



SDIR

Standardized coordinate systems / layouts of robots

Slide 1 28.11.2013



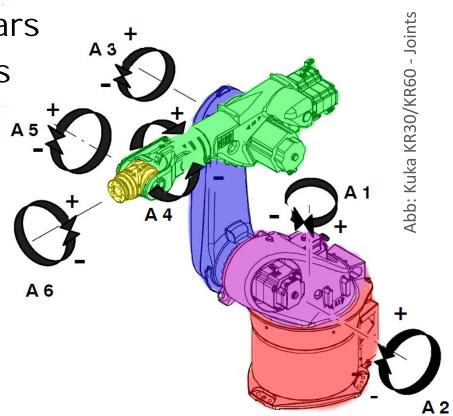


- AC Servomotors
- Repeatability of 0.07mm
- Cyclical absolute positioning system

Lifetime 10 – 15 years

Installation positions

- Base mounted
- Roof mounted
- Wall mounted





Intro KUKA KR 30-L16

Workspace

KR 30 L16 Zentralhand, Nenn-Traglast 16 kg

Achse	Bewegungsbereich softwarebegrenzt	Geschwindig- keit
1	±185°	100 °/s
2	+35° bis -135°	80 °/s
3	+158° bis -120°	80 °/s
4	±350°	230 °/s
5	±130°	165 °/s
6	±350°	249 °/s
0	1000	240 /5

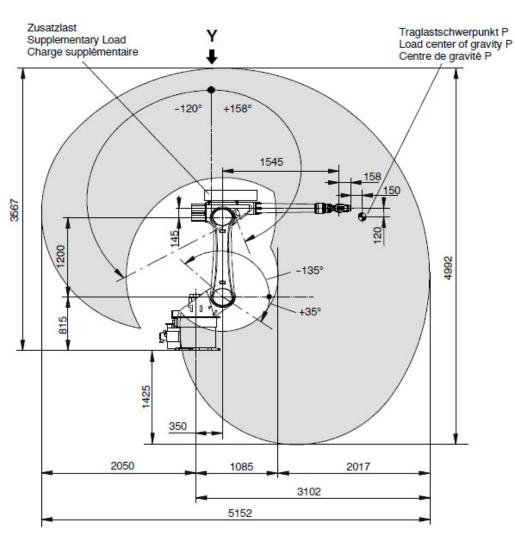


Abb: Kuka KR30 L16 - Workspace

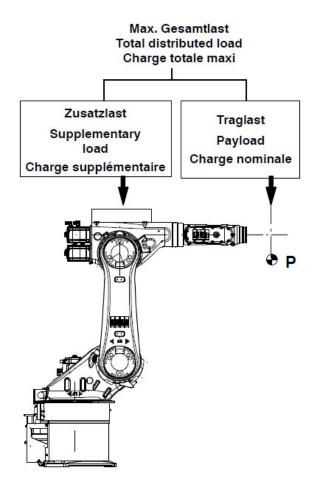


Intro KUKA KR 30-L16

Weight: 700kg

Payload: 16kg

Supplementary load: 35kg







 Given the angles of every single rotary joint (in a kinematic chain)

 one can compute position and orientation of the ToolCenterPoint (TCP)

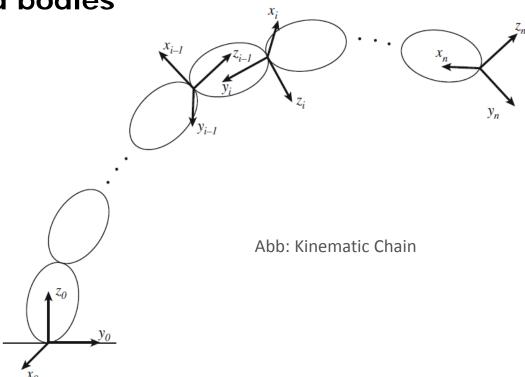
 by performing coordinate transformations for every joint consecutively (forward kinematics)





- robotic arm abstracted as series of:
 - single joints

rigid bodies





What we want to explain!

- how to calculate the position of a robot arm with given joint angles
- a mathematical convention for coordinate system transformation



Denavit Hartenberg Convention



Denavit-Hartenberg-Convention

- mathematical convention
- describes transformation of
 - a local coordinate system
 - within a kinematic chain
- with the help of 4 (system specific) parameters
 - d
 - a
 - a
 - **0**



Some lexical conventions



Denavit-Hartenberg-Convention

- each transformation performed from the *i-th* to *i+1-th* coordinate system
- corresponding parameters get index i
- Transformation Matrix is T_i^{i+1}

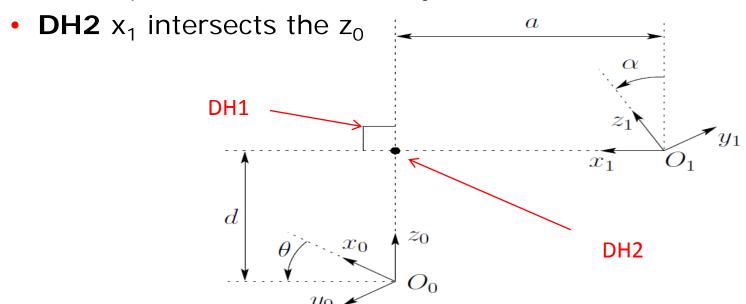


The Convention



Denavit-Hartenberg-Convention

- Convention is based on how to place the specific coordinate systems in each axis
- Two basic constraints:
 - DH1 x₁ is perpendicular to z₀

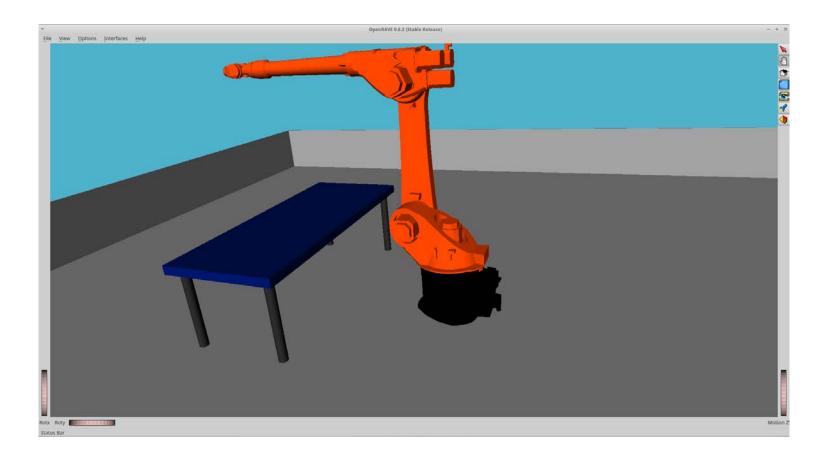




But how to fulfill these constraints?



 Visualisation example Kuka KR30 L16 from the openRave VM

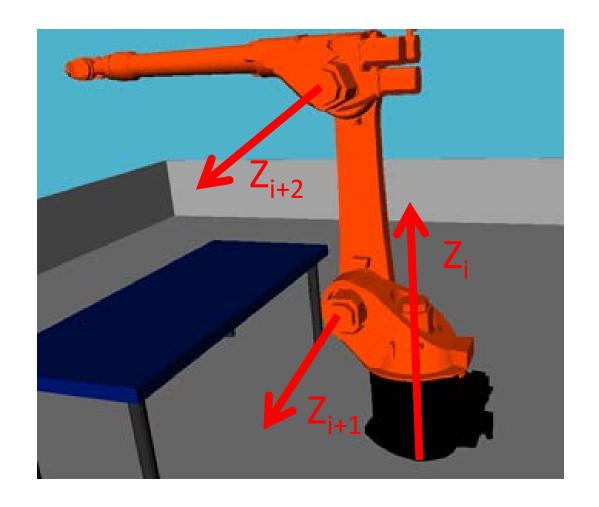




z-axis



z-axis always placed in the rotation axis





y-axis





 y-axis always creates a right handed coordinate system with z- and x-axis

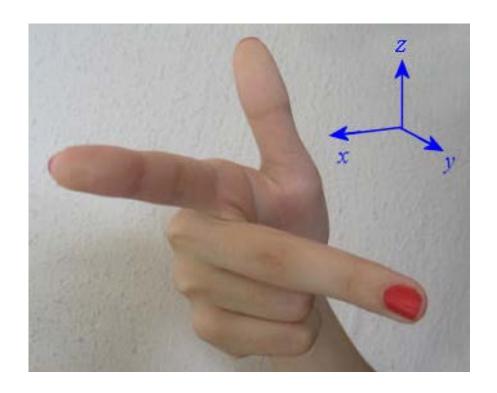


Abb: http://middletownhighschool.wikispaces.com



x-axis and the origin of the coordinate system



- 4 different constellations for z_i and z_{i+1}
- 1. base coordinate system
- 2. z_i and z_{i+1} are not coplanar
- 3. z_i and z_{i+1} parallel
- 4. z_i and z_{i+1} intersects



4 different constellations for z_i and z_{i+1}



1. base coordinate system

- 2. z_i and z_{i+1} are not coplanar
- 3. z_i and z_{i+1} parallel
- 4. z_i and z_{i+1} intersects



x-axis: base coordinate system

z-axis:

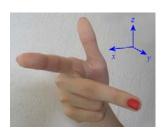
rotation axis

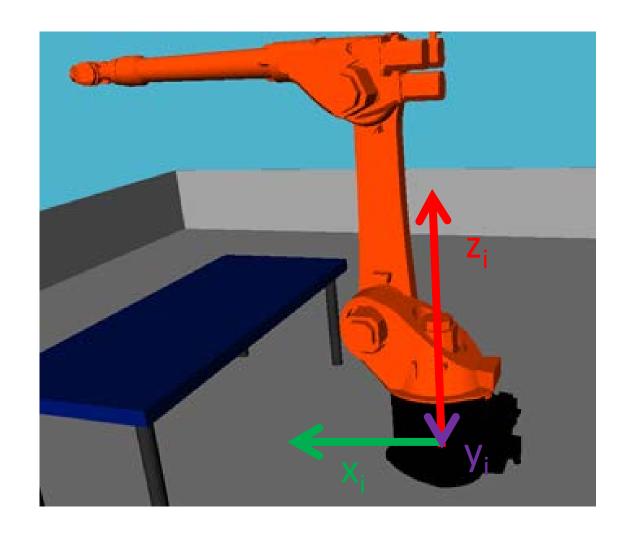
x-axis:

free of choice

y-axis:

right hand rule







- 4 different constellations for z_i and z_{i+1}
- 1. base coordinate system



- 2. z_i and z_{i+1} are not coplanar
 - 3. z_i and z_{i+1} parallel
 - 4. z_i and z_{i+1} intersects



not coplanar z-axes

- 2 vectors are coplanar, if they are within the same plane
- not coplanar =>
 - not parallel
 - no intersection





z-axis:

rotation axis

x-axis:

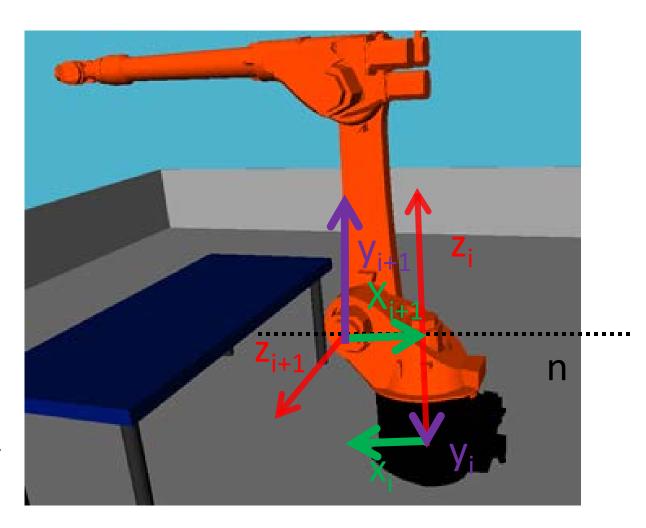
normal to z-axes

y-axis:

right hand rule

Origin:

intersection xi+1 –zi+1





- 4 different constellations for z_i and z_{i+1}
- 1. base coordinate system
- 2. z_i and z_{i+1} are not coplanar
- $3. z_i$ and z_{i+1} parallel
 - 4. z_i and z_{i+1} intersects





z-axis:

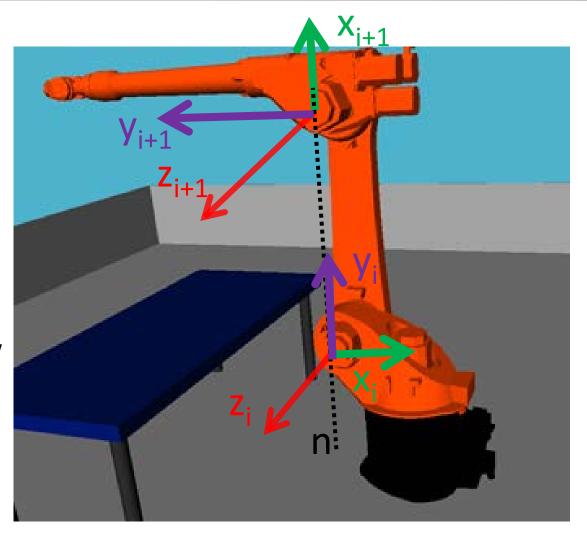
rotation axis

x-axis:

- infinite normal
- Choose normal through origin of last cs
- points towards new joint

y-axis:

right hand rule





- 4 different constellations for z_i and z_{i+1}
- 1. base coordinate system
- 2. zi and zi+1 are not coplanar
- 3. zi and zi+1 parallel







- z-axis: rotation axis
- x-axis:
 - normal to the plane of z_i and z_{i+1}
 - direction of x-axis is arbitrary
- place origin in the intersection point of z_i and z_{i+1}

y-axis: right hand rule



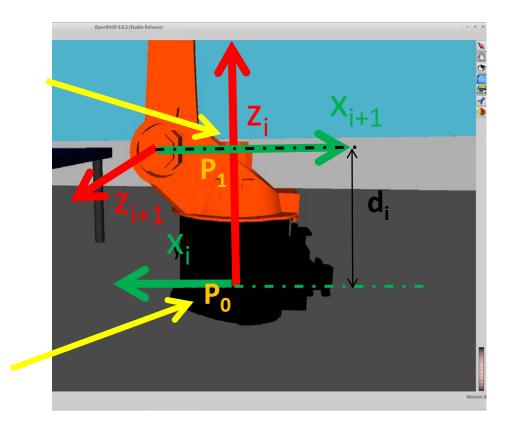
Deriving the parameters



- We need the 4 DH-parameters
 - d
 - a
 - α
 - θ
- describe the relation between two successive coordinate systems
- used for transformation from coordinate system into successor

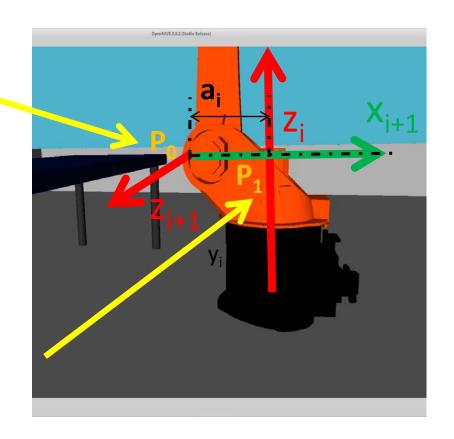


 d_i is the depth between the origin i (P₀) and the intersection of the z_i- and the x_{i+1}-axis (P₁)



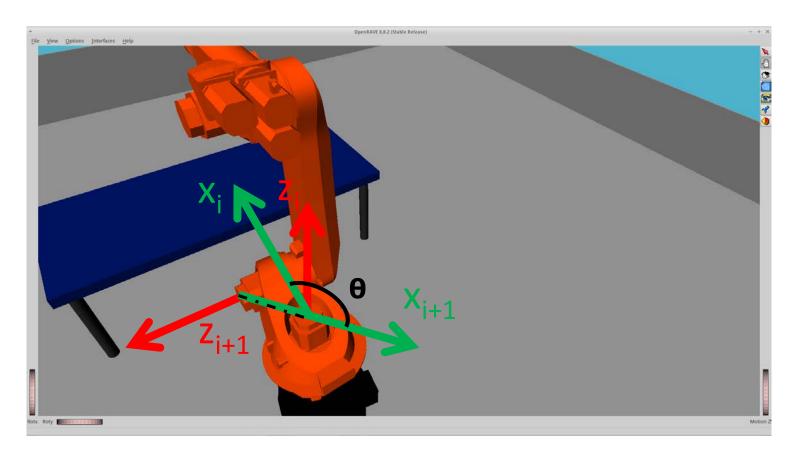


- a_i is the distance between the z-axes along the new x_{i+1} -axis
- distance origin i+1 and intersection x_{i+1} and z_i



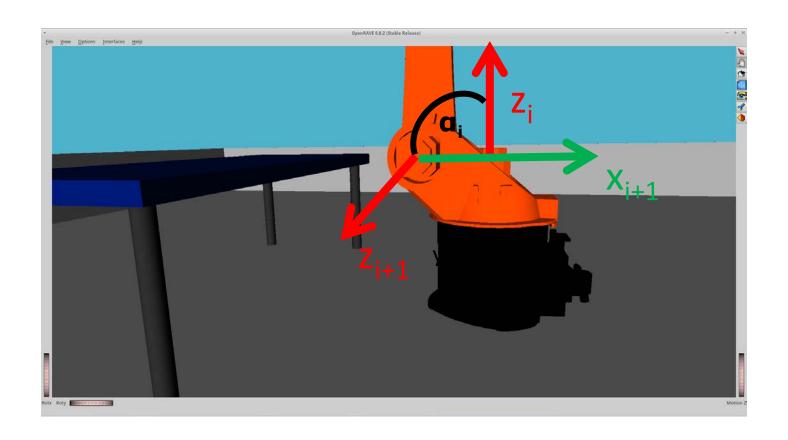


 θ_i is the angle between the old and the new xaxis rotating around z_i-axis





 a_i is the angle between the z-axes rotating around x_{i+1}-axis





Using the parameters



Using the parameters

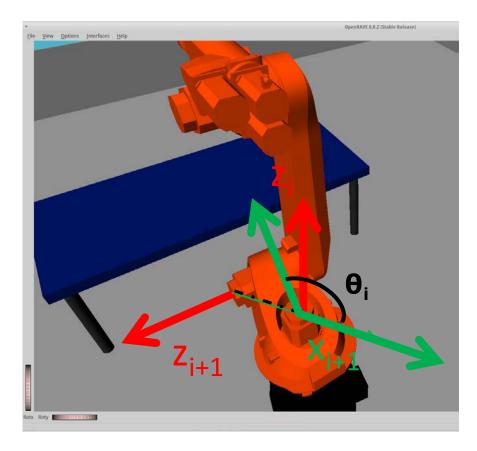
- performing the transformation by using the parameters
- 4 individual transformations
 - Rotation of θ around z_i: Rot(θ, z_i)
 - Translation of d along z_i: Trans(d, z_i)
 - Translation of a along x_{i+1}: Trans(a, x_{i+1})
 - Rotation of a **around** x_{i+1} : $Rot(a, x_{i+1})$





- Rotation of θ around z_i : $Rot(\theta, zi)$
- x_i same alignment as x_{i+1}

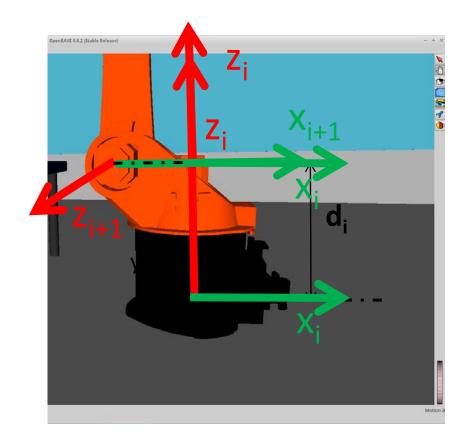
[cosθi sinθi	–sinθi cosθi	0	$\begin{bmatrix} 0 \\ 0 \end{bmatrix}$
0 0	0	1 0	0





Translation of d on z_i: Trans(d, z_i)

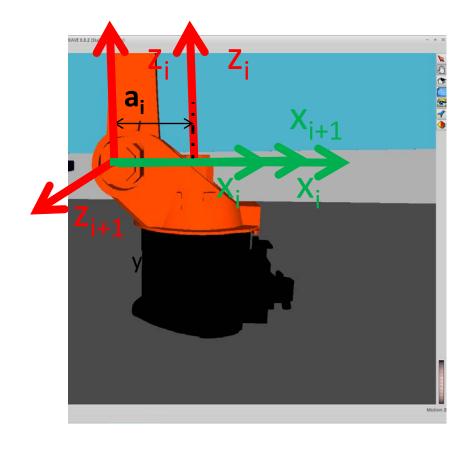
$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & \mathbf{di} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$





- Translation of **a on** x_{i+1} : Trans(a, x_{i+1})
- Origin i and i+1 at same position

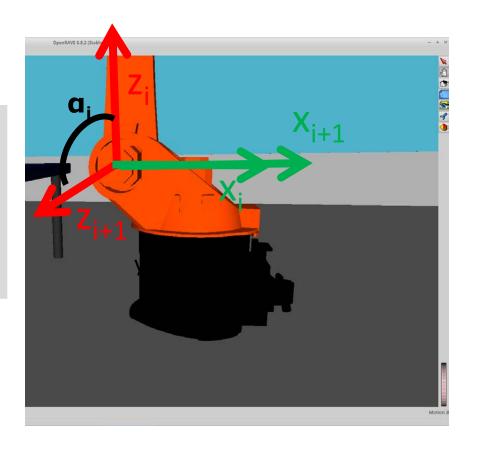
[1	0	0	ai
0	1	0	0
0	0	1	0
Lo	0	0	<i>ai</i> 0 0 1





• Rotation of a around x_{i+1} : $Rot(a, x_{i+1})$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos\alpha i & -\sin\alpha i & 0 \\ 0 & \sin\alpha i & \cos\alpha i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Complete transformation

- Transformation is concatenation of each single transformation
- $Rot(\theta, z_i) * Trans(d, z_i) * Trans(a, x_{i+1}) * Rot(a, x_{i+1})$

$$T_{i}^{i+1}(\theta i, di, ai, \alpha i) = \begin{bmatrix} \cos \theta & -\sin \theta \cos \alpha & \sin \theta \sin \alpha & a \cos \theta \\ \sin Q\theta & \cos \theta \cos \alpha & -\cos \theta \sin \alpha & a \sin \theta \\ 0 & \sin \alpha i & \cos \alpha i & d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

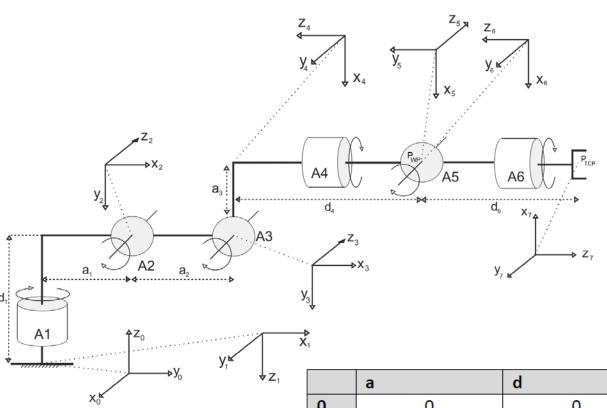




- 4 parameters used (a, d, θ, a)
- Important how to allign the coordinate system
 - z points along the rotation axis
 - y completes the right hand system
 - x is the normal between z-axes
- d distance between x-axes
- a distance between z-axes
- θ rotation between x-axes around z_i
- a rotation between z-axes around x_{i+1}



Abstraction of the Kuka KR30 L16

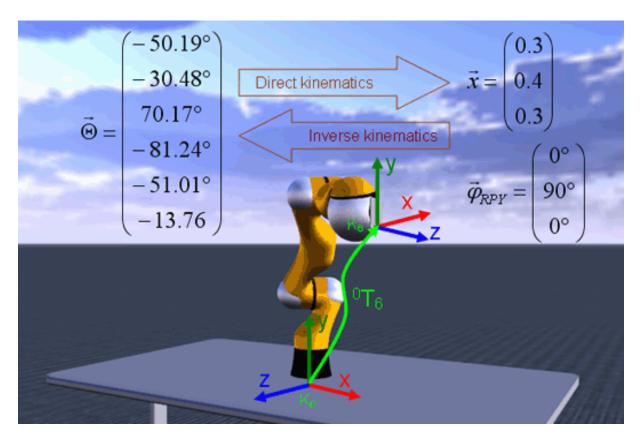


	a	d	θ	α
0	0	0	$^{\pi}/_{2}$	π
1	0.350	- 0.815	Θ1	$\pi/_2$
2	1.200	0	Θ2	0
3	- 0.145	0	$\Theta 3 + \pi/2$	$-\pi/_{2}$
4	0	- 1.545	04	$\pi/2$
5	0	0	<i>05</i>	$-\pi/_{2}$
6	0	- 0.158	$\Theta6 + \pi$	π

Abb: Abstraction of the Kuka KR30 L16



 Problem: Given the angles of each rotary joint of a robot, what is the position and the orientation of the TCP





TCP Orientation and Position

$$\mathsf{M} = \begin{pmatrix} & & & T \\ \hline 0 & 0 & 0 & 1 \end{pmatrix}$$

- The rotation matrix R describes the relative
- orientation to the base coordinate System
- The translation vector T describes the relative
- position to the base coordinate System
- Gives us Orientation and Position of the TCP



Description of the Orientation

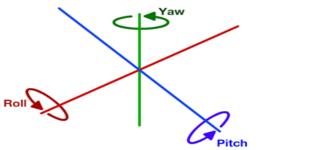
Description by rotation matrices

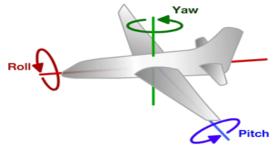
How can we describe the relative orientation in a less abstract way?

Solution: roll-pitch-yaw angles



Roll Pitch Yaw Angles



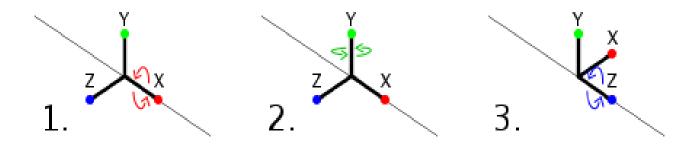


describe orientations by sequential (basic) rotations around x-, y- and z-axis Extrinsic rotations around a fixed coordinate system: $R_{ex} = R_x(\alpha) \cdot R_y(\beta) \cdot R_z(\gamma)$

Intrinsic rotations around an object coordinate system: $R_{in} = R_z(\gamma) \cdot R_u(\beta) \cdot R_x(\alpha)$



 A rotation of +/-90° around the second rotation axis sets the third rotation axis parallel to the axis of the first rotation

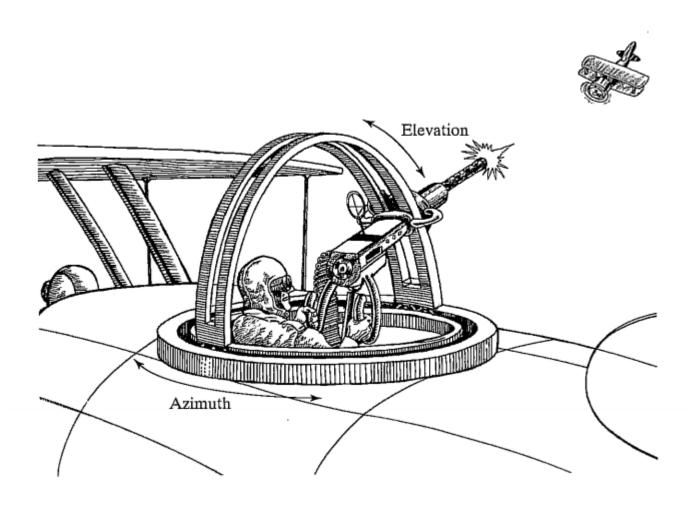


- → X and Z share the same rotation axis XZ
- the third dimension of the rotation system is lost
- Infinite rotation solutions arise:

$$R_{XZ}(\alpha + \gamma) = R_X(\alpha) + R_Z(\gamma)$$



Gimbal Locks (2)







$$\mathsf{R} = \begin{pmatrix} \cos(\alpha)\cos(\beta) & \cos(\alpha)\sin(\beta)\sin(\gamma) - \sin(\alpha)\cos(\gamma) & \cos(\alpha)\sin(\beta)\cos(\gamma) + \sin(\alpha)\sin(\gamma) \\ \sin(\alpha)\cos(\beta) & \sin(\alpha)\sin(\beta)\sin(\gamma) + \cos(\alpha)\cos(\gamma) & \sin(\alpha)\sin(\beta)\cos(\gamma) - \cos(\alpha)\sin(\gamma) \\ -\sin(\beta) & \cos(\beta)\sin(\gamma) & \cos(\beta)\cos(\gamma) \end{pmatrix}$$

$$R = R_x(\gamma) \cdot R_y(\beta) \cdot R_z(\alpha) = \begin{pmatrix} r_{00} & r_{01} & r_{02} \\ r_{10} & r_{10} & r_{12} \\ r_{20} & r_{21} & r_{22} \end{pmatrix}$$

pitch:

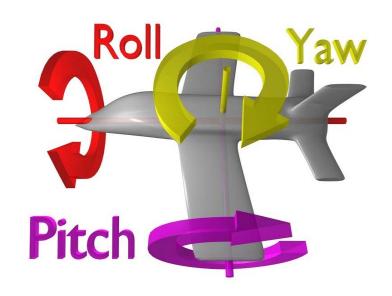
$$\beta = atan2(-r_{20}, \sqrt{r_{00}^2 \cdot r_{10}^2})$$
 oll:

roll:

$$\alpha = \begin{cases} 0 & \text{if } |\beta| = \pm \frac{\Pi}{2} \\ atan2(\frac{r_{10}}{\cos \beta}, \frac{r_{00}}{\cos \beta}) & \text{if } |\beta| \neq \pm \frac{\Pi}{2} \end{cases}$$

pitch:

$$\gamma = \begin{cases} \frac{\beta}{|\beta|} atan2(r_{01}, r_{11}) & \text{if } |\beta| = \pm \frac{\Pi}{2} \\ atan2(\frac{r_{21}}{\cos \beta}, \frac{r_{22}}{\cos \beta}) & \text{if } |\beta| \neq \pm \frac{\Pi}{2} \end{cases}$$

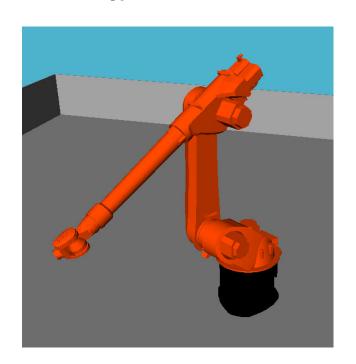


There may be more than one solution



Example:

$$q_0 = 0^{\circ}$$
 $q_1 = 30^{\circ}$
 $q_2 = 90^{\circ}$
 $q_3 = -120^{\circ}$
 $q_4 = 90^{\circ}$
 $q_5 = -15^{\circ}$
 $q_6 = 0^{\circ}$



TransformationMatrix for 0 to 1:

$$T_1^0 = T \begin{pmatrix} q_0 + \theta_0 \\ d_0 \\ \alpha_0 \\ a_0 \end{pmatrix}$$
$$T_1^0 = T \begin{pmatrix} q_0 + 90 \\ 0.0 \\ 180 \\ 0.0 \end{pmatrix}$$

$$T_1^0(q_0 = 0) = \begin{pmatrix} 0.0 & 1.0 & 0.0 & 0.0 \\ 1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & -1.0 & 0.0 \\ 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 180.0 pitch: 0.0 yaw: 90.0

TransformationMatrix for 1 to 2:

$$T_2^1 = T \begin{pmatrix} q_1 + \theta_1 \\ d_1 \\ \alpha_1 \\ a_1 \end{pmatrix}$$

$$T_2^1 = T \begin{pmatrix} q_1 + 0 \\ -0.815 \\ 90 \\ 0.35 \end{pmatrix}$$

$$T_2^1(q_0 = 0) = \begin{pmatrix} 1.0 & 0.0 & 0.0 & 0.35 \\ 0.0 & 0.0 & -1.0 & 0.0 \\ 0.0 & 1.0 & 0.0 & -0.815 \\ 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 90.0 pitch: 0.0 yaw: 0.0

$$T_2^1(q_0 = 30) = \begin{pmatrix} 0.866 & 0.0 & 0.5 & 0.303 \\ 0.5 & 0.0 & -0.866 & 0.175 \\ 0.0 & 1.0 & 0.0 & -0.815 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 90.0 pitch: 0.0 yaw: 30.0

TransformationMatrix for 2 to 3:

$$T_3^2 = T \begin{pmatrix} q_2 + \theta_2 \\ d_2 \\ \alpha_2 \\ a_2 \end{pmatrix}$$

$$T_3^2 = T \begin{pmatrix} a_2 \\ q_2 + 0 \\ 0.0 \\ 0 \\ 1.2 \end{pmatrix}$$

$$T_3^2(q_0 = 0) = \begin{pmatrix} 1.0 & 0.0 & 0.0 & 1.2 \\ 0.0 & 1.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 1.0 & 0.0 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 0.0 pitch: 0.0 yaw: 0.0

$$T_3^2(q_0 = 90) = \begin{pmatrix} 0.0 & -1.0 & 0.0 & 0.0 \\ 1.0 & 0.0 & 0.0 & 1.2 \\ 0.0 & 0.0 & 1.0 & 0.0 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 0.0 pitch: 0.0 yaw: 90.0

TransformationMatrix for 4 to 5:

$$T_5^4 = T \begin{pmatrix} q_4 + \theta_4 \\ d_4 \\ \alpha_4 \\ a_4 \end{pmatrix}$$
$$T_5^4 = T \begin{pmatrix} q_4 + 0 \\ -1.545 \\ 90 \\ 0.0 \end{pmatrix}$$

$$T_5^4(q_0 = 0) = \begin{pmatrix} 1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & -1.0 & 0.0 \\ 0.0 & 1.0 & 0.0 & -1.545 \\ 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 90.0 pitch: 0.0 yaw: 0.0

$$T_5^4(q_0 = 90) = \begin{pmatrix} 0.0 & 0.0 & 1.0 & 0.0 \\ 1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 0.0 & -1.545 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 90.0 pitch: 0.0 yaw: 90.0

TransformationMatrix for 5 to 6:

$$T_6^5 = T \begin{pmatrix} q_5 + \theta_5 \\ d_5 \\ \alpha_5 \\ a_5 \end{pmatrix}$$

$$T_6^5 = T \begin{pmatrix} q_5 + 0 \\ 0.0 \\ -90 \\ 0.0 \end{pmatrix}$$

$$T_6^5(q_0 = 0) = \begin{pmatrix} 1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 1.0 & 0.0 \\ 0.0 & -1.0 & 0.0 & 0.0 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: -90.0 pitch: 0.0 yaw: 0.0

$$T_6^5(q_0 = -15) = \begin{pmatrix} 0.966 & 0.0 & 0.259 & 0.0 \\ -0.259 & 0.0 & 0.966 & 0.0 \\ 0.0 & -1.0 & 0.0 & 0.0 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: -90.0 pitch: 0.0 yaw: -15.0

TransformationMatrix for 6 to 7:

$$T_7^6 = T \begin{pmatrix} q_6 + \theta_6 \\ d_6 \\ \alpha_6 \\ a_6 \end{pmatrix}$$

$$\begin{pmatrix} a_6 + 180 \end{pmatrix}$$

$$T_7^6 = T \begin{pmatrix} a_6 \\ q_6 + 180 \\ -0.158 \\ 180 \\ 0.0 \end{pmatrix}$$

$$T_7^6(q_0 = 0) = \begin{pmatrix} -1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & -1.0 & -0.158 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 180.0 pitch: 0.0 yaw: 180.0

$$T_7^6(q_0 = 0) = \begin{pmatrix} -1.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & -1.0 & -0.158 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 180.0 pitch: 0.0 yaw: 180.0

RESULTS:

$$T_7^0(q_i = 0, 0, 0, 0, 0, 0, 0) = \begin{pmatrix} 0.0 & 1.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 1.0 & 3.253 \\ 1.0 & 0.0 & 0.0 & 0.96 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 0.0 pitch: -90.0 yaw: -90.0

$$T_7^0(q_i = 0, 30, 90, -120, 90, -15) = \begin{pmatrix} -0.949 & -0.25 & 0.194 & 0.838 \\ 0.289 & -0.433 & 0.854 & 1.534 \\ -0.129 & 0.866 & 0.483 & 0.589 \\ \hline 0.0 & 0.0 & 0.0 & 1.0 \end{pmatrix}$$

roll: 60.853 pitch: 7.435 yaw: 163.064



What we wanted you to know

- Introduction into the KUKA 30
- Kinematic Chain
- DH Parameters
- Position and orientation in forward kinematics