

# PHYS 202 Formula Sheet

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**Simple Harmonic Oscillators** Consider a mass attached to a spring. Let  $x(t)$  be the function of displacement of the mass from the equilibrium position. Suppose that the spring constant is  $k$ . By Newton's 2nd Law,

$$m\ddot{x} = -kx \quad \text{or} \quad \ddot{x} = -\frac{k}{m}x$$

Where  $\dot{x} := \frac{d}{dt}x$

The following function solves the equation.

$$x(t) = \text{Re}(\tilde{A}e^{ii\omega_0 t}) = A \cos(\omega_0 t + \phi)$$

$A, \omega_0$  is referred as the amplitude and the natural frequency of the oscillator. Also,

$$A = \sqrt{\frac{2E}{k}} \quad \text{and} \quad \omega_0 = \sqrt{\frac{k}{m}}$$

**Phase Conventions** Velocity leads Displacement by a phase of  $\pi/2$ . Acceleration leads Velocity by a phase of  $\pi/2$

Say  $V \sim \cos(\omega t)$  and  $I \sim \cos(\omega t + \phi)$  for some positive phase  $\phi \leq \pi$ . The current leads the voltage and the voltage trails the current.

**Simple RLC** Consider a circuit where R, L, C is connected in parallel. Let the current be  $I$ . By the loop rule,

$$-\frac{q}{C} - RI - L\dot{I} = 0 \quad \text{or} \quad \frac{q}{C} + R\dot{q} + L\ddot{q} = 0$$

Rewrite this in the following form.

$$\ddot{q} + \frac{R}{L}\dot{q} + \frac{q}{LC} = 0$$

Compare this with the equation for damped driven oscillators.

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = 0$$

So the following isomorphism holds

$$x \mapsto q \quad \text{then} \quad (m, b, k) \mapsto (L, R, 1/C)$$

In a parallel circuit, the current through each circuit component is identical. By the complexified Ohms Law  $\tilde{V} = Z\tilde{I}$ . Recall the impedances.

$$Z_R = R \quad \text{and} \quad Z_C = \frac{1}{i\omega C} \quad \text{and} \quad Z_L = i\omega L$$

Thus, the voltage of the resistor leads the voltage on the capacitor by phase  $\pi/2$ . Likewise, the voltage on the resistor trails the voltage on the Inductor by  $\pi/2$ .

**Circuit Filters and Loglog plot** Using inductors and capacitors, it is possible to filter out signals of high or low frequency. Consider the behavior of circuit elements in high and low frequency.

$$\begin{aligned} \lim_{\omega \rightarrow 0} Z_L = \lim_{\omega \rightarrow 0} i\omega L = 0 \quad \text{and} \quad \lim_{\omega \rightarrow \infty} Z_L = \lim_{\omega \rightarrow \infty} i\omega L = \infty \\ \lim_{\omega \rightarrow 0} Z_C = \lim_{\omega \rightarrow 0} \frac{1}{i\omega C} = \infty \quad \text{and} \quad \lim_{\omega \rightarrow \infty} Z_C = \lim_{\omega \rightarrow \infty} \frac{1}{i\omega C} = 0 \end{aligned}$$

The inductor will block signals of high frequency but allow the passage of signals of low frequency. Hence, inductors act as a **low-pass** filter. On the other hand, capacitors block signals of low frequency and allow the passage of high frequency signals. Hence, capacitors act as a **high-pass** filter.

**Corner frequency vs Resonant frequency** For an RLC circuit, it is possible to tune the frequency such that the combined impedance reach zero. This frequency is called the resonant frequency. For a circuit involving one R, L, C, the resonant frequency is computed by the following formula.

$$\omega_r = \frac{1}{\sqrt{LC}}$$

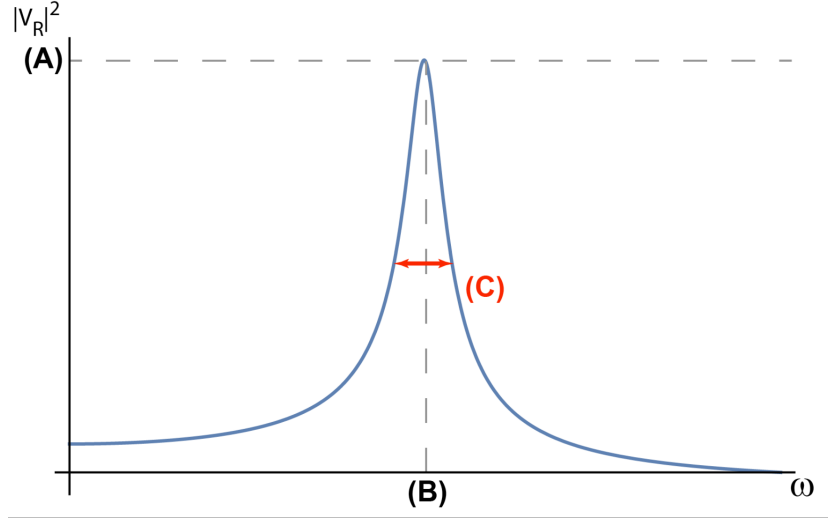
For an RL or an RC circuit, the imaginary part of the impedance cannot reach zero. It is possible to define a corner frequency where the circuit behavior changes drastically. It is the frequency where  $Im(Z_L) = R$  or  $Im(Z_C) = R$ . In other words,

$$\omega_c = \frac{1}{RC} \quad \text{or} \quad \frac{R}{L}$$

### Dimensions of C and L

$$[L] = H = \Omega \cdot s \quad \text{and} \quad [C] = \frac{s}{\Omega}$$

**Power Resonance Curve** For an RLC circuit, it is possible to plot the relationship between the angular frequency of the input voltage and the power lost through the resistor. This curve is called the Power Resonance curve.



$P \sim V^2$ . The Full-Width-Half-Maximum refers to the width of the curve at the half maximum point. The FWHM of the Power Resonance Curve is exactly  $\gamma = R/L$ , the damping factor. Be careful of the factor of  $2\pi$  when the x-axis is set as frequency (Hz).

Also, use the dimension  $[\omega] = \text{rad/s}$  and  $[f] = \text{Hz}$ . The frequency refers to cycles per second.

**Q-factor** For damped driven oscillators, the Q-factor is an important number.

$$Q := \frac{\omega_0}{\gamma} = \frac{A_{res}}{A_0}$$

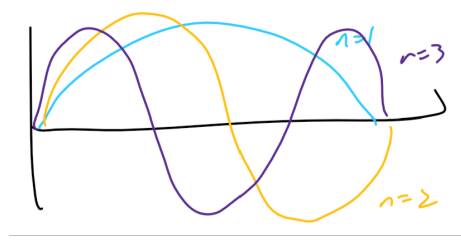
**Boundary conditions for N masses** The solutions for the n mass oscillators are in the form of:

$$\psi(m, t) = Ae^{i(\omega t + k_m a)} + Be^{i(\omega t - k_m a)}$$

Plugging into the 2nd order DE, we derive an expression for the angular frequency.

$$\omega_m = 2\omega_0 \sin(k_m \frac{a}{2})$$

$k_m$  is the mth wave number. Recall that  $k := \frac{2\pi}{\lambda}$ .  $\lambda_n$  can be computed by drawing diagrams.



With some algebraic hassle, it is possible to derive the expressions for  $k_m$ .  
For closed-closed and open-open ends:

$$k_m a = \frac{m\pi}{n+1} \quad \text{or} \quad k_m = \frac{m\pi}{a(n+1)} = \frac{m\pi}{L}$$

Where  $m \in \mathbb{Z}^+$

For open-open ends:

$$k_m a = \frac{m\pi}{(2n+1)/2} \quad \text{or} \quad k_m = \frac{m\pi}{L}$$

Where  $m \in \mathbb{Z}^+$

**Free end Distance relation** Always set the origin to be distance  $a/2$  apart from the free end. This is because the two masses at the boundary must be symmetric. Refer to pset 5-1.

**Transverse waves** From the geometry of the springs, we use approximation. Let  $\theta$  be the angle between the horizontal axis and the string.  $\tan(\theta) \approx \theta = \Delta y/a$ . Consequently, we arrive at:

$$k \mapsto T/a$$

**Dispersion Relation** The differential equation of the masses in the center oscillators provide a closed form equation for the angular frequency in terms of the wave number  $k$ .

$$\omega(k) = 2\omega_0 \sin(ka/2)$$

where  $a$  is the distance between the masses.

**Dispersion Relation 2** The dispersion relation defines the wave number  $k$ .

$$\frac{\partial^2 \psi}{\partial t^2} = c^2 \frac{\partial^2 \psi}{\partial x^2} \quad \text{then} \quad \omega^2 = c^2 k^2$$

And  $c$  is called the phase velocity of the wave. The wave number depends on the frequency of the wave, which is not necessarily the normal mode frequency

**Nodes and Antinodes** In a standing wave, nodes are the points that do not move. Max amplitude is achieved at antinodes.

**Waves traveling in different medium, same tension** Consider a transverse wave moving from one string of linear mass density  $\mu_1$  to another string with linear mass density  $\mu_2$ . The velocity of the waves on each string is entirely determined by the lmd.

$$(v_1, v_2) = \left( \sqrt{\frac{T}{\mu_1}}, \sqrt{\frac{T}{\mu_2}} \right)$$

Let the incident wave to be in the form of

$$\psi_i(x, t) := f_i(t - x/v_1)$$

We make a natural assumption that the combined wavefunction must be smooth with respect to position. Let  $f_t, f_r$  be the simplified translated wavefunction and the simplified reflected wavefunction. We derive

$$\frac{f_r}{f_i} = \frac{v_2 - v_1}{v_1 + v_2} \quad \text{and} \quad \frac{f_t}{f_i} = \frac{2v_2}{v_1 + v_2}$$

**Natural conditions on the string displacements** We assume that the wavefunction is continuous and differentiable at all positions. Also,

$$\dot{\psi}(x, 0) = 0$$

allows us to easily complexify the solution.

#### Crash-intro to Fourier Transform

$$\boxed{f(x) = \int_{-\infty}^{\infty} C(k) e^{ikx} dk} \quad \text{where} \quad \boxed{C(k) = \frac{1}{2\pi} \int_{-\infty}^{\infty} f(x) e^{-ikx} dx} \quad (43)$$

**Non-dispersive Waves** refers to waves in which the variance of frequency and wavelength of the wave does not affect the velocity of the wave. A good example is a transverse wave on a string.

$$v = \sqrt{\frac{T}{\mu}}$$

where  $T$  is the tension of the string and  $\mu$  refers to mass density.

**Mechanical impedance and transmission across different tension** We define mechanical impedance of a string as follows.

$$Z = \frac{F}{v} = \sqrt{T\mu}$$

Mechanical impedance is analogous to drag force the string exerts on the ends. That is  $Z \mapsto b$ . Using impedance, we can write out the reflection and

transmission coefficients. Let  $Z_1, Z_2$  denote the mechanical impedance of line 1 and line 2 where the wave is traveling from line 1 to line 2. The reflection and transmission coefficients are written as:

$$R = \frac{Z_1 - Z_2}{Z_1 + Z_2} \quad \text{and} \quad T = \frac{2Z_1}{Z_1 + Z_2}$$

Reflection happens by a small amount, and transmission is dependant on the original string. Perfect transmission happens when impedences are matched. That is,  $Z_1 = Z_2$ .

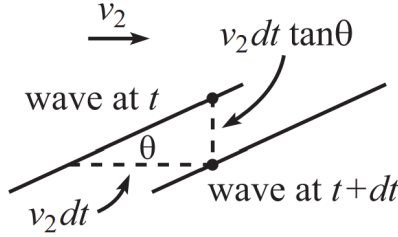
**Space-Time relation of traveling waves** We know, mathematically, that the solutions to the wave equations are in the form of

$$\psi(x, t) = f(x - vt)$$

Where  $v$  is the longitudinal speed of the force. By applying the chain rule, we can deduce

$$\dot{\psi} = -v\psi'$$

This can also be deduced by drawing the following diagram



**Figure 16**

**Energy and Power of a traveling wave** Considering the string as a conglomerate of segments, we can retrieve a formula for the energy density of the wave. Note that the potential energy of the string is computed by  $Tdl$  where  $dl$  refers to stretch. The kinetic energy is related to the time derivative, and the potential energy is related to the space derivative. Applying the wave equation, we derive

$$\mathcal{E} = \mu\dot{\psi}^2 = \mu v^2(\psi')^2$$

So the wave equation somewhat coagulates the space and time dependance of energy. The energy density of a wave is product of the lmd and square of the time derivative of the wave.

It makes sense that the power transmission is the negativ product of linear energy density and transmission speed. This can be derived rigorously using  $\dot{\psi} = -v\psi'$ .

$$P(x, t) = -v\mathcal{E}$$

**Analysis of Standing waves using impedance** Fixed ends can be considered as a string connected to another string with infinite impedance. Free ends likewise can be considered as string connected to another spring with zero impedance. Enforcing continuity and smoothness we can derive an equation for standing waves.

**Choosing the correct type of wave form** The solutions to the wavefunction come in the form of

$$\psi(x, t) = Ae^{i(kx - \omega t)} \quad \text{or} \quad Ae^{i(\omega t - kx)}$$

When imposing the boundary condition which is space-dependant, it is more useful to adapt the latter form.

**Crash intro to optics** The four Maxwell equations govern the behavior of EM waves. We are especially interested in the case of waves traveling in isotropic media. That means, zero charge density and linear current density. The four Maxwell Equations are presented as below.

$$\begin{aligned} \nabla \cdot \vec{E} &= -\mu_0 \vec{H} & \nabla \cdot \vec{H} &= -\epsilon_0 \vec{E} \\ \dot{\vec{E}} &= 0 & \dot{\vec{H}} &= 0 \end{aligned}$$

The field  $\vec{H}$  is rigorously defined in PM 11.9, but for now, just remember

$$\vec{H} = \frac{1}{\mu_0} \vec{B}$$

$\mu$  refers to permeability and  $\epsilon$  refers to permittivity. The value of permeability is usually fixed to be  $\mu_0$  for transparent medium. The value of permittivity depends on the medium. The dielectric constant is defined as

$$\kappa := \frac{\epsilon}{\epsilon_0}$$

The velocity of an EM wave, aka light, depends on the traveling medium. The index of refraction is defined as

$$n := \frac{c}{v}$$

. Note that the index is defined as the reciprocal of the more intuitive definition.

From E&M, recall that the energy transmission was governed by the Poynting vector,

$$\vec{S} := \vec{E} \times \vec{H}$$

From the Maxwell's equations, we deduce the magnitude of  $\vec{H}$ .

$$H = \frac{nE}{Z_0}$$

Where  $Z_0 := \sqrt{\mu_0/\epsilon_0} = 377\Omega$  is defined as the impedance of free space.

We also deduce that irradiance (or intensity) is proportional to square of the E field.

$$I = \frac{n}{2Z_0} E_0^2$$

### **Isomorphism btw transmission lines and EM waves**

Remember from Morin 8.1, we defined how a signal travels through a transmission line. Two signals appear, which is the voltage wave  $V$  and the current wave  $E$ . Let  $L_0, C_0$  denote the linear inductance and the capacitance. We obtained the result that

$$v = \sqrt{\frac{1}{L_0 C_0}}$$

Also, these two waves are isomorphic to the EM waves. The isomorphism is given as follows

$$V \mapsto E \quad I \mapsto B/\mu_0$$

We also know

$$Z = V/I \quad \text{and} \quad E = cB$$

where  $c$  is the velocity of the wave given by  $1/\sqrt{\epsilon\mu}$

With some algebra, we deduce

$$Z = nZ_{free}$$

. To obtain the result, use the assumption that permeability is constant for transparent media.



**Jones Calculus for polarization** Consider an EM wave traveling in isotropic media. It is a convention to consider the electric field of the wave for polarization. The electric field has both x and y components which are sinusoids dependant on time and the transmission axis z. That is,

$$\vec{E} = \hat{x}E_x + \hat{y}E_y \quad \text{where}$$

$$E_x = E_{x0} \cos(kz - \omega t) \quad \text{and} \quad E_y = E_{y0} \cos(kz - \omega t + \phi)$$

Complexifying  $E_x, E_y$ , we can write

$$\tilde{E}_x = E_{x0} e^{i(kz - \omega t)} \quad \text{and} \quad \tilde{E}_y = E_{y0} e^{i(kz - \omega t + \phi)}$$

So, the vector  $\tilde{\vec{E}}$  can be written as follows

$$\tilde{\vec{E}} = \begin{bmatrix} E_{x0} \\ E_{y0} e^{i\phi} \end{bmatrix} e^{i(kz - \omega t)}$$

The exponential term outside the matrix is insignificant to describe polarization. We define the constant matrix as the **Jones vector** of the polarization. Factoring out a global phase factor, a Jones matrix is in the form of

$$L \begin{bmatrix} 1 \\ e^{i\phi} \end{bmatrix} \quad \text{or} \quad R \begin{bmatrix} e^{i\phi} \\ 1 \end{bmatrix}$$

for  $\phi \in [0, \pi]$ . The first matrix represents a light in which the y-axis has a *slower* phase. Shift the y-sinusoid of the EM wave to deduce that the light is left polarized. Similarly, the second matrix represents a right polarized light.

The effect of an optical element can be represented as a linear transform on the Jones vector. We call this 2x2 matrix a **Jones Matrix**. So far, we have covered two major optical elements, the linear polarizer and the waveplate. Using the bra-ket notation, their Jones matrix can be written as follows.

$$L_{\vec{v}} = |\vec{v}\rangle\langle\vec{v}| \quad \text{and} \quad W(\hat{f}, \hat{s}, \phi) = e^{i\phi} |\hat{s}\rangle\langle\hat{s}| + |\hat{f}\rangle\langle\hat{f}|$$

**Some useful implications of the Maxwell equations** We know that the EM wave equations are in the form of

$$\vec{E} = \vec{E}_0 e^{i(\vec{k}\vec{r} - \omega t)} \quad \text{and} \quad \vec{B} = \vec{B}_0 e^{i(\vec{k}\vec{r} - \omega t)}$$

Applying the Maxwell equations allow us to make the following conclusions.

The wavevector, or the direction of propagation, is perpendicular to both the electric and the magnetic field.

$$\vec{k} \cdot \vec{E} = \vec{k} \cdot \vec{B} = 0$$

The magnitude of the Efield and the Bfield are proportional.

$$E = cB$$

The cross product of the wavevector and the electric field yields the magnetic field multiplied by the angular frequency.

$$\vec{k} \times \vec{E} = \omega \vec{B}$$

Finally, the Poynting vector provides the energy propagation of an EM wave.

$$\vec{S} = \frac{1}{\mu_0} \vec{E} \times \vec{B}$$

The velocity of the wave is the angular frequency over the magnitude of the wavevector.

$$v = \omega/k$$

**Waves carry Momentum** We have seen that waves transfer energy. But how can a wave have momentum? To answer this question, we consider a free charge in the transmission axis. Let  $\hat{k}$  be the transmission axis and  $q$  be a charge sitting on this axis. The E and B field propagate in a way that their vectors are perpendicular to each other and  $\hat{k}$ .

We wish to compute the infinitesimal amount of work and momentum exerted on the free charge. The electric field exerts force in the same direction of the movement of the particle. Thus,

$$dW = F_E dx = (qE)(v_E dt)$$

Assuming the movement of the particle is nearly perpendicular to  $\hat{k}$ , the magnetic field also exerts a force on the particle.

$$dp = mv_E = ma_E dt = F_B dt = qv_E B dt$$

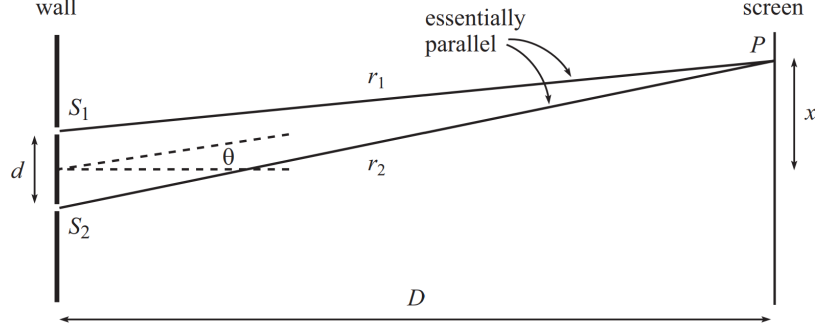
Also remember  $E = cB$ . Thus,  $cdp = dW$  and by integration,  $cp = E$ .

$$p = \frac{E}{c}$$

as desired. □

### The double slit experiment

A vertical wavefront approaches a wall that has two slits. As the wavefront hits the wall, two circular wavefronts are formed by the Huygens principle. The two wavefronts are in phase by construction.



Remember that for 2D circular waves, the amplitude decreases by a factor of  $\sqrt{r}$ . With some algebra, we deduce the irradiance as a function of  $x$ .

$$\frac{I(x)}{I(0)} = \frac{D}{\sqrt{x^2 + D^2}} \cos^2 \left( \frac{kd}{2} \frac{x}{\sqrt{x^2 + D^2}} \right) = \frac{D}{\sqrt{x^2 + D^2}} \cos^2 \left( \frac{d\pi}{2\lambda} \frac{x}{\sqrt{x^2 + D^2}} \right)$$

For  $x \ll D$ ,

$$\boxed{I_{tot}/I = \cos^2 \left( \frac{d}{D} \frac{x}{\lambda} \pi \right)}$$

The argument of the cosine square function can be interpreted as the screen distance  $x$  projected to the wall space converted to some phase factor by  $\lambda$ .

**Multislit experiment** Now, consider the same apparatus as the double slit, but instead, include  $N$  slits. We proceed with the assumption that

$$d \ll D \quad \text{and} \quad x \ll D \quad \text{and} \quad \theta \approx 0$$

Also, the phase difference between two consecutive rays are

$$\delta := ka \sin(\theta) := k' a$$

We also know that the amplitude of the wave decreases by a factor of  $\sqrt{d}$  for cylindrical waves, where  $d$  is the distance travelled. In the slit experiments, the amplitude of a single ray depends on the angle  $\theta$ . Define

$$A(\theta) = \sqrt{\frac{\cos(\theta)}{D}} A_{src}$$

Assuming  $\theta$  small,

$$A(\theta) \approx A(0)$$

We first derive the amplitude for angle  $\theta$  where there are  $N$  slits, each a distance  $d$  apart.

$$A_{tot}(\theta) = A(\theta) |1 + e^{i\delta} + e^{2i\delta} + \dots| = A(0) \frac{\sin(N\delta/2)}{\sin \delta/2}$$

Also note

$$A_{tot}(0) = A(0) |1 + 1 + 1 + \dots| = nA(0)$$

Thus,

$$\frac{A_{tot}(\theta)}{A_{tot}(0)} = \frac{\sin(N\delta/2)}{N \sin(\delta/2)}$$

Intensity is proportional to the square of the amplitude.

$$\frac{I_{tot}(\theta)}{I_{tot}(0)} = \left( \frac{\sin(N\delta/2)}{N \sin(\delta/2)} \right)^2$$

**Wide Slits** It is possible to derive the continuum case by taking the limit. However, the suggested solution is using the integral. Otherwise, it is hard to see that the intensity is dependant on the slit width. We finally reach,

$$|A| \propto a \operatorname{sinc} \left( \frac{k'a}{2} \right) \quad \text{and} \quad I \propto a^2 \operatorname{sinc}^2 \left( \frac{k'a}{2} \right)$$

where  $k' = k \sin(\theta)$

**Diffraction and Reflection** The angle of incident and the angle of reflect is defined to be the angle between the ray and the normal axis. It is not necessary that these two angle agree with each other. If any of the rays exit the surface, we call this ray the **diffracted** ray. If the incident angle matches the reflected angle, we refer to the phenomenon as **reflection**

To compute the phase difference of a diffracted ray, consider the change of difference traveled.