

WPI

Lecture 10

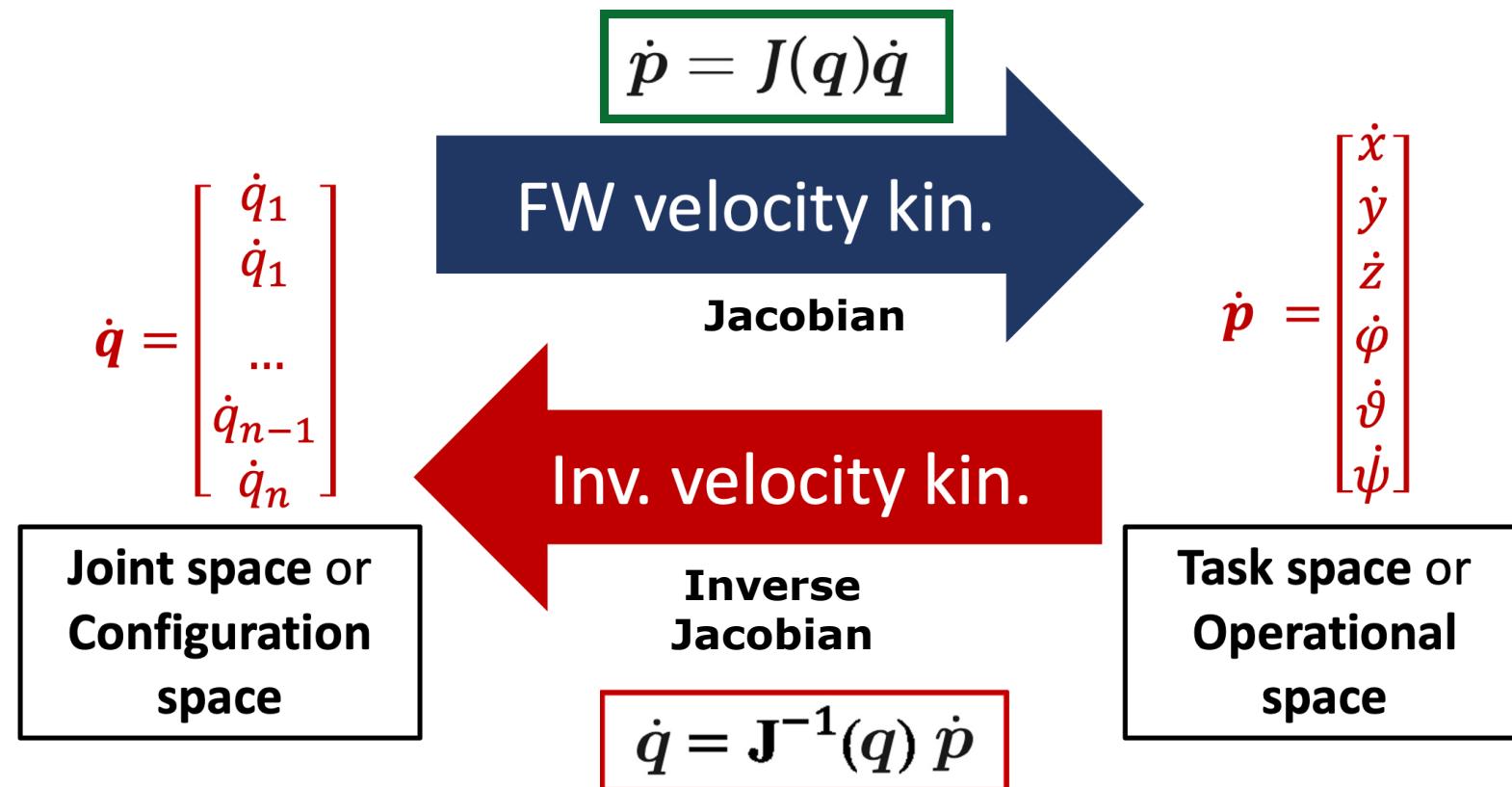
Cont. Differential Kinematics, Jacobian for under-and-over-actuated manipulators and Velocity Manipulability Ellipsoids

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Velocity (Differential) Kinematics

- Control the **velocity** of the **end effector**



How to calculate the Geometric Jacobian?

$$\mathbf{q} = \begin{bmatrix} q_1 \\ q_2 \\ \dots \\ q_{n-1} \\ q_n \end{bmatrix}$$
$$\mathbf{p} = \begin{bmatrix} x \\ y \\ z \\ \varphi \\ \vartheta \\ \psi \end{bmatrix}$$

- $\dot{\mathbf{p}} = \mathbf{J}(\mathbf{q})\dot{\mathbf{q}}$

- $\mathbf{J}(\mathbf{q}) = \begin{bmatrix} \mathbf{J}_p \\ \mathbf{J}_o \end{bmatrix} = \begin{bmatrix} \mathbf{J}_v \\ \mathbf{J}_\omega \end{bmatrix}$ $(3 \times n)$
 $(6 \times n)$

- $\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{\varphi} \\ \dot{\vartheta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} \mathbf{J}_p \\ \mathbf{J}_o \end{bmatrix} \dot{\mathbf{q}}$

How to calculate the Geometric Jacobian?

- Solve for Linear velocity and Angular velocity separately

- Linear
- Angular

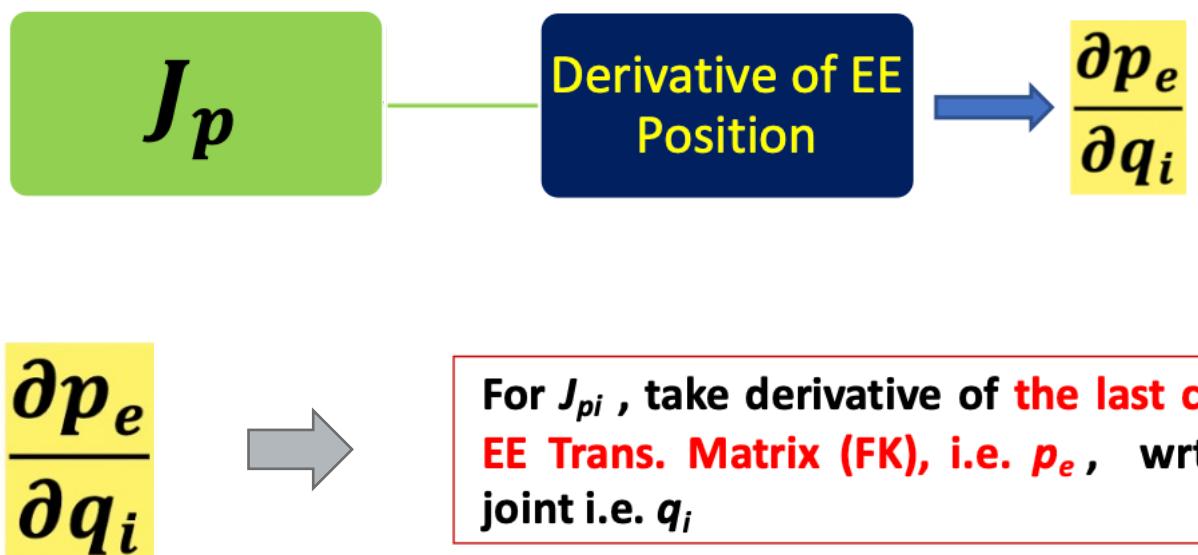
$$\dot{\mathbf{p}} = \mathbf{J}(\mathbf{q})\dot{\mathbf{q}}$$
$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} \mathbf{J}_p \\ \mathbf{J}_o \end{bmatrix} \begin{bmatrix} \dot{\mathbf{q}} \end{bmatrix}$$

(3 × n)

(3 × n)

How to calculate the Linear velocity J_p

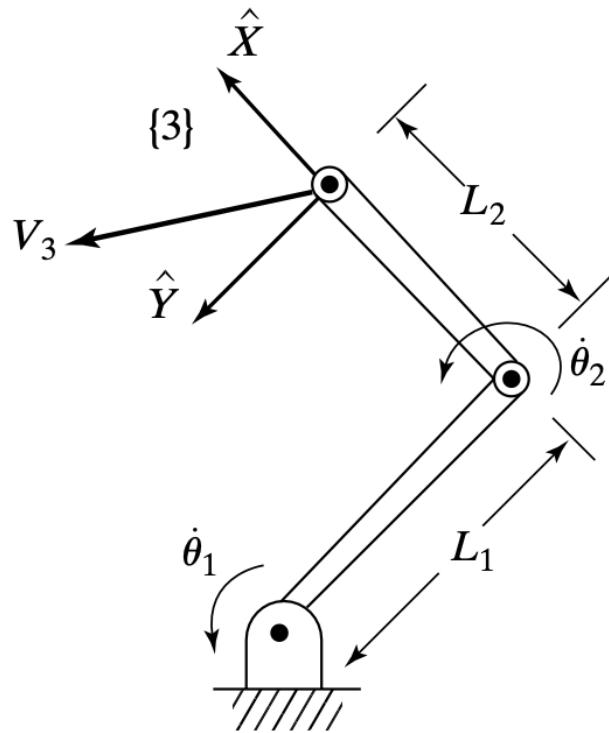
Procedure:



- Derive the Forward Kinematics (FK)
- Write position equations of the end-effector (p_e)
- Take derivative for velocity

For J_{pi} , take derivative of the last column of EE Trans. Matrix (FK), i.e. p_e , wrt the i -th joint i.e. q_i

How to calculate the Linear velocity J_p - Solution



$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} -l_1 \sin(\theta_1) - l_2 \sin(\theta_1 + \theta_2) & -l_2 \sin(\theta_1 + \theta_2) \\ l_1 \cos(\theta_1) + l_2 \cos(\theta_1 + \theta_2) & l_2 \cos(\theta_1 + \theta_2) \\ 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

3 x 2

6 x 2

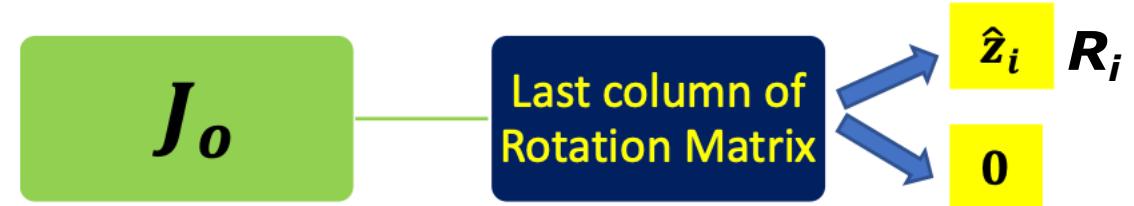
How to calculate the Angular velocity J_o

Procedure:

- Last column of Rotation Matrix

For J_{oi} , simply insert the last column of R

Note: if the i th column represents a prismatic joint, simply insert ZERO!



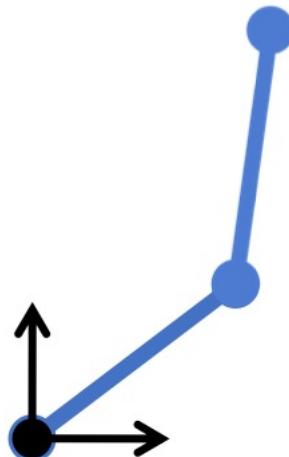
How to calculate the Angular velocity J_o - Solution

Procedure:

- Last column of Rotation Matrix

For J_{oi} , simply insert the last column of R

Note: if the i th column represents a prismatic joint, simply insert ZERO!



$$T_1^0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2^0 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1 c_1 \\ s_1 & c_1 & 0 & a_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



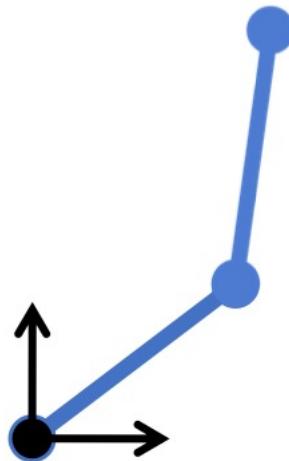
$$J = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} & -a_2 s_{12} \\ a_1 c_1 + a_2 c_{12} & a_2 c_{12} \\ 0 & 0 \end{bmatrix}$$

How to calculate the Angular velocity J_o - Solution

Procedure:

- Last column of Rotation Matrix

For J_{oi} , simply insert the last column of R
Note: if the i th column represents a prismatic joint, simply insert ZERO!



$$T_1^0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2^0 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1c_1 \\ s_1 & c_1 & 0 & a_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$J = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} \\ a_1c_1 + a_2c_{12} & a_2c_{12} \\ 0 & 0 \end{bmatrix}$$

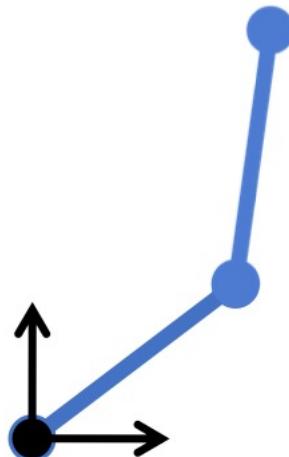
How to calculate the Angular velocity J_o - Solution

Procedure:

- Last column of Rotation Matrix

For J_{oi} , simply insert the last column of R

Note: if the i th column represents a prismatic joint, simply insert ZERO!



$$T_1^0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2^0 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1c_1 \\ s_1 & c_1 & 0 & a_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



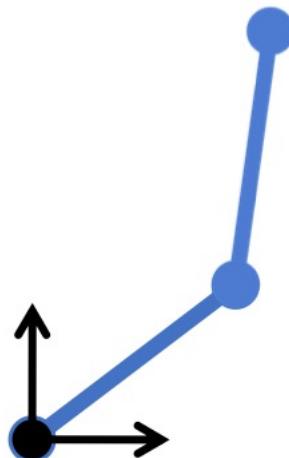
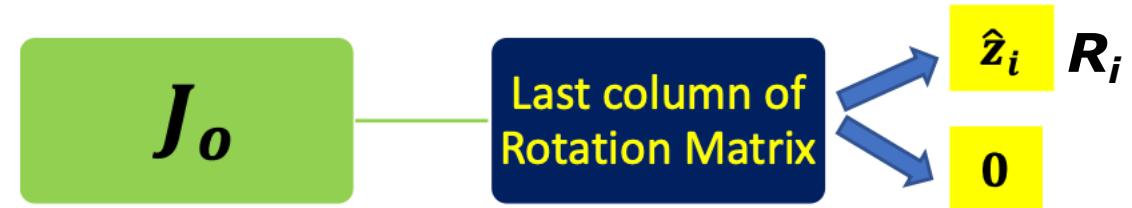
$$J = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} \\ a_1c_1 + a_2c_{12} & a_2c_{12} \\ 0 & 0 \end{bmatrix}$$

How to calculate the Angular velocity J_o - Solution

Procedure:

- Last column of Rotation Matrix

For J_{oi} , simply insert the last column of R
Note: if the i th column represents a prismatic joint, simply insert ZERO!

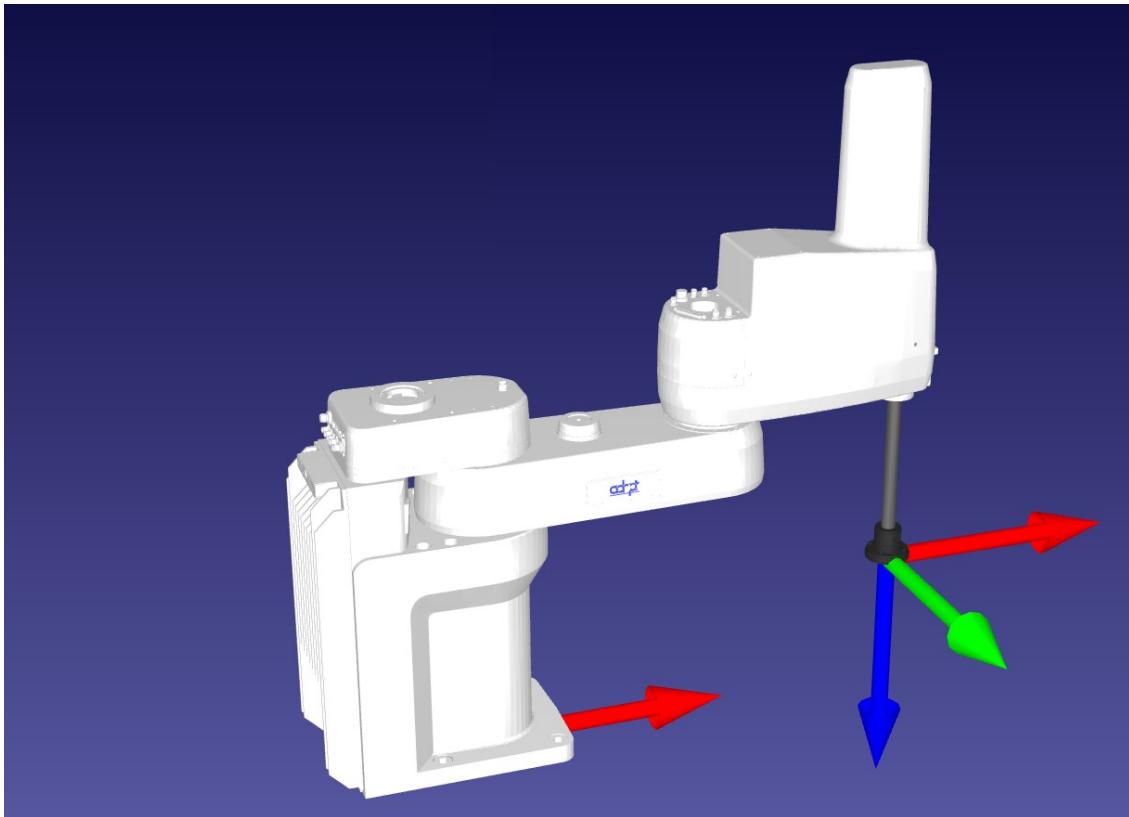


$$T_1^0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2^0 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1c_1 \\ s_1 & c_1 & 0 & a_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$J = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} \\ a_1c_1 + a_2c_{12} & a_2c_{12} \\ 0 & 0 \\ 0 & 1 \end{bmatrix}$$

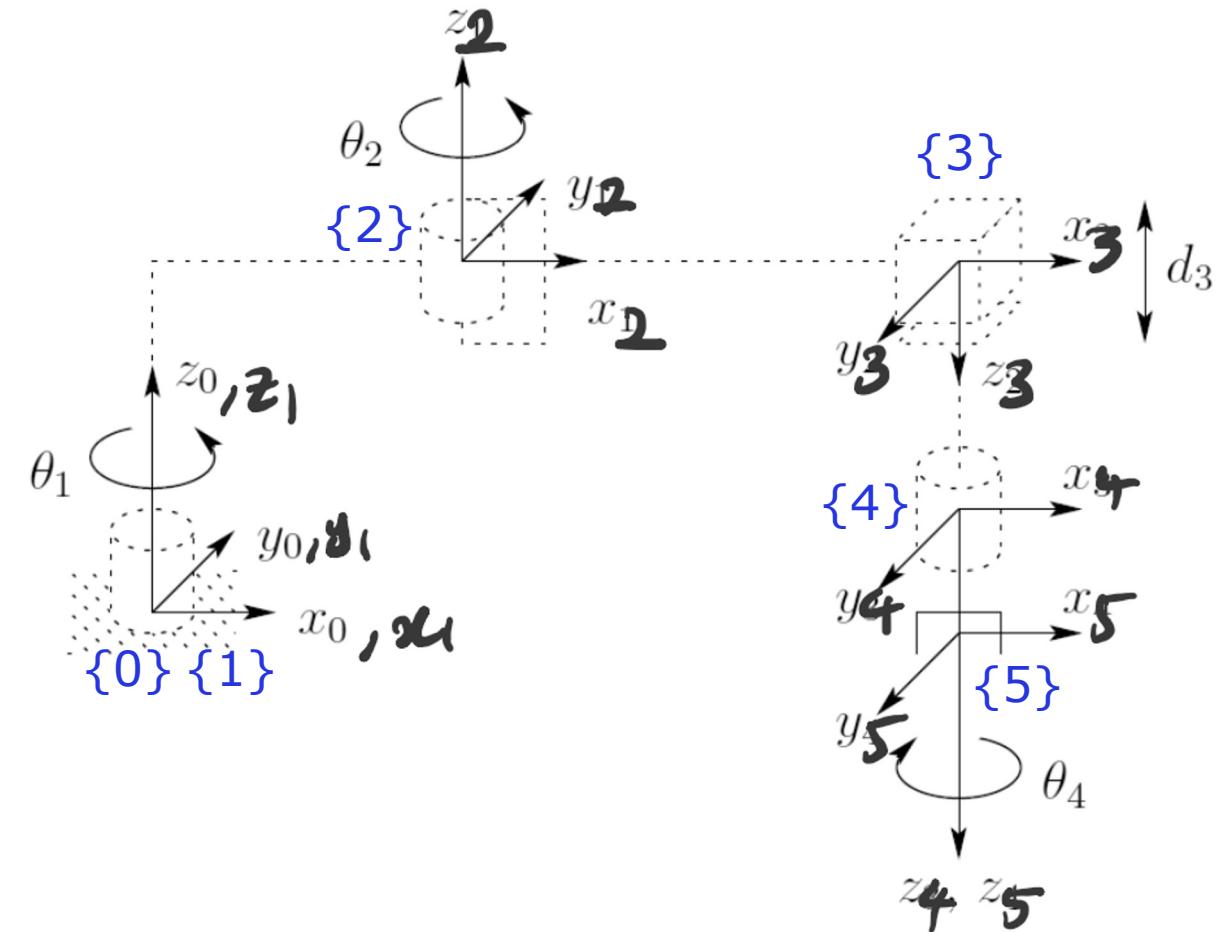
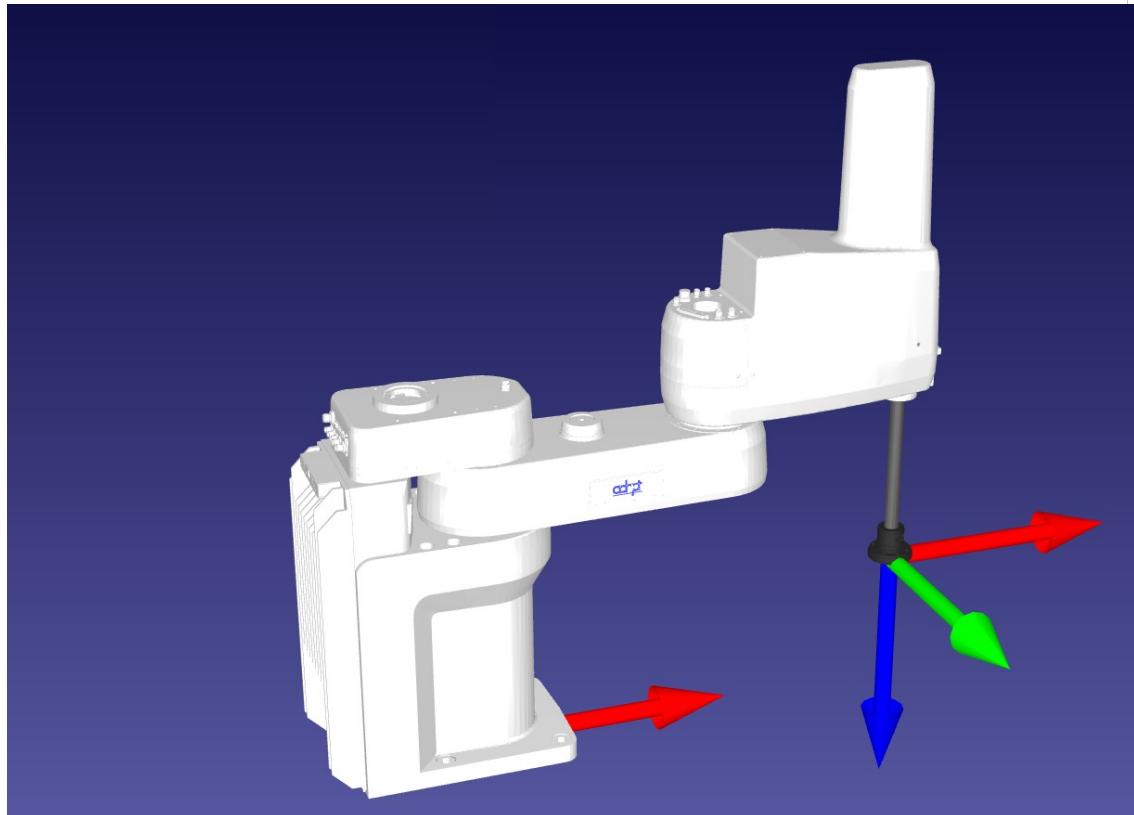
Adept Cobra s600



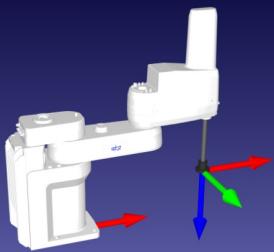
Specifications

Brand	Adept
Model	Cobra s600
Type	Scara Robot
Axes	4
Payload	2.0 kg
Reach	600 mm
Repeatability	0.018 mm
Weight	41 kg

J_p plus J_o for Cobra - Example 1

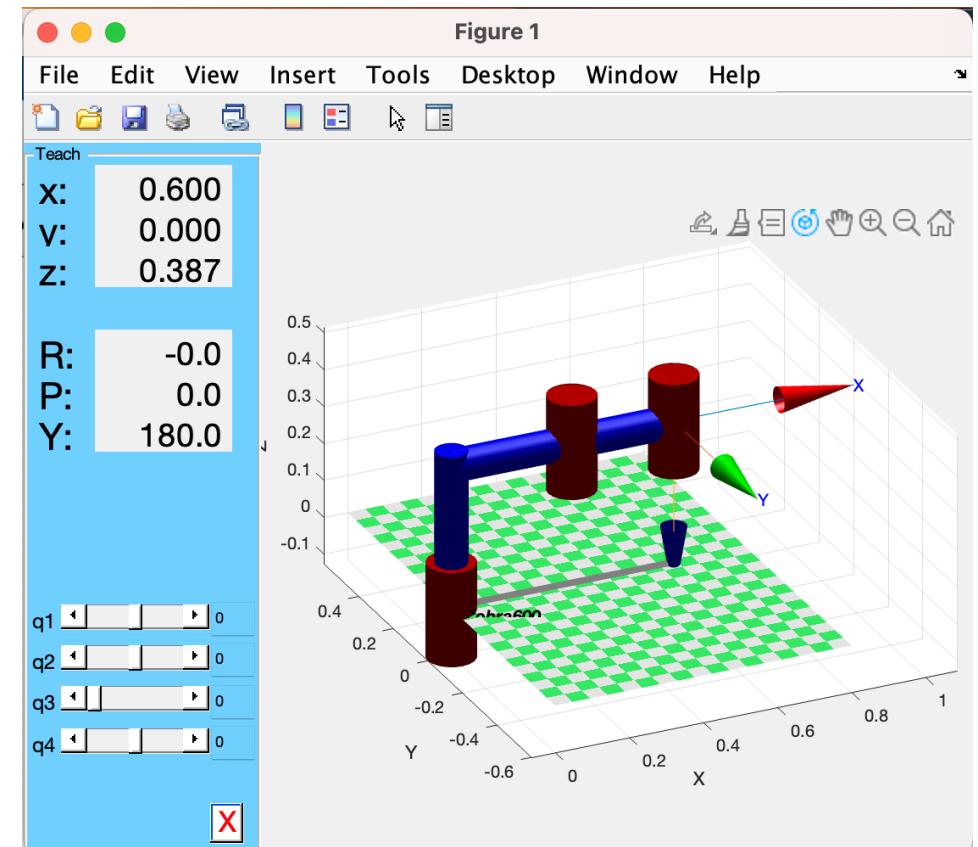


J_p plus J_o for Cobra - Example 1 - MATLAB

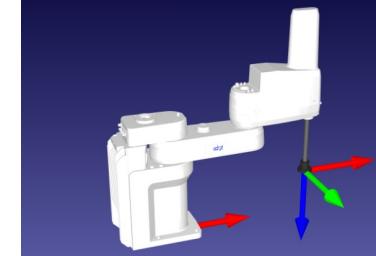


```
% Load SCARA robot  
mdl_cobra600  
c600  
c600.teach()
```

```
c600 =  
  
Cobra600 [Adept]::: 4 axis, RRPR, stdDH, slowRNE  
+-----+-----+-----+-----+  
| j | theta | d | a | alpha | offset |  
+-----+-----+-----+-----+  
| 1 | q1 | 0.387 | 0.325 | 0 | 0 |  
| 2 | q2 | 0 | 0.275 | 3.14159 | 0 |  
| 3 | 0 | q3 | 0 | 0 | 0 |  
| 4 | q4 | 0 | 0 | 0 | 0 |  
+-----+-----+-----+-----+
```



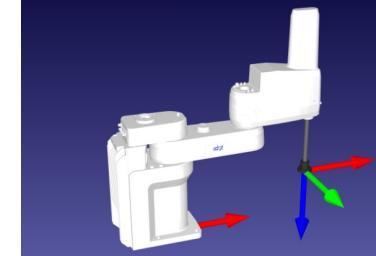
J_p plus J_o for Cobra - Example 1



$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & \boxed{a_1c_1 + a_2c_{12}} \\ s_{124} & c_{124} & 0 & \boxed{a_1s_1 + a_2s_{12}} \\ 0 & 0 & -1 & \boxed{-d_3 - d_4} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$J(q) = \left[\begin{array}{cccc} -a_1s_1 - a_2s_{12} & -a_2s_{12} & 0 & 0 \\ a_1c_1 + a_2c_{12} & a_2c_{12} & 0 & 0 \\ 0 & 0 & -1 & 0 \end{array} \right]$$

J_p plus J_o for Cobra - Example 1



$$T_1^0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} z_1$$

$$T_2^0 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1c_1 \\ s_1 & c_1 & 0 & a_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} z_2$$

$$T_3^0 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1c_1 + a_2c_{12} \\ s_{12} & c_{12} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

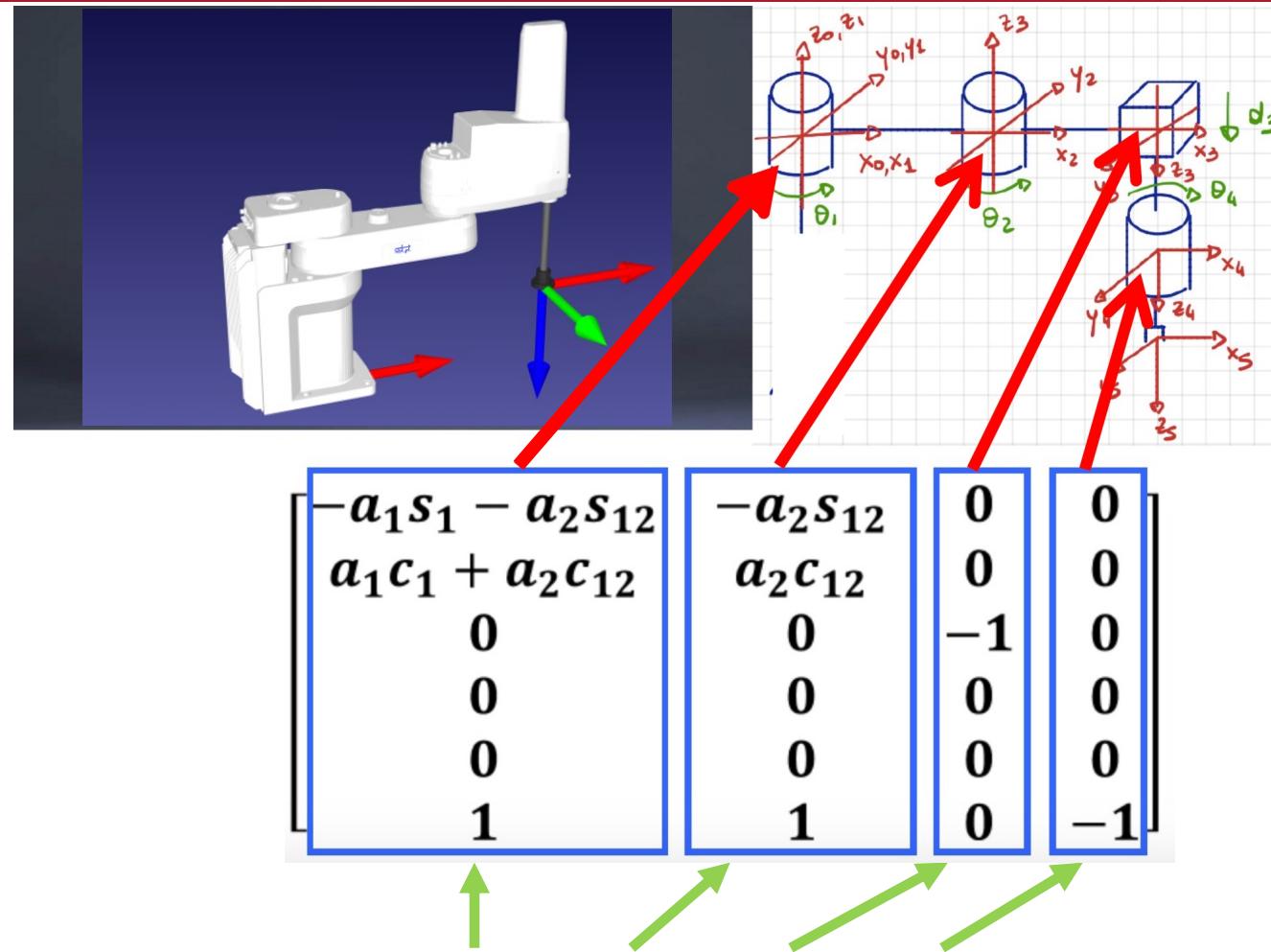
$$T_4^0 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1c_1 + a_2c_{12} \\ s_{12} & c_{12} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} z_4$$



$$J(q) = \left[\begin{array}{cccc} -a_1s_1 - a_2s_{12} & -a_2s_{12} & 0 & 0 \\ a_1c_1 + a_2c_{12} & a_2c_{12} & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{array} \right]$$

J_{o1} z₁
 J_{o2} z₂
 J_{o3} ≠ z₃ (prismatic)
 J_{o4} z₄

J_p plus J_o for Cobra - Example 1 - Full Jacobian



$$J = [J_1 \ J_2 \ J_3 \ J_4] = \begin{bmatrix} J_{p1} & J_{p2} & J_{p3} & J_{p4} \\ J_{o1} & J_{o2} & J_{o3} & J_{o4} \end{bmatrix} = \begin{bmatrix} J_p \\ J_o \end{bmatrix}$$

MATLAB

Full Jacobian of Cobra - Example 1

```
% Forward Kinematics  
syms q1 q2 d3 q4 real
```

```
FK = c600.fkine([q1 q2 d3 q4])
```

```
[ cos(q1 + q2 - q4),  sin(q1 + q2 - q4),  1.2246e-16*sin(q1 + q2),  0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]  
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2),  0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]  
[1.2246e-16*sin(q4),  1.2246e-16*cos(q4),  0,  0]  
[ 0,  0,  0,  1]
```

MATLAB

Full Jacobian of Cobra - Example 1

$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & a_1c_1 + a_2c_{12} \\ s_{124} & c_{124} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
% Forward Kinematics  
syms q1 q2 d3 q4 real  
  
FK = c600.fkine([q1 q2 d3 q4])
```

```
[ cos(q1 + q2 - q4), sin(q1 + q2 - q4), 1.2246e-16*sin(q1 + q2), 0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]  
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2), 0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]  
[1.2246e-16*sin(q4), 1.2246e-16*cos(q4), -1, 0.3870 - d3]  
[ 0, 0, 0, 1]
```

MATLAB

Full Jacobian of Cobra - Example 1

$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & a_1c_1 + a_2c_{12} \\ s_{124} & c_{124} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
% Forward Kinematics
syms q1 q2 d3 q4 real

FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t
```

```
[ cos(q1 + q2 - q4), sin(q1 + q2 - q4), 1.2246e-16*sin(q1 + q2), 0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2), 0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]
[1.2246e-16*sin(q4), 1.2246e-16*cos(q4),
[ 0, 0, -1,
[ 0, 0, 0, 0.3870 - d3]
[ 0, 0, 0, 1]
```

Pe =

```
0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)
0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)
0.3870 - d3
```

MATLAB

Full Jacobian of Cobra - Example 1

$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & a_1c_1 + a_2c_{12} \\ s_{124} & c_{124} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
% Forward Kinematics
syms q1 q2 d3 q4 real

FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t

% Jacobian
Jo = c600.jacob0([q1 q2 d3 q4])
```

```

J0 = [cos(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) - 1.2246e-16*sin(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) - sin(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)), [1.2246e-16*cos(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) + cos(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + sin(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)), [3.9801e-17*cos(q2) - 1.2246e-16*cos(q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + 1.2246e-16*sin(q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) + 3.3678e-17, [1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4), [1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4), [1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,

```

$$\begin{bmatrix} -a_1 s_1 - a_2 s_{12} \\ a_1 c_1 + a_2 c_{12} \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$J = [J_1$$

MATLAB

Full Jacobian of Cobra - Example 1

$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & a_1c_1 + a_2c_{12} \\ s_{124} & c_{124} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
% Forward Kinematics
syms q1 q2 d3 q4 real

FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t

% Jacobian
Jo = c600.jacob0([q1 q2 d3 q4])
```

```
[ cos(q1 + q2 - q4), sin(q1 + q2 - q4), 1.2246e-16*sin(q1 + q2), 0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2), 0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]
[ 1.2246e-16*sin(q4), 1.2246e-16*cos(q4), -1, 0.3870 - d3]
[ 0, 0, 0, 1]
```

Pe =

```
0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)
0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)
0.3870 - d3
```

```
Jo =
[cos(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) - 1.2246e-16*sin(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) - sin(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)),
[1.2246e-16*cos(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) + cos(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + sin(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)),
[ 3.9801e-17*cos(q2) - 1.2246e-16*cos(q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + 1.2246e-16*sin(q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) + 3.3678e-17,
[ 1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
[ 1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
[ 1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

```
- 4.1243e-33*sin(q1 + q2) - cos(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)) - sin(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)),
4.1243e-33*cos(q1 + q2) + cos(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - sin(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)),
3.3678e-17 - 1.2246e-16*cos(q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - 1.2246e-16*sin(q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)),
1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

$$J = [J_1 \quad J_2]$$

$$\begin{bmatrix} -a_1s_1 - a_2s_{12} \\ a_1c_1 + a_2c_{12} \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} \quad \begin{bmatrix} -a_2s_{12} \\ a_2c_{12} \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

MATLAB

Full Jacobian of Cobra - Example 1

$$T_5^0 = \begin{bmatrix} c_{124} & -s_{124} & 0 & a_1c_1 + a_2c_{12} \\ s_{124} & c_{124} & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
% Forward Kinematics
syms q1 q2 d3 q4 real
```

```
FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t
```

```
% Jacobian
```

```
Jo = c600.jacob0([q1 q2 d3 q4])
```

```
[ cos(q1 + q2 - q4), sin(q1 + q2 - q4), 1.2246e-16*sin(q1 + q2), 0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2), 0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]
[ 1.2246e-16*sin(q4), 1.2246e-16*cos(q4), -1, 0.3870 - d3]
[ 0, 0, 0, 1]
```

Pe =

$$\frac{0.2750*\cos(q1 + q2) + 0.3250*\cos(q1) + 1.2246e-16*d3*\sin(q1 + q2)}{0.2750*\sin(q1 + q2) + 0.3250*\sin(q1) - 1.2246e-16*d3*\cos(q1 + q2)}$$

$$\frac{}{0.3870 - d3}$$

Jo =

```
[cos(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) - 1.2246e-16*sin(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) - sin(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)),
[1.2246e-16*cos(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) + cos(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + sin(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)),
[ 3.9801e-17*cos(q2) - 1.2246e-16*cos(q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + 1.2246e-16*sin(q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) + 3.3678e-17,
[ 1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
[ 1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
[ 1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

```
- 4.1243e-33*sin(q1 + q2) - cos(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)) - sin(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)), 1.2246e-16*sin(q1 + q2),
4.1243e-33*cos(q1 + q2) + cos(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - sin(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)), -1.2246e-16*cos(q1 + q2),
3.3678e-17 - 1.2246e-16*cos(q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - 1.2246e-16*sin(q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)),
1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

$$J = [J_1 \quad J_2 \quad J_3]$$

$$\begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} & 0 \\ a_1c_1 + a_2c_{12} & a_2c_{12} & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 0 \end{bmatrix}$$

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```
% Forward Kinematics
syms q1 q2 d3 q4 real

FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t

% Jacobian
Jo = c600.jacob0([q1 q2 d3 q4])
```

$$\begin{aligned} & [\cos(q_1 + q_2 - q_4), \sin(q_1 + q_2 - q_4), 1.2246e-16\sin(q_1 + q_2), 0.2750\cos(q_1 + q_2) + 0.3250\cos(q_1) + 1.2246e-16d_3\sin(q_1 + q_2)] \\ & [\sin(q_1 + q_2 - q_4), -\cos(q_1 + q_2 - q_4), -1.2246e-16\cos(q_1 + q_2), 0.2750\sin(q_1 + q_2) + 0.3250\sin(q_1) - 1.2246e-16d_3\cos(q_1 + q_2)] \\ & [1.2246e-16\sin(q_4), 1.2246e-16\cos(q_4), -1, \\ & [0, 0, 0, 0], 0.3870 - d_3] \end{aligned}$$

Pe =

$$\begin{aligned} & 0.2750\cos(q_1 + q_2) + 0.3250\cos(q_1) + 1.2246e-16d_3\sin(q_1 + q_2) \\ & 0.2750\sin(q_1 + q_2) + 0.3250\sin(q_1) - 1.2246e-16d_3\cos(q_1 + q_2) \\ & 0.3870 - d_3 \end{aligned}$$

Jo =

$$\begin{aligned} & [\cos(q_1 + q_2 - q_4)*(0.3250\sin(q_2 - q_4) - 0.2750\sin(q_4) + 1.2246e-16d_3\cos(q_4)) - 1.2246e-16\sin(q_1 + q_2)*(3.9801e-17\cos(q_2) + 3.3678e-17) - \sin(q_1 + q_2 - q_4)*(0.3250\cos(q_2 - q_4) + 0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)), \\ & 1.2246e-16\cos(q_1 + q_2)*(3.9801e-17\cos(q_2) + 3.3678e-17) + \cos(q_1 + q_2 - q_4)*(0.3250\cos(q_2 - q_4) + 0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)) + \sin(q_1 + q_2 - q_4)*(0.3250\sin(q_2 - q_4) - 0.2750\sin(q_4) + 1.2246e-16d_3\cos(q_4)), \\ & [3.9801e-17\cos(q_2) - 1.2246e-16\cos(q_4)*(0.3250\cos(q_2 - q_4) + 0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)) + 1.2246e-16\sin(q_4)*(0.3250\sin(q_2 - q_4) - 0.2750\sin(q_4) + 1.2246e-16d_3\cos(q_4)) + 3.3678e-17, \\ & 1.2246e-16\cos(q_1 + q_2 - q_4)*\sin(q_4) - 1.2246e-16\sin(q_1 + q_2) + 1.2246e-16\sin(q_1 + q_2 - q_4)*\cos(q_4), \\ & [1.2246e-16\cos(q_1 + q_2) - 1.2246e-16\cos(q_1 + q_2 - q_4)*\cos(q_4) + 1.2246e-16\sin(q_1 + q_2 - q_4)*\sin(q_4), \\ & 1.4998e-32*\cos(q_4)^2 + 1.4998e-32*\sin(q_4)^2 + 1, \\ & [-4.1243e-33\sin(q_1 + q_2) - \cos(q_1 + q_2 - q_4)*(0.2750\sin(q_4) - 1.2246e-16d_3\cos(q_4)) - \sin(q_1 + q_2 - q_4)*(0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)), 1.2246e-16\sin(q_1 + q_2), \\ & 4.1243e-33\cos(q_1 + q_2) + \cos(q_1 + q_2 - q_4)*(0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)) - \sin(q_1 + q_2 - q_4)*(0.2750\sin(q_4) - 1.2246e-16d_3\cos(q_4)), -1.2246e-16\cos(q_1 + q_2), \\ & 3.3678e-17 - 1.2246e-16\cos(q_4)*(0.2750\cos(q_4) + 1.2246e-16d_3\sin(q_4)) - 1.2246e-16\sin(q_4)*(0.2750\sin(q_4) - 1.2246e-16d_3\cos(q_4)), -1, \\ & 1.2246e-16\cos(q_1 + q_2 - q_4)*\sin(q_4) - 1.2246e-16\sin(q_1 + q_2) + 1.2246e-16\sin(q_1 + q_2 - q_4)*\cos(q_4), 0, 1.2246e-16\sin(q_1 + q_2)], \\ & 1.2246e-16\cos(q_1 + q_2) - 1.2246e-16\cos(q_1 + q_2 - q_4)*\cos(q_4) + 1.2246e-16\sin(q_1 + q_2 - q_4)*\sin(q_4), 0, -1.2246e-16\cos(q_1 + q_2)], \\ & 1.4998e-32*\cos(q_4)^2 + 1.4998e-32*\sin(q_4)^2 + 1, 0, -1] \end{aligned}$$

$$J = [J_1 \ J_2 \ J_3 \ J_4] = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} & 0 & 0 \\ a_1c_1 + a_2c_{12} & a_2c_{12} & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 1 & 0 & -1 \end{bmatrix}$$

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% Forward Kinematics
syms q1 q2 d3 q4 real
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```
FK = c600.fkine([q1 q2 d3 q4])
Pe = FK.t
```

```
% Jacobian
```

```
Jo = c600.jacob0([q1 q2 d3 q4])
```

```
[ cos(q1 + q2 - q4), sin(q1 + q2 - q4), 1.2246e-16*sin(q1 + q2), 0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)]
[ sin(q1 + q2 - q4), -cos(q1 + q2 - q4), -1.2246e-16*cos(q1 + q2), 0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)]
[ 1.2246e-16*sin(q4), 1.2246e-16*cos(q4), -1, 0.3870 - d3]
[ 0, 0, 0, 1]

Pe =
0.2750*cos(q1 + q2) + 0.3250*cos(q1) + 1.2246e-16*d3*sin(q1 + q2)
0.2750*sin(q1 + q2) + 0.3250*sin(q1) - 1.2246e-16*d3*cos(q1 + q2)
0.3870 - d3
```

Jo =

```
[cos(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) - 1.2246e-16*sin(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) - sin(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)),
[1.2246e-16*cos(q1 + q2)*(3.9801e-17*cos(q2) + 3.3678e-17) + cos(q1 + q2 - q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + sin(q1 + q2 - q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)),
[ 3.9801e-17*cos(q2) - 1.2246e-16*cos(q4)*(0.3250*cos(q2 - q4) + 0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) + 1.2246e-16*sin(q4)*(0.3250*sin(q2 - q4) - 0.2750*sin(q4) + 1.2246e-16*d3*cos(q4)) + 3.3678e-17,
[ 1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
[ 1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
[ 1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

```
- 4.1243e-33*sin(q1 + q2) - cos(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)) - sin(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)), 1.2246e-16*sin(q1 + q2),
[ 4.1243e-33*cos(q1 + q2) + cos(q1 + q2 - q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - sin(q1 + q2 - q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)), -1.2246e-16*cos(q1 + q2),
[ 3.3678e-17 - 1.2246e-16*cos(q4)*(0.2750*cos(q4) + 1.2246e-16*d3*sin(q4)) - 1.2246e-16*sin(q4)*(0.2750*sin(q4) - 1.2246e-16*d3*cos(q4)),
[ 1.2246e-16*cos(q1 + q2 - q4)*sin(q4) - 1.2246e-16*sin(q1 + q2) + 1.2246e-16*sin(q1 + q2 - q4)*cos(q4),
[ 1.2246e-16*cos(q1 + q2) - 1.2246e-16*cos(q1 + q2 - q4)*cos(q4) + 1.2246e-16*sin(q1 + q2 - q4)*sin(q4),
[ 1.4998e-32*cos(q4)^2 + 1.4998e-32*sin(q4)^2 + 1,
```

$$J = [J_1 \ J_2 \ J_3 \ J_4] = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} & 0 & 0 \\ a_1c_1 + a_2c_{12} & a_2c_{12} & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 1 & 0 & -1 \end{bmatrix}$$

NOTE : A lot of terms are equal to zero in the equation (Jo) above

Recap: Geometric Jacobian

- For a robotic manipulator, the Jacobian is a $6 \times n$ matrix, where n is the number of joints:

$$J = [J_1 \ J_2 \ J_3 \ J_4] = \begin{bmatrix} J_{p1} & J_{p2} & J_{p3} & J_{p4} \\ J_{o1} & J_{o2} & J_{o3} & J_{o4} \end{bmatrix} = \begin{bmatrix} J_p \\ J_o \end{bmatrix}$$

- We Solve Jacobian for each joint i.e., each column
- We Solve for Position (J_p i.e., upper half) Separately
- We Solve for Orientation (J_o i.e., lower half) Separately



Under / Fully / Over - actuated manipulator

$$\nu = \begin{bmatrix} J(q) \\ \dot{q} \end{bmatrix}$$

uncontrollable d.o.f.
 $N < 6$
under-actuated

$$\nu = \begin{bmatrix} J(q) \\ \dot{q} \end{bmatrix}$$

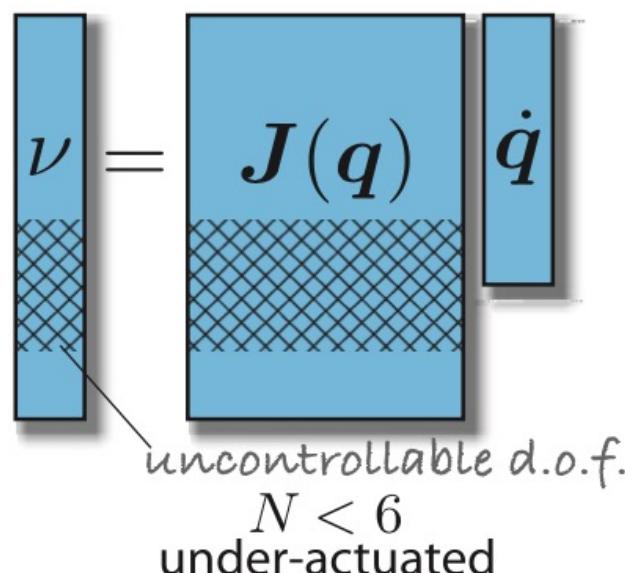
$N = 6$
fully-actuated

$$\nu = \begin{bmatrix} J(q) \\ \text{locked joints} \\ \dot{q} \end{bmatrix}$$

$N > 6$
over-actuated

Jacobian for under-actuated manipulator

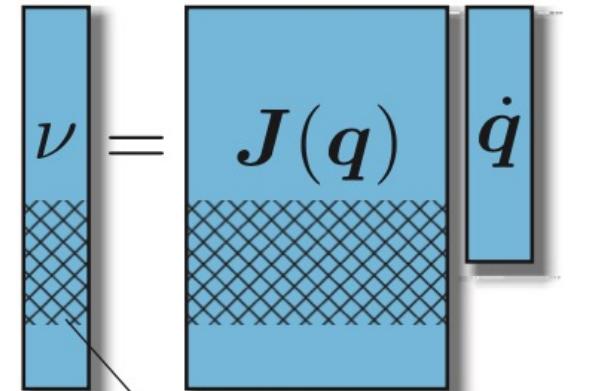
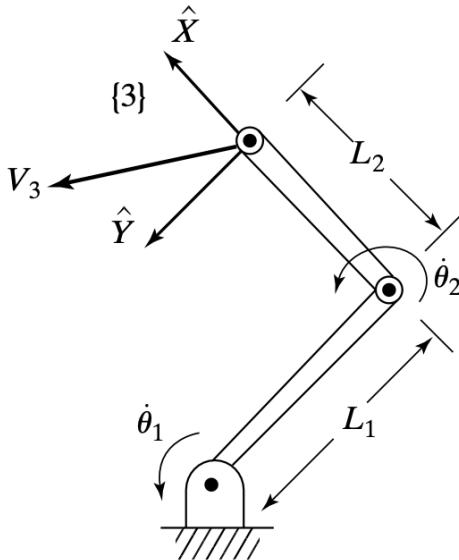
- An under-actuated robot has $N < 6$, and a Jacobian that is taller than it is wide.
- The system of equations is under-constrained but the system can be *squared up* by deleting some rows of v and J
 - accepting that some Cartesian degrees of freedom are not controllable given the low number of joints



Jacobian for under-Actuated “RR” - Example 2

$$\dot{q} = J(q)^{-1} \nu$$

```
>> mdl_planar2  
>> qn = [1 1];  
  
>> J = p2.jacob0(qn)  
J =  
-1.7508 -0.9093  
0.1242 -0.4161  
0 0  
0 0  
0 0  
1.0000 1.0000
```



```
>> qd = pinv(J) * [0.1 0 0 0 0 0]'  
qd =  
-0.0698  
0.0431
```

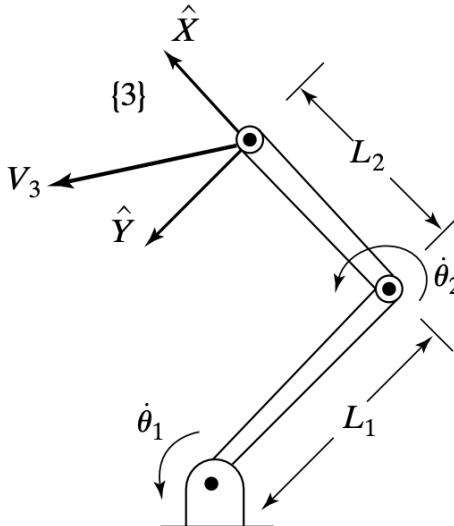
```
>> xd = J*qd;  
>> xd'  
ans =  
0.0829 -0.0266 0 0 0 -0.0266
```

Jacobian for under-Actuated “RR” - Example 2

$$\begin{pmatrix} \nu_x \\ \nu_y \\ \nu_z \\ \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} J_{xy} \\ J_0 \end{pmatrix} \begin{pmatrix} \dot{q}_1 \\ \dot{q}_2 \end{pmatrix}$$

$$\dot{\mathbf{q}} = \mathbf{J}(\mathbf{q})^{-1} \boldsymbol{\nu}$$

$${}^0 \boldsymbol{\nu} = {}^0 \mathbf{J}(\mathbf{q}) \dot{\mathbf{q}}$$



$$\begin{pmatrix} \nu_x \\ \nu_y \end{pmatrix} = J_{xy} \begin{pmatrix} \dot{q}_1 \\ \dot{q}_2 \end{pmatrix}$$

$$\begin{pmatrix} \dot{q}_1 \\ \dot{q}_2 \end{pmatrix} = J_{xy}^{-1} \begin{pmatrix} \nu_x \\ \nu_y \end{pmatrix}$$

```
>> Jxy = J(1:2,:);
>> qd = inv(Jxy) * [0.1 0]';
qd =
-0.0495
-0.0148
>> xd = J*qd;
>> xd'
ans =
0.1000    0.0000
```

$$\boldsymbol{\nu} = \begin{pmatrix} \mathbf{J}(\mathbf{q}) & \dot{\mathbf{q}} \end{pmatrix}$$

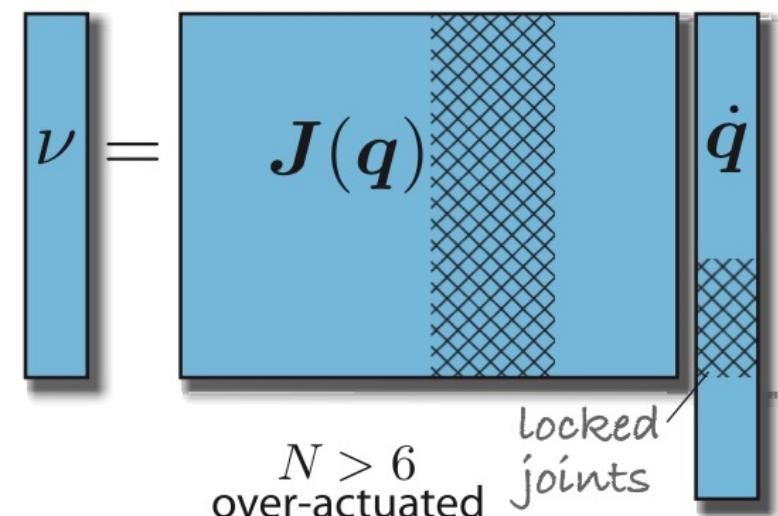
uncontrollable d.o.f.
 $N < 6$
under-actuated

0 0 -0.0642

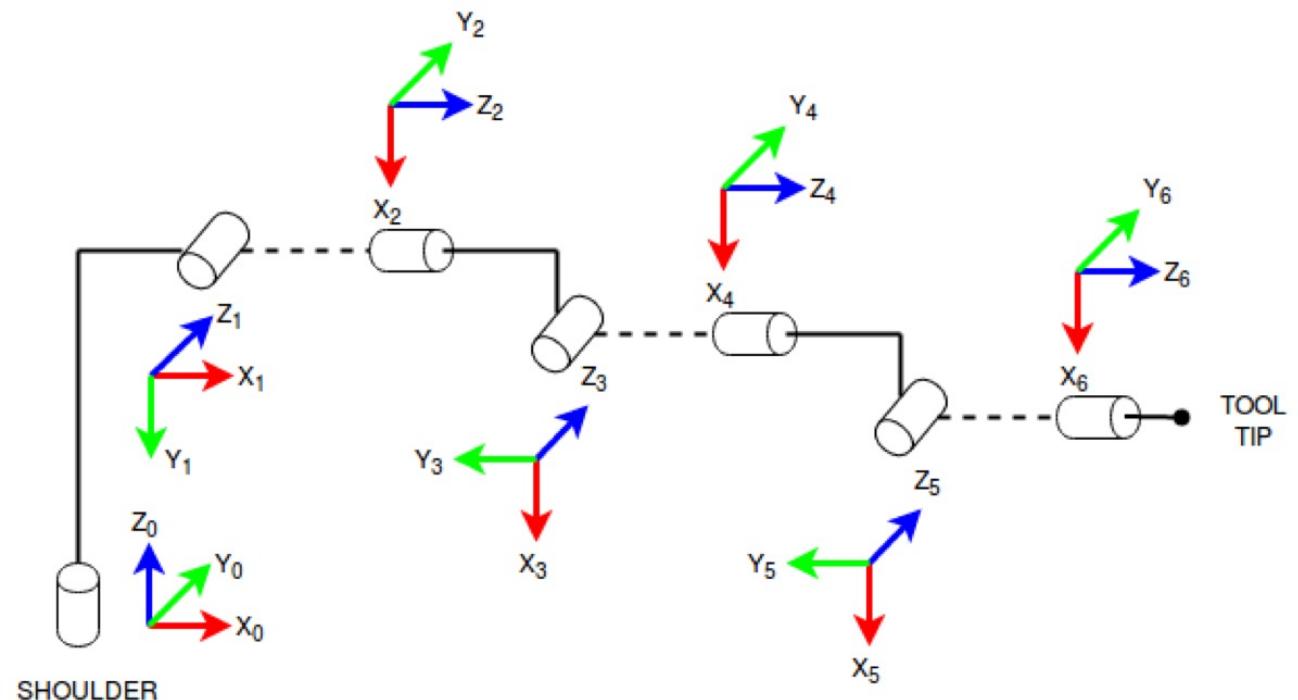
Over-actuated “Redundant” manipulators

- An over-actuated or redundant robot has $N > 6$, and a Jacobian that is wider than it is tall
- The system of equations is under-constrained and the best we can do is find a least-squares solution. Alternatively, we can *square up* the Jacobian to make it invertible by deleting some columns – effectively *locking* the corresponding joints

- $\dot{q} = J(q)^{-1} \nu$
↓
- $\dot{q} = J(q)^+ \nu$
↓
- $\dot{q} = \underbrace{J(q)^+ \nu}_{\text{end-effector motion}} + \underbrace{N N^+ \dot{q}_{\text{null}}}_{\text{null-space motion}}$



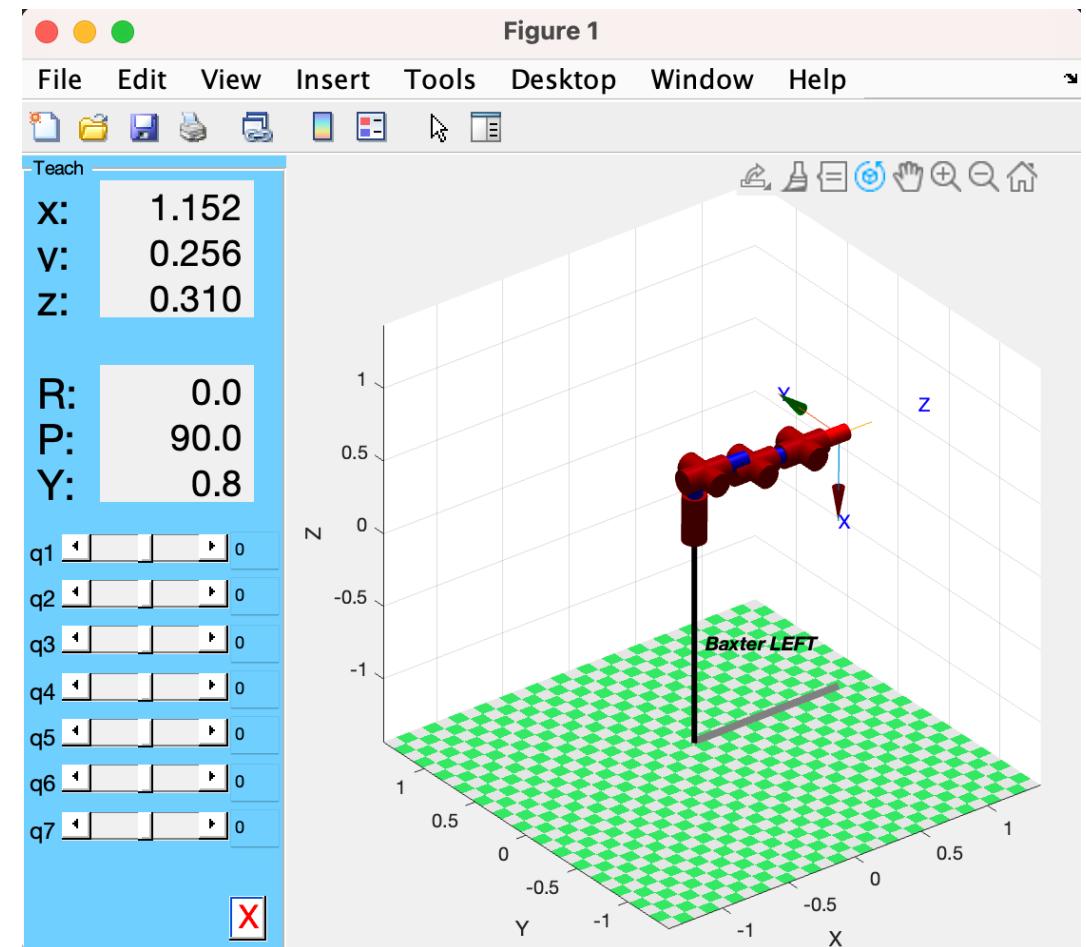
Baxter (7 DoF)



Baxter (7 DoF) - Robotics Toolbox (RTB)

```
>> mdl_baxter  
>> TE = SE3(0.8, 0.2, -0.2) * SE3.Ry(pi);  
>> q = left.ikine(TE)
```

```
>> J = jacob0(left, q);  
>> about J  
J [double] : 6x7 (336 bytes)
```



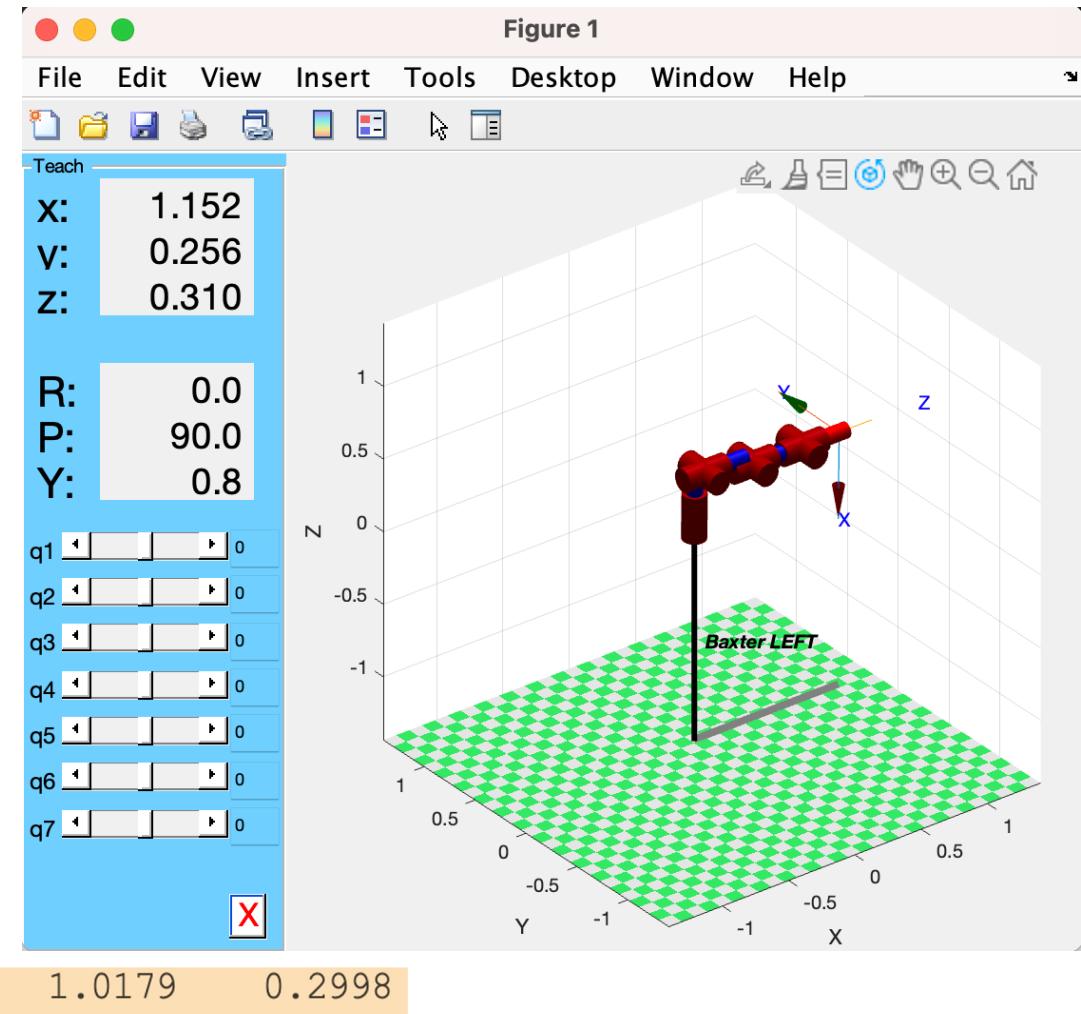
Jacobian for Over-actuated “Baxter” - Example 3

```
>> mdl_baxter  
>> TE = SE3(0.8, 0.2, -0.2) * SE3.Ry(pi);  
>> q = left.ikine(TE)
```

```
>> J = jacob0(left, q);  
>> about J  
J [double] : 6x7 (336 bytes)
```

```
>> xd = [0.2 0.2 0.2 0 0 0]';  
>> qd = pinv(J) * xd;  
>> qd'  
ans =  
0.0895 -0.0464 -0.4259 0.6980 -0.4248 1.0179 0.2998
```

$$\dot{q} = J(q)^+ \nu$$



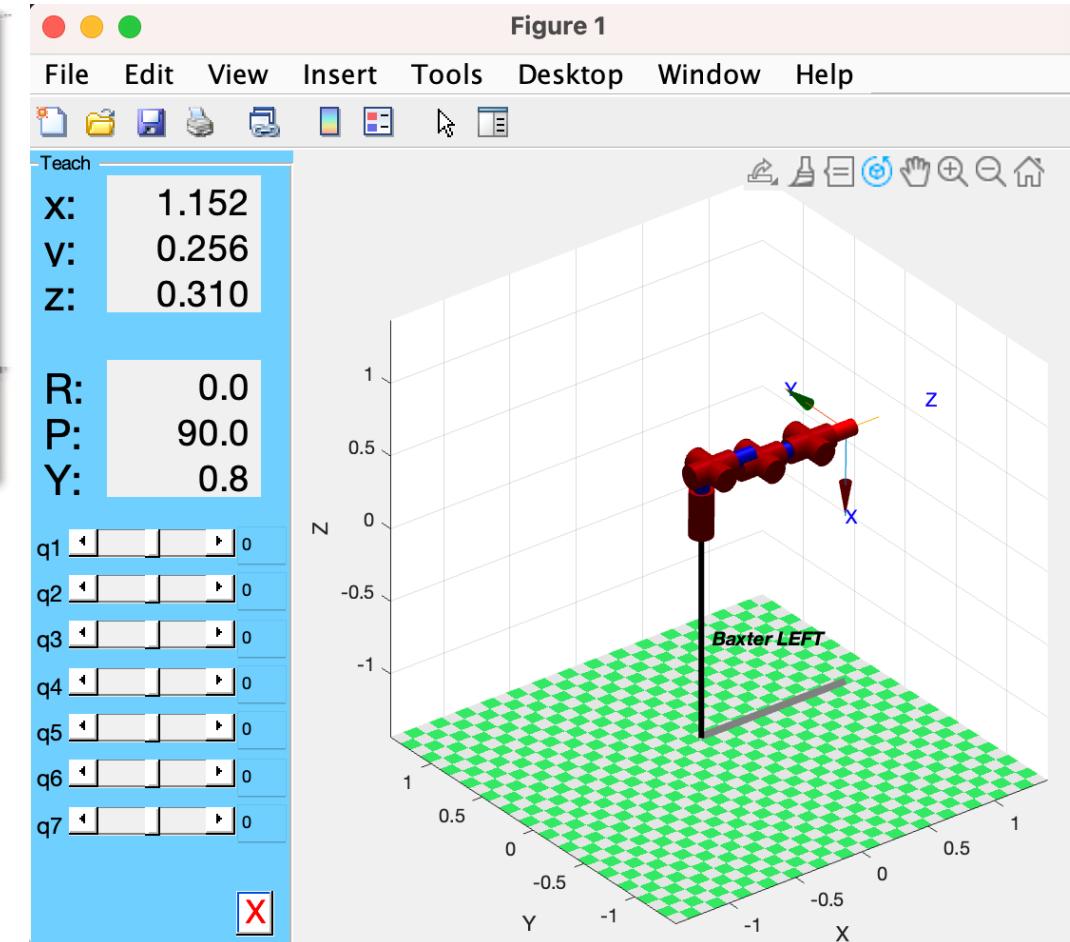
Jacobian for Over-actuated “Baxter” - Example 3

```
>> rank(J)
ans =
6
```

```
>> N = null(J)
N =
-0.2244
-0.1306
0.6018
0.0371
-0.7243
0.0653
0.2005
```

$$\nu = \begin{matrix} J(q) \\ \vdots \end{matrix}$$

*N > 6
over-actuated* *locked joints*



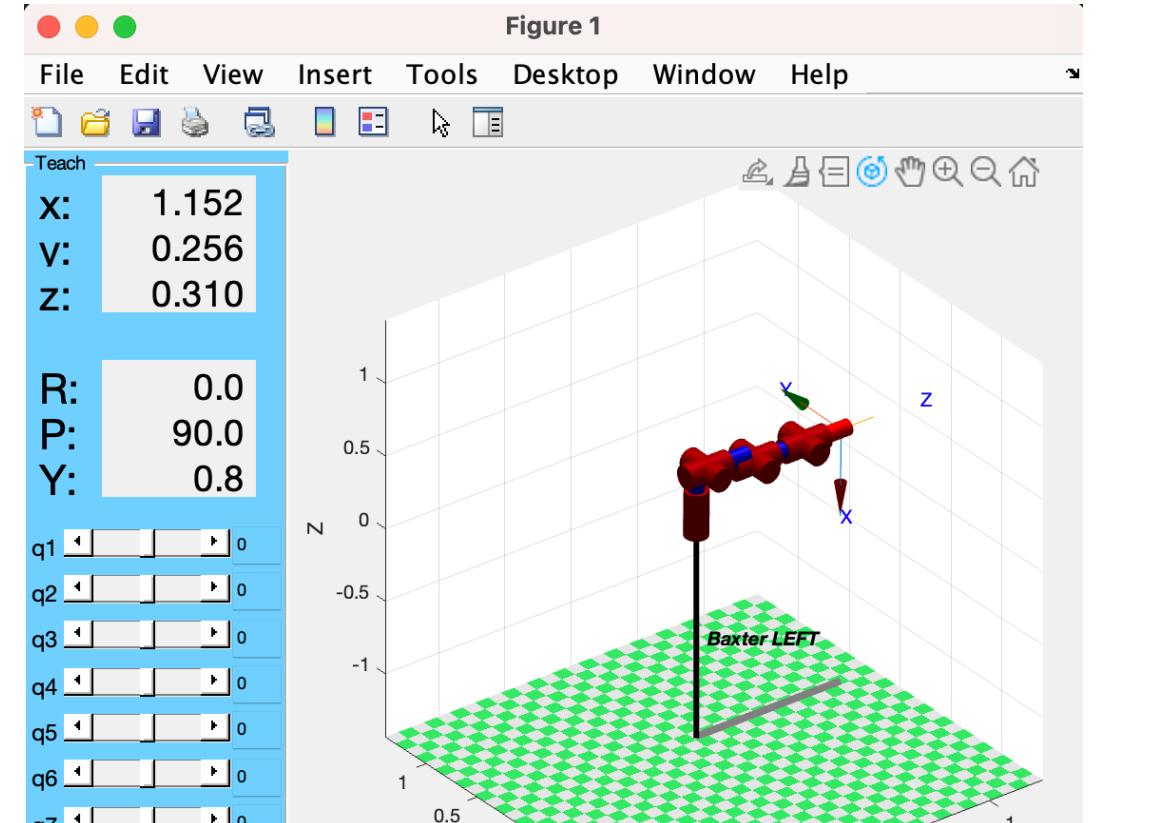
Jacobian for Over-actuated “Baxter” - Example 3

```
>> norm( J * N(:,1))  
ans =  
2.6004e-16
```

$$\dot{q} = \underbrace{J(q)^+ \nu}_{\text{end-effector motion}} + \underbrace{NN^+ \dot{q}_{\text{null}}}_{\text{null-space motion}}$$

```
>> qd_null = [0 0 0 0 1 0 0]';
```

```
>> qp = N * pinv(N) * qd_null;  
>> qp'  
0.1625 0.0946 -0.4359 -0.0269 0.5246 -0.0473 -0.1452
```

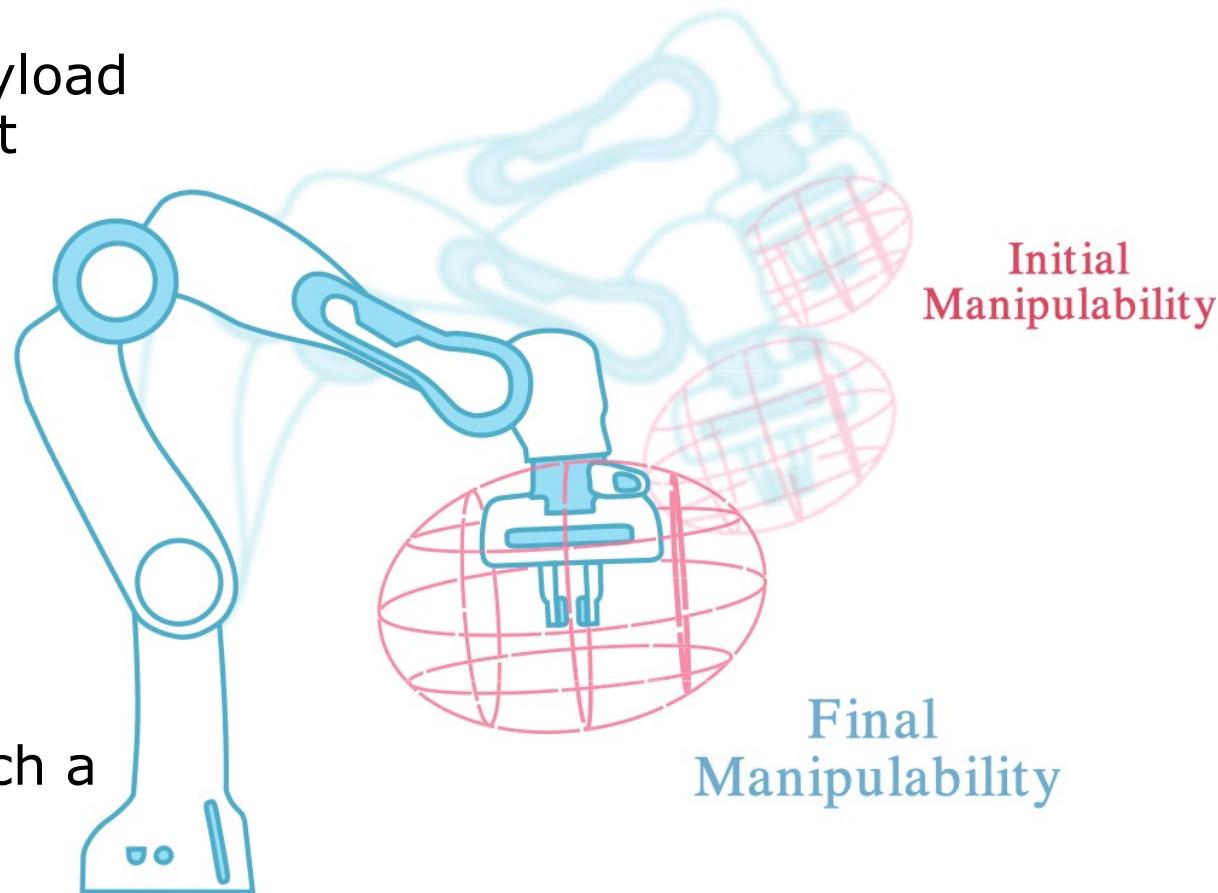


```
>> norm( J * qp)  
ans =  
1.9541e-16
```



Manipulability

- Ability to move and control the tool or payload attached to the end of the arm in different directions and orientations
- Quantifies how effectively the robot can manipulate objects within its workspace
- Influenced by several factors:
 - kinematics
 - dynamics
 - joint configuration
- A highly manipulable robotic arm can reach a wide range of positions and orientations



Manipulability

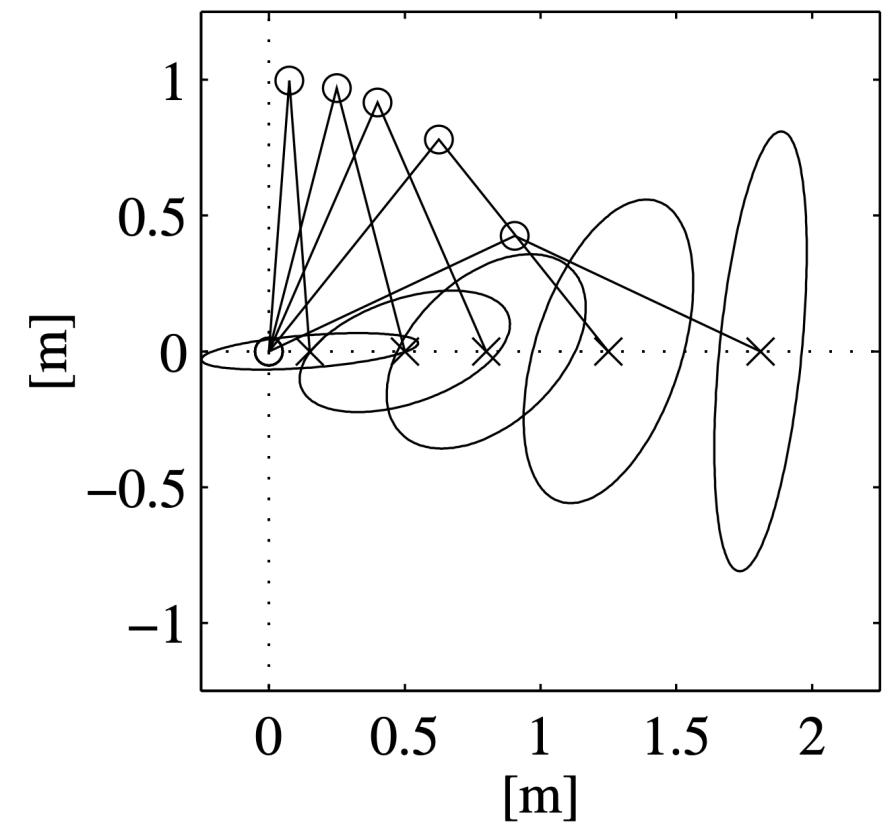
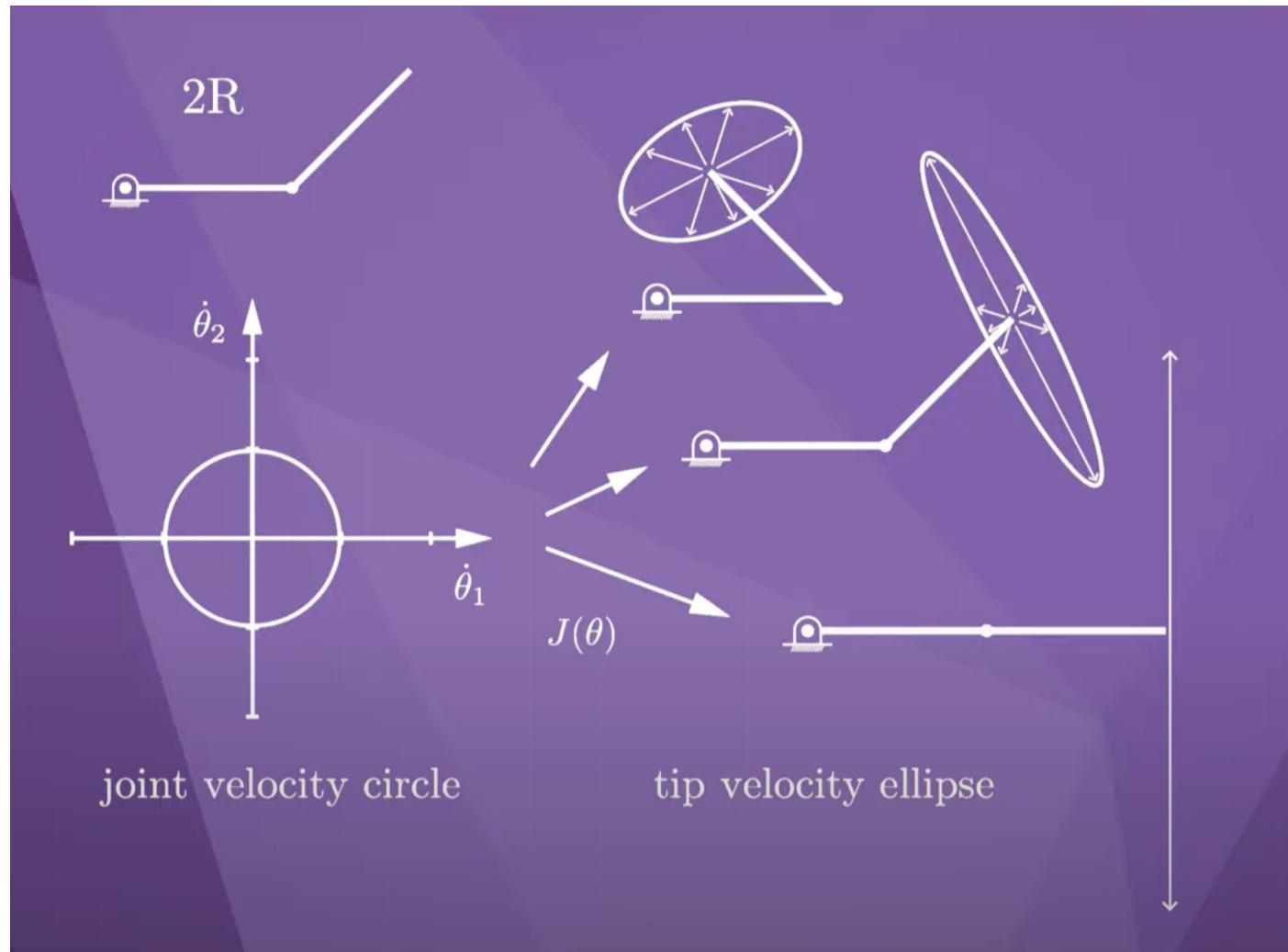
- Represents the attitude of a manipulator to arbitrary change end-effector position and orientation using the velocity manipulability ellipsoid
- Consider the set of joint velocities of constant (unit) norm:

$$\dot{\mathbf{q}}^T \dot{\mathbf{q}} = 1$$

(this equation describes the points on the surface of a sphere in the joint velocity space)

$$\dot{\mathbf{q}} = J(\mathbf{q})^{-1} \boldsymbol{\nu} \longrightarrow \boldsymbol{\nu}^T (J(\mathbf{q}) J(\mathbf{q})^T)^{-1} \boldsymbol{\nu} = 1$$

Manipulability Ellipsoid - RR planar



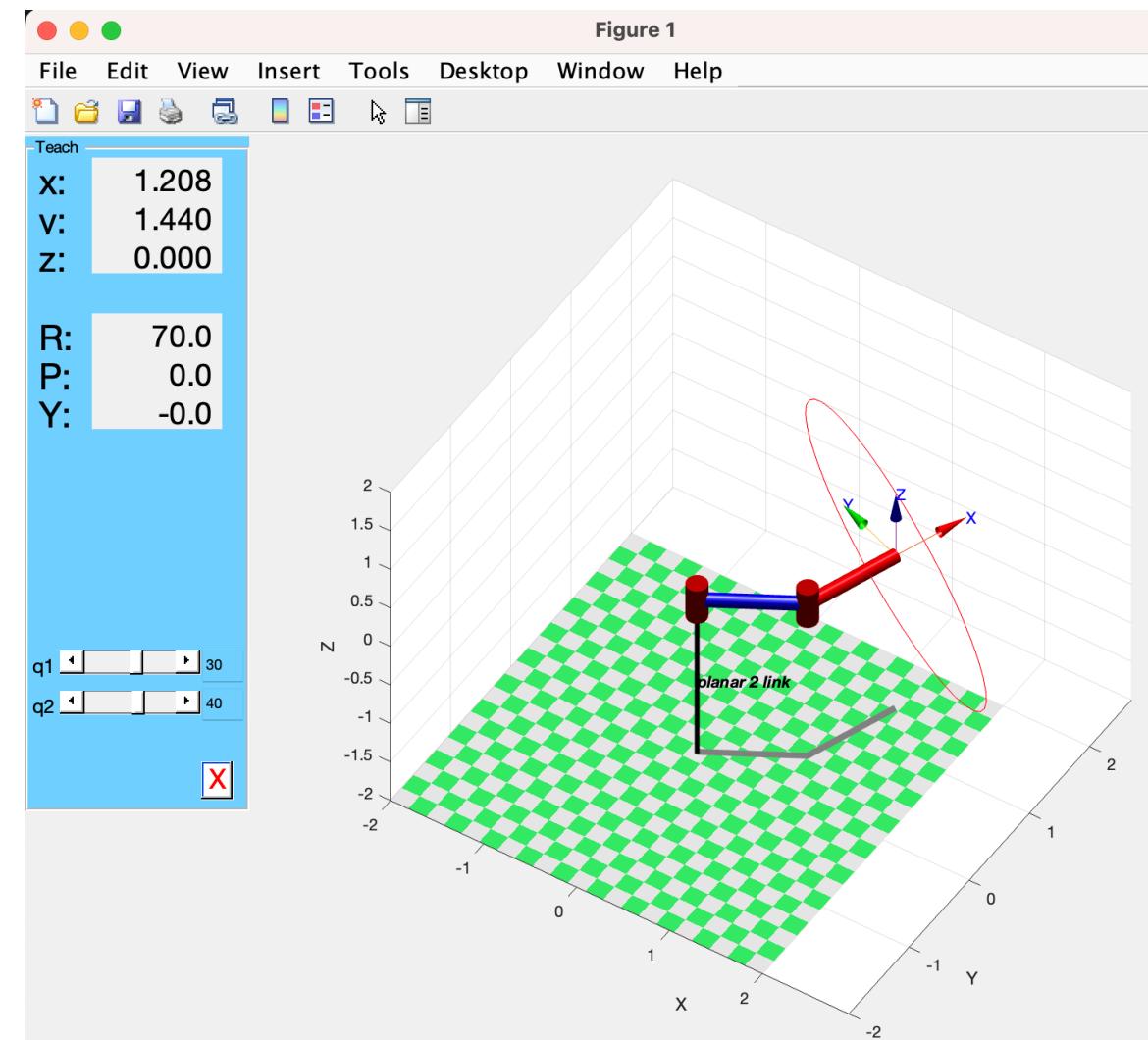
Manipulability Ellipsoid - RR planar

$$\boldsymbol{\nu}^T \left(J(\boldsymbol{q}) J(\boldsymbol{q})^T \right)^{-1} \boldsymbol{\nu} = 1$$

```
mdl_planar2
p2

qns = [30 40];
p2.vellipse(qns, 'deg')

p2.teach('callback', @(r,q) r.vellipse(q))
```



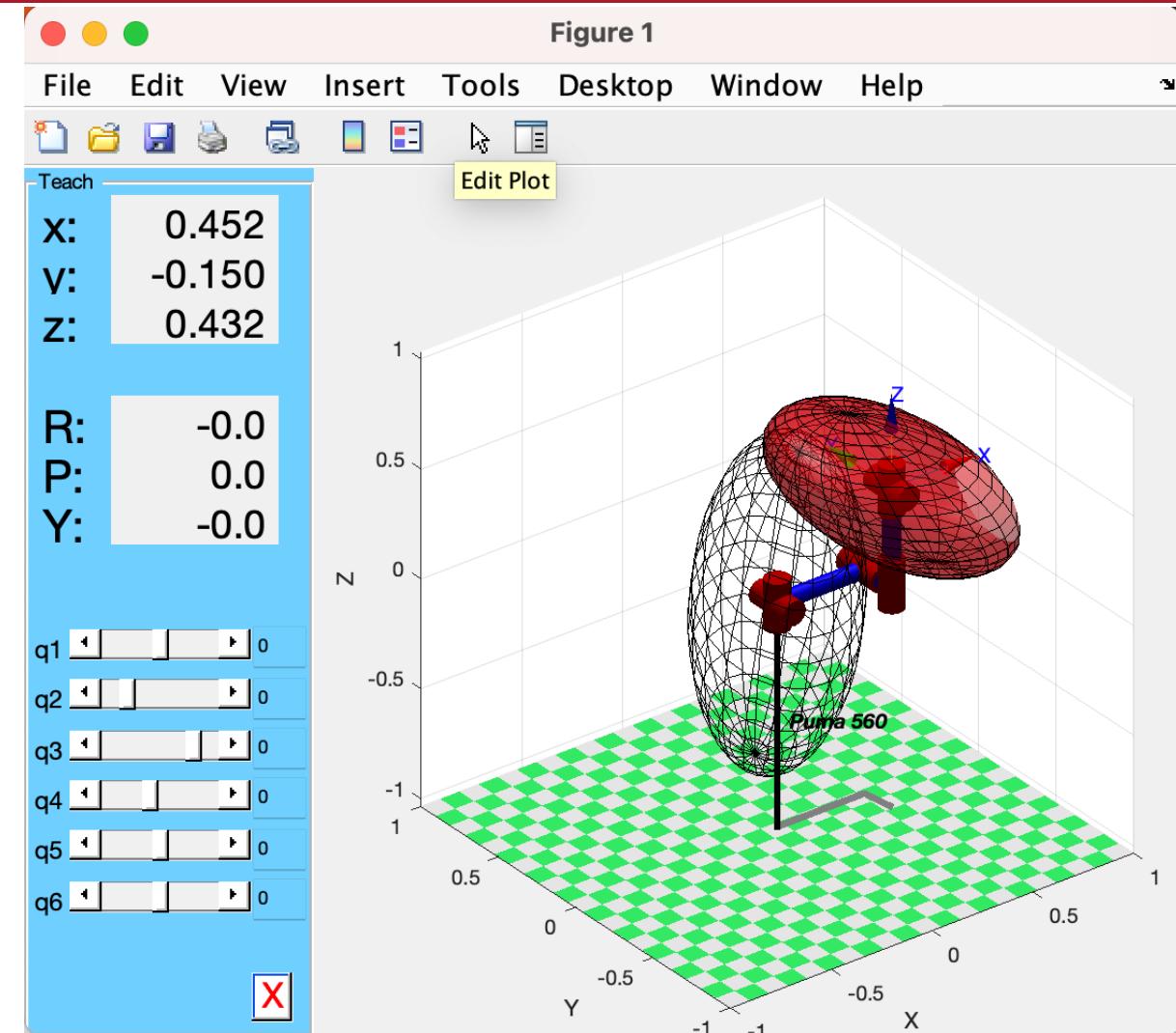
Manipulability Ellipsoid - PUMA 560

$$\boldsymbol{\nu}^T \left(J(\boldsymbol{q}) J(\boldsymbol{q})^T \right)^{-1} \boldsymbol{\nu} = 1$$

```
mdl_puma560
p560

J = p560.jacob0(qn)
Jp = J(1:3, :)

plot_ellipse(Jp * Jp')
```



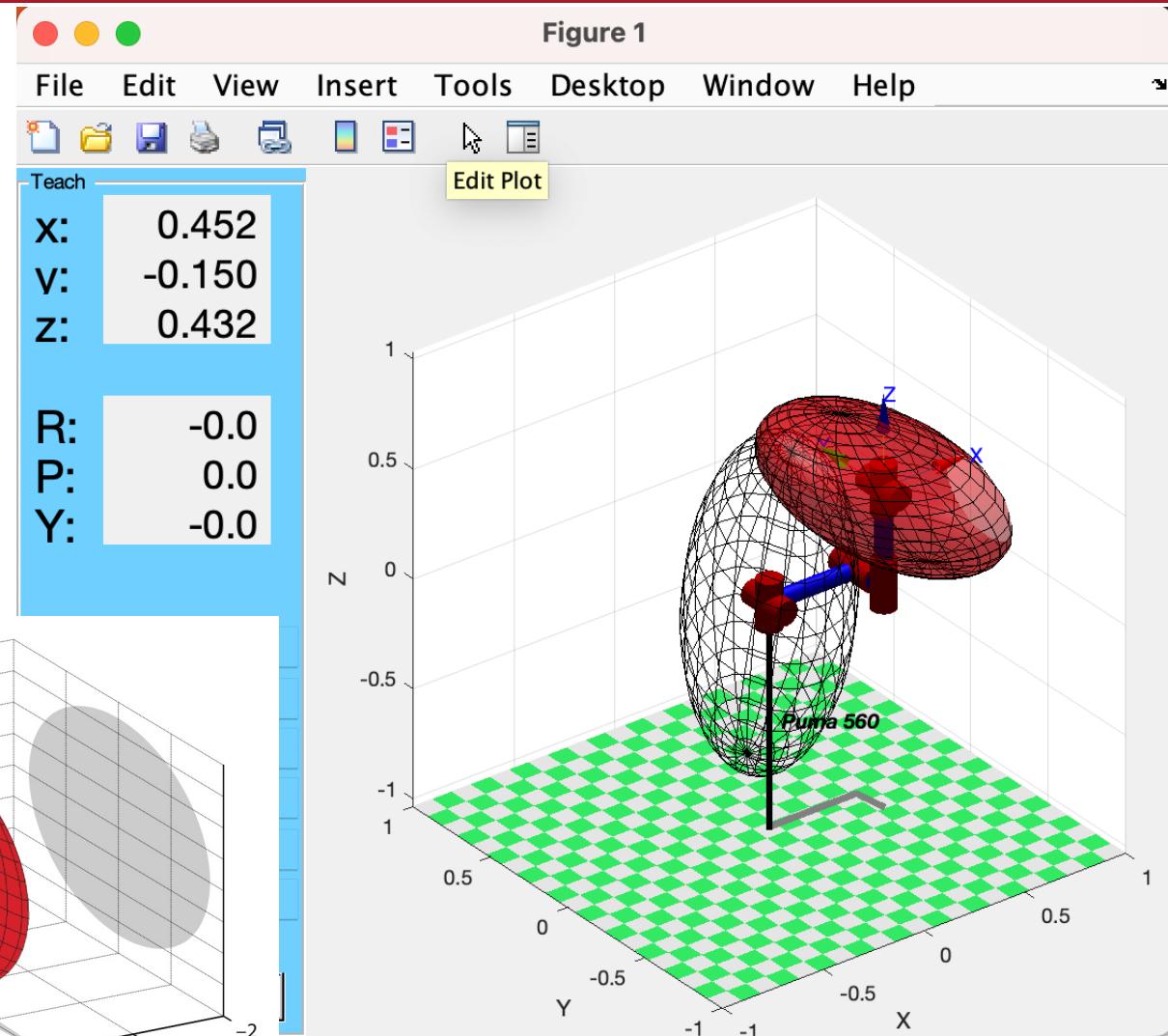
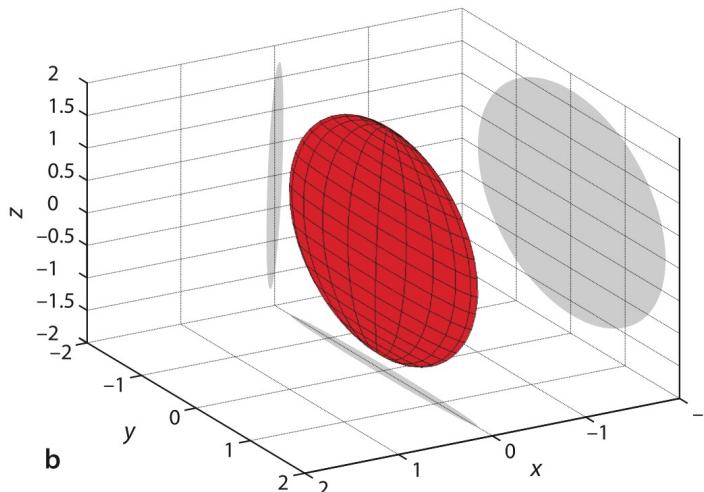
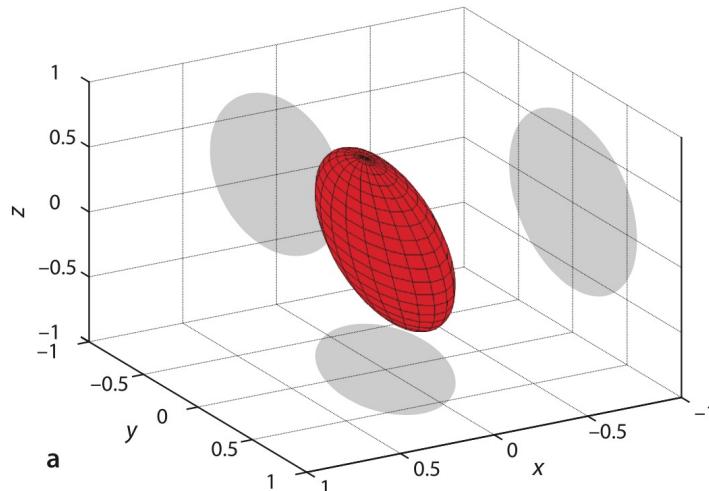
Manipulability Ellipsoid - PUMA 560

$$\boldsymbol{\nu}^T \left(J(\boldsymbol{q}) J(\boldsymbol{q})^T \right)^{-1} \boldsymbol{\nu} = 1$$

```
mdl_puma560
p560

J = p560.jacob0(qn)
Jp = J(1:3, :)

plot_ellipse(Jp * Jp')
p560.vellipse(qn, 'trans');
p560.vellipse(qn, 'rot')
```



Manipulability measure

- A global representative measure of manipulation ability can be obtained by considering the volume of the ellipsoid. This volume is proportional to the quantity:

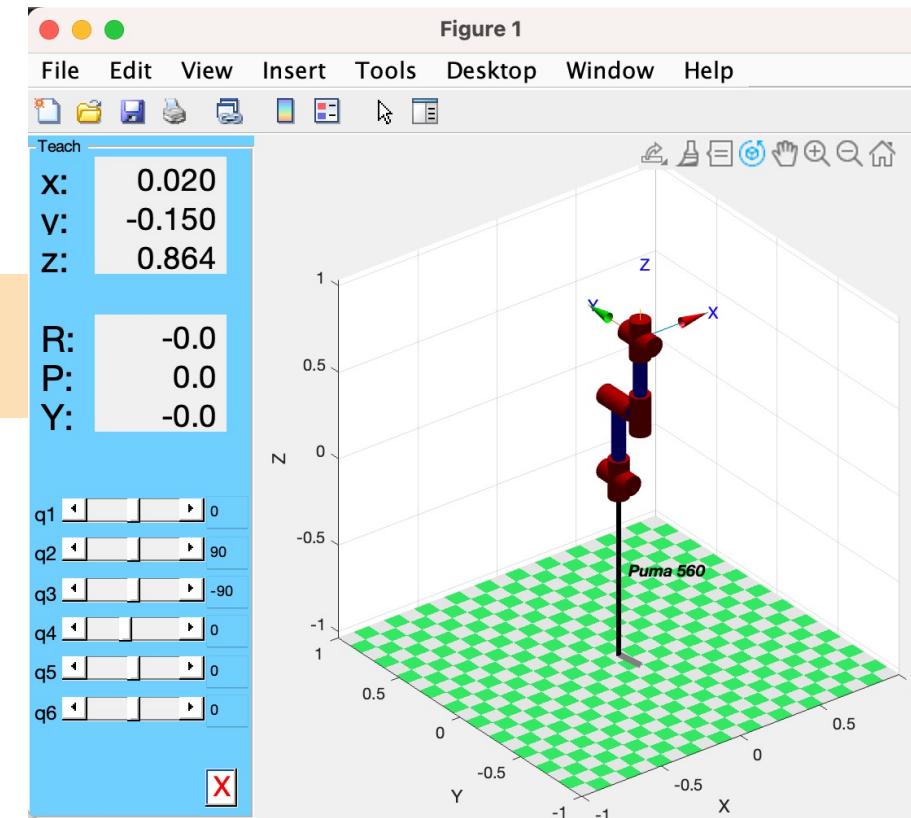
$$m = \sqrt{\det(JJ^T)}$$

Manipulability measure - PUMA 560

- A global representative measure of manipulation ability can be obtained by considering the volume of the ellipsoid. This volume is proportional to the quantity:

$$m = \sqrt{\det(JJ^T)}$$

```
>> p560.maniply(qr)
Manipulability: translation 0.00017794, rotation 0
```

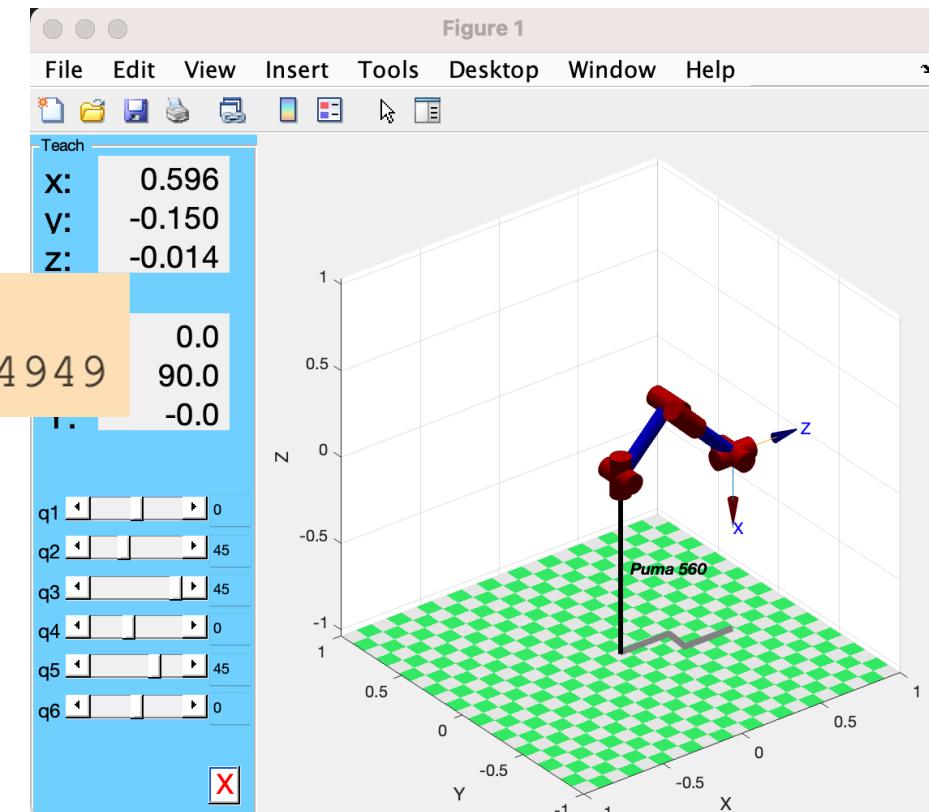


Manipulability measure - PUMA 560

- A global representative measure of manipulation ability can be obtained by considering the volume of the ellipsoid. This volume is proportional to the quantity:

$$m = \sqrt{\det(JJ^T)}$$

```
>> p560.maniplty(qn)
Manipulability: translation 0.111181, rotation 2.44949
```



... end of Lecture 10

