SUJIT K GUCHHAIT¹, SOURAV DEWAN², JAYANTA K SAHA³, P.K.MITRA⁴ Dept. of Metallurgical & Material Engineering, Jadavpur University, Kolkata-700032

³ Institutes for Steel Development & Growth (INSDAG), Kolkata-700019

Abstract-- Salt spray test, autoclave corrosion test, SO₂ salt spray test, and Relative humidity test are generally used to assess atmospheric corrosion in laboratories at accelerated rates. However no test can absolutely simulate the service condition. One can get only approximate corrosion rates using the aforesaid tests which serve as an indicative of corrosion behavior of the material in a service condition. The present work is aimed at creating specific environmental condition in laboratory to get the corrosion test done in short duration to compare with on field exposure test which would otherwise take years to complete. In this work recreation of atmospheric environment of DIGHA was tried and it was tried to simulate in such a manner that the results of laboratory test could be compared with long time field exposure at Digha. Weathering steel was taken for experimentations. Potentiostatic electrochemical tests route was adopted to simulate atmospheric condition of Digha. Laboratory test results compared well with 18 month field exposure data in terms of corrosion rate, SEM and Ramon Spectroscopy matching.

Key Words: Weathering steel, Laboratory simulation, Corrosion, Field test, SEM, Raman Spectroscopy

1. INTRODUCTION

Panossian, Z. et al. showed that weathering steels (WS) have 1-2.5% of alloying elements especially Cu, Cr, P etc and have a tendency to form a specific type of rust which helps in decreasing the corrosion rate after long exposures.¹ The rate of rust formation depends on the access of oxygen in the presence of moisture and air. According to J.K.Saha rust formation process slows down as the process progresses because the rust layers acts as a barrier to the ingress of the oxygen². In weathering steels the rust layer is more adherent in nature and reduces the rate of rust growth. From M.Pourbaix concept, it has been seen that the typical behavior of weathering steel is due to the passivation during drying and lack of activation during wetting³. S.Feliu et al reported that air borne chloride (0.5mg/100cm²/day), average wetness time < 60 %, industrial pollutants (SO2< 2.1 mg/100cm²/day) are the favorable parameters to formed a stable rust on weathering steel, like ⁴⁻⁵.

Marine atmosphere have high percentage of relative humidity and airborne salt. Corrosion rate in chloride environment gets reduced in special grade weathering steel. Many authors have studied the corrosion products formed on carbon since and the authors. This is a preprint of a paper that has been submitted for publication in the 4Journal of Control on carbon since and the authors. This is a preprint of a paper that has been submitted for publication in the 4Journal of Control on the 4Journal of Control on the 4Journal of Control of

rust phase feriod the Sitema (viceOOH) transforms to the more stable goethite (α -FeOOH). With increasing exposure time continuous transformation of α -FeOOH occurs to either protective γ Fe₂O₃ or α Fe₂O₃ as well as amorphous δ FeOOH². Pourbaix diagram³ for iron-Na₂SO₄ shows passivity between pH 9 to 12.5 due to formation of iron hydroxide. Jayanta K Saha² reported that when weathering steels are exposed to the Digha a protective layer of α Fe₂O₃, γ Fe₂O₃, γ FeOOH, δ FeOOH and α Fe₂O₃, α FeOOH, γ FeOOH are formed during 18 months and 42 months on field explosion respectively.

Since passive layer formation is supposed to cause the decreasing corrosion rate of weathering steels with increasing exposure time, it was envisaged to induce on weathering steel formation of passive layer corresponding to Digha. Digha exhibits a typical marine atmosphere in India. Passive layer on weathering steel was formed potentiostatically in the laboratory. Aqueous solution corresponding to Digha environment was taken for the Potentiostatic experiments.

2. EXPERIMENTAL & RESULTS

The composition of WS used for this purpose is given in the table 1.a.

Composition	С	Mn	Cu	Cr	Ni	S	P	Si	Fe
(wt%)									
WS	0.09	0.38	0.35	0.45	0.27	0.01	0.11	0.41	balance

Table.1.a: chemical composition of WS

Test sample of WS as per ASTM Standard was exposed at Digha which is a marine site having trace amount of SO₂ in the environment with appreciable amount of chloride ions. The samples were exposed for 18 months and their corrosion rate were measured by DC corrosion using Gamry potentionstat (fig.1.a) Rust morphology was characterized by scanning electron microscope (SEM) model JEOL S3400, Japan (fig1.b.),

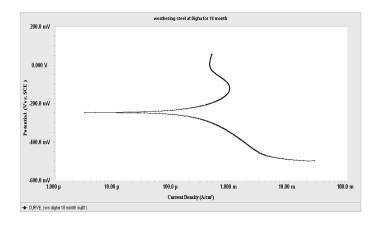


Fig 1.a. PD tests of 18 month on field WS in 3.5% NaCl solution , scan rate 1 mV/s $\,$

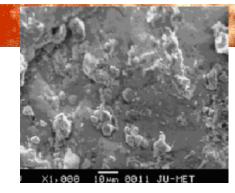


Fig.1.b. SEM of Rust Exposed for 18 month at Digha WS

Raman spectroscopy was used to identify the phases present in rust using Nicolet Almega dispersive Raman Spectroscope by exciting the laser beam of He-Ne of 532 nm focused through Olympus microscope at 50X. Raman peaks were identified according to spectra for the various iron oxide and hydroxide compounds from the references (Table 1.d).

The weathering steel samples were cut into number of pieces and were polished through 120, 180, 1/0, 2/0 emery papers and were finally cloth polished. To accelerate corrosion process electrolyte 0.01 N chloride solution was taken. For making the solution near neutral its pH was adjusted to 8.8 by adding KOH solution. The Potentiodynamic polarization of the sample in this solution was done to find out the passive region using GAMRY POTENTIOSTAT. Scanning rate used was 1mV/s (fig.1.c).

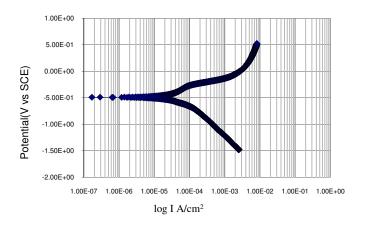


Fig 1.c.: Polarization curve of Weathering Steel in 0.01 (N) KCl solutions at pH 8.8

Once the passive region was found, a number of Potentiostatic current transient experiments at E=400mV and at 450 mV vs. SCE were carried out for different time durations i.e 30 mins, 60 mins, 110 mins. Once the passivation was done, it was then exposed to 3.5% NaCl solution for Potentiodynamic test to get the electrochemical corrosion rate (table 1.c). Potentiodynamic tests of exposed WS samples were also done in 3.5% NaCl solution. The details of results are given in the table.2.b. SEM of the both fields exposed and

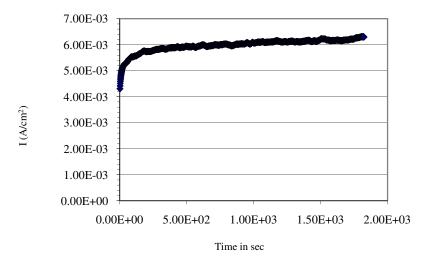


Fig.1.d. Current transient in 0.01(N) KCl(pH 8.8) at a passivation potential of 400mV for 30 mins

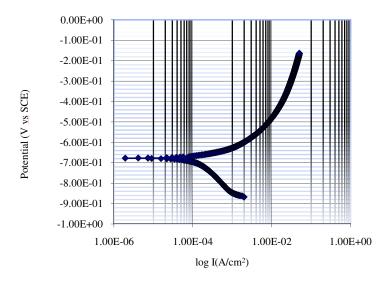


Fig.1.e. PD of WS in 3.5% NaCl solution after passivation for 30 $\,$ mins at E=400 mV $\,$

Table.1.b. Polarization Data of Digha WS sample after 18 months exposed

	Icorr	Ecorr	
Site	(μ A/cm ²)	(mV)	
Digha	102.1	-251.8	

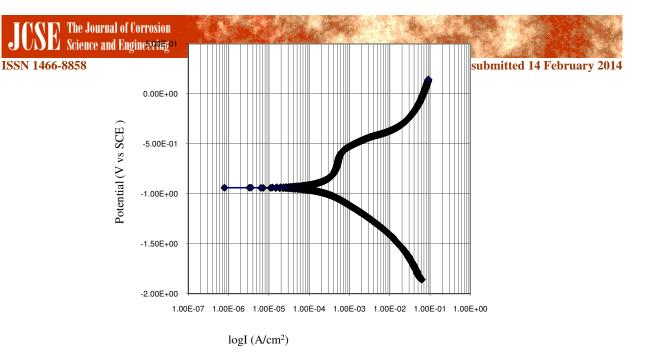


Fig 1.f. Polarization curve of WS in 0.01(N) KCl(pH 8.8) after passivation for 60mins at E=400mV

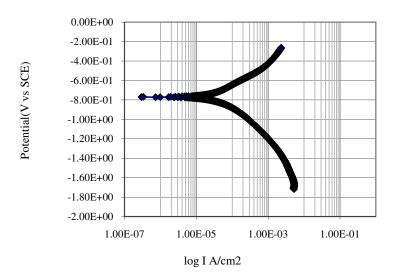


Fig.1.g.PD of WS in 3.5% NaCl solution after passivation for 110mins at E=400mV

Table 1.c. Polarization Data of WS after Passivation

After passivation for selected time at 400mV			
Time	Icorr	Ecorr	
	$(\mu A/cm^2)$	(mV)	
110 mins	40	-770	
60 mins	220	-807	
30 mins	102	-690	

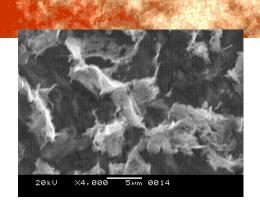


Fig.1.h .SEM of WS Passivation at 400 mV for 30 minute in 0.01 KCl (pH 8.8).

Table.1.d Raman Phases of Digha WS sample after 18 months exposed

Phase	Raman Shift (cm ⁻¹)
γ Fe ₂ O ₃	265.37
δ FeOOH	392.92
γ FeOOH	241.60
γ FeOOH	1292.10
α Fe ₂ O ₃	491.01

Table.1.e. Raman Phases of Digha WS sample after passivation for 30 mins at 400 mV

Phase	Raman Shift (cm ⁻¹)
α FeOOH	302.07
δ FeOOH	392.84
α FeOOH	687.82
α Fe ₂ O ₃	1319.01
γ Fe ₂ O ₃	1425.63
γ FeOOH	313.94
γ Fe ₂ O ₃	395.69
β FeOOH	723.40
$\gamma \ { m Fe_2O_3}$	1422.78



3. DISCUSSION:

The objective of passivating the sample in 0.001 (N) KCl solutions at pH 8.8 was to effect formation of oxide/hydroxide layer similar to field exposure. From fig 1.c. it can be seen that 0.4V vs. SCE is well within the passive region. Fig 1.d shows the current transient curve at 0.4V vs. SCE while fig 1.e-1.g are the polarization curve in 3.5% NaCl solutions after passivation at 0.4V vs. SCE for 30 minutes, 60 minutes, and 110 minutes respectively. It can be seen that I_{corr} and E_{corr} of the sample passivated for 30 minutes is closest to the sample which was field exposed for 18 months (table 1.b & 1.c).

The morphology of the oxide/hydroxide layer formed after passivation at 0.4V vs. SCE for 30 minutes is shown in fig 1.h and compares well with that of 18 months field exposed sample shown in fig.1.b.

After 18 month exposure at Digha Raman spectroscopy detected major peaks γ Fe₂O₃ (265.37 cm⁻¹), δ FeOOH (392.92 cm^{-1}) , γ FeOOH $(241.60 \text{ cm}^{-1} \text{ and } 1292.1 \text{ cm}^{-1})$, α Fe₂O₃ (491.01 cm^{-1}) (table 1.d). WS sample shows better corrosion resistance property due to the presence of δ FeOOH phase. But there is evidence on the presence of γ FeOOH phase on the WS. As the time of exposure is increased, there is a tendency of β FeOOH getting converted to y FeOOH and reduction of severity of corrosion environment. According to N.Sato, y FeOOH is the top layer of passive film as claimed by most investigators ¹⁵⁻¹⁶. Rust morphology of the laboratory simulated sample was also analyzed by Raman spectroscopy. The major phases are very similar to the on field exposed sample. The major phases are α FeOOH (302.07 cm⁻¹, & 687.82 cm⁻¹), δ FeOOH (392.84 cm⁻¹), α Fe₂O₃ (1319.01 cm⁻¹), γ Fe₂O₃ (395.69, 1425.63, 1422.78 cm⁻¹), γ FeOOH (313.94 cm⁻¹), β FeOOH (723.4 cm⁻¹) ¹) (Table 1.e). Laboratory accelerated corroded WS sample consist α FeOOH, which is formed from the first oxy hydroxide y FeOOH phase. These two phases are less protective against corrosion and further phase transformation takes place. β FeOOH phases present due to the presence of chloride ion present in the solution.

4. CONCLUSION

WS forms passive layers in Na₂SO₄ solution. Rust morphology and analysis of simulated weathering process on weathering steels compared well to field exposed weathering steels at Digha. Raman characterization of passivated WS panels showed the presence of γ FeOOH along with α Fe₂O₃, γ Fe₂O₃, δ FeOOH and α Fe₂O₃, α FeOOH, which are very similar to the rust of WS exposed after 18 months. Laboratory simulation by passivating weathering steel at 400 mV for 30 min was almost similar with the oxidation state of weathering steel exposed for 18 months at Digha with respect to Icorr & Ecorr values .It is thus concluded that laboratory simulation by passivating WS at 400 mV for 30 minutes, is almost similar with the oxidation state of WS



- 1. Panossian, Z.; Almeida, N.L.; Seixas, F.J. *Corrosão Atmosférica de Metais no Estado de São Paulo*, Boletim 57 IPT, São Paulo, 1991
- 2. J.K.Saha, Corrosion Constructional Steels In Marine & Industrial Environment:Frontter Work In Atmospheric Corrosion, USA, (Springer) (ISBN 978-81-322-0719-1)
- 3. M.Pourbaix, The Linear Bilogarithmic Law for Atmospheric Corrosion, Wiley, New York, (1982)
- 4. S.Feliu, M.Morcillo & Jr.S.Feliu, The Prediction of Atmospheric Corrosion from Meteorological and Pollution Parameters I: Annual Corrosion, Corrosion Science, 34(1993) p 403
- 5. S.Felik, M.Morcillo & Jr.S.Felik, The Prediction of Atmospheric Corrosion from Meteorological and Pollution Parameters II: Long Term Forecast, Corrosion Science, 34(1993) p 415
- 6. Misawa, T.; Hashimoto, K.; Shimodaira, S. "The Mechanism of Formation of Iron Oxide and Oxyhydroxides in Aqueous Solutions at Room Temperature", *Corr. Sci.*, v. 14, p. 131-149, 1974.
- 7. Misawa, T.; Yamashita, M.; Miyuki, H.; Nagano, H. Protective rust layer formed on weathering steel by atmospheric corrosion for a quarter of a century, *Journal of the Iron and Steel Institute of Japan*, v. 79, n. 1, p. 69-75, 1993.
- 8. Silva, S.V. Caracterização dos Produtos de Corrosão em Função da Composição Química de Aços Carbono, M.Sc. Dissertation, EPUSP, São Paulo-SP, Brazil, p. 125, 1999 (In Portuguese).
- 9. Marco, J.F.; Garcia, M.; Gancedo, J.R.; Martín-Luengo, M.A.; Joseph; G. *Characterization of the corrosion products formed on carbon steel after exposure to the open atmosphere in the Antarctic and Easter Island, Corr. Sci.*, v. 42, p. 753-771, 2000.
- 10. Raman, A.; Razvan, A.; Kuban, B.; Clement, K.A.; Graves, E. Characteristics of the Rust From Weathering Steels in Louisiana Bridge Spans, *Corrosion*, v. 42, n. 8, p. 447-455, 1986.
- 11. Oh, S.J.; Cook, D.C.; Townsend, H.E. Characterization of Iron Oxides Commonly Formed as Corrosion Productson Steel, *Hyperfine Interactions*, v. 112, p. 59-65,1998.
- 12. Ronda, M.; Gómez, J.; Leiva, P.; Ruiz, D.; Balmayor, M.; Navarro, A.; Laza, M.; Ibarra, E. Caracterización de los Productos de Corrosión del Acero Dulce Expuesto en un Ambiente Industrial-Costero Durante un Año, *Corrosão e Proteção de Materiais*, v. 16, n. 3, p. 30-34, 1997.
- 13. Oh, S.J.; Cook, D.C.; Carpio, J.J. Characterization of the Corrosion Products Formed on Carbon Steel in a Marine Environment, *Journal of the Korean Physical Society*, v. 36, n. 2, p. 106-110, 2000.
- 14. H.Kihira. S.Ito & T.Murata,. The Behavior of Phosphorous during Passivation of Weathering Steel by Protective Patina Formation, Corrosion Science, 31(1990) p 383-388