS

4.5 Numerical scheme

4.5.1 Time discretization

In the following we present a possibility of discretization of the Navier-Stokes equations, that was used in this thesis. Starting from equations (3.8)–(3.9), we now want to use the so called Crank-Nicolson discretization to solve these equations. Let $[0, T] = \cup_{i=0}^{N} [t_i, t_{i+1}]$ be the time interval, and

$\Delta t = t_{i+1} - t_i$ the time step. We apply a backward Euler discretization to the time derivative $\partial \mathbf{u}/\partial t$

$$\frac{\partial \mathbf{u}}{\partial t} \approx \frac{\mathbf{u}^{i+1} - \mathbf{u}^i}{\Delta t}, \tag{4.26}$$

where $\mathbf{u}^i$ is an approximation of $\mathbf{u}(t_i)$ at the time level i. A midpoint Crank-Nicolson scheme may be written as:

$$\rho \frac{\mathbf{u}^{i+1} - \mathbf{u}^i}{\Delta t} + \rho[\nabla \mathbf{u} \cdot (\mathbf{u} - \mathbf{w})]^{i+1/2} - \nabla \cdot (\mu \Delta \mathbf{u}^{\mathrm{i}+1/2} - \mathbf{p}^{\mathrm{i}+1/2} I) = \mathbf{f}^{\mathrm{i}+1/2}, \tag{4.27}$$

$$\nabla \mathbf{u}^{i+1} = 0, \tag{4.28}$$

where we set $\mathbf{u}^{\mathrm{i}+1/2} = \frac{\mathbf{u}^i + \mathbf{u}^{i+1}}{2}$. The convective term may be written as

$$\rho[\nabla \mathbf{u} \cdot (\mathbf{u} - \mathbf{w})]^{i+1/2} = \rho[\nabla \mathbf{u}^{i+1/2} \cdot (\mathbf{u}^{i+1/2} - \mathbf{w}^{i+1/2})]. \tag{4.29}$$

We linearize the term above with

$$\rho[\nabla \mathbf{u}^{i+1/2} \cdot (\mathbf{u}^{i+1/2} - \mathbf{w}^{i+1/2})] \approx \rho[\nabla \mathbf{u}^{i+1/2} \cdot (\mathbf{u}^i - \mathbf{w}^i)]. \tag{4.30}$$

Moreover, the stress tensor σ is discretized as follows

$$\nabla \cdot \sigma \approx \nabla \cdot \sigma^i = \nabla \cdot (\mu \Delta \mathbf{u}^{\mathrm{i}+1/2} - p^{\mathrm{i}+1/2} I). \tag{4.31}$$

The resulting discretization yields to

$$\rho \frac{\mathbf{u}^{i+1} - \mathbf{u}^i}{\Delta t} + \rho[\nabla \mathbf{u}^{i+1/2} \cdot (\mathbf{u}^i - \mathbf{w}^i)] - \nabla \cdot (\mu \Delta \mathbf{u}^{\mathrm{i}+1/2} - \mathbf{p}^{\mathrm{i}+1/2} I) = \mathbf{f}^{\mathrm{i}+1/2}, \tag{4.32}$$

$$\nabla \mathbf{u}^{i+1} = 0, \tag{4.33}$$

Actually I used

$$\rho \frac{\mathbf{u}^{i+1} - \mathbf{u}^i}{\Delta t} + \rho[\nabla \mathbf{u}^{i+1/2} \cdot (\mathbf{u}^i - \mathbf{w}^i)] - \nabla \cdot (\mu \Delta \mathbf{u}^{\mathrm{i}+1/2} - \mathbf{p}^{\mathrm{i}+1} I) = \mathbf{f}^{\mathrm{i}+1/2}, \tag{4.34}$$

$$\nabla \mathbf{u}^{i+1} = 0, \tag{4.35}$$

4.5.2 Spatial discretization

Starting from the scheme (4.32)–(4.33) for the Navier-Stokes equations, the unknown velocity $\mathbf{u}^{\mathrm{i}+1}$ and the pressure $\mathbf{p}^{\mathrm{i}+1}$ are denoted as the trial functions in the trial spaces V and Q given by

$$V = \{\, \mathbf{u} \in [H^1(\Omega)]^2 \mid \mathbf{u}_{|\partial\Omega_{top} \cup \Omega_{bottom}} = \mathbf{0} \,\}$$
$$Q = \{\, \mathbf{u} \in [H^1(\Omega)]^2 \mid \mathbf{u}_{|\partial\Omega_{top} \cup \Omega_{bottom}} = \mathbf{0} \,\}$$

We multiply the Navier-Stokes equations, respectively, by the test functions v and q. We choose $v \in \hat{V} = \{\, v \in [H^1(\Omega)]^2 \mid v_{|\partial\Omega_{top} \cup \Omega_{bottom}} = 0 \,\}$, and $q \in \hat{Q}$ (SPECIFY $\hat{Q}$).

Write precisely the spaces, this is a mess

Let us use the inner product $\langle f, g \rangle = \int_\Omega f g \, d\Omega$. Thus, from the weak formulation (4.14)

Problem: find $(\mathbf{u}^{i+1}, \mathbf{p}^{i+1}) \in \hat{V} \times \hat{Q}$ such that

$$\langle \rho \frac{u^{i+1} - u^i}{\Delta t}, v \rangle_\Omega + \langle \rho \nabla u^{mid} \cdot u^i, v \rangle_\Omega - \langle v \nabla \cdot (\nabla u^{mid}), v \rangle_\Omega + \langle \nabla p^{mid}, v \rangle_\Omega = \langle f^{mid}, v \rangle_\Omega \tag{4.36}$$

$$\langle \nabla \cdot u^{i+1}, q \rangle_\Omega = 0. \tag{4.37}$$

Chapter 5

Verification

5.1 Method of manifactured solutions (MMS)

A test problem for which we can easily check the answer is performed using the *manufactured solutions*. The idea behind MMS is the following: we use an exact solution to some PDE that has been constructed by solving the problem *backwards*. Let us suppose we want to solve a differential equation of the form

$$Du = g,$$

where D is the differential operator, u is the solution, and g is a source term. In the method of exact solution (MES), one chooses the function g and then inverts the operator in order to solve for u. In MMS, one first manufactures a solution u, and then applies D to u to find g.

We want to apply the manufactured solution technique to solve the Stokes equation. Let Ω be the unit square $\Omega = [0,1]^2$, and

$$\begin{cases} -\nabla \cdot (\nu \nabla \mathbf{u} - pI) = f, & \text{in } \Omega \\ \nabla \cdot \mathbf{u} = 0, & \text{in } \Omega \end{cases}$$

where kinematic viscosity $\nu = 1/8$. Let

$$\partial\Omega = \partial\Omega_{inflow} \cup \partial\Omega_{outflow} \cup \partial\Omega_{sides}$$

where $\partial\Omega_{inflow}$, $\partial\Omega_{outflow}$, and $\partial\Omega_{sides}$ are the top, bottom, and lateral boundaries, respectively. We assume no-slip boundary conditions on the sides of the square, while an inflow and outflow velocity is applied, respectively, on the upper and lower boundaries, as follows

$$\begin{cases} \mathbf{u}(x,y) = \begin{bmatrix} 0 \\ x(1-x) \end{bmatrix}, & \text{on } \partial\Omega_{inflow} \cup \partial\Omega_{outflow} \\ \mathbf{u}(x,y) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, & \text{on } \partial\Omega_{sides} \end{cases}$$

As a first example, we use the following manufactured solution:

$$\mathbf{u}_{exact} = \begin{bmatrix} 0 \\ x(1-x) \end{bmatrix}, \quad p_{exact} = \frac{1}{2} - y.$$

Let $\mathbf{u}_h$ and p_h be two two approximate solutions obtained from the simulation, we now want compute the errors

- $||\mathbf{u}_{exact} - \mathbf{u}_h||_{L^2}$,
- $|\mathbf{u}_{exact} - \mathbf{u}_h|_{H^1}$ (seminorm),
- $||p_{exact} - p_h||_{L^2}$.

in order to compare our exact solution with the manufactured one. Using the previous exact solution, the error is 0, since the method for solving the problem is exact for polynomials, as shown below

N	$\|\|\mathbf{u_{exact}} - \mathbf{u_h}\|\|_{\mathbf{L^2}}$	$\|\mathbf{u_{exact}} - \mathbf{u_h}\|_{\mathbf{H^1}}$	$\|\|\mathbf{p_{exact}} - \mathbf{p_h}\|\|_{\mathbf{L^2}}$
4	2.7373×10^{-14}	3.2162×10^{-13}	2.7373×10^{-14}
8	1.3173×10^{-12}	7.5841×10^{-11}	1.3172×10^{-12}
16	8.4791×10^{-14}	9.1285×10^{-12}	8.4791×10^{-14}
32	9.0508×10^{-14}	1.6039×10^{-11}	9.0580×10^{-14}
64	6.3504×10^{-13}	9.5275×10^{-11}	6.3504×10^{-13}

A difference exact solution that could be used is:

$$\mathbf{u}_{exact} = \begin{bmatrix} 0 \\ sin(\pi x) \end{bmatrix}, \quad p_{exact} = \frac{1}{2} - y.$$

In the following tables, the convergence rate k was computed, according to:

$$k = \frac{log(\frac{E_{i+1}}{E_i})}{log(\frac{h_{i+1}}{h_i})}$$

where we are assuming that $E_i \sim h_i^k$ and $E_{i+1} \sim h_{i+1}^k$.
The following table shows a second order convergence rate in H^1, as confirmed by the convergence plot.

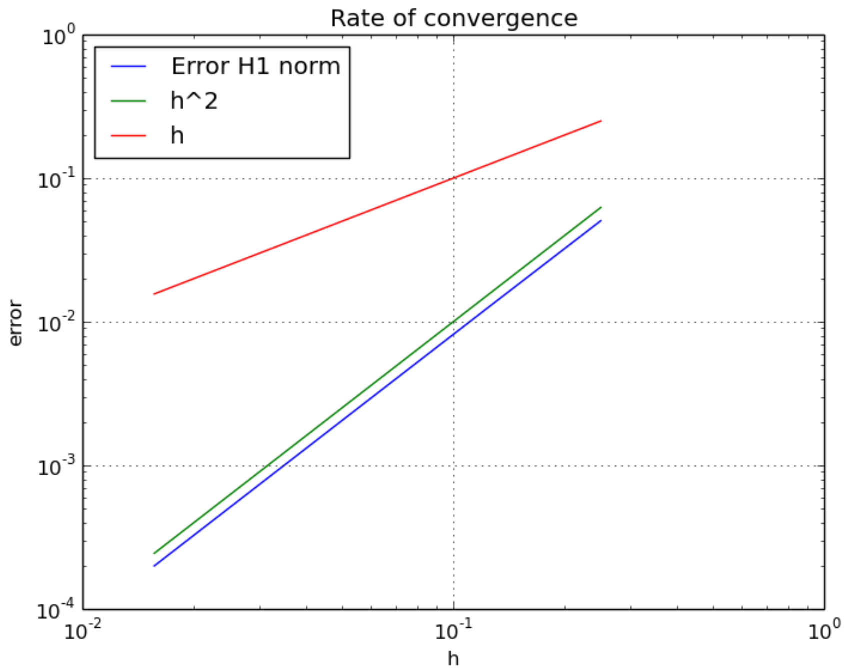

Figure 5.1: The plot shows a second order convergence, since the blue and green lines are parallel.

N	$\|\|\mathbf{u}_{\text{exact}} - \mathbf{u}_h\|\|_{L^2}$	$\|\mathbf{u}_{\text{exact}} - \mathbf{u}_h\|_{H^1}$	Rate in L^2	Rate in H^1
4	1.9388×10^{-3}	5.0548×10^{-2}		
8	2.4515×10^{-4}	1.2733×10^{-2}	2.9834	1.9890
16	3.0745×10^{-5}	3.1896×10^{-3}	2.9952	1.9971
32	3.8465×10^{-6}	7.9780×10^{-4}	2.9987	1.9992
64	4.8092×10^{-7}	1.9948×10^{-4}	2.9997	1.9998

N	$\|\|p_{\text{exact}} - p_h\|\|_{L^2}$	Rate in L^2
4	1.4420×10^{-4}	
8	1.1896×10^{-5}	3.5995
16	1.0089×10^{-6}	3.5596
32	8.7143×10^{-8}	3.5332
64	8.0070×10^{-9}	3.4440

5.2 Pressure-driven channel flow (2D)

A typical test problem is finding the solution of the Navier-Stokes equations in a two-dimensional pressure-driven channel. We consider a viscous flow between parallel plates, where the geometry is the unit square $[0,1]^2$, and the kinematic viscosity is $\nu = 1/8$. We assume that both plates are fixed, i.e. no-slip boundary conditions are applied to the velocity at the upper and lower walls, and Neumann boundary conditions $\sigma \cdot \vec{n} = 0$ are applied at the inlet and outlet. Dirichlet boundary conditions are applied to the pressure at the inlet and outlet, with $p = 1$ at the inlet and $p = 0$ at the outlet. The initial condition for the velocity is $\mathbf{u} = (0,0)$. As a reference value in order to verify the agreement of our solution, we use the x-component of the velocity at the point $(x, y) = (1, 0.5)$ at final time $T = 0.5$. The value reported on the FEniCS book [PUT REFERENCE] is $u_x(1, 0.5, T = 0.5) \approx 0.44321183655681595$, while the one obtained in our results is 0.443217320106.

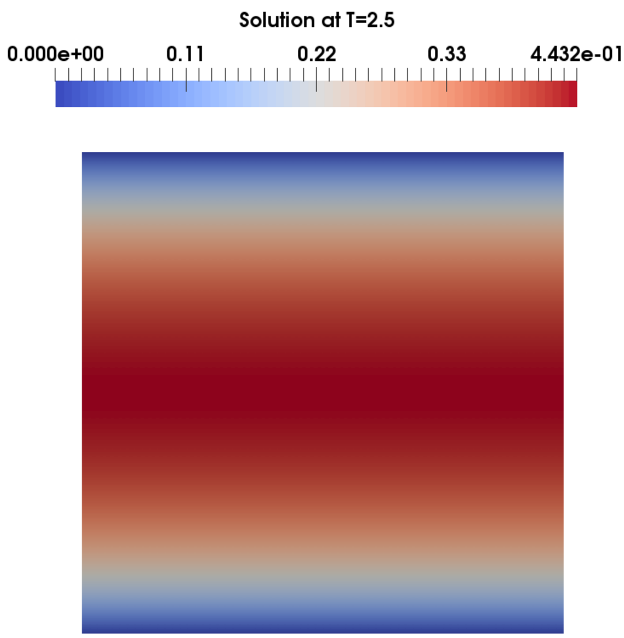

Figure 5.2: The plot shows the solution $u(x, y)$ for $\nu = 1/8$.

5.3 Driven cavity

A typical benchmark problem for fluid flow solvers in the two-dimensional lid-driven cavity problem. We consider a square cavity Ω with sides of unit length, i.e. $\Omega = [0,1] \times [0,1]$, kinematic viscosity $\nu = 1/1000$, and density $\rho = 1$. No-slip boundary conditions are imposed on each edge of the square, except at the upper edge where the velocity is set to $\mathbf{u} = (1,0)^T$, as follows

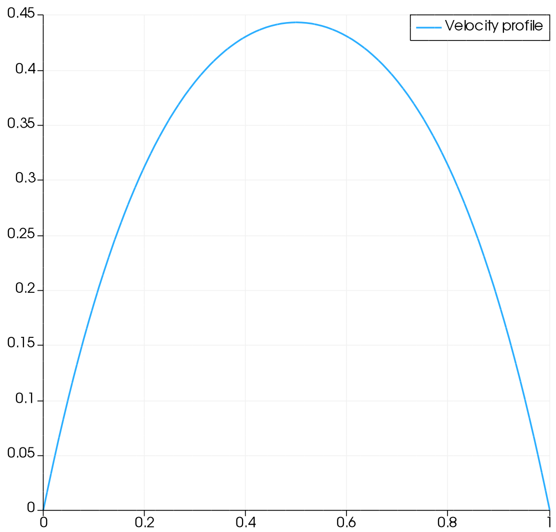

Figure 5.3: Velocity profile at the points $(0.5, 1)$ and $(0.5, 0)$.

$$\begin{cases} \mathbf{u} = \mathbf{0}, & \text{on } \partial\Omega \backslash \Gamma \\ \mathbf{u} = (1, 0)^T, & \text{on } \Gamma \end{cases}$$

where $\Gamma = \{ \mathbf{x} = (x, y)^T \in \partial\Omega \mid y = 1 \}$. We use finite elements on triangular grids of the type $\mathcal{P}_2 - \mathcal{P}_1$. The initial condition for the velocity is set to zero. The resulting flow is a vortex developing in the upper right corner and then traveling towards the center of the square as the flow evolves.

To verify the correctness of the solver, we consider the minimum of the *stream function*. The stream function ψ allows us to satisfy the continuity equation and then solve the momentum equation directly for the single variable ψ. It is defined by

$$\mathbf{u} = \nabla \times \psi = (\frac{\partial \psi}{\partial y}, -\frac{\partial \psi}{\partial x}),$$

and it can be computed by solving the Poisson problem

$$-\nabla^2 \psi = \omega,$$

where ω is the vorticity given by

$$\omega = \nabla \times \mathbf{u} = \frac{\partial u_y}{\partial x} - \frac{\partial u_x}{\partial y}.$$

As a reference value, we use the one reported on the FEniCS book [REFERENCE], where the solution at the final time $T = 2.5$ was computed using the spectral element code Semtex with up to 80×80 10^{th} order elements, heavily refined in the area in the vicinity of the minimum of the stream function. The time-stepping for computing the reference solution was handled by a third order implicit discretization, and a very short time step was used to minimize temporal errors. The obtained reference value was $min(\psi) = -0.061077$.

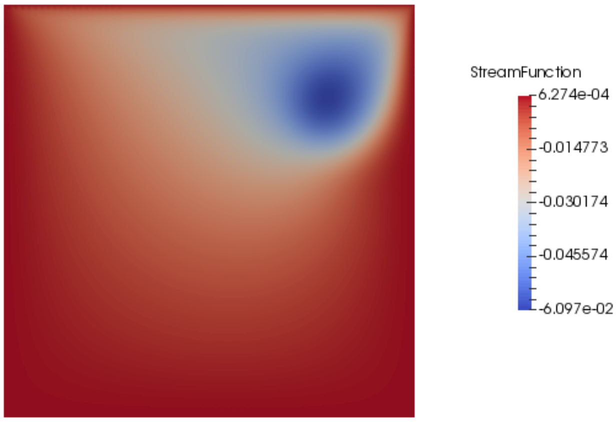

Figure 5.4: The plot shows the stream function, and its minimum value -0.06097 (THIS IS OYVIND'S).

In our case, a Crank-Nicolson (second order) discretization was used, with $\theta = 0.5$. A 64×64 number of elements was used, with $dt = 0.0125$ as time step. Hence, the obtained value was $min(\psi) = -0.061121$, in fair agreement with the reference one.

(MISSING: PUT MY STREAM FUNCTION, OYVIND'S, AND THE ERROR BETWEEN THEM.
NOTE: Oyvind's stream function minimum is not exactly the same as the fenics book, what should I put then as a reference?)

5.4 ALE test case

See Vegard

5.5 ALE + elasticity test case

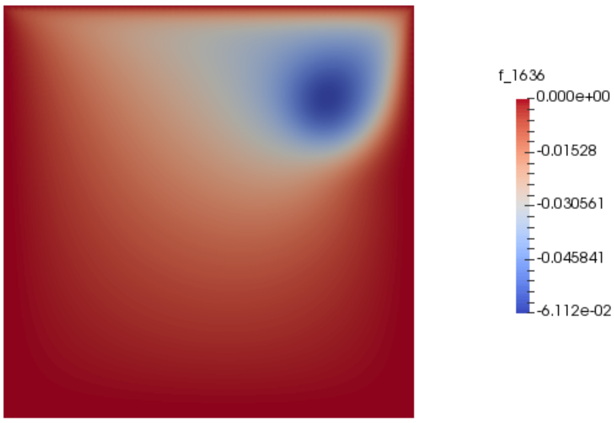

Figure 5.5: The plot shows the stream function, and its minimum value -0.061121.

Chapter 6

Numerical results

Chapter 7

Discussion

Chapter 8

Conclusions