Thesis Title

Institution Name

Author Name

Day Month Year

Kapittel 1

Verification and validation.

The goal of this is section is to verify and validate the different numerical schemes implemented. To solve a real world problem FSI-problem we need to know that we are solving the right equations and that the equations are solved right. By verification of code means that we make sure we are solving the given equation in the right fashion. This can be done with a convergence test, using the method of manufactured solution for instance. We can then check with mathematical theory to see if our solution converges with decreasing time-step or increasing number of cells in our computation.

1.1 Verification

1.2 Validation

After the code has been verified to see that we are indeed computing in the right fashion. We have to see that it is the right equations that are being solved. This is achieved using known benchmark tests. These tests supply us with a problem setup, initial and boundary conditions, and lastly results that we can compare with. In the following we will look at tests for the fluid solvers both alone, testing laminar to turbulent flow, and with solid. We will test the solid solver, and lastly the entire coupled FSI problem.

1.2.1 Taylor-Green vortex

1.2.2 Fluid-Structure Interaction between an elastic object and laminar incompressible flow

Problem Defintion

Domain

The computational domain resembles the classic cfd benchmark with an added bar, with dimensions:

The box: L = 2.5, H = 0.41The bar: l = 0.35, h = 0.02

The circle is positioned at (0.2, 0.2) making it 0.05 of center from bottom to top, this is done to induce oscillations to an otherwise laminar flow.

Boundary conditions:

The fluid velocity has a parabolic profile on the inlet that changes over time:

$$u(0,y) = 1.5u_0 \frac{y(H-y)}{(\frac{H}{2})^2}$$
$$u(0,y,t) = u(0,y) \frac{1 - \cos(\frac{\pi}{2}t)}{2} \text{ for } t < 2.0$$
$$u(0,y,t) = u(0,y) \text{ for } t \le 2.0$$

We set no slip on the floor"and "ceilingso to speak.

On the fluid solid interface the boundary conditions are set to:

$$\sigma_f n_f = \sigma_s n_s$$
 on $\Gamma^0(interface)$

In our variational form we leave this out and so implying that they are equal.

CSM test

Parameters

Tabell 1.1: My caption

Parameters	CSM1	CSM2	CSM3
$\rho_f[10^3 \frac{kg}{m^3}]$	1	1	1
$\nu_f [10^{-3} \frac{m^2}{s}]$	1	1	1
u_0	0	0	0
$\rho_s[10^3 \frac{kg}{m^3}]$	1	1	1
ν_s	0.4	0.4	0.4
$\mu_s[10^6 \frac{m^2}{s}]$	0.5	2.0	0.5
g	2	2	2

FSI test

Tabell 1.2: Parameters

Parameters	FSI1	FSI2	FSI3
$\rho_f[10^3 \frac{kg}{m^3}]$	1	1	1
$\nu_f [10^{-3} \frac{m^2}{s}]$	1	1	1
u_0	0.2	1	2
$\mathrm{Re} = \frac{Ud}{ u_f}$	20	100	200
$\rho_s[10^3 \frac{kg}{m^3}]$	1	10	1
ν_s	0.4	0.4	0.4
$\mu_s[10^6 \frac{m^2}{s}]$	0.5	0.5	2

Results: In my monolithic

Tabell 1.3: FSI 1

Cells	Dofs	ux of A $[x10^{-3}]$	uy of A $[x10^{-3}]$	Drag	Lift	Spaces
2698	7095	0.0234594	0.797218	14.4963	0.915801	P1-P1-P1 stab= 0.01
2698	23563	0.02271	0.80288	14.1736	0.787891	P2-P2-P1
2698	23563	0.00581116	0.000000738678	12.07	0.02345	P2-P2-P1 without weighting
10792	92992	0.0227341	0.808792	14.1855	0.801044	P2-P2-P1
43168	369448	0.227352	0.812595	14.227	0.797242	P2-P2-P1
ref	ref	0.0227	0.8209	14.295	0.7638	ref

Bibliografi

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