Robotics 1

Trajectory planning

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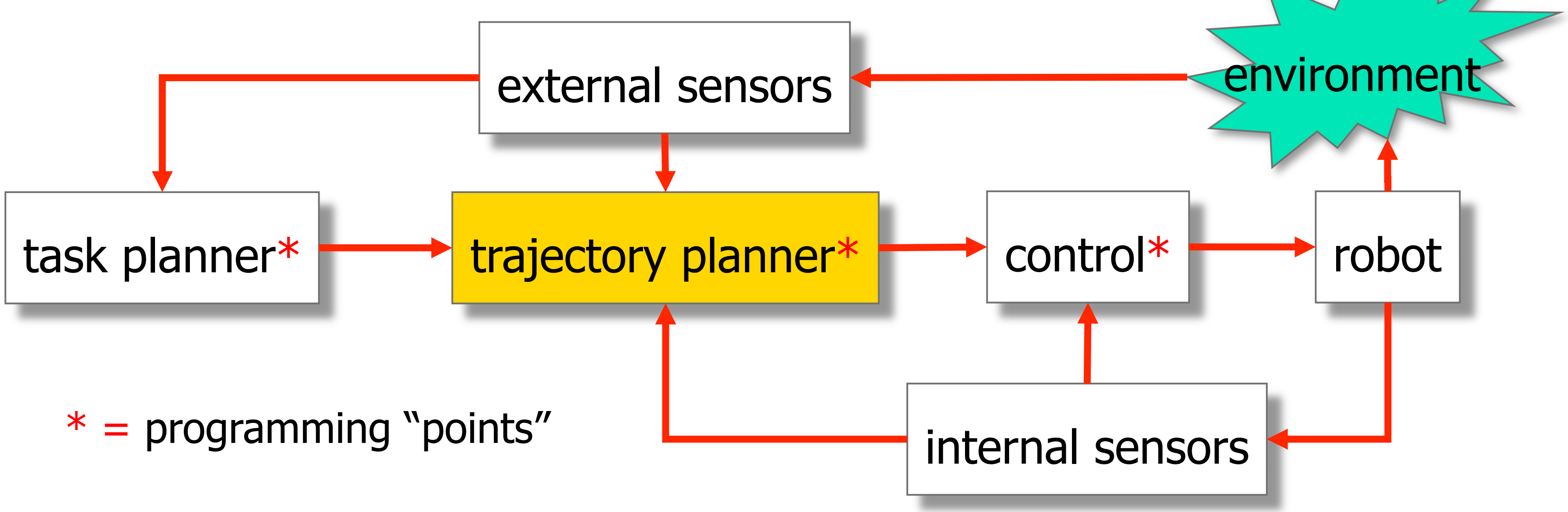
Trajectory planner interfaces

functional robot units



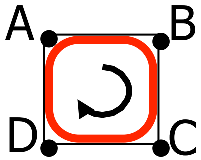
robot action described as a sequence of poses or configurations (with possible exchange of contact forces) → **TRAJECTORY PLANNER** → reference profile/values (continuous or discrete) for the robot controller

Trajectory definition
a standard procedure for industrial robots

1. define Cartesian pose points (position+orientation) using the teach-box
2. program an (average) velocity between these points, as a 0-100% of a maximum system value (different for Cartesian- and joint-space motion)
3. linear interpolation in the joint space between points sampled from the built trajectory

examples of additional features

a) over-fly



b) sensor-driven STOP

c) circular path through 3 points

main drawbacks

- semi-manual programming (as in "first generation" robot languages)
- limited visualization of motion

➡ a mathematical formalization of trajectories is useful/needed

From task to trajectory

TRAJECTORY $\begin{cases} \text{of motion } p_d(t) \\ \text{of interaction } F_d(t) \end{cases}$

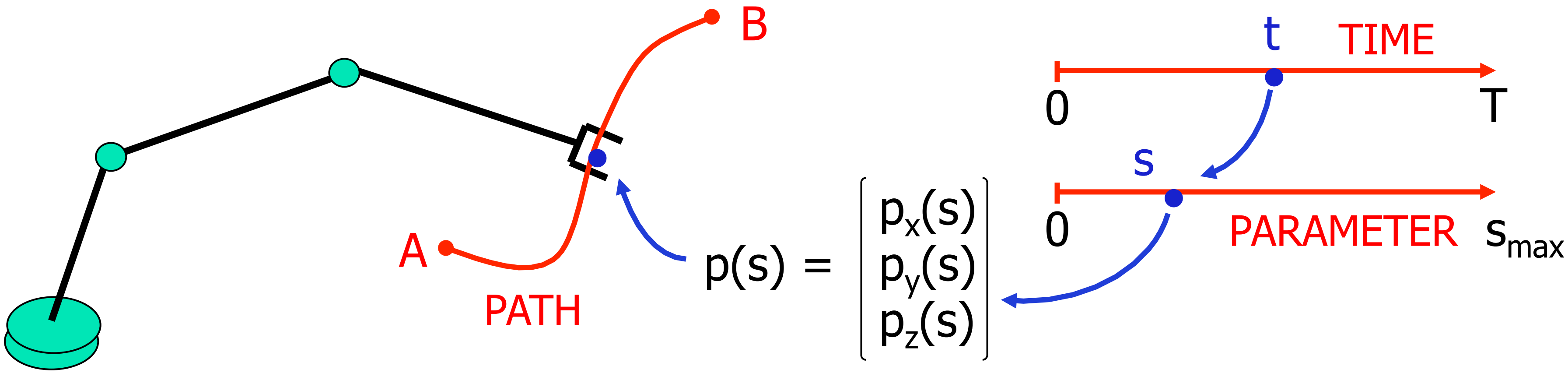
||

GEOMETRIC PATH — parameterized by s: $p=p(s)$ (e.g., s is the arc length)

+

TIMING LAW — describes the time evolution of $s=s(t)$

$\Rightarrow p(s(t))$



$$p(s) = \begin{bmatrix} p_x(s) \\ p_y(s) \\ p_z(s) \end{bmatrix}$$

example: TASK planner provides A, B
TRAJECTORY planner generates p(t)

Trajectory planning
operative sequence

TASK planning

1

- sequence of pose points ("knots") in Cartesian space
  - interpolation in Cartesian space
- Cartesian geometric path (position + orientation): $p = p(s)$
  - path sampling and kinematic inversion

2

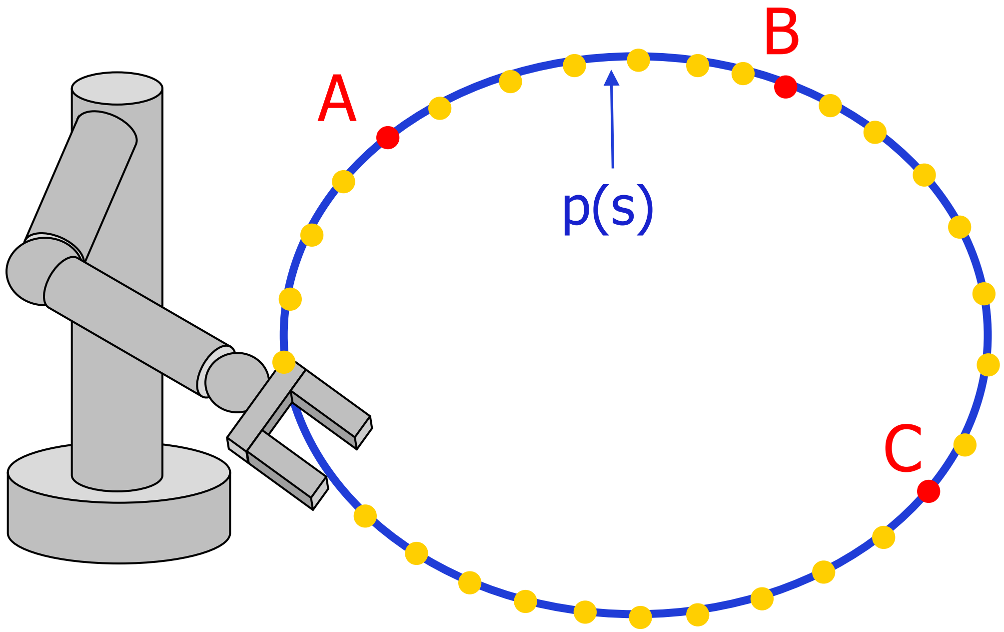
- sequence of "knots" in joint space
  - interpolation in joint space
- geometric path in joint space: $q = q(\lambda)$

analytic inversion

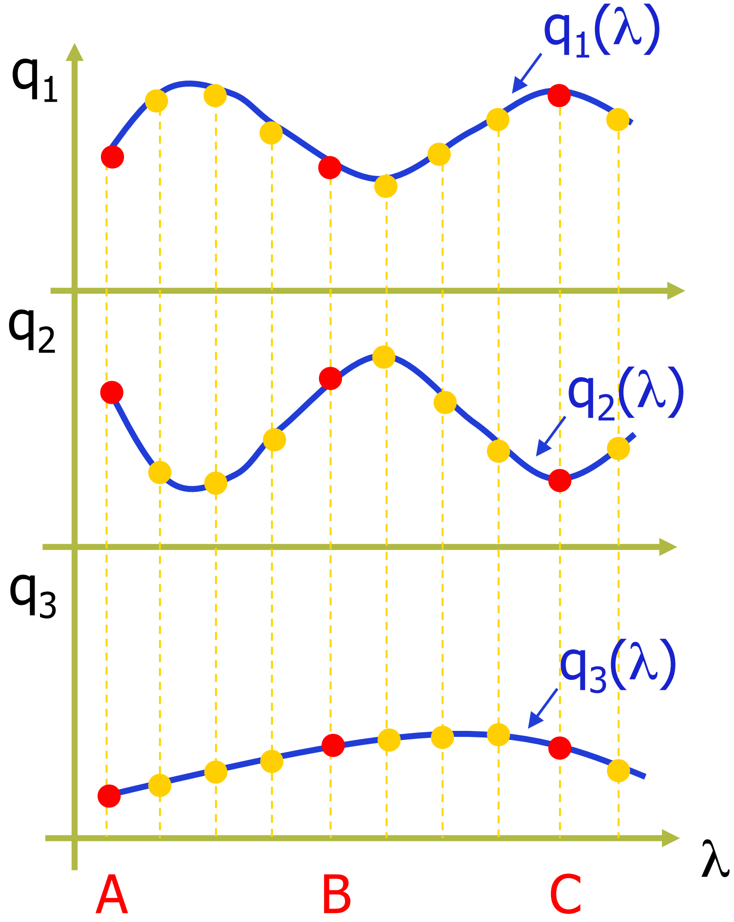
additional issues to be considered in the planning process

- obstacle avoidance
- on-line/off-line computational load
- sequence 2 is more "dense" than 1

Example



Cartesian space



joint space

Cartesian vs. joint trajectory planning

- planning in Cartesian space
  - allows a more direct visualization of the generated path
  - obstacle avoidance, lack of "wandering"
- planning in joint space
  - does not need on-line kinematic inversion
- issues in kinematic inversion
  - $\dot{q}$ e $\ddot{q}$ (or higher-order derivatives) may also be needed
    - Cartesian task specifications involve the geometric path, but also bounds on the associated timing law
  - for redundant robots, choice among ∞^{n-m} inverse solutions, based on optimality criteria or additional auxiliary tasks
  - off-line planning in advance is not always feasible
    - e.g., when interaction with the environment occurs or sensor-based motion is needed

Path and timing law

- after choosing a path, the trajectory definition is completed by the choice of a timing law

$$p = p(s) \quad \Rightarrow s = s(t) \qquad \text{(Cartesian space)}$$

$$q = q(\lambda) \quad \Rightarrow \lambda = \lambda(t) \qquad \text{(joint space)}$$

  - if $s(t) = t$, path parameterization is the natural one given by time
- the timing law
  - is chosen based on task specifications (stop in a point, move at constant velocity, and so on)
  - may consider optimality criteria (min transfer time, min energy,…)
  - constraints are imposed by actuator capabilities (max torque, max velocity,…) and/or by the task (e.g., max acceleration on payload)

note: on parameterized paths, a space-time decomposition takes place

e.g., in Cartesian space

$$\dot{p}(t) = \frac{dp}{ds}\dot{s} \qquad \ddot{p}(t) = \frac{dp}{ds}\ddot{s} + \frac{d^2p}{ds^2}\dot{s}^2$$

Trajectory classification

- space of definition
  - Cartesian, joint
- task type
  - point-to-point (PTP), multiple points (knots), continuous, concatenated
- path geometry
  - rectilinear, polynomial, exponential, cycloid, …
- timing law
  - bang-bang in acceleration, trapezoidal in velocity, polynomial, …
- coordinated or independent
  - motion of all joints (or of all Cartesian components) start and ends at the same instants (say, t=0 and t=T) = single timing law

  or
  - motions are timed independently (according to the requested displacement and robot capabilities) – mostly only in joint space

Relevant characteristics

- computational efficiency and memory space
  - e.g., store only the coefficients of a polynomial function
- predictability (vs. “wandering” out of the knots) and accuracy (vs. “overshoot” on final position)
- flexibility (allowing concatenation, over-fly, …)
- continuity
  (at least $\mathbf{C}^1$, but also up to jerk = $\frac{da}{dt}$)

Trajectory planning in joint space

- $q = q(t)$ or $q = q(\lambda)$, $\lambda = \lambda(t)$
- it is sufficient to work component-wise (q_i in vector q)
- an implicit definition of the trajectory, by solving a problem with specified boundary conditions in a given class of functions
- typical classes: polynomials (cubic, quintic,…), (co)sinusoids, clothoids, …
- imposed conditions
  - passage through points (interpolation)
  - initial, final, intermediate velocity
  - initial, final acceleration
  - continuity up to the k-th order time derivative ($\mathbf{C}^k$)

many of the following methods and remarks can be directly applied also to Cartesian trajectory planning (and vice versa)!

Cubic polynomial

$\boxed{q(0) = q_{in}}$ $\boxed{q(T) = q_{fin}}$ $\boxed{\dot{q}(0) = v_{in}}$ $\boxed{\dot{q}(T) = v_{fin}}$ ← 4 conditions

$$q(\tau) = q_{in} + \Delta q\,\underbrace{[a\tau^3 + b\tau^2 + c\tau + d]}$$

$\Delta q = q_{fin} - q_{in}$

$\tau = t/T,\ \tau \in [0, 1]$

4 coefficients → "doubly normalized" polynomial $q_N(\tau)$

$q_N(0) = 0 \Leftrightarrow d = 0$ $\qquad$ $q_N(1) = 1 \Leftrightarrow a + b + c = 1$

$q_N'(0) = dq_N/d\tau|_{\tau=0} = c = v_{in}T/\Delta q$ $\qquad$ $q_N'(1) = dq_N/d\tau|_{\tau=1} = 3a + 2b + c$
$= v_{fin}T/\Delta q$

special case: $v_{in} = v_{fin} = 0$ (rest-to-rest)

$q_N'(0) = 0 \Leftrightarrow c = 0$

$$\left.\begin{array}{l} q_N(1) = 1 \Leftrightarrow a + b = 1 \\ q_N'(1) = 0 \Leftrightarrow 3a + 2b = 0 \end{array}\right\} \Leftrightarrow \begin{array}{l} a = -2 \\ b = 3 \end{array}$$

Quintic polynomial

$$q(\tau) = a\tau^5 + b\tau^4 + c\tau^3 + d\tau^2 + e\tau + f$$

6 coefficients

$\tau = t/T,\ \tau \in [0, 1]$

allows to satisfy 6 conditions, for example (in normalized time τ)

$\boxed{q(0) = q_0}$ $\boxed{q(1) = q_1}$ $\boxed{q'(0) = v_0 T}$ $\boxed{q'(1) = v_1 T}$ $\boxed{q''(0) = a_0 T^2}$ $\boxed{q''(1) = a_1 T^2}$

$$\begin{aligned} q(\tau) = {} & (1 - \tau)^3[q_0 + (3q_0+v_0T)\tau + (a_0T^2+6v_0T+12q_0)\tau^2/2] \\ & + \tau^3\,[q_1 + (3q_1 - v_1T)(1-\tau) + (a_1T^2 - 6v_1T+12q_1)\,(1 - \tau)^2/2] \end{aligned}$$

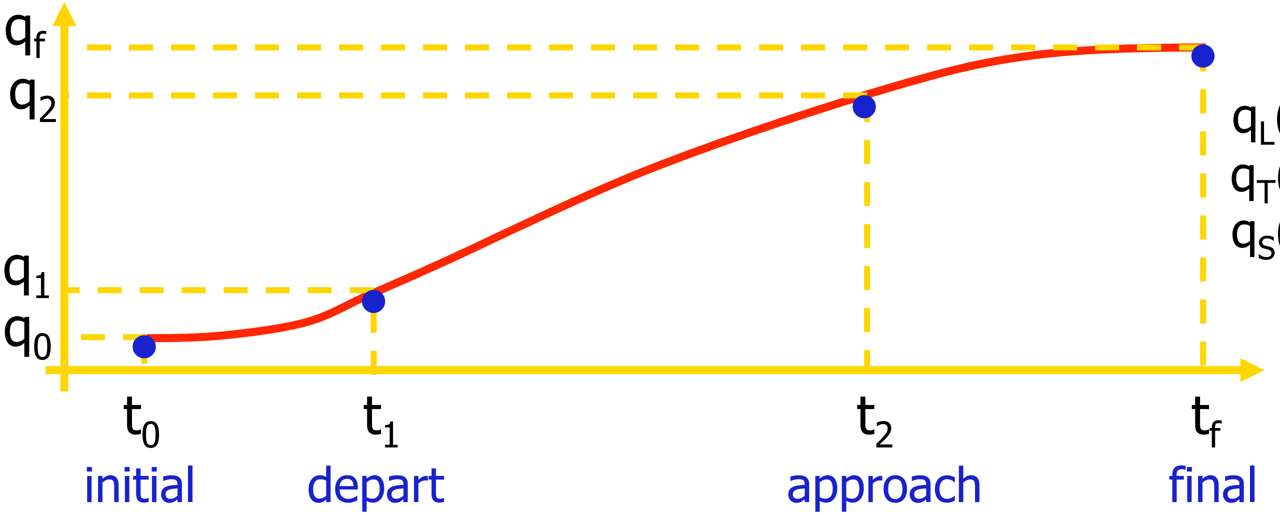
special case: $v_0 = v_1 = a_0 = a_1 = 0$

$$q(\tau) = q_0 + \Delta q\,[6\tau^5 - 15\tau^4 + 10\tau^3]$$

$\Delta q = q_1 - q_0$

4-3-4 polynomials

three phases (Lift off, Travel, Set down) in pick-and-place operations



$q_L(t)$ = 4th order polynomial
$q_T(t)$ = 3rd order polynomial
$q_S(t)$ = 4th order polynomial

14 coefficients

boundary conditions

$$q(t_0) = q_0 \quad q(t_1^-) = q(t_1^+) = q_1 \quad q(t_2^-) = q(t_2^+) = q_2 \quad q(t_f) = q_f$$

6 passages

$$\dot{q}(t_0) = \dot{q}(t_f) = 0 \qquad \ddot{q}(t_0) = \ddot{q}(t_f) = 0$$

4 initial/final velocity/acceleration

$$\dot{q}(t_i^-) = \dot{q}(t_i^+) \qquad \ddot{q}(t_i^-) = \ddot{q}(t_i^+) \quad i = 1,2$$

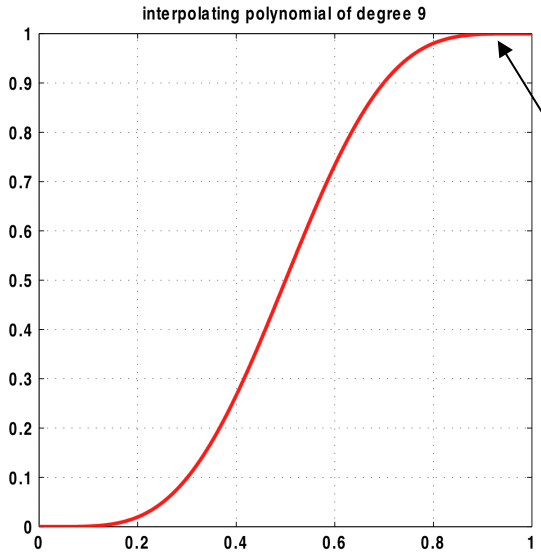
4 continuity

Higher-order polynomials

- a suitable solution class for satisfying symmetric boundary conditions (in a PTP motion) that impose zero values on higher-order derivatives
  - the interpolating polynomial is always of odd degree
  - the coefficients of such (doubly normalized) polynomial are always integers, alternate in sign, sum up to unity, and are zero for all terms up to the power = (degree-1)/2
- in all other cases (e.g., for interpolating a large number N of points), their use is not recommended
  - N-th order polynomials have N-1 maximum and minimum points
  - oscillations arise out of the interpolation points (wandering)

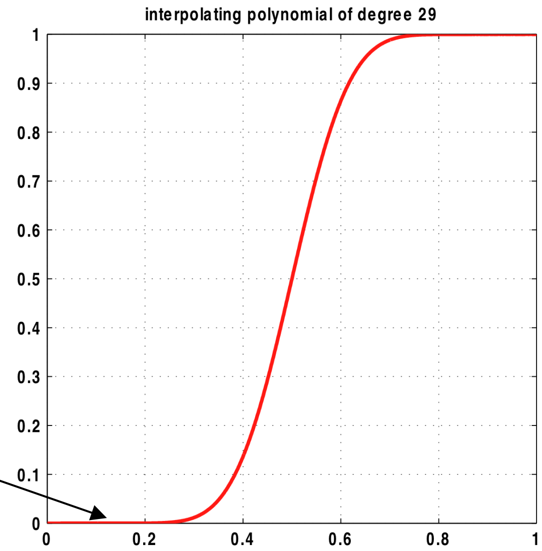
Numerical examples

9th degree



4 derivatives are zero

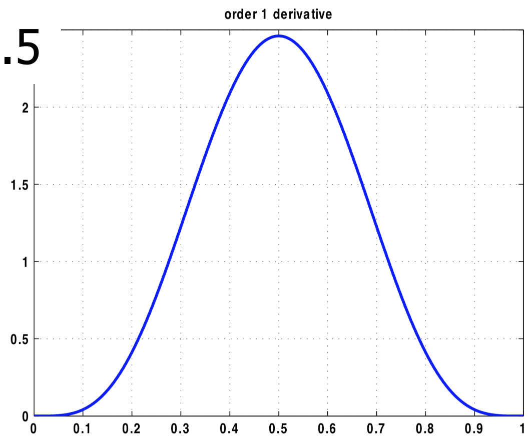
14 derivatives are zero!



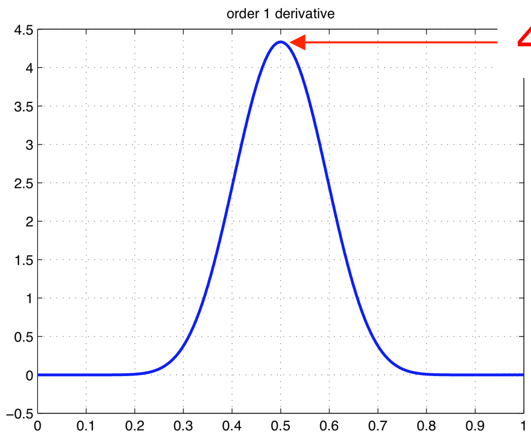
29th degree

no overshoot nor wandering

2.5



normalized velocity



4.5!!

velocity peaking at midpoint

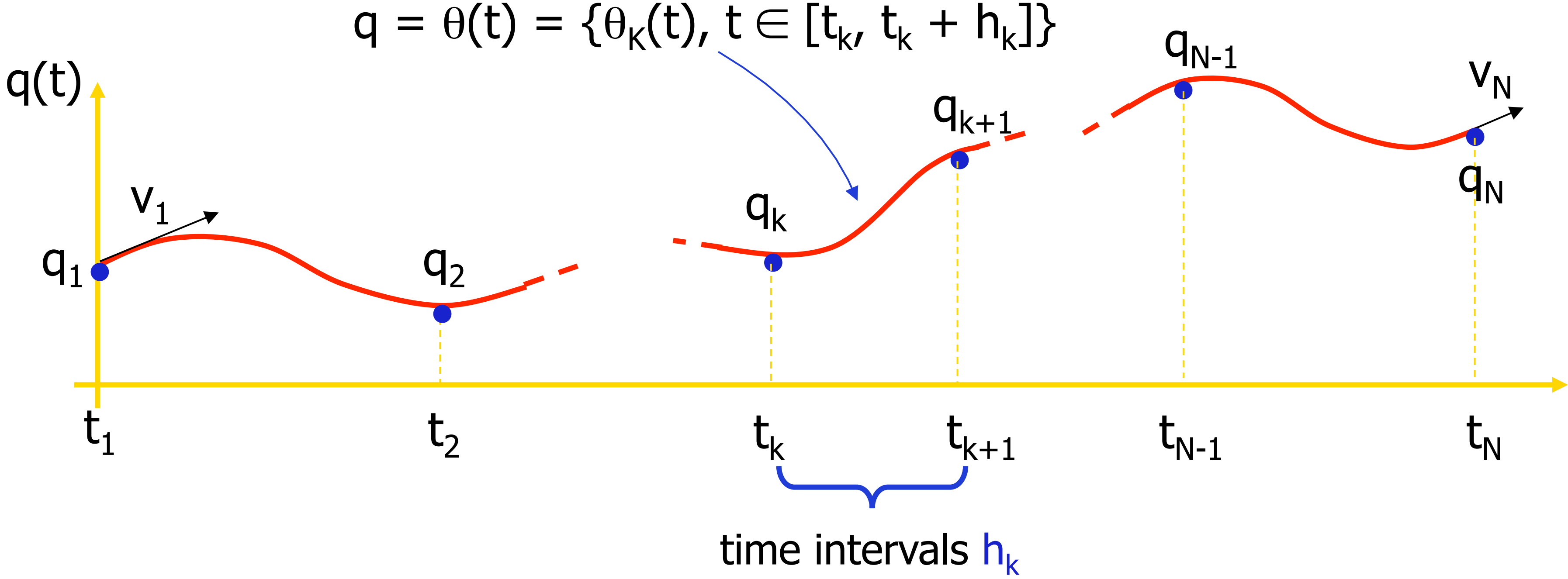
Interpolation using splines

- problem

  interpolate N knots, with continuity up to the second derivative
- solution

  spline: N-1 cubic polynomials, concatenated so as to pass through N knots and being continuous in velocity and acceleration in the N-2 internal knots
- 4(N-1) coefficients
- 4(N-1)-2 conditions, or
  - 2(N-1) of passage (for each cubic, in the two knots at its ends)
  - N-2 of continuity for velocity (at the internal knots)
  - N-2 of continuity for acceleration (at the internal knots)
- 2 free parameters are still left over
  - can be used, e.g., to assign initial and final velocities, v_1 and v_N
- presented next in terms of time t, but similar in terms of space λ

Building a spline



$$\boxed{\theta_K(\tau) = a_{k0} + a_{k1}\,\tau + a_{k2}\,\tau^2 + a_{k3}\,\tau^3}$$

$\tau \in [0, h_k]$, $\tau = t - t_k$ $(k = 1, \ldots, N-1)$

continuity conditions
for velocity and acceleration

$$\dot{\theta}_K(h_k) = \dot{\theta}_{K+1}(0) \qquad k = 1, \ldots, N-2$$
$$\ddot{\theta}_K(h_k) = \ddot{\theta}_{K+1}(0)$$

An efficient algorithm

1. if all velocities v_k at internal knots were known, then each cubic in the spline would be uniquely determined by

$$\theta_K(0) = q_K = a_{K0} \qquad \dot{\theta}_K(0) = v_K = a_{K1}$$

$$\begin{pmatrix} h_K^2 & h_K^3 \\ 2h_K & 3h_K^2 \end{pmatrix} \begin{pmatrix} a_{K2} \\ a_{K3} \end{pmatrix} = \begin{pmatrix} q_{K+1} - q_K - v_K h_K \\ v_{K+1} - v_K \end{pmatrix} \quad (1)$$

2. impose the continuity for accelerations (N-2 conditions)

$$\ddot{\theta}_K(h_k) = 2\, a_{K2} + 6\, a_{K3}\, h_K = \ddot{\theta}_{K+1}(0) = 2\, a_{K+1,2}$$

3. expressing the coefficients a_{k2}, a_{k3}, $a_{k+1,2}$ in terms of the still unknown knot velocities (see step 1.) yields a linear system of equations that is always (easily) solvable

$$\begin{pmatrix} & & \\ & A(h) & \\ & & \end{pmatrix} \begin{pmatrix} v_2 \\ v_3 \\ \vdots \\ v_{N-1} \end{pmatrix} = \begin{pmatrix} \\ b(h,q,v_1,v_N) \\ \\ \end{pmatrix}$$

tri-diagonal matrix always invertible

unknown

to be substituted then back in (1)

known vector

Structure of A(h)

$$
\begin{pmatrix}
2(h_1+h_2) & h_1 & & & \\
h_3 & 2(h_2+h_3) & h_2 & & \\
 & \ddots & \ddots & \ddots & \\
 & & h_{N-2} & 2(h_{N-3}+h_{N-2}) & h_{N-3} \\
 & & & h_{N-1} & 2(h_{N-2}+h_{N-1})
\end{pmatrix}
$$

diagonally dominant matrix (for $h_k > 0$)
[the same matrix for all joints]

Structure of $b(h,q,v_1,v_N)$

$$\begin{pmatrix} \frac{3}{h_1 h_2}\left[h_1^2(q_3 - q_2) + h_2^2(q_2 - q_1)\right] - h_2 v_1 \\ \frac{3}{h_2 h_3}\left[h_2^2(q_4 - q_3) + h_3^2(q_3 - q_2)\right] \\ \vdots \\ \frac{3}{h_{N-3} h_{N-2}}\left[h_{N-3}^2(q_{N-1} - q_{N-2}) + h_{N-2}^2(q_{N-2} - q_{N-3})\right] \\ \frac{3}{h_{N-2} h_{N-1}}\left[h_{N-2}^2(q_N - q_{N-1}) + h_{N-1}^2(q_{N-1} - q_{N-2})\right] - h_{N-2} v_N \end{pmatrix}$$

Properties of splines

- the spline is the solution with minimum curvature among all interpolating functions having continuous second derivative
- a spline is uniquely determined from the set of data $q_1,\ldots,q_N$, $h_1,\ldots,h_{N-1}$, v_1, v_N
- the total transfer time is $T = \Sigma h_k = t_N - t_1$
- the time intervals h_k can be chosen so as to minimize T (linear objective function) under (nonlinear) bounds on velocity and acceleration in [0,T]
- for cyclic tasks ($q_1=q_N$), it is preferable to simply impose continuity of velocity and acceleration at $t_1=t_N$ as the "squaring" conditions
  - in fact, even choosing $v_1=v_N$ doesn't guarantee acceleration continuity
  - in this way, the first=last knot will be handled as all other internal knots
- when initial and final accelerations are also assigned, the spline construction can be suitably modified

A modification

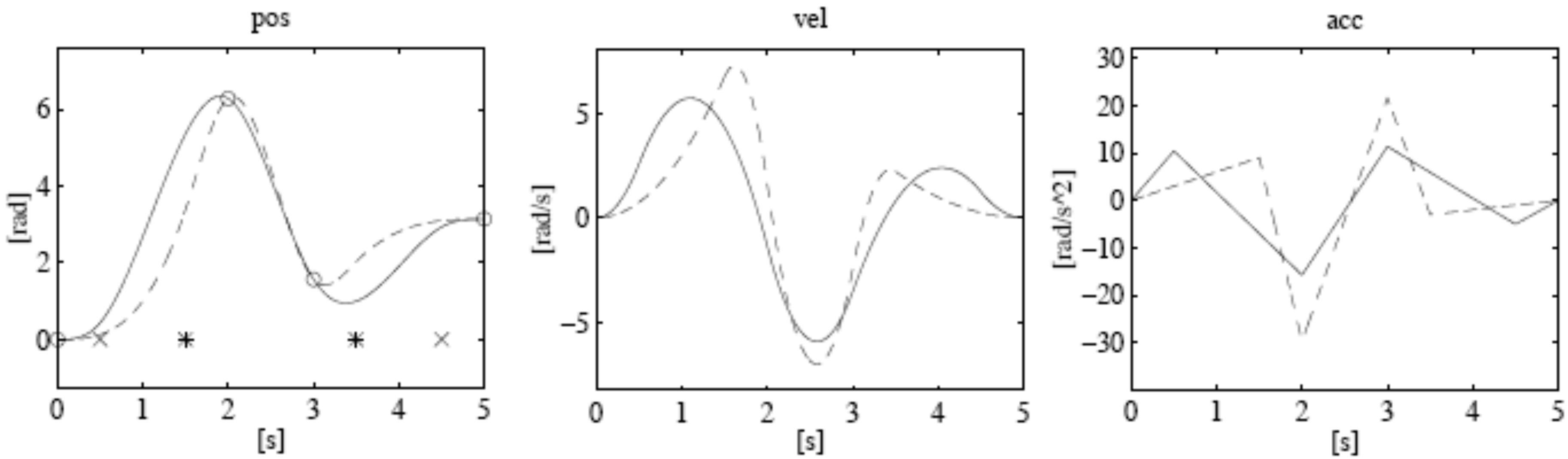
handling assigned initial and final accelerations

- two more parameters are needed in order to impose also the initial acceleration α_1 and final acceleration α_N
- two "fictitious knots" are inserted in the first and last original intervals, increasing the number of cubic polynomials from N-1 to N+1
- in these two knots only continuity conditions on position, velocity and acceleration are imposed

  $\Rightarrow$ two free parameters are left over (one in the first cubic and the other in the last cubic), which are used to satisfy the boundary conditions on acceleration
- depending on the (time) placement of the two additional knots, the resulting spline changes

A numerical example

- N=4 knots (3 cubic polynomials)
  - joint values $q_1 = 0$, $q_2 = 2\pi$, $q_3 = \pi/2$, $q_4 = \pi$
  - at $t_1 = 0$, $t_2 = 2$, $t_3 = 3$, $t_4 = 5$ (thus, $h_1 = 2$, $h_2 = 1$, $h_3 = 2$)
  - boundary velocities $v_1 = v_4 = 0$
- 2 added knots for imposing accelerations at ends (5 cubic polynomials)
  - boundary accelerations $\alpha_1 = \alpha_4 = 0$
  - two placements: at $t_1' = 0.5$ and $t_4' = 4.5$ ($\times$), or $t_1'' = 1.5$ and $t_4'' = 3.5$ ($*$)



——— = placement′   --------- = placement″