

# **ECE 329 REVIEW FOR EXAM 2**

**NANCY ZHAO & YUAN CHENG**

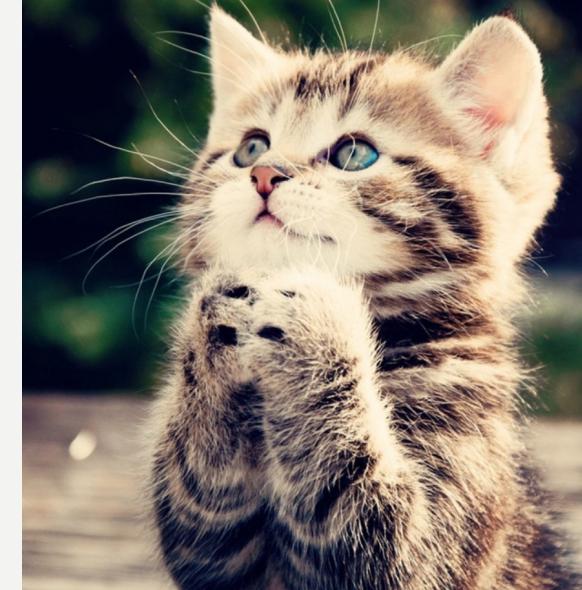
# EXAM 2 INFO

- ECEB 2013 (for Section C)
  - ECEB 2015 (for Section X)
  - ECEB 2017 (for Section E)
  - Wednesday 7- 8: 15 PM
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- Wednesday 5: 30 – 6:45 PM (for Conflict)
  - ONE 3 X 5 inch card of notes allowed

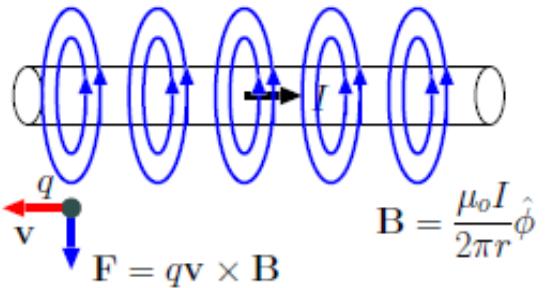


# CONCEPT LIST

- Ampere's law (lecture 12 & 13)
- Faraday's law (lecture 14)
- Inductance (lecture 15)
- Charge conservation (lecture 16 & 17)
- TEM wave solutions (lecture 18 & 19)



# AMPERE'S LAW



$$B = \frac{\mu_0 I}{2\pi r} \hat{\phi}$$

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_0 I_C$$

$$\mathbf{H} \equiv \mu_0^{-1} \mathbf{B}$$

$$I_C = \int_S \mathbf{J} \cdot d\mathbf{S}$$

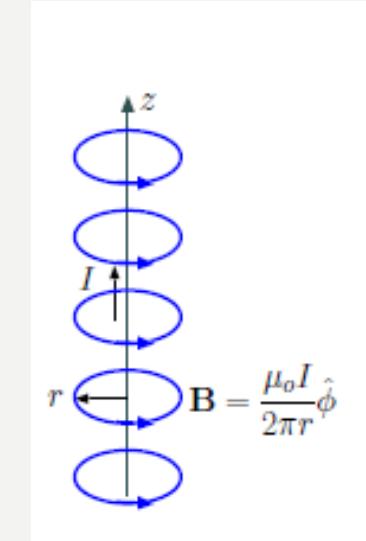
- $I_C$  stands for the net sum of all filament currents  $I_n$  crossing any surface  $S$  bounded by path  $C$
- The direction of flow is given by the “right-hand-rule”

$$\begin{aligned}\nabla \times \mathbf{H} &= \mathbf{J} \\ \nabla \cdot \mathbf{B} &= 0\end{aligned}$$

$$\oint_C \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot d\mathbf{S}$$

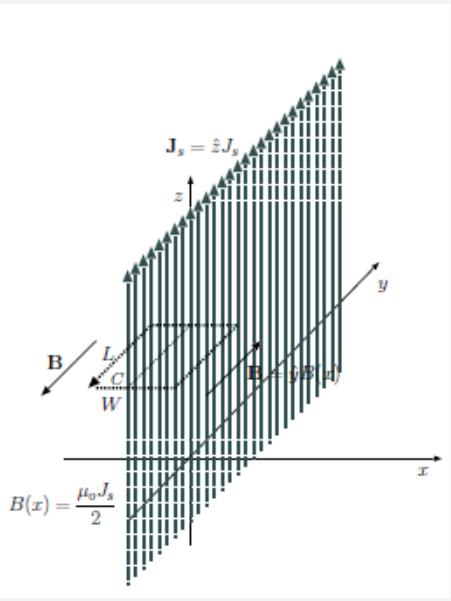
$$\mathbf{J}(x, y, z) = \mathbf{J}_s(y, z) \delta(x - x_o)$$

$$\mathbf{J}(x, y, z) = \hat{z} I(z) \delta(x - x_o) \delta(y - y_o)$$



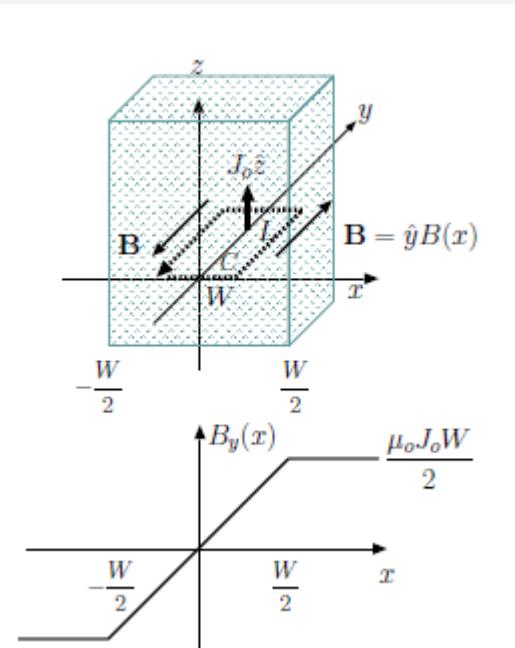
- This is the volumetric current density representation of a surface current density  $\mathbf{J}_s(x, y)$  measured in A/m units flowing on  $x = x_o$  surface.
- This is the line current  $I(z)$  measured in A units flowing in  $z$ -direction along a filament defined by the intersections of  $x = x_o$  and  $y = y_o$  surfaces.

# DRAW THE LOOP



$$B(x)L + 0 - B(-x)L + 0 = \mu_0 J_s L$$

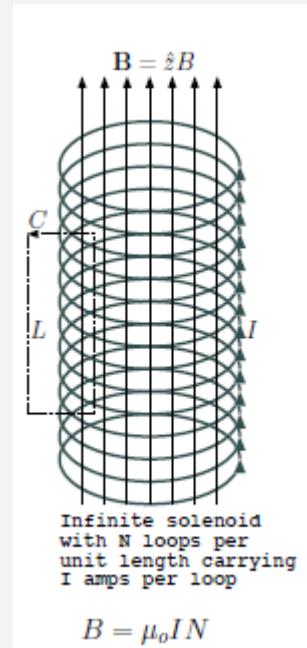
$$\mathbf{B} = \hat{y} \frac{\mu_0 J_s}{2} \text{sgn}(x) \text{ and } \mathbf{H} = \hat{y} \frac{J_s}{2} \text{sgn}(x)$$



$$B(x)L + 0 - B(-x)L + 0 = \mu_0 J_o 2xL \Rightarrow B(x) = \mu_0 J_o x$$

$$B(x)L + 0 - B(-x)L + 0 = \mu_0 J_o WL \Rightarrow B(x) = \mu_0 J_o \frac{W}{2}$$

$$\mathbf{H} = \begin{cases} \hat{y} J_o x, & |x| < \frac{W}{2} \\ \hat{y} J_o \frac{W}{2} \text{sgn}(x), & \text{otherwise} \end{cases}$$



$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_0 I_C \Rightarrow LB = \mu_0 INL$$

$$B = \mu_0 I N \text{ and } \mathbf{H} = \hat{z} I N$$

$\mathbf{B} = 0$  for the exterior region

# FARADAY'S LAW

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = - \int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}$$

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\frac{d}{dt} \int_S \mathbf{B} \cdot d\mathbf{S}$$

$$\Psi \equiv \int_S \mathbf{B} \cdot d\mathbf{S}$$

$$\mathcal{E} = -\frac{d\Psi}{dt}, \quad \text{Faraday's law}$$

$$\mathcal{E} = \oint_C \mathbf{E} \cdot d\mathbf{l}$$

$$I = \frac{\mathcal{E}}{R}$$

$$\mathcal{E} = \oint_C (\mathbf{E} + \mathbf{v} \times \mathbf{B}) \cdot d\mathbf{l}$$

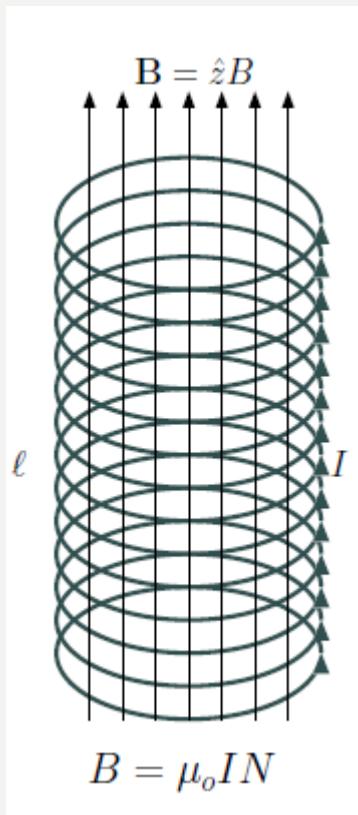
- The right hand side of the integral form equation above includes the flux of rate of change of magnetic field  $\mathbf{B}$  over surface  $S$ .
- $\Psi$  is the rate of change of magnetic flux.
- Induced emf (short for electro-motive force) represents the work done per unit charge moved once around path  $C$ .
- According to Faraday's law it appears that a non-zero emf can always be caused by magnetic flux variations  $d\Psi/dt$  independent of how the variations are produced — the possibilities are:
  1. Fixed  $C$ , but time-varying  $\mathbf{B}$ ,
  2.  $\mathbf{B} = \text{const.}$  (in space and time), but time-varying  $C$  (rotating or changing size),
  3. An inhomogeneous static  $\mathbf{B} = \mathbf{B}(r)$  in the measurement frame and  $C$  in motion.

# INDUCTANCE

$$L \equiv \frac{n\Psi}{I}$$

$$\mathcal{E} = -L \frac{dI}{dt}$$

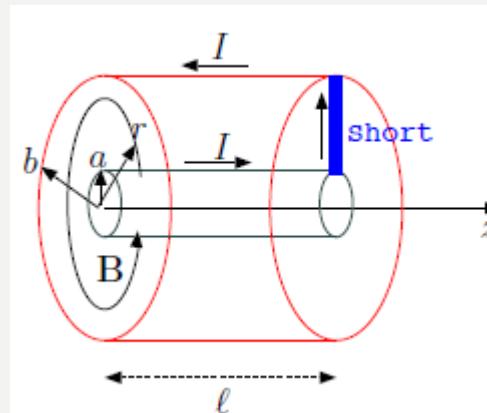
- This is the self-inductance and emf for an inductor consisting of n-loops.



- Inductance of long solenoid:**
- Consider a long solenoid with length  $\ell$ , cross-sectional area  $A$ , density of  $N$  loops per unit length and  $n = N\ell$  is the number of turns of the solenoid.

$$\mathbf{B} = \mu_0 I N \hat{z}$$

$$L = \frac{n\Psi}{I} = \frac{N\ell(\mu_0 I N)A}{I} = N^2 \mu_0 A \ell$$



- Inductance of shorted coax:**
- Consider a coaxial cable of some length  $\ell$  which is “shorted” at one end (with a wire connecting the inner and outer conductors)

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_0 I_C$$

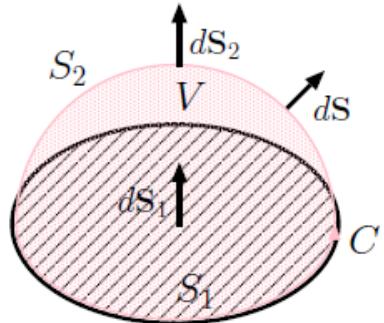
$$B_\phi 2\pi r = \mu_0 I$$

$$B_\phi = \frac{\mu_0 I}{2\pi r}$$

$$\Psi = \int_S \mathbf{B} \cdot d\mathbf{S} = \ell \frac{\mu_0}{2\pi} I \int_a^b \frac{dr}{r} = \ell \frac{\mu_0}{2\pi} \ln \frac{b}{a} I$$

$$L \equiv \frac{\ln \frac{b}{a}}{2\pi} \ell \mu_0$$

# CHARGE CONSERVATION



$$\int_V \frac{\partial \rho}{\partial t} dV = - \oint_S \mathbf{J} \cdot d\mathbf{S}$$

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot \mathbf{J}$$

- Continuity equation is a mathematical re-statement of the principle of conservation of charge.

$$\nabla \cdot \mathbf{D} = \rho \quad \text{Gauss's law}$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \quad \text{Faraday's law}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}, \quad \text{Ampere's law}$$

$$\hat{n} \cdot (\mathbf{D}^+ - \mathbf{D}^-) = \rho_s$$

$$\hat{n} \cdot (\mathbf{B}^+ - \mathbf{B}^-) = 0$$

$$\hat{n} \times (\mathbf{E}^+ - \mathbf{E}^-) = 0$$

$$\hat{n} \times (\mathbf{H}^+ - \mathbf{H}^-) = \mathbf{J}_s$$

$$\begin{aligned} \mathbf{D} &= \epsilon \mathbf{E} \\ \mathbf{B} &= \mu \mathbf{H} \end{aligned}$$

- The modified Ampere's law postulated by Maxwell under the assumption that Gauss's law is also valid under time-varying conditions, leads to some specific predictions about how time-varying fields should behave.

- $\mathbf{M}$  is referred to as magnetization field;  $\chi_m$  is a dimensionless parameter called magnetic susceptibility.

$$\mathbf{H} = \mu_o^{-1} \mathbf{B} - \mathbf{M}$$

$$\mathbf{B} = \mu_o(1 + \chi_m)\mathbf{H} = \mu\mathbf{H}$$

# TEM WAVE SOLUTIONS

$$-\nabla^2 \mathbf{E} = -\mu \frac{\partial}{\partial t} \nabla \times \mathbf{H}$$

$$\nabla^2 \mathbf{E} = \mu \epsilon \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

$$\frac{\partial^2 \mathbf{E}}{\partial x^2} + \frac{\partial^2 \mathbf{E}}{\partial y^2} + \frac{\partial^2 \mathbf{E}}{\partial z^2} = \mu \epsilon \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

$$\mathbf{E}(\mathbf{r}, t) = \hat{x} E_x(z, t)$$

$$\frac{\partial^2 E_x}{\partial z^2} = \mu \epsilon \frac{\partial^2 E_x}{\partial t^2}$$

$$E_x = \cos(\omega(t \mp \frac{z}{v}))$$

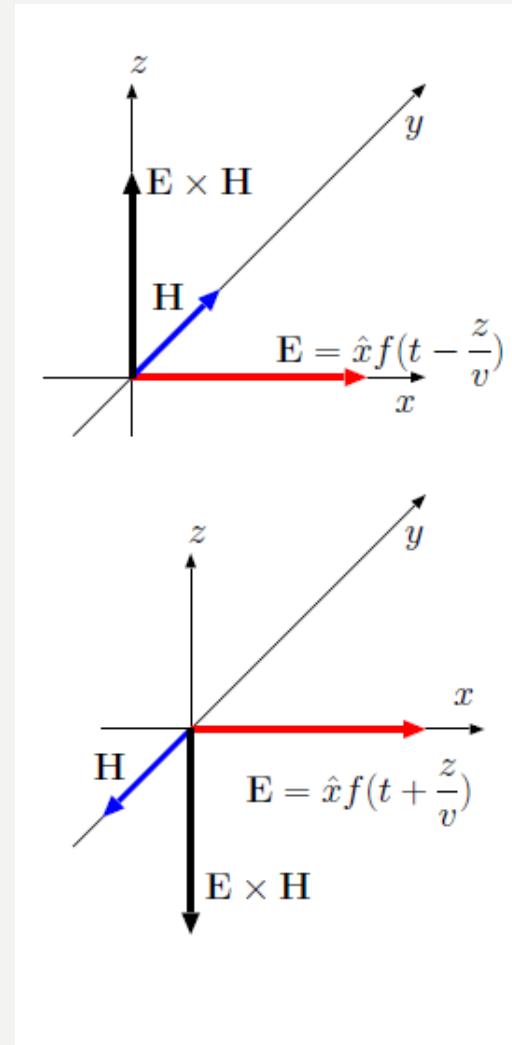
$$v \equiv \frac{1}{\sqrt{\mu \epsilon}}$$

$$\mathbf{H} = \pm \hat{y} \sqrt{\frac{\epsilon}{\mu}} \cos(\omega(t \mp \frac{z}{v}))$$

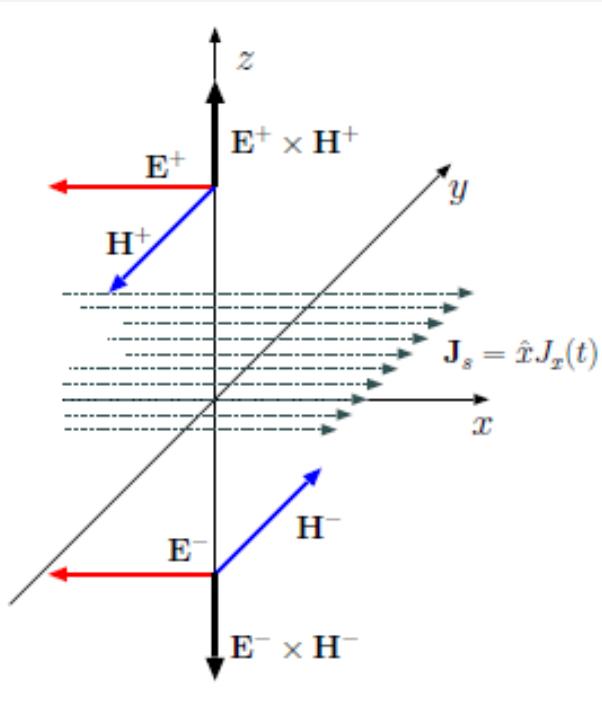
$$\eta \equiv \sqrt{\frac{\mu}{\epsilon}}$$

- The curl of Faraday's law combines with the Ampere's law to produce the 3D vector wave equation.

- 1D scalar wave equation is a field solution that only depends on z and t and “polarized” in x-direction.



# TEM WAVE SOLUTIONS



$$\mathbf{J}_s = \hat{x}f(t) \text{ on } z = 0 \text{ plane}$$

1.  $E_x$  and  $H_y$  waveforms are proportional to delayed versions of surface current  $J_x(t)$  at each location  $z$  above and below the current sheet, with the reference directions of  $E$  and  $J_s$  opposing one another.
2. Fields  $E^\pm$  are continuous on  $z = 0$  surface in compliance with tangential boundary condition equations.
3. Fields  $H^\pm$  exhibit a discontinuity on  $z = 0$  surface that matches the current density of the same surface, once again in compliance with tangential boundary condition equations.
4. Opposing  $E$  and  $J_s$  vectors on  $z = 0$  plane indicate that the surface is acting as a source of radiated energy

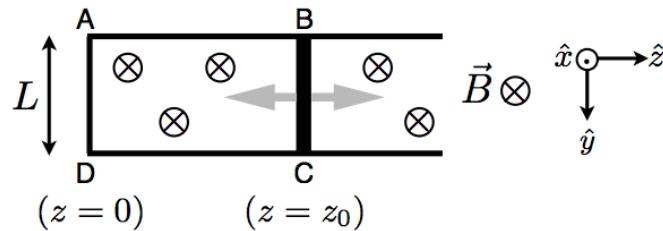
$$\mathbf{E}^\pm = -\hat{x} \frac{\eta f(t \mp \frac{z}{v})}{2} \text{ and } \mathbf{H}^\pm = \mp \hat{y} \frac{f(t \mp \frac{z}{v})}{2} \text{ in regions } z \gtrless 0$$

# PRACTICE PROBLEMS

3. Consider a hollowed out cylinder centered on the z-axis with inner radius  $a$  and outer radius  $b$  such that it is described by  $a < r < b$ . The hollow cylinder conducts a uniform current density of  $\mathbf{J} = J_0 \hat{z}$  A/m<sup>2</sup> in the region  $a < r < b$ . Outside this region, that is for  $r > b$  and  $r < a$ , the charge and current densities are zero.
- Using the integral form of Ampere's law find  $\mathbf{B}$  everywhere. (You can simplify your answer using  $I = J_0 \cdot A$ )
  - For  $r > b$  what does the magnetic field  $\mathbf{B}$  produced by a hollow cylinder look like? (Hint: See Lecture 12 online, this is the magnetic analog to a hollow sphere of charge).

# PRACTICE PROBLEMS

4. As shown in the diagram below, a pair of conducting rails separated by a distance  $L$  is connected at  $z = 0$  to a fixed conducting rod (AD) and at  $z = z_0$  to a conducting armature (BC) that can slide along the rail in the  $\pm\hat{z}$  direction. A constant magnetic field  $\mathbf{B} = -B_0 \hat{x}$  exists in the region, which is shown pointing down into the page in the diagram. The armature is mechanically pulled in the  $+\hat{z}$  direction at a constant velocity  $\mathbf{v} = v_0 \hat{z}$  m/s from its starting position at  $z = z_0$ , and the changing magnetic flux through the loop ABCD induces an electromotive force  $\mathcal{E}$  and thus a current  $I_0$  around the conducting loop.



- What is the emf  $\mathcal{E}$  induced in the loop ABCD?
- What is the magnitude and direction of the induced current  $I_0$  in terms of the resistance  $R$  of the conducting loop ABCD?
- What is the magnitude and direction of the Lorentz force  $\mathbf{F} = q(\mathbf{v} \times \mathbf{B})$  that is exerted on the armature by the magnetic field  $\mathbf{B}$ ? **Hint:** express your answer in terms of the induced current  $I_0$ .
- Now consider that the armature is no longer moved mechanically (though it is still free to move in response to Lorentz forces) and that a projectile of mass  $M$  is attached to it. A constant current of magnitude  $I'$  is introduced into the loop at point A such that it flows along the contour ABCD. The magnetic field generated by this current loop is negligibly small compared to the background magnetic field  $\mathbf{B}$ , and the mass of the armature is negligibly small compared to  $M$ . What is the magnitude and direction of the acceleration  $\mathbf{a}$  of the projectile? **Hint:**  $\mathbf{F} = M\mathbf{a}$ .

# PRACTICE PROBLEMS

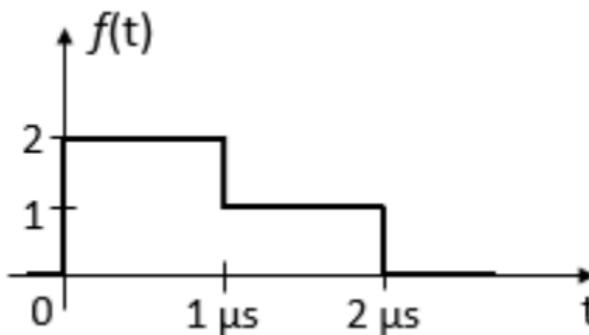
3.

- a) For current density  $\mathbf{J} = (5z^2 \hat{x} + 4x^3y \hat{y} + 3z(y - y_o)^2 \hat{z}) \text{ A/m}^2$ , which is time independent, find the charge density  $\rho(0, t)$  at the origin  $(0,0,0)$  as a function of time  $t$ , if  $\rho = 0$  at that location and time  $t = 0$ ,  $y_o = 2 \text{ m}$ , and coordinates  $x$ ,  $y$ , and  $z$  are specified in meter units. **Hint:** use the continuity equation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \mathbf{J} = 0.$$

# PRACTICE PROBLEMS

3. (25 points) Consider a time varying sheet current  $\mathbf{J}_s$  in  $yz$ - plane at  $x = 0$ . In  $x > 0$  region, the magnetic field of the plane wave caused by the sheet current is  $\mathbf{H}(x, t) = f(t - \frac{x}{c})\hat{y} \text{ A/m}$ . Assume all region is free space. The plot for  $f(t)$  is shown below.



- a) (8 points) Plot  $H_y(t = 4\mu\text{s}, x)$  vs.  $x$  for  $x \in [-1500 \text{ m}, +1500 \text{ m}]$ . Be sure to clearly label all axis.

# PRACTICE PROBLEMS

- b) (8 points) Plot  $H_y(t, x = 1200 \text{ m})$  vs.  $t$  for  $t \in [0, 10\mu\text{s}]$ . Be sure to clearly label all axis.
- c) (9 points) Plot  $\mathbf{E}(t = 4\mu\text{s}, x)$  vs.  $x$  for  $x \in [-1500 \text{ m}, +1500 \text{ m}]$ . You only need to plot the non-zero components of  $\mathbf{E}$ . Be sure to indicate the component and clearly label all axis.

Thanks  
a  
Bunch!

