

# Model Predictive Control

## Lecture 2: Modeling and Simulation

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02619 Model Predictive Control

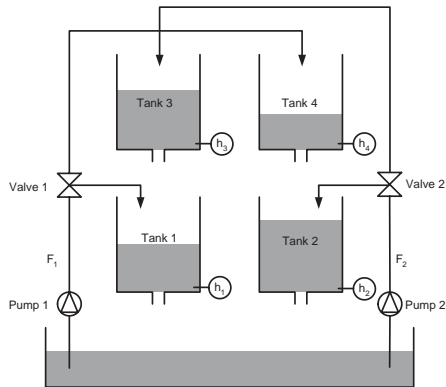


# Learning Objectives

After this lecture you should be able to

- ➊ Apply conservation of mass to develop simple first-principle models
- ➋ Simulate systems described by ODEs using Matlab
- ➌ Compute steady-states and linearize a system around a steady state
- ➍ Discretize a linear continuous-time state space system
- ➎ Derive transfer functions for linear state-space systems
- ➏ Do simulations of stochastic systems
- ➐ Discretize a continuous-time stochastic system

## 4-Tank System - Motivating Example



# Conservation Principle

Physical models are based on conservation principles.

- 1 Conservation of mass
- 2 Conservation of energy
- 3 Conservation of momentum (force)

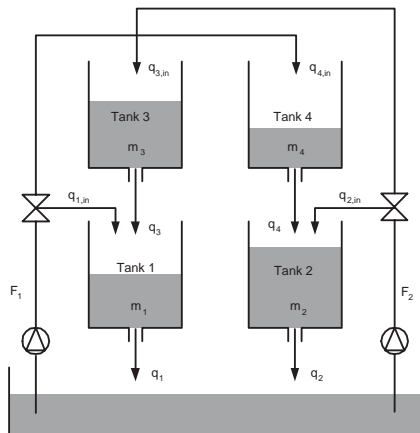
The general derivation of the system equations have the form

$$\text{Accumulated} = \text{Influx} - \text{Outflux} + \overbrace{\text{Produced} - \text{Consumed}}^{\text{=Generated}}$$

For non-reactive systems the generation term is absent

$$\text{Accumulated} = \text{Influx} - \text{Outflux}$$

## Example - Tank 1



Accumulated = In - Out

with

$$\text{Accumulated} = m_1(t + \Delta t) - m_1(t)$$

$$\text{In} = \rho q_{1,in}(t)\Delta t + \rho q_3(t)\Delta t$$

$$\text{Out} = \rho q_1(t)\Delta t$$

$$\underbrace{m_1(t + \Delta t) - m_1(t)}_{\text{Accumulated}} = \underbrace{\rho q_{1,in}(t)\Delta t + \rho q_3(t)\Delta t}_{\text{In}} - \underbrace{\rho q_1(t)\Delta t}_{\text{Out}}$$

## Example - Tank 1

### 1 Conservation of mass

$$\underbrace{m_1(t + \Delta t) - m_1(t)}_{\text{Accumulated}} = \underbrace{\rho q_{1,in}(t)\Delta t + \rho q_3(t)\Delta t}_{\text{In}} - \underbrace{\rho q_1(t)\Delta t}_{\text{Out}}$$

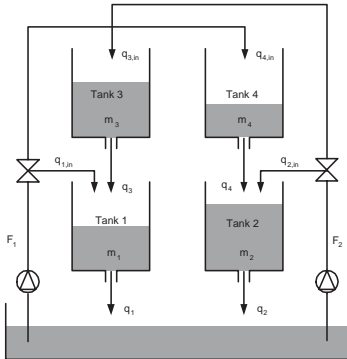
### 2 Divide by $\Delta t$

$$\frac{m_1(t + \Delta t) - m_1(t)}{\Delta t} = \rho q_{1,in}(t) + \rho q_3(t) - \rho q_1(t)$$

### 3 Let $\Delta t \rightarrow 0$

$$\frac{dm_1(t)}{dt} = \rho q_{1,in}(t) + \rho q_3(t) - \rho q_1(t)$$

# 4-Tank System - Model



## Mass balances

$$\frac{dm_1}{dt}(t) = \rho q_{1,in}(t) + \rho q_3(t) - \rho q_1(t) \quad m_1(t_0) = m_{1,0}$$

$$\frac{dm_2}{dt}(t) = \rho q_{2,in}(t) + \rho q_4(t) - \rho q_2(t) \quad m_2(t_0) = m_{2,0}$$

$$\frac{dm_3}{dt}(t) = \rho q_{3,in}(t) - \rho q_3(t) \quad m_3(t_0) = m_{3,0}$$

$$\frac{dm_4}{dt}(t) = \rho q_{4,in}(t) - \rho q_4(t) \quad m_4(t_0) = m_{4,0}$$

## Inflows

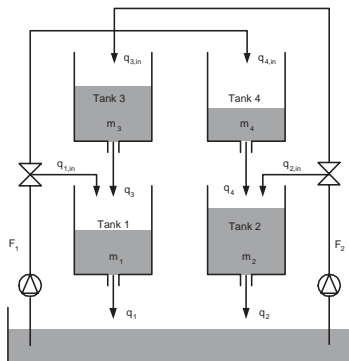
$$q_{1,in}(t) = \gamma_1 F_1(t) \quad q_{2,in}(t) = \gamma_2 F_2(t)$$

$$q_{3,in}(t) = (1 - \gamma_2) F_2(t) \quad q_{4,in}(t) = (1 - \gamma_1) F_1(t)$$

## Outflows

$$q_i(t) = a_i \sqrt{2gh_i(t)} \quad h_i(t) = \frac{m_i(t)}{\rho A_i} \quad i \in \{1, 2, 3, 4\}$$

# 4-Tank System - Model



System of ordinary differential equations

$$\dot{x}(t) = f(x(t), u(t)) \quad x(t_0) = x_0$$

with the vectors defined as

$$x = \begin{bmatrix} m_1 \\ m_2 \\ m_3 \\ m_4 \end{bmatrix} \quad u = \begin{bmatrix} F_1 \\ F_2 \end{bmatrix}$$

This is a **non-stiff** ODE system  
as all processes take place on the same time-scale



# Generic Input-Output Model



$\frac{dx(t)}{dt} = f(x(t), u(t))$	$x(t_0) = x_0$	Process model
$y(t) = g(x(t))$		Sensor function
$z(t) = h(x(t))$		Output function

# Simulation in Matlab

## The model

$$\dot{x}(t) = f(t, x, u, p) \quad x(t_0) = x_0$$

may be implemented in Matlab as

```
function xdot = ProcessModel(t,x,u,p)
% Process Model    dx/dt = f(t,x,u,p)
%
% Computes the RHS of dx/dt = f(t,x,u,p)
% It stores the result in xdot.
```

...

and called using

```
[T,X] = ode15s(@ProcessModel,[t0 tf],x0,odeOptions,u,p)
```

## Model for the 4-Tank System

```
function xdot = FourTankSystem(t,x,u,p)
% FOURTANKSYSTEM Model dx/dt = f(t,x,u,p) for 4-tank System
%
% This function implements a differential equation model for the
% 4-tank system.
%
% Syntax: xdot = FourTankSystem(t,x,u,p)

% Unpack states, MVs, and parameters
m      = x;                % Mass of liquid in each tank [g]
F       = u;                % Flow rates in pumps [cm3/s]
a       = p(1:4,1);        % Pipe cross sectional areas [cm2]
A       = p(5:8,1);        % Tank cross sectional areas [cm2]
gamma   = p(9:10,1);       % Valve positions [-]
g       = p(11,1);         % Acceleration of gravity [cm/s2]
rho     = p(12,1);         % Density of water [g/cm3]

% Inflows
qin = zeros(4,1);
qin(1,1) = gamma(1)*F(1);   % Inflow from valve 1 to tank 1 [cm3/s]
qin(2,1) = gamma(2)*F(2);   % Inflow from valve 2 to tank 2 [cm3/s]
qin(3,1) = (1-gamma(2))*F(2); % Inflow from valve 2 to tank 3 [cm3/s]
qin(4,1) = (1-gamma(1))*F(1); % Inflow from valve 1 to tank 4 [cm3/s]

% Outflows
h = m./(rho*A);            % Liquid level in each tank [cm]
qout = a.*sqrt(2*g*h);      % Outflow from each tank [cm3/s]

% Differential equations
xdot = zeros(4,1);
xdot(1,1) = rho*(qin(1,1)+qout(3,1)-qout(1,1)); % Mass balance Tank 1
xdot(2,1) = rho*(qin(2,1)+qout(4,1)-qout(2,1)); % Mass balance Tank 2
xdot(3,1) = rho*(qin(3,1)-qout(3,1));           % Mass balance Tank 3
xdot(4,1) = rho*(qin(4,1)-qout(4,1));           % Mass balance Tank 4
```

# Define Simulation Parameters

```
% -----  
% Parameters  
% -----  
  
a1 = 1.2272      %[cm2] Area of outlet pipe 1  
a2 = 1.2272      %[cm2] Area of outlet pipe 2  
a3 = 1.2272      %[cm2] Area of outlet pipe 3  
a4 = 1.2272      %[cm2] Area of outlet pipe 4  
  
A1 = 380.1327    %[cm2] Cross sectional area of tank 1  
A2 = 380.1327    %[cm2] Cross sectional area of tank 2  
A3 = 380.1327    %[cm2] Cross sectional area of tank 3  
A4 = 380.1327    %[cm2] Cross sectional area of tank 4  
  
gamma1 = 0.45;    % Flow distribution constant. Valve 1  
gamma2 = 0.40;    % Flow distribution constant. Valve 2  
  
g = 981;          %[cm/s2] The acceleration of gravity  
rho = 1.00;       %[g/cm3] Density of water  
  
p = [a1; a2; a3; a4; A1; A2; A3; A4; gamma1; gamma2; g; rho];  
% -----
```

# Simulation Scenario and Simulation

```
% -----  
% Simulation scenario  
% -----  
t0 = 0.0;           % [s] Initial time  
tf = 20*60;         % [s] Final time  
  
m10 = 0.0;          % [g] Liquid mass in tank 1 at time t0  
m20 = 0.0;          % [g] Liquid mass in tank 2 at time t0  
m30 = 0.0;          % [g] Liquid mass in tank 3 at time t0  
m40 = 0.0;          % [g] Liquid mass in tank 4 at time t0  
  
F1 = 300;           % [cm3/s] Flow rate from pump 1  
F2 = 300;           % [cm3/s] Flow rate from pump 2  
  
x0 = [m10; m20; m30; m40];  
u = [F1; F2]  
% -----
```

Simulate the system

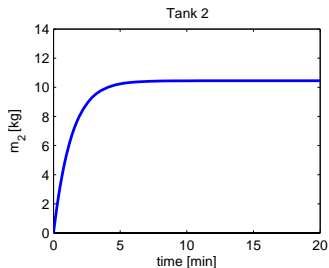
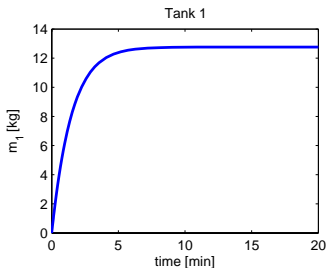
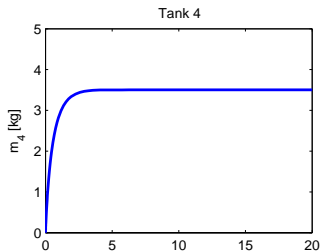
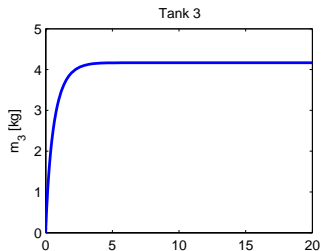
```
% -----  
% Compute the solution / Simulate  
% -----  
% Solve the system of differential equations  
[T,X] = ode15s(@FourTankSystem,[t0 tf],x0,[],u,p);
```

# Computation of additional variables

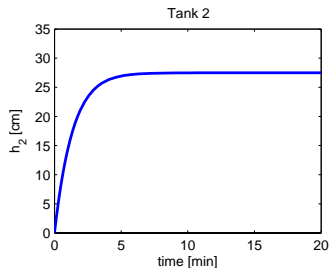
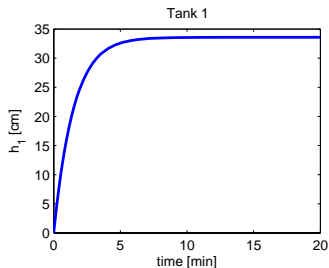
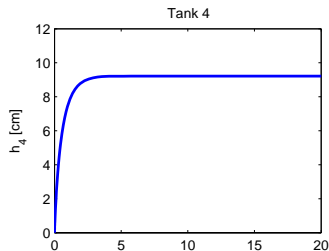
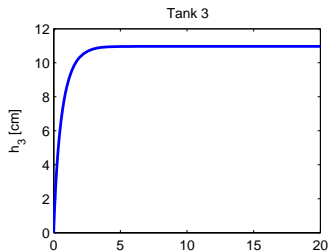
## Compute additional variables for plotting

```
% -----  
% help variables  
[nT,nX] = size(X);  
a = p(1:4,1)';  
A = p(5:8,1)';  
  
% Compute the measured variables  
H = zeros(nT,nX);  
for i=1:nT  
    H(i,:) = X(i,:)./(rho*A);  
end  
  
% Compute the flows out of each tank  
Qout = zeros(nT,nX);  
for i=1:nT  
    Qout(i,:) = a.*sqrt(2*g*H(i,:));  
end  
% -----
```

# Masses in the Tanks

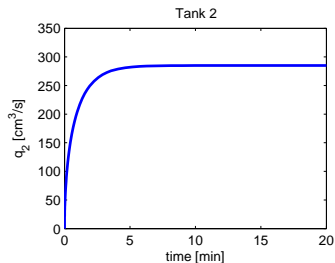
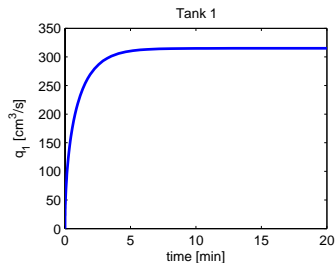
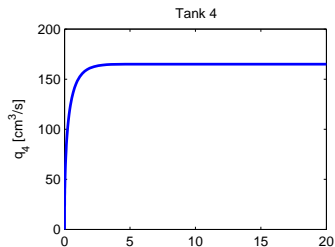
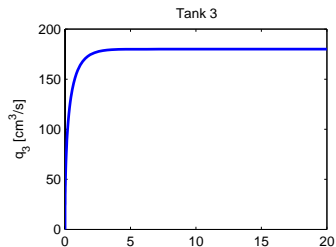


# Levels in the Tanks





# Outflow Rates



# Discrete-Time Generic Input-Output Model



$$x_{k+1} = F(x_k, u_k)$$

Discrete-time process model

$$y_k = g(x_k)$$

Sensor function

$$z_k = h(x_k)$$

Output function

## Zero-order-hold for MVs

$$u(t) = u_k \quad t_k \leq t < t_{k+1}$$

## Continuous-time process model to discrete-time process model

$$F(x_k, u_k) = x_k + \int_{t_k}^{t_{k+1}} f(x(t), u_k) dt$$

# Difference Equation

The difference equation

$$x_{k+1} = F(x_k, u_k)$$

with

$$F(x_k, u_k) = x_k + \int_{t_k}^{t_{k+1}} f(x(t), u_k) dt$$

can be computed by numerical solution of

$$\frac{dx}{dt}(t) = f(x(t), u_k) \quad x(t_k) = x_k \quad t_k \leq t < t_{k+1}$$

such that

$$x_{k+1} = x(t_{k+1})$$

# Discrete-Time Simulation using Matlab

## The discrete-time model

$$x_{k+1} = F(x_k, u_k) \quad F(x_k, u_k) = x_k + \int_{t_k}^{t_{k+1}} f(x(t), u_k) dt$$

$$y_k = g(x_k)$$

$$z_k = h(x_k)$$

may be simulated in Matlab using

```
for i=0:N
    k=i+1;
    y(:,k) = g(x(:,k));
    z(:,k) = h(x(:,k));
    [Tk,Xk] = ode15s(@f,[t(k) t(k+1)],x(:,k),odeOptions,u(:,k));
    x(:,k+1) = Xk(end,:)' ;
    T = [T; Tk];
    X = [X; Xk];
end
```

## Example - 4-Tank System



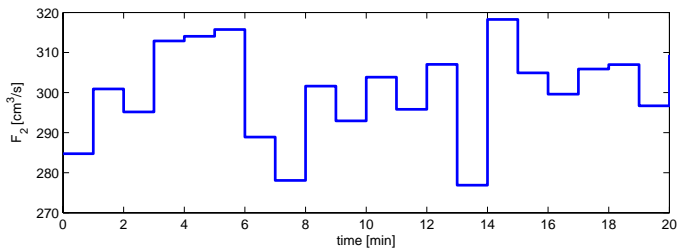
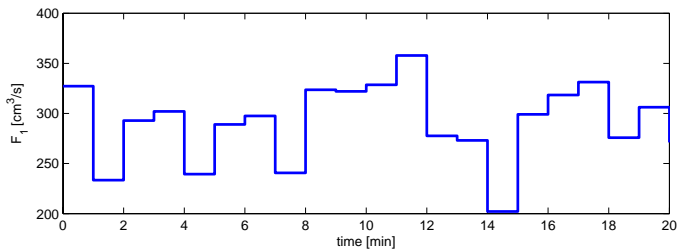
$$x_{k+1} = F(x_k, u_k)$$

$$y_k = g(x_k)$$

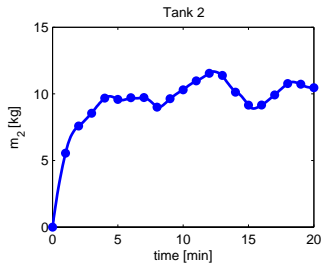
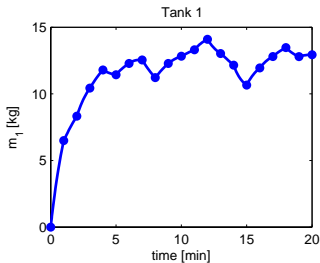
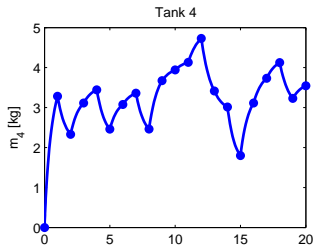
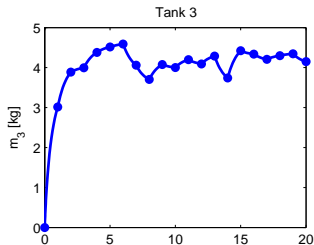
$$z_k = h(x_k)$$

```
X = zeros(0,nx);  
T = zeros(0,1);  
  
x(:,1) = x0;  
for k = 1:N-1  
    y(:,k) = FourTankSystemSensor(x(:,k),p); % Sensor function  
    z(:,k) = FourTankSystemOutput(x(:,k),p); % Output function  
  
    [Tk,Xk] = ode15s(@FourTankSystem,[t(k) t(k+1)],x(:,k),[],u(:,k),p);  
    x(:,k+1) = Xk(end,:)' ;  
  
    T = [T; Tk];  
    X = [X; Xk];  
end  
k = N;  
y(:,k) = FourTankSystemSensor(x(:,k),p);  
z(:,k) = FourTankSystemOutput(x(:,k),p);
```

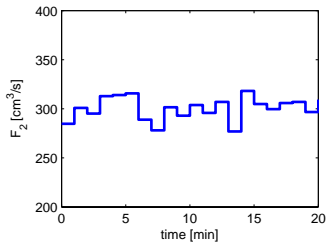
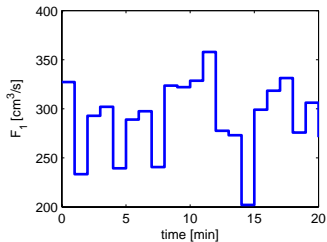
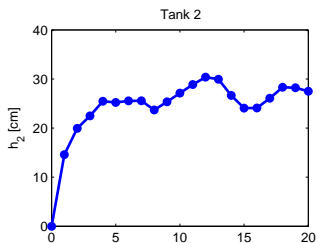
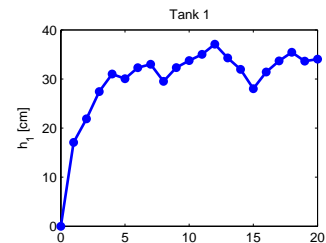
# Flow Rate Scenario



# Quadruple Tank Process - States

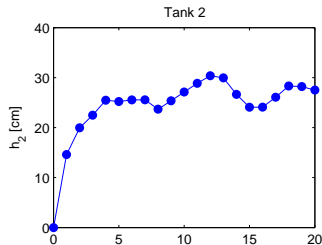
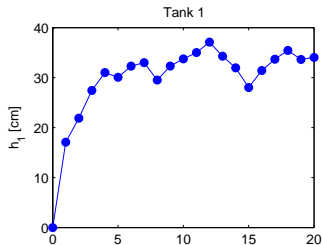
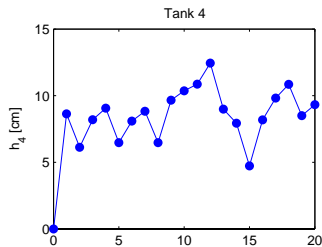
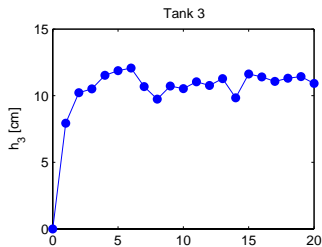


# Quadruple Tank Process - Inputs and Outputs





# Quadruple Tank Process - Sensors



# Stochastic Simulation

$\mathbf{x}_{k+1} = F(\mathbf{x}_k, u_k, \mathbf{w}_k)$	Process model
$\mathbf{y}_k = g(\mathbf{x}_k) + \mathbf{v}_k$	Sensor function
$\mathbf{z}_k = h(\mathbf{x}_k)$	Output function

$\mathbf{x}_0 \sim N(\bar{\mathbf{x}}_0, P_0)$	Unknown initial state
$\mathbf{w}_k \sim N_{iid}(0, Q)$	Process noise
$\mathbf{v}_k \sim N_{iid}(0, R)$	Measurement (sensor) noise

# A Stochastic Realization

The stochastic variables

$$\begin{aligned}\mathbf{w}_k &\sim N_{iid}(0, Q) & Q &= LL' \\ \mathbf{e}_k &\sim N_{iid}(0, I)\end{aligned}$$

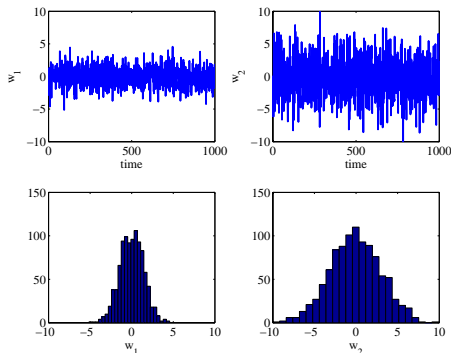
are related by

$$\mathbf{w}_k = L\mathbf{e}_k$$

As a normal distribution is completely characterized by its means and covariance, this relation can be proved by

$$\begin{aligned}E\{\mathbf{w}_k\} &= E\{L\mathbf{e}_k\} = LE\{\mathbf{e}_k\} = 0 \\ V\{\mathbf{w}_k\} &= \langle \mathbf{w}_k, \mathbf{w}_k \rangle = \langle L\mathbf{e}_k, L\mathbf{e}_k \rangle = L \underbrace{\langle \mathbf{e}_k, \mathbf{e}_k \rangle}_{=I} L' = LL' = Q\end{aligned}$$

# Stochastic Realization in Matlab



$$w_k \sim N_{iid}(0, Q)$$

$$Q = LL'$$

$$e_k \sim N_{iid}(0, I)$$

$$w_k = Le_k$$

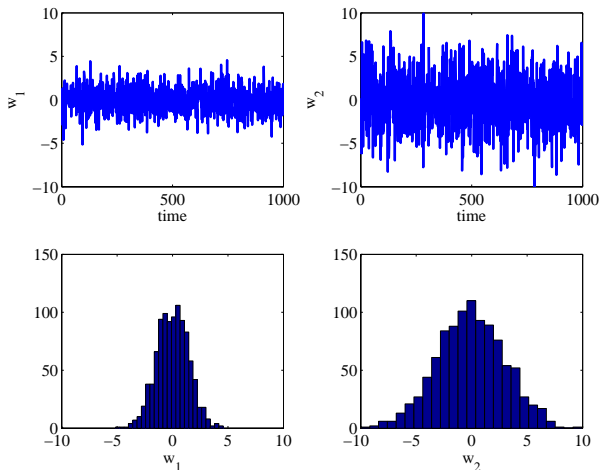
```
Q = [2 1; 1 10];  
L = chol(Q)';
```

```
MySeed = 100;  
randn('state', MySeed);  
w = L*randn(2,1000);
```

```
% You can use any number  
% Makes the random sequence reproducible  
% Generation of the random sequence
```

# Stochastic Process Noise

$$w_k \sim N_{iid}(0, Q)$$



## Process noise

$$\begin{bmatrix} \mathbf{F}_1 \\ \mathbf{F}_2 \end{bmatrix} = \begin{bmatrix} F_{1s} \\ F_{2s} \end{bmatrix} + \begin{bmatrix} \mathbf{w}_1 \\ \mathbf{w}_2 \end{bmatrix}$$

$$\begin{bmatrix} F_{1s} \\ F_{2s} \end{bmatrix} = \begin{bmatrix} 300 \\ 300 \end{bmatrix} \quad \begin{bmatrix} \mathbf{w}_1 \\ \mathbf{w}_2 \end{bmatrix} \sim N_{iid} \left( \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 30^2 & 0 \\ 0 & 10^2 \end{bmatrix} \right)$$

## Measurement noise

$$\mathbf{y} = \begin{bmatrix} \mathbf{y}_1 \\ \mathbf{y}_2 \\ \mathbf{y}_3 \\ \mathbf{y}_4 \end{bmatrix} = \begin{bmatrix} h_1 \\ h_2 \\ h_3 \\ h_4 \end{bmatrix} + \begin{bmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \\ \mathbf{v}_3 \\ \mathbf{v}_4 \end{bmatrix} \quad \mathbf{v} = \begin{bmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \\ \mathbf{v}_3 \\ \mathbf{v}_4 \end{bmatrix} \sim N \left( \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 1^2 & 0 & 0 & 0 \\ 0 & 1^2 & 0 & 0 \\ 0 & 0 & 1^2 & 0 \\ 0 & 0 & 0 & 1^2 \end{bmatrix} \right)$$

## Outputs

$$\mathbf{z} = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = \begin{bmatrix} h_1 \\ h_2 \end{bmatrix}$$

# Stochastic Simulation - Definition of Simulation Scenario

```
t0 = 0.0;           % [s] Initial time
tf = 20*60;         % [s] Final time
Ts = 10;            % [s] Sample Time
t = [t0:Ts:tf]';    % [s] Sample instants
N = length(t);

m10 = 0;            % [g] Liquid mass in tank 1 at time t0
m20 = 0;            % [g] Liquid mass in tank 2 at time t0
m30 = 0;            % [g] Liquid mass in tank 3 at time t0
m40 = 0;            % [g] Liquid mass in tank 4 at time t0

F1 = 300;           % [cm3/s] Flow rate from pump 1
F2 = 300;           % [cm3/s] Flow rate from pump 2

x0 = [m10; m20; m30; m40];
u = [repmat(F1,1,N); repmat(F2,1,N)];

% Process Noise
Q = [20^2 0; 0 40^2];
Lq = chol(Q,'lower');
w = Lq*randn(2,N);

% Measurement Noise
R = eye(4);
Lr = chol(R,'lower');
v = Lr*randn(4,N);
```

# Stochastic Simulation - Matlab Script

```
nx = 4; nu = 2; ny = 4; nz = 2;
x = zeros(nx,N);
y = zeros(ny,N);
z = zeros(nz,N);

X = zeros(0,nx);
T = zeros(0,1);

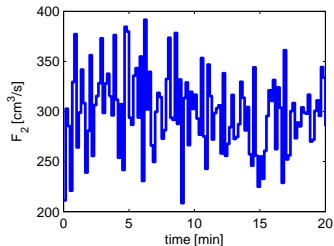
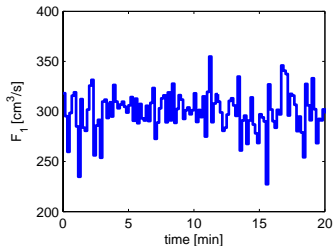
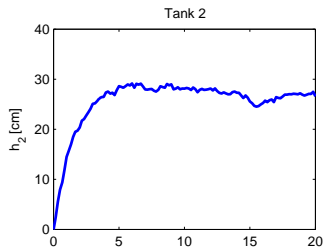
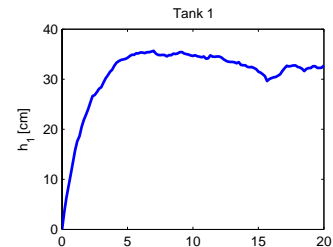
x(:,1) = x0;
for k = 1:N-1
    y(:,k) = FourTankSystemSensor(x(:,k),p)+v(:,k); % Sensor function
    z(:,k) = FourTankSystemOutput(x(:,k),p);          % Output function

    [Tk,Xk] = ode15s(@FourTankSystem,[t(k) t(k+1)],x(:,k),[],...
                    u(:,k)+w(:,k),p);
    x(:,k+1) = Xk(end,:)' ;

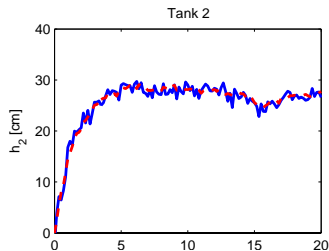
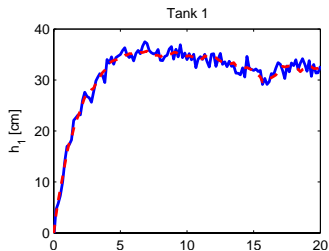
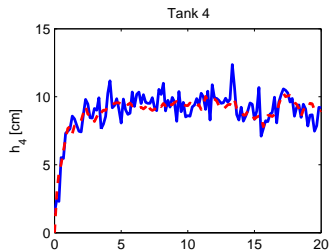
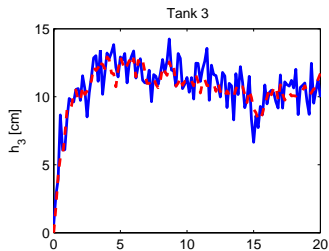
    T = [T; Tk];
    X = [X; Xk];
end
k = N;
y(:,k) = FourTankSystemSensor(x(:,k),p)+v(:,k); % Sensor function
z(:,k) = FourTankSystemOutput(x(:,k),p);          % Output function
```



# Stochastic Process Simulation - Input-Output



# Stochastic Process Simulation - Measurements



## Steady-State (Equilibrium Point)

$$\dot{x}(t) = f(x(t), u(t)) \quad x(t_0) = x_0$$

Steady state (equilibrium point)  $(x_s, u_s)$ . Given  $u(t) = u_s$  solve

$$0 = f(x_s, u_s)$$

`fsolve` in Matlab

```
xs0 = 5000*ones(4,1); % Initial guess of steady state
us  = [300; 300];      % Steady-state inputs
xs  = fsolve(@FourTankSystemWrap,xs0,[],us,p)
```

with

```
function xdot = FourTankSystemWrap(x,u,p)
xdot = FourTankSystem(0,x,u,p);
```

# Linearization of Continuous-Time Model

$$\dot{x}(t) = f(x(t), u(t)) \quad x(t_0) = x_0$$

Steady state (equilibrium point)  $(x_s, u_s)$ . Given  $u(t) = u_s$  solve

$$0 = f(x_s, u_s)$$

Taylor expansion

$$\begin{aligned} f(x(t), u(t)) &\approx \overbrace{f(x_s, u_s)}^{=0} + \overbrace{\left(\frac{\partial f}{\partial x}(x_s, u_s)\right)}^{=A} \overbrace{(x(t) - x_s)}^{=X(t)} + \overbrace{\left(\frac{\partial f}{\partial u}(x_s, u_s)\right)}^{=B} \overbrace{(u(t) - u_s)}^{=U(t)} \\ &= AX(t) + BU(t) \end{aligned}$$

$$\dot{X}(t) = \frac{d}{dt}(x(t) - x_s) = \frac{dx(t)}{dt} - \frac{dx_s}{dt} = \frac{dx(t)}{dt} - 0 = \dot{x}(t)$$

Then

$$\dot{X}(t) = AX(t) + BU(t) \quad X(t_0) = X_0 = x_0 - x_s$$

$$\begin{aligned}\dot{x}(t) &= f(x(t), u(t)) & x(t_0) &= x_0 \\ y(t) &= g(x(t)) \\ z(t) &= h(x(t))\end{aligned}$$

Steady-state  $(x_s, u_s, y_s, z_s)$

$$0 = f(x_s, u_s) \quad y_s = g(x_s) \quad z_s = h(x_s)$$

Deviation variables

$$\begin{aligned}X(t) &= x(t) - x_s & X_0 &= x_0 - x_s \\ U(t) &= u(t) - u_s & Y(t) &= y(t) - y_s & Z(t) &= z(t) - z_s\end{aligned}$$

Linear system

$$\begin{aligned}\dot{X}(t) &= AX(t) + BU(t) & X(t_0) &= X_0 & A &= \frac{\partial f}{\partial x}(x_s, u_s) & B &= \frac{\partial f}{\partial u}(x_s, u_s) \\ Y(t) &= CX(t) \\ Z(t) &= C_z X(t) & C &= \frac{\partial g}{\partial x}(x_s, u_s) & C_z &= \frac{\partial h}{\partial x}(x_s, u_s)\end{aligned}$$

$$\begin{aligned}\dot{x}(t) &= f(x(t), u(t)) & x(t_0) &= x_0 \\ y(t) &= g(x(t), u(t))\end{aligned}$$

Steady-state  $(x_s, u_s, y_s)$

$$0 = f(x_s, u_s) \quad y_s = g(x_s, u_s)$$

Deviation variables

$$\begin{aligned}X(t) &= x(t) - x_s & X_0 &= x_0 - x_s \\ U(t) &= u(t) - u_s \\ Y(t) &= y(t) - y_s\end{aligned}$$

Linear system

$$\begin{aligned}\dot{X}(t) &= AX(t) + BU(t) & X(t_0) &= X_0 \\ Y(t) &= CX(t) + DU(t)\end{aligned} \quad \begin{aligned}A &= \frac{\partial f}{\partial x}(x_s, u_s) & B &= \frac{\partial f}{\partial u}(x_s, u_s) \\ C &= \frac{\partial g}{\partial x}(x_s, u_s) & D &= \frac{\partial g}{\partial u}(x_s, u_s)\end{aligned}$$

## Example - Linearization of 4-Tank System

$$\dot{X}(t) = AX(t) + BU(t) \quad X(t_0) = X_0$$

$$Y(t) = CX(t)$$

$$Z(t) = C_z X(t)$$

$$X(t) = x(t) - x_s \quad U(t) = u(t) - u_s$$

$$Y(t) = y(t) - y_s \quad Z(t) = z(t) - z_s$$

$$u_s = \begin{bmatrix} F_{1s} \\ F_{2s} \end{bmatrix} = \begin{bmatrix} 300 \text{ cm}^3/\text{s} \\ 300 \text{ cm}^3/\text{s} \end{bmatrix}$$

$$z_s = \begin{bmatrix} h_{1s} \\ h_{2s} \end{bmatrix} = \begin{bmatrix} 33.6 \text{ cm} \\ 27.5 \text{ cm} \end{bmatrix}$$

$$x_s = \begin{bmatrix} m_{1s} \\ m_{2s} \\ m_{3s} \\ m_{4s} \end{bmatrix} = \begin{bmatrix} 12765 \text{ g} \\ 10449 \text{ g} \\ 4168 \text{ g} \\ 3502 \text{ g} \end{bmatrix}$$

$$y_s = \begin{bmatrix} h_{1s} \\ h_{2s} \\ h_{3s} \\ h_{4s} \end{bmatrix} = \begin{bmatrix} 33.6 \text{ cm} \\ 27.5 \text{ cm} \\ 11.0 \text{ cm} \\ 9.2 \text{ cm} \end{bmatrix}$$

## Example - Linearization of 4-Tank System

$$\dot{X}(t) = AX(t) + BU(t) \quad X(t_0) = X_0$$

$$Y(t) = CX(t)$$

$$Z(t) = C_z X(t)$$

with the matrices

$$A = \begin{bmatrix} -\frac{1}{T_1} & 0 & \frac{1}{T_3} & 0 \\ 0 & -\frac{1}{T_2} & 0 & \frac{1}{T_4} \\ 0 & 0 & -\frac{1}{T_3} & 0 \\ 0 & 0 & 0 & -\frac{1}{T_4} \end{bmatrix} \quad B = \begin{bmatrix} \rho\gamma_1 & 0 \\ 0 & \rho\gamma_2 \\ 0 & \rho(1-\gamma_2) \\ \rho(1-\gamma_1) & 0 \end{bmatrix}$$
$$C = \begin{bmatrix} \frac{1}{\rho A_1} & 0 & 0 & 0 \\ 0 & \frac{1}{\rho A_2} & 0 & 0 \\ 0 & 0 & \frac{1}{\rho A_3} & 0 \\ 0 & 0 & 0 & \frac{1}{\rho A_4} \end{bmatrix} \quad C_z = \begin{bmatrix} \frac{1}{\rho A_1} & 0 & 0 & 0 \\ 0 & \frac{1}{\rho A_2} & 0 & 0 \end{bmatrix}$$

and time constants defined by

$$T_i = \frac{A_i \sqrt{2gh_{i,s}}}{a_i g} = \frac{A_i}{a_i} \sqrt{\frac{2h_{i,s}}{g}} \quad i = \{1, 2, 3, 4\}$$



## Example - Linearization 4-Tank System

```
% -----  
% Parameters  
% -----  
ap = [a1; a2; a3; a4];    % [cm2] Pipe cross sectional areas  
At = [A1; A2; A3; A4];    % [cm2] Tank cross sectional areas  
gam = [gamma1; gamma2];   % [-] Valve constants  
g = 981;                  % [cm/s2] The acceleration of gravity  
rho = 1.00;               % [g/cm3] Density of water  
  
p = [ap; At; gamma; g; rho];  
  
% -----  
% Steady State  
% -----  
us = [300; 300]           % [cm3/s] Flow rates  
xs0 = [5000; 5000; 5000; 5000] % [g] Initial guess on xs  
  
xs = fsolve(@FourTankSystemWrap,xs0,[],us,p)  
ys = FourTankSystemSensor(xs,p)  
zs = FourTankSystemOutput(xs,p)  
  
% -----  
% Linearization  
% -----  
hs = ys;  
T = (At./ap).*sqrt(2*hs/g)  
  
A=[-1/T(1) 0 1/T(3) 0;0 -1/T(2) 0 1/T(4);0 0 -1/T(3) 0;0 0 0 -1/T(4)]  
B=[rho*gam(1) 0;0 rho*gam(2); 0 rho*(1-gam(2)); rho*(1-gam(1)) 0]  
C=diag(1./(rho*At))  
Cz=C(1:2,:)
```

## Example - Linearization 4-Tank System

---

$$A = \begin{bmatrix} -0.012338 & 0 & 0.021592 & 0 \\ 0 & -0.013637 & 0 & 0.023555 \\ 0 & 0 & -0.021592 & 0 \\ 0 & 0 & 0 & -0.023555 \end{bmatrix}$$

$$B = \begin{bmatrix} 0.45 & 0 \\ 0 & 0.4 \\ 0 & 0.6 \\ 0.55 & 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 0.0026307 & 0 & 0 & 0 \\ 0 & 0.0026307 & 0 & 0 \\ 0 & 0 & 0.0026307 & 0 \\ 0 & 0 & 0 & 0.0026307 \end{bmatrix}$$

$$C_z = \begin{bmatrix} 0.0026307 & 0 & 0 & 0 \\ 0 & 0.0026307 & 0 & 0 \end{bmatrix}$$

# Continuous-Time Transfer Function

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) & x(0) &= x_0 \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$

Define the Laplace transform

$$F(s) = \mathcal{L}\{f(t)\} = \int_0^{\infty} e^{-st} f(t) dt$$

such that

$$\begin{aligned}\mathcal{L}\{x(t)\} &= X(s) & \mathcal{L}\{u(t)\} &= U(s) & \mathcal{L}\{y(t)\} &= Y(s) \\ \mathcal{L}\{\dot{x}(t)\} &= sX(s) - x_0\end{aligned}$$

Then

$$\begin{aligned}sX(s) - x_0 &= AX(s) + BU(s) & \Leftrightarrow \\ X(s) &= (sI - A)^{-1}x_0 + (sI - A)^{-1}BU(s)\end{aligned}$$

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) & x(0) &= x_0 \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$

The LaPlace transforms of this system are

$$\begin{aligned}X(s) &= (sI - A)^{-1}x_0 + (sI - A)^{-1}BU(s) \\ Y(s) &= CX(s) + DU(s) \\ &= C(sI - A)^{-1}x_0 + \overbrace{[C(sI - A)^{-1}B + D]}^{=G(s)} U(s) \\ &= C(sI - A)^{-1}x_0 + G(s)U(s)\end{aligned}$$

Let  $x_0 = 0$ . Then

$$Y(s) = G(s)U(s) \quad G(s) = C(sI - A)^{-1}B + D$$

$G(s)$  is the transfer function of the system

# Continuous-Time Transfer Function

The continuous-time linear time-invariant system

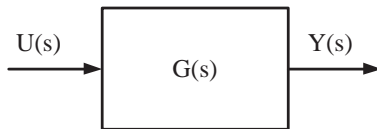
$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) & x(0) &= 0 \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$

can be represented as the input-output function in the LaPlace domain

$$Y(s) = G(s)U(s)$$

with the transfer function

$$G(s) = C(sI - A)^{-1}B + D$$



## Poles-Zero Representation - SISO system

$$\begin{aligned} G(s) &= C(sI - A)^{-1}B + D \\ &= K_{zp} \frac{(s - z_1)(s - z_2) \dots (s - z_{n_z})}{(s - p_1)(s - p_2) \dots (s - p_n)} = K_{zp} \frac{\prod (s - z_i)}{\prod (s - p_i)} \end{aligned}$$

- The poles are computed as the eigenvalues of  $A$ :  $p = \text{eig}(A)$
- The zeros are computed as the generalized eigenvalues of

$$\overbrace{\begin{bmatrix} A & B \\ C & D \end{bmatrix}}^{=M} \begin{bmatrix} x \\ u \end{bmatrix} = z \overbrace{\begin{bmatrix} I & 0 \\ 0 & 0 \end{bmatrix}}^{=N} \begin{bmatrix} x \\ u \end{bmatrix}$$

$$z = \text{eig}(M, N) \quad (|z| < \infty)$$

- The constant  $K_{zp}$  is computed by

$$K_{zp} = G(s) \frac{\prod (s - p_i)}{\prod (s - z_i)} \quad s \neq p_i, z_i$$

## Example

$$G(s) = 2 \frac{(s - 3)}{(s - 0)(s + 4)(s + (2 + 3i))(s + (2 - 3i))}$$

Constant:  $K_{zp} = 2$

Zero:  $z = 3$

Poles:  $p_1 = 0$ ,  $p_2 = -4$ ,  $p_3 = -2 \pm 3i$

This is equivalent with

$$G(s) = 2 \frac{(s - 3)}{s(s + 4)(s^2 + 4s + 13)} = K \frac{(\beta s + 1)}{s(\tau_1 s + 1)(\tau^2 s^2 + 2\zeta\tau s + 1)}$$

$$\beta = -1/3$$

$$\tau_1 = 1/4$$

$$\tau = \frac{1}{\sqrt{13}} \quad \zeta = \frac{4/13}{2\sqrt{13}} = \frac{2}{13\sqrt{13}}$$

$$K = 2(-3)/(4 \cdot 13) = -3/26$$

## Some Elementary Continuous-Time Transfer Functions

$$Y(s) = G(s)U(s)$$

$$G(s) = \frac{1}{s} \quad \text{Integrator}$$

$$G(s) = \frac{K}{\tau s + 1} \quad \text{First order system}$$

$$G(s) = \frac{K}{(\tau_1 s + 1)(\tau_2 s + 1)} \quad \text{Second order system - damped}$$

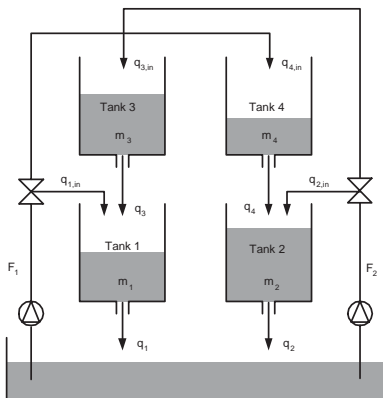
$$G(s) = \frac{K}{(\tau s + 1)^n} \quad \text{n'th order system}$$

$$G(s) = \frac{K}{\tau^2 s^2 + 2\tau\zeta s + 1} \quad \text{Second order system - underdamped}$$

$$G(s) = \frac{K(\beta s + 1)}{(\tau_1 s + 1)(\tau_2 s + 1)} \quad \text{Second order system with zero}$$



# 4-Tank System - Model



$$T_1 = \frac{A_1}{a_1} \sqrt{\frac{2h_{1,s}}{g}} = 81.0 \text{ s} = 1.35 \text{ min}$$

$$T_2 = \frac{A_2}{a_2} \sqrt{\frac{2h_{2,s}}{g}} = 73.3 \text{ s} = 1.22 \text{ min}$$

$$T_3 = \frac{A_3}{a_3} \sqrt{\frac{2h_{3,s}}{g}} = 46.3 \text{ s} = 0.77 \text{ min}$$

$$T_4 = \frac{A_4}{a_4} \sqrt{\frac{2h_{4,s}}{g}} = 42.5 \text{ s} = 0.71 \text{ min}$$

$$K = G(0) = -C_z A^{-1} B$$

$$K_{11} = 0.0959 \text{ s/cm}^2$$

$$K_{21} = 0.1061 \text{ s/cm}^2$$

$$K_{12} = 0.1279 \text{ s/cm}^2$$

$$K_{22} = 0.0772 \text{ s/cm}^2$$

$$\begin{bmatrix} Z_1(s) \\ Z_2(s) \end{bmatrix} = \begin{bmatrix} \frac{K_{11}}{T_1 s + 1} & \frac{K_{12}}{(T_3 s + 1)(T_1 s + 1)} \\ \frac{K_{21}}{(T_4 s + 1)(T_2 s + 1)} & \frac{K_{22}}{T_2 s + 1} \end{bmatrix} \begin{bmatrix} U_1(s) \\ U_2(s) \end{bmatrix}$$

# Linear System of First-Order Differential Equations

The linear system of first order differential equations

$$\dot{x}(t) = Ax(t) + Bu(t) \quad x(t_0) = x_0$$

has the solution

$$x(t) = e^{A(t-t_0)}x_0 + \int_{t_0}^t e^{A(t-\tau)}Bu(\tau)d\tau$$

You can convince yourself about this solution by reviewing the solution of

$$\frac{dp(t)}{dt} + ap(t) = q(t)$$

This equation is known from calculus.

# Discretization

## Discrete time

$$t_k = t_0 + kT_s \quad k = 0, 1, 2 \dots$$

## States at discrete times

$$x_k = x(t_k)$$

## Zero-order-hold of the inputs

$$u(t) = u_k \quad t_k \leq t < t_{k+1}$$

## Consider the linear differential equation

$$\dot{x}(t) = Ax(t) + Bu(t) \quad x(t_k) = x_k$$

## Then

$$\begin{aligned} x_{k+1} &= x(t_{k+1}) = e^{A(t_{k+1}-t_k)} x_k + \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-\tau)} B u(\tau) d\tau \\ &= [e^{AT_s}] x_k + \left[ \int_0^{T_s} e^{A\eta} B d\eta \right] u_k \end{aligned}$$

# Discrete-Time Linear Model

The continuous linear time-invariant model

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) & x(t_0) &= x_0 \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$

is equivalent with the discrete linear time-invariant model

$$\begin{aligned}x_{k+1} &= A_d x_k + B_d u_k \\ y_k &= C_d x_k + D_d u_k\end{aligned}$$

with

$$\begin{aligned}A_d &= e^{AT_s} & B_d &= \int_0^{T_s} e^{A\tau} B d\tau \\ C_d &= C & D_d &= D\end{aligned}$$

$(A_d, B_d)$  can be computed by

$$\begin{bmatrix} A_d & B_d \\ 0 & I \end{bmatrix} = \exp \left( \begin{bmatrix} A & B \\ 0 & 0 \end{bmatrix} T_s \right)$$

## ZOH Discretization of Linear System

$$\begin{bmatrix} A_d & B_d \\ 0 & I \end{bmatrix} = \exp \left( \begin{bmatrix} A & B \\ 0 & 0 \end{bmatrix} T_s \right)$$

### Matlab implementation

```
function [Abar,Bbar]=c2dzoh(A,B,Ts)

[nx,nu]=size(B);
M = [A B; zeros(nu,nx) zeros(nu,nu)];
Phi = expm(M*Ts);
Abar = Phi(1:nx,1:nx);
Bbar = Phi(1:nx,nx+1:nx+nu);
```

A =

-0.012338	0	0.021592	0
0	-0.013637	0	0.023555
0	0	-0.021592	0
0	0	0	-0.023555

B =

0.45	0
0	0.4
0	0.6
0.55	0

$T_s = 10$ . [Ad,Bd]=c2dzoh(A,B,10)

Ad =

0.8839	0	0.1823	0
0	0.8725	0	0.1957
0	0	0.8058	0
0	0	0	0.7901

Bd =

4.2335	0.5791
0.5729	3.7392
0	5.3965
4.9002	0

# Discrete-Time Transfer Function

$$x_{k+1} = Ax_k + Bu_k$$

$$y_k = Cx_k + Du_k$$

Z-transform (unilateral)

$$F(z) = \mathcal{Z}\{f_k\} = \sum_{k=0}^{\infty} z^{-k} f_k$$

$$X(z) = \mathcal{Z}\{x_k\} \quad U(z) = \mathcal{Z}\{u_k\} \quad Y(z) = \mathcal{Z}\{y_k\}$$

$$\mathcal{Z}\{x_{k+1}\} = zX(z) - zx_0$$

$$zX(z) - zx_0 = AX(z) + BU(z) \quad \Leftrightarrow$$

$$X(z) = (zI - A)^{-1}zx_0 + (zI - A)^{-1}BU(z)$$

$$\begin{aligned}x_{k+1} &= Ax_k + Bu_k \\y_k &= Cx_k + Du_k\end{aligned}$$

$$X(z) = (zI - A)^{-1}zx_0 + (zI - A)^{-1}BU(z)$$

$$\begin{aligned}Y(z) &= CX(z) + DU(z) \\&= C(zI - A)^{-1}zx_0 + \overbrace{\left[ C(zI - A)^{-1}B + D \right]}^{=G(z)} U(z) \\&= C(zI - A)^{-1}zx_0 + G(z)U(z)\end{aligned}$$

Let  $x_0 = 0$ . Then

$$Y(z) = G(z)U(z) \quad G(z) = C(zI - A)^{-1}B + D$$



# Discrete-Time Transfer Function

The discrete-time linear time-invariant system

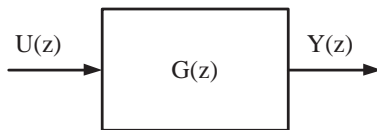
$$\begin{aligned}x_{k+1} &= Ax_k + Bu_k & x_0 &= 0 \\y_k &= Cx_k + Du_k\end{aligned}$$

can be represented as the input-output function in the Z-domain

$$Y(z) = G(z)U(z)$$

with the transfer function

$$G(z) = C(zI - A)^{-1}B + D$$



## Poles-Zero Representation - SISO system

$$\begin{aligned} G(z) &= C(zI - A)^{-1}B + D \\ &= K_{zp} \frac{(z - z_1)(z - z_2) \dots (z - z_{n_z})}{(z - p_1)(z - p_2) \dots (z - p_n)} = K_{zp} \frac{\prod(z - z_i)}{\prod(z - p_i)} \end{aligned}$$

- The poles are computed as the eigenvalues of  $A$ :  $p = \text{eig}(A)$
- The zeros are computed as the generalized eigenvalues of

$$\overbrace{\begin{bmatrix} A & B \\ C & D \end{bmatrix}}^{=M} \begin{bmatrix} x \\ u \end{bmatrix} = z \overbrace{\begin{bmatrix} I & 0 \\ 0 & 0 \end{bmatrix}}^{=N} \begin{bmatrix} x \\ u \end{bmatrix}$$

$$z = \text{eig}(M, N) \quad (|z| < \infty)$$

- The constant  $K_{zp}$  is computed by

$$K_{zp} = G(z) \frac{\prod(z - p_i)}{\prod(z - z_i)} \quad z \neq p_i, z_i$$

# Stochastic Systems

- Physical systems evolve in continuous time
- Some of the phenomena occurring are stochastic
- Question: How to convert a continuous-time stochastic model to a discrete time stochastic model

In particular, we cannot extend a system of ODEs

$$\frac{dx}{dt}(t) = f(x(t), u(t)) \quad x(t_0) = x_0$$

to a system of stochastic differential equations in the following form

$$\frac{d\mathbf{x}}{dt}(t) = f(\mathbf{x}(t), u(t)) + \sigma(\mathbf{x}(t), u(t))\mathbf{w}(t) \quad \text{Not well-defined}$$

as the last expression is not well-defined mathematically

# Stochastic Systems

Hence, the following is not well-defined

$$\frac{dx}{dt}(t) = f(x(t), u(t), w(t)) \quad x(t_0) = x_0 \quad \text{Not well-defined}$$

for continuous stochastic disturbances  $w(t)$ .

We can assume that

$$w(t) = w_k \quad t_k \leq t < t_{k+1} \quad t_{k+1} = t_k + T_s$$

Then a specific realization  $\{w_k\}$  leads to

$$\frac{dx}{dt}(t) = f(x(t), u(t), w_k) \quad t_k \leq t < t_{k+1} \quad x(t_k) = x_k$$

from which  $x(t)$  is computed. The problem with this construct is that the stochastic properties depends on  $T_s$  and does not have the correct properties in the limit  $T_s \rightarrow 0$ .

# Stochastic Differential Equation - with Ito interpretation

The approximation of deterministic differential equation

$$x(t + \delta t) - x(t) = f(x(t), u(t))\delta t + o(\delta t)$$

is extended to the stochastic case

$$\mathbf{x}(t + \delta t) - \mathbf{x}(t) = f(\mathbf{x}(t), u(t))\delta t + \sigma(\mathbf{x}(t), u(t)) [\mathbf{w}(t + \delta t) - \mathbf{w}(t)] + o(\delta t)$$

using increments  $\Delta \mathbf{w}(t)$  that are independent and normally distributed

$$\Delta \mathbf{w}(t) = [\mathbf{w}(t + \delta t) - \mathbf{w}(t)] \sim N_{iid}(0, I\delta t) = \sqrt{\delta t} N_{iid}(0, I)$$

In the limit  $\delta t \rightarrow 0$

$$d\mathbf{x}(t) = f(\mathbf{x}(t), u(t))dt + \sigma(\mathbf{x}(t), u(t))d\mathbf{w}(t)$$

# Stochastic Differential Equation - with Ito interpretation

$$d\mathbf{x}(t) = f(\mathbf{x}(t), u(t))dt + \sigma(\mathbf{x}(t), u(t))d\mathbf{w}(t)$$

with  $\{\mathbf{w}(t)\}$  being a standard Wiener Process (Brownian motion)

- ❶  $\mathbf{w}(t)$  is normally distributed
- ❷  $\mathbf{w}(t)$  is independent of  $\mathbf{w}(s)$  for all  $s \neq t$
- ❸  $E\{\mathbf{w}(t)\} = 0$
- ❹  $E\{d\mathbf{w}(t)d\mathbf{w}(t)'\} = I dt$

The integral equation corresponding to the Stochastic Differential Equation (SDE) is

$$\mathbf{x}(t) = \mathbf{x}(t_0) + \int_{t_0}^t f(\mathbf{x}(s), u(s))ds + \int_{t_0}^t \sigma(\mathbf{x}(s), u(s))d\mathbf{w}(s)$$

with the integrals interpreted as Ito integrals (forward Euler integrals).

# Stochastic Systems - Discrete Time

$$\begin{aligned} \mathbf{x}_{k+1} &= F(\mathbf{x}_k, u_k, \mathbf{w}_k) & \mathbf{x}_0 &\sim N(\bar{\mathbf{x}}_0, P_0) & \mathbf{w}_k &\sim N(0, Q) \\ \mathbf{y}_k &= g(\mathbf{x}_k) + \mathbf{v}_k & \mathbf{v}_k &\sim N(0, R) \\ \mathbf{z}_k &= h(\mathbf{x}_k) \end{aligned}$$

# Stochastic Systems - Discrete Time

$$\begin{aligned} \mathbf{x}_{k+1} &= F(\mathbf{x}_k, u_k, \mathbf{w}_k) & \mathbf{x}_0 &\sim N(\bar{x}_0, P_0) & \mathbf{w}_k &\sim N(0, Q) \\ \mathbf{y}_k &= g(\mathbf{x}_k) + \mathbf{v}_k & \mathbf{v}_k &\sim N(0, R) \\ \mathbf{z}_k &= h(\mathbf{x}_k) \end{aligned}$$

Steady-state (equilibrium point): Given  $u_s = 0$  and  $w_s = 0$ , compute

$$x_s = F(x_s, u_s, 0) \quad R(x_s) = x_s - F(x_s, u_s, 0) = 0$$

and

$$y_s = g(x_s)$$

$$z_s = h(x_s)$$

Deviation variables

$$\mathbf{X}(t) = \mathbf{x}(t) - x_s \quad U(t) = u(t) - u_s$$

$$\mathbf{Y}(t) = \mathbf{y}(t) - y_s \quad \mathbf{Z}(t) = \mathbf{z}(t) - z_s$$



# Stochastic Systems - Discrete Time

$$\begin{aligned} \mathbf{x}_{k+1} &= F(\mathbf{x}_k, u_k, \mathbf{w}_k) & \mathbf{x}_0 &\sim N(\bar{\mathbf{x}}_0, P_0) & \mathbf{w}_k &\sim N(0, Q) \\ \mathbf{y}_k &= g(\mathbf{x}_k) + \mathbf{v}_k & \mathbf{v}_k &\sim N(0, R) \\ \mathbf{z}_k &= h(\mathbf{x}_k) \end{aligned}$$

can be approximated by the linear discrete-time stochastic system

$$\begin{aligned} \mathbf{X}_{k+1} &= A\mathbf{X}_k + BU_k + G\mathbf{w}_k & \mathbf{X}_0 &\sim N(\bar{\mathbf{X}}_0, P_0), \mathbf{w}_k \sim N(0, Q) \\ \mathbf{Y}_k &= C\mathbf{X}_k + \mathbf{v}_k & \mathbf{v}_k &\sim N(0, R) \\ \mathbf{Z}_k &= C_z\mathbf{X}_k \end{aligned}$$

around the steady-state  $(x_s, u_s, y_s, z_s)$ . The matrices  $(A, B, G, C, C_z)$  are defined by

$$\begin{aligned} A &= \frac{\partial F}{\partial x}(x_s, u_s, 0) & B &= \frac{\partial F}{\partial u}(x_s, u_s, 0) & G &= \frac{\partial F}{\partial w}(x_s, u_s, 0) \\ C &= \frac{\partial g}{\partial x}(x_s) & C_z &= \frac{\partial h}{\partial x}(x_s) \end{aligned}$$

# Stochastic Systems - Linear Continuous-Discrete Time

$$d\mathbf{x}(t) = A\mathbf{x}(t)dt + Gd\mathbf{w}(t)$$

Let  $\mathbf{x}(t_0) \sim N(\bar{\mathbf{x}}_0, P_0)$  and let  $\{\mathbf{w}(t)\}$  be a standard Wiener process. The solution to this system is

$$\mathbf{x}(t) = e^{A(t-t_0)}\mathbf{x}(t_0) + \int_{t_0}^t e^{A(t-s)}Gd\mathbf{w}(s)$$

and has the distribution

$$\mathbf{x}(t) \sim N(\bar{\mathbf{x}}(t), P(t))$$

$$\bar{\mathbf{x}}(t) = E\{\mathbf{x}(t)\} = e^{A(t-t_0)}\bar{\mathbf{x}}(t_0)$$

$$P(t) = V\{\mathbf{x}(t)\} = e^{A(t-t_0)}P(t_0)e^{A'(t-t_0)} + \int_{t_0}^t e^{A(t-s)}GG'e^{A'(t-s)}ds$$

## Mean

$$\begin{aligned}\bar{x}(t) &= E \{ \mathbf{x}(t) \} \\ &= E \left\{ e^{A(t-t_0)} \mathbf{x}(t_0) + \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right\} \\ &= e^{A(t-t_0)} E \{ \mathbf{x}(t_0) \} + E \left\{ \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right\} \\ &= e^{A(t-t_0)} \bar{x}(t_0)\end{aligned}$$

## Covariance

$$\begin{aligned}P(t) &= E \{ (\mathbf{x}(t) - \bar{x}(t))(\mathbf{x}(t) - \bar{x}(t))' \} \\ &= e^{A(t-t_0)} E \{ (\mathbf{x}(t_0) - \bar{x}(t_0))(\mathbf{x}(t_0) - \bar{x}(t_0))' \} e^{A'(t-t_0)} \\ &\quad + e^{A(t-t_0)} E \left\{ (\mathbf{x}(t_0) - \bar{x}(t_0)) \left( \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right)' \right\} \\ &\quad + E \left\{ \left( \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right) (\mathbf{x}(t_0) - \bar{x}(t_0))' \right\} e^{A'(t-t_0)} \\ &\quad + E \left\{ \left( \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right) \left( \int_{t_0}^t e^{A(t-s)} G d\mathbf{w}(s) \right)' \right\} \\ &= e^{A(t-t_0)} P(t_0) e^{A'(t-t_0)} + \int_{t_0}^t e^{A(t-s)} G G' e^{A'(t-s)} ds\end{aligned}$$

# Stochastic Systems - Linear Continuous-Discrete Time

$$\begin{aligned}\mathbf{x}_{k+1} = \mathbf{x}(t_{k+1}) &= e^{A(t_{k+1}-t_k)} \mathbf{x}(t_k) + \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G d\mathbf{w}(s) \\ &= e^{AT_s} \mathbf{x}_k + \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G d\mathbf{w}(s) \\ &= e^{AT_s} \mathbf{x}_k + \mathbf{w}_k\end{aligned}$$

with

$$\mathbf{w}_k = \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G d\mathbf{w}(s)$$

$$\mathbf{w}_k \sim N_{iid}(0, \bar{Q})$$

$$\begin{aligned}\bar{Q} &= E \{ \mathbf{w}_k \mathbf{w}_k' \} = E \left\{ \left( \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G d\mathbf{w}(s) \right) \left( \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G d\mathbf{w}(s) \right)' \right\} \\ &= \int_{t_k}^{t_{k+1}} e^{A(t_{k+1}-s)} G G' e^{A'(t_{k+1}-s)} ds = \int_0^{T_s} e^{A\tau} G G' e^{A'\tau} d\tau\end{aligned}$$

# Stochastic Systems - Linear Continuous-Discrete Time

$$d\mathbf{x}(t) = A\mathbf{x}(t)dt + Gd\mathbf{w}(t)$$

is equivalent to

$$\mathbf{x}_{k+1} = \bar{A}\mathbf{x}_k + \mathbf{w}_k \quad \mathbf{x}_0 \sim N(\bar{x}_0, P_0), \quad \mathbf{w}_k \sim N_{iid}(0, \bar{Q})$$

with

$$\bar{A} = e^{AT_s}$$

$$\bar{Q} = \int_0^{T_s} e^{A\tau} G G' e^{A'\tau} d\tau$$

The matrices  $(\bar{A}, \bar{Q})$  can be computed by

$$\begin{bmatrix} \Phi_{11} & \Phi_{12} \\ 0 & \Phi_{22} \end{bmatrix} = \exp \left( \begin{bmatrix} -A & GG' \\ 0 & A' \end{bmatrix} T_s \right)$$

$$\bar{A} = \Phi'_{22}$$

$$\bar{Q} = \Phi'_{22} \Phi_{12}$$

# Stochastic Systems - Linear Continuous-Discrete Time

The continuous-discrete stochastic system with ZOH input  $u(t)$

$$\begin{aligned}d\mathbf{x}(t) &= (A\mathbf{x}(t) + Bu(t))dt + Gd\mathbf{w}(t) & \mathbf{x}_0 &\sim N(\bar{x}_0, P_0) \\ \mathbf{y}(t_k) &= C\mathbf{x}(t_k) + \mathbf{v}(t_k) & \{\mathbf{w}(t)\} &\text{ standard Wiener process} \\ \mathbf{z}(t_k) &= C_z\mathbf{x}(t_k) & \mathbf{v}(t_k) &= \mathbf{v}_k \sim N_{iid}(0, R)\end{aligned}$$

is equivalent to the discrete-time stochastic system

$$\begin{aligned}\mathbf{x}_{k+1} &= \bar{A}\mathbf{x}_k + \bar{B}u_k + \bar{G}\mathbf{w}_k & \mathbf{x}_0 &\sim N(\bar{x}_0, P_0) & \mathbf{w}_k &\sim N_{iid}(0, \bar{Q}) \\ \mathbf{y}_k &= C\mathbf{x}_k + \mathbf{v}_k & \mathbf{v}_k &\sim N(0, R) \\ \mathbf{z}_k &= C_z\mathbf{x}_k\end{aligned}$$

$$\begin{aligned}\bar{A} &= e^{AT_s} & \bar{B} &= \int_0^{T_s} e^{A\tau} d\tau B \\ \bar{G} &= I & \bar{Q} &= \int_0^{T_s} e^{A\tau} GG' e^{A'\tau} d\tau\end{aligned}$$

$$\begin{aligned}\begin{bmatrix} \bar{A} & \bar{B} \\ 0 & I \end{bmatrix} &= \exp\left(\begin{bmatrix} A & B \\ 0 & 0 \end{bmatrix} T_s\right) \\ \begin{bmatrix} \Phi_{11} & \Phi_{12} \\ 0 & \Phi_{22} \end{bmatrix} &= \exp\left(\begin{bmatrix} -A & GG' \\ 0 & A' \end{bmatrix} T_s\right) \\ \bar{Q} &= \Phi'_{22}\Phi_{12}\end{aligned}$$

# Learning Objectives

After this lecture you should be able to

- ➊ Apply conservation of mass to develop simple first-principle models
- ➋ Simulate systems described by ODEs using Matlab
- ➌ Compute steady-states and linearize a system around a steady state
- ➍ Discretize a linear continuous-time state space system
- ➎ Derive transfer functions for linear state-space systems
- ➏ Do simulations of stochastic systems
- ➐ Discretize a continuous-time stochastic system

## Exercise 1

Consider the 4-tank system with the parameters given in p. 12. Let  $F_{1s} = 250 \text{ cm}^3/\text{s}$  and  $F_{2s} = 325 \text{ cm}^3/\text{s}$ .

- 1 Compute the steady-state of this system
- 2 Simulate the response for a 5, 10, and 25% step increase in  $F_1$ , respectively.
- 3 Linearize the model at steady state. What is  $(A, B, C, D)$  for the continuous-time system?
- 4 Discretize the system using a sample time of  $T_s = 4$  seconds. What is  $(A, B, C, D)$  for the discrete time system.
- 5 Simulate step responses for a 5, 10, and 25% step increase in  $F_1$ , respectively using the linear model. Compare these responses to the responses of the nonlinear model.
- 6 Compute the continuous-time and discrete-time transfer functions for this 4-tank system. What are the gain, poles and zeros for these systems?



## Exercise 2

Consider the continuous-time system

$$\begin{aligned}d\mathbf{x}(t) &= A\mathbf{x}(t)dt + B(u(t)dt + \sigma d\mathbf{w}(t)) \\ &= (A\mathbf{x}(t) + Bu(t))dt + B\sigma d\mathbf{w}(t)\end{aligned}$$

with  $\sigma$  being 10% of the mean value (steady state value) of  $u(t)$ . Consider the above model applied for the 4-tank system (see Exercise 1).

- Discretize this system (for the 4-tank system example)
- Simulate the discrete time stochastic system. Make time series plot and histograms of the outputs.

## Questions and Comments

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