

Sensitivity of Nozzle Guide Vane Flow Capacity to Geometric Changes

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Abstract

Optimal design of gas turbines depends on the accurate prediction of mass flow rate passing through all engine stages. This quantity is limited by the high-pressure turbine nozzle guide vanes (NGVs). NGV mass flow rate prediction remains a major challenge to engine designers. The lack of accurate mass flow rate prediction is driven by many uncertainties: the effect of small and unavoidable manufacturing variations; computational and conceptual difficulties in modelling 3D flows; and uncertainty of the effects of small changes in design.

This thesis presents a simplified approach to modelling the NGV capacity (a pseudo-dimensionless mass flow rate). 2D CFD is used to simulate several mechanisms which drive capacity change for a commercial aero engine NGV. Cases without film or convection cooling are used to investigate the effects of casting variations. These baselines also allow comparison of this study's 2D capacity predictions with the manufacturer's 3D predictions. 2D and 3D are shown to be in good agreement at low pressure ratios, but at higher ratios the 2D cases under-predict the limiting (choked) mass flow rate due to unchoked secondary flows in 3D geometry.

Simulations then investigate several necessary NGV design features: the extent of the trailing edge, which contributes to the turning of flow in the NGV; the extent of the trailing edge cutback, which ensures that film cooling holes are not blocked; and the addition of pressure side film cooling, which may be required by future designs. Each of these features affects the NGV capacity. The capacity change is recorded over a range of pressure ratios typical of the geometry and design operating conditions of the part. Changes in aerodynamic performance are also discussed, these being loss and whirl angle error.

The key finding of the study is that all capacity prediction errors ultimately result from a lack of information about the effective cross-sectional area of the flow passage at various pressure ratios and chordwise locations. The thesis presents heuristics that circumvent this problem to some extent with the available data, concluding with the prediction that future heuristics can use exponentially larger (and 3D) data sets to make highly accurate and rapid capacity predictions.

Thanks

I was never much of a writer. I was never much of a scientist either, which probably isn't the wisest thing to admit in an MSc thesis. Nonetheless, over the unusual course of my degree, I've been lucky enough to know several people who've helped me to write, helped me to do science, and perhaps most crucially, helped me to stick at it.

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Nomenclature

Romans

p	Pressure
Q_{23}	Rate of heat addition, ideal Brayton cycle
\dot{m}_i	Mass flow rate, ideal Brayton cycle
T	Temperature
H_{LV}	Jet fuel lower heating value
\dot{m}_f	Fuel mass flow rate, ideal Brayton cycle
r_p	Engine pressure ratio, ideal Brayton cycle
\dot{m}	Nozzle mass flow rate
u	Velocity
A	Nozzle throat area
r	Nozzle pressure ratio
r_c	Nozzle critical pressure ratio, 0.5379
A_{eff}	Nozzle effective throat area
\hat{u}	Local velocity unit vector on sonic line
\hat{r}	Sonic line local unit direction vector
dL	Infinitesimal length on sonic line
L	Nozzle guide vane characteristic length for Reynolds number
Re	Reynolds number
M	Mach number
y	Distance from wall within boundary layer
y_+	Dimensionless distance from wall within boundary layer
u_f	Friction velocity within boundary layer
τ_w	Wall shear stress
C_f	Wall skin friction coefficient
C_{pt}	Total pressure loss coefficient
C_{Gao}	Total pressure loss coefficient (Gao)
Y	Coolant/mainstream mass flow rate ratio
x	Distance
\dot{m}_c	Film coolant mass flow rate
A_h	Cooling hole cross-sectional area
M_{isent}	Nozzle guide vane surface isentropic Mach number

Greeks

η_{th}	Thermal efficiency, ideal Brayton cycle
η_h	Heating efficiency, ideal Brayton cycle
ρ	Density
Γ	Nozzle flow capacity
σ	Scale constant
Γ_c	Choked nozzle flow capacity
δ	Approximate maximum thickness of a turbulent boundary layer
μ	Dynamic viscosity
ζ	Kinetic energy loss coefficient
λ	Iterative substitute for p_{0c}
ζ_c	Coolant loss coefficient
Γ_{in}	Film cooled nozzle flow capacity at domain inlet
Γ_{out}	Film cooled nozzle flow capacity at domain outlet
Γ_c	Film coolant plenum flow capacity

Subscripts

$i1, i2, i3, i4$	Ideal Brayton cycle salient points
0	Total
1	At the domain inlet
2	At the domain outlet
uc	Uncooled case
$wake$	Within the nozzle guide vane wake region
cp	At the cooling plenum domain boundary
c	At the cooling hole exit

Constants

γ	Ratio of specific heats for air, ≈ 1.4
c_p	Specific heat of air at constant pressure, $\approx 1121 \frac{J}{kgK}$
R	Specific gas constant for air, $287.058 \frac{J}{kgK}$

Abbreviations

NGV	Nozzle guide vane
CFD	Computational fluid dynamics
IC	Internal combustion
FMG	Full multi-grid initialisation (Fluent)
k- ω SST	Menter's shear stress transport turbulence model
2D	2-dimensional
3D	3-dimensional
XWB	Extra-wide body (Airbus A350 XWB with Trent XWB)
KE	Kinetic energy
PR	Pressure ratio
CMC	Ceramic matrix composite
OPR	Overall pressure ratio
84K	84,000 <i>lbf</i> thrust
97K	97,000 <i>lbf</i> thrust

Chapter 1

Introduction

Jet engines cannot achieve a reversible, adiabatic cycle. Although the principle of operation is based on the ideal Brayton thermodynamic cycle, the design space for a real engine is bounded by the capabilities of the available materials, the means of manufacture, and the design of the components. The differences between the ideal cycle and the real engine operation cannot be fully understood using contemporary low-order models. Consequently it remains extremely difficult to accurately predict the engine core mass flow rate, despite this quantity being essential for optimal engine design.

A key factor in overall engine size, and thus weight, is the required geometric throat area of the high pressure turbine nozzle guide vanes (NGVs). These are the set of stationary vanes upstream of the rotor, which impart whirl to the hot high-pressure combustion products leaving the combustor. The NGV annulus sets the mass flow rate through the engine core, and thus sizes the engine, but it is not a perfect nozzle and is subject to losses. Lack of knowledge of loss mechanisms typically leads to over-prediction of the NGV capacity. When the manufactured engine operating condition is adjusted to achieve the required thrust, the aerodynamic matching of components is compromised.

This thesis analyses the high-pressure turbine NGVs. The study investigates how the pseudo-dimensionless mass flow rate, *flow capacity*, is affected by various design parameters necessary to achieve a cooled, long-life NGV. Furthermore the sensitivity of flow capacity to small manufacturing tolerance errors is characterised. Further analyses examine the aerodynamic performance of this component in terms of its ability to impart the correct whirl angle to the post-combustor flow with minimal loss, so as to most efficiently deliver the flow to the high pressure turbine and beyond.

1.1 Motivation

For the engine manufacturer, the penalty for over-predicting flow capacity is an engine with a larger nacelle, as the bypass air must be ducted around a larger core. For the aircraft manufacturer, this incurs the severe penalties of increased drag and increased weight, affecting fuel consumption, range, and passenger capacity.

The requirement for an accurate core mass flow rate prediction may be illustrated by consideration of the ideal Brayton thermodynamic cycle, which is plotted in Figure 1.1.

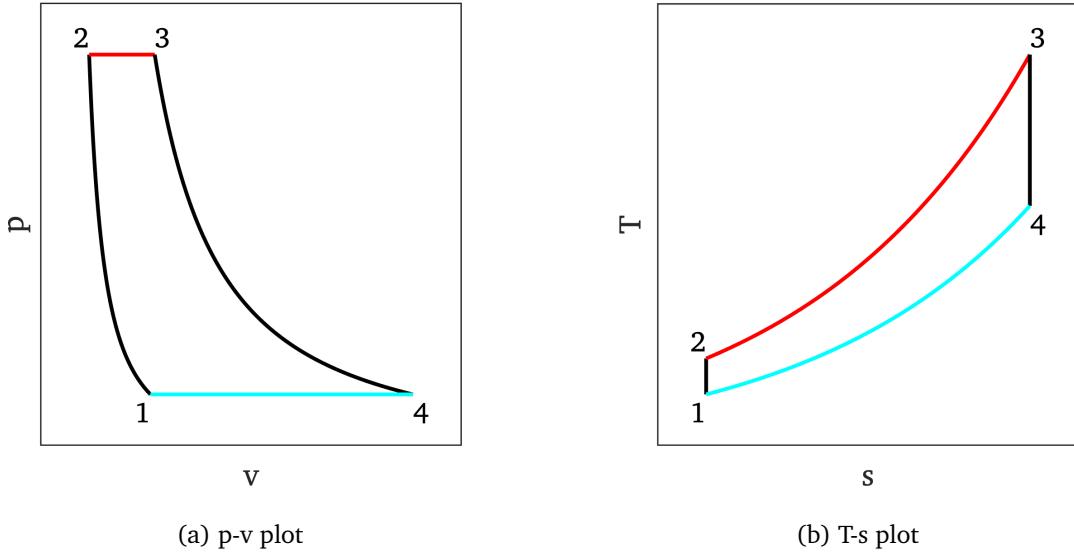


Figure 1.1: p - v and T - s plots of the Brayton thermodynamic cycle

Basic analysis of the ideal Brayton cycle shows that its thermal efficiency is equal to

$$\eta_{th} = 1 - \left(\frac{p_{i1}}{p_{i2}} \right)^{\frac{\gamma-1}{\gamma}} \quad (1.1)$$

where the subscript i denotes that this analysis is of an ideal cycle. For maximum thermal efficiency, it is thus desirable to maximise the pressure increase produced by the engine's compressor, which is responsible for the process of isentropic compression between stations 1 and 2. The compression ratio is limited in practice by the pressure increase that is achievable by contemporary compressors, which must balance the goal with the avoidance of stall, the need for a wide range of operating conditions, and the avoidance of excess complexity from adding additional spools. Cruise-condition compression ratio is thus a design specification which sets the value of p_{i2} .

The engine's combustor is responsible for the process of isobaric heat addition between stations 2 and 3. The rate of heat addition to the flow is given by

$$Q_{23} = \dot{m}_i c_p (T_{i3} - T_{i2}) \quad (1.2)$$

where \dot{m}_i is the mass flow rate through an ideal engine core. For the purpose of illustration, the influences of bleed and cooling air mass flow rate are not considered, and \dot{m}_i is taken to be the mass flow rate through the engine compressor, combustor, nozzle guide vanes, and turbine. c_p is the specific heat of air at constant pressure and T_{i2} is derived from the compressor inlet temperature T_{i1} via isentropic compression as

$$T_{i2} = T_{i1} \left(\frac{p_{i2}}{p_{i1}} \right)^{\frac{\gamma-1}{\gamma}} \quad (1.3)$$

combining to express the heat added as

$$Q_{23} = \dot{m}_i c_p \left[T_{i3} - T_{i1} \left(\frac{p_{i2}}{p_{i1}} \right)^{\frac{\gamma-1}{\gamma}} \right] \quad (1.4)$$

It is desirable to maximise the specific power of the engine in order to build the smallest engine possible. This is achieved by maximising the heat added to the flow, which would result in an increase

in in T_{i3} . A technological limitation is once again presented: the maximum T_{i3} is limited by the avoidance of overheating the post-combustor nozzle guide vanes, for which heat management is of prime concern to the field. T_{i3} is thus a design specification.

Heat addition is well controlled for in contemporary lean-burn engines, where it may be modelled by the relationship

$$Q_{23} = \eta_h H_{LV} \dot{m}_f \quad (1.5)$$

where \dot{m}_f is the fuel mass flow rate, H_{LV} is the lower heating value of jet fuel and η_h is a constant to account for inefficiencies of heat addition beyond the scope of the present illustration. The above equations combine to show that the required fuel mass flow rate may be modelled by the expression

$$\frac{\dot{m}_f}{\dot{m}_i} = \frac{c_p}{\eta_h H_{LV}} \left(T_{i3} - T_{i1} r_p^{\frac{\gamma-1}{\gamma}} \right) \quad (1.6)$$

where r_p is the compression ratio, $\frac{p_{i2}}{p_{i1}}$. It is shown that the core mass flow rate, \dot{m}_i , must be accurately predicted if the engine is to be accurately maintained at the optimal operating conditions allowed by its construction. r_p and T_{i3} are known design specifications, T_{i1} is a measurable ambient condition, and all other terms are approximately constant.

The design of any jet engine depends on accurate prediction of \dot{m}_i . It is shown that this is directly tied to the performance and operational margins of the upstream engine components. Predictability of \dot{m}_i also affects the design of every downstream turbine stage. If it differs from its expected value due to a poor prediction, all subsequent turbine stages will be sized for an incorrect mass flow rate. The resulting errors in flow velocity and pressure will compound with each additional stage, leading to increasingly incorrect specification of turbine sizes and turning angles.

Guiffre' and Pini [1] performed numerical analysis to discuss scaleable guidelines for turbine stage design, validating their model using high-fidelity CFD. Correct stage matching was found to be highly dependent on matching the *volumetric flow ratio*, defined by the authors as a stage's total-to-static density ratio. To accurately quantify this parameter within the analytical and computational methods discussed in this thesis, mass flow rate would need to be predicted correctly.

A strong understanding of NGV mass flow rate predictability should allow engine-makers to pre-empt geometric changes that happen to NGVs during service, such as erosion and cooling hole blockage. It should also account for geometric uncertainties arising from the manufacturing process. While this study advocates for improved accuracy of capacity predictions, emphasis is placed on how these predictions are limited by the unpredictability of real-world manufacture and service.

Section 1.2 will outline the analysis involved in parameterising and predicting mass flow rate. The section will also present the alternative metric of *flow capacity* as a more useful way of characterising mass flow rate independently of the NGV upstream total pressure and temperature. Defining a purely geometric mass flow rate capacity allows for experimental testing of NGVs without recreating the extreme boundary conditions to which real NGVs are exposed. Setting the correct pressure ratio is sufficient, as the subsequent derivation will show. This expedites the testing of different NGV geometries' effects on mass flow rate.

1.2 Flow capacity: background, definition, and derivation

The capacity of an internal combustion engine is an intuitive concept. It is simple to derive from the engine's geometry, it has tangible units of volume, and it provides an heuristic for the engine's size, performance, and air mass flow rate. The design of turbomachinery invites an analogous concept to that of IC engine capacity, but a definition is not so obvious. Mass flow rate through an engine's nozzle guide vane is a function of the NGV's geometry and of its boundary conditions. If the mass flow rate can be quantified in a way which mitigates the boundary conditions, then the effects of an NGV's geometry on its mass flow rate may be isolated. A particular NGV will thus have a mass flow rate capacity, just as a particular IC cylinder has a volumetric capacity.

In 1 dimension, an engine nozzle may be modelled as a compressible flow from an upstream reservoir of total pressure p_0 , accelerating to velocity u and density ρ through a nozzle of cross-sectional area A . Mass flow rate through the nozzle is thus

$$\dot{m} = \rho A u \quad (1.7)$$

where density may be expressed as a function of *pressure ratio*, the ratio of the nozzle pressure to the total pressure

$$\rho = \frac{p_0}{RT_0} \left(\frac{p}{p_0} \right)^{\frac{1}{\gamma}} \quad (1.8)$$

and velocity is given by conservation of energy as

$$u = \sqrt{2 \left(\frac{\gamma}{\gamma-1} \right) \left[\frac{p_0}{\rho_0} - \frac{p}{\rho} \right]} \quad (1.9)$$

The above equations combine to express mass flow rate through the nozzle as

$$\dot{m} = A \frac{p_0}{RT_0} \left(\frac{p}{p_0} \right)^{\frac{1}{\gamma}} \sqrt{2 \left(\frac{\gamma}{\gamma-1} \right) \left[\frac{p_0}{\left(\frac{p_0}{RT_0} \right)} - \frac{p}{\left(\frac{p_0}{RT_0} \right) \left(\frac{p}{p_0} \right)^{\frac{1}{\gamma}}} \right]} \quad (1.10)$$

which simplifies to

$$\dot{m} = \frac{p_0}{\sqrt{T_0}} A \sqrt{\frac{\gamma}{R}} \left(\frac{p}{p_0} \right)^{\frac{1}{\gamma}} \sqrt{\left(\frac{2}{\gamma-1} \right) \left[1 - \left(\frac{p}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right]} \quad (1.11)$$

Using \dot{m} from Equation 1.11, capacity is defined as

$$\Gamma = \frac{\sqrt{T_0}}{p_0} \dot{m} \quad (1.12)$$

This provides an expression of mass flow rate independent of upstream total pressure p_0 and upstream total temperature T_0 . For isentropic flow, the expression is purely a function of throat area A and pressure ratio $\frac{p}{p_0}$:

$$\Gamma = A \sqrt{\frac{\gamma}{R}} \left(\frac{p}{p_0} \right)^{\frac{1}{\gamma}} \sqrt{\left(\frac{2}{\gamma-1} \right) \left[1 - \left(\frac{p}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right]} \quad (1.13)$$

For throat area A and pressure ratio r :

$$\Gamma(A, r) = \sqrt{\frac{2\gamma}{R(\gamma-1)}} A \sqrt{r^{\frac{2}{\gamma}} \left(1 - r^{\frac{\gamma-1}{\gamma}}\right)} \quad (1.14)$$

This expression has its maximum value at the critical pressure ratio

$$r_c = \left(\frac{\gamma+1}{2}\right)^{\frac{1}{1-\gamma}} \quad (1.15)$$

At lower ratios, the nozzle is choked and mass flow rate cannot increase further. Choked capacity is given by

$$\Gamma_c(A) = \sqrt{\frac{2\gamma}{R(\gamma-1)}} A \sqrt{\left(\frac{\gamma+1}{2}\right)^{\frac{2}{1-\gamma}} \left[1 - \left(\frac{\gamma+1}{2}\right)^{-1}\right]} \quad (1.16)$$

which simplifies to

$$\Gamma_c(A) = A \sqrt{\frac{\gamma}{R}} \left(\frac{\gamma+1}{2}\right)^{\frac{1+\gamma}{2(1-\gamma)}} \quad (1.17)$$

It is shown that the capacity of one-dimensional isentropic nozzle flow is a function of only the flow's minimum area, provided the flow is choked and the ratio of specific heats is assumed constant.

Section 1.3 will introduce the structure of the following chapters, which are to analyse the capacity of 2-dimensional and 3-dimensional nozzle flows, presenting and discussing analytical techniques for applying the 1D capacity equation to 2D and 3D data. In such cases, capacity will be defined by equation 1.12.

1.3 Research structure

The present study seeks to categorise and examine the ways in which nozzle guide vane flow departs from 1-dimensional compressible flow. These departures are numerous and diverse. The study's scope is to include 2 categories of phenomena: difficulties in predicting the mass flow rate through real nozzle guide vanes, and difficulties in quantifying and modelling the loss incurred by various practical solutions to the need for NGV coolant flow.

Although NGV flow capacity is arguably to be maximised in pursuit of greater power, and loss is certainly to be minimised in pursuit of greater efficiency, it is practical to divide efforts according to the areas of NGV engineering where limitations are present. The present study has identified 3 such areas.

- NGV casting processes causing variations in overall shape and throat area, limiting the predictability of flow capacity.
- Trailing edge machining processes causing variations in trailing edge shape, resulting in complex variations in the flow field near the downstream extremity of the trailing edge, with corresponding variations in flow capacity.
- Sensitivity of flow capacity to the addition of extra film cooling holes on the NGV leading edge suction side, including sensitivity to their exact location.

NGVs are cast to high precision. Chapter 3 will present the variations that nonetheless exist among sets of vanes that are intended to be identical. These variations are shown to affect the NGVs' geometric throat area. The chapter discusses the challenges inherent in finding a definition of throat area that usefully predicts the flow capacity of an NGV. The effects of 2-dimensional flow phenomena and geometric variations are presented as confounding factors when considering 2D nozzle flow as opposed to 1D. Further complexity is shown to arise when extending analyses to 3D, where 3D CFD data gathered by Rolls-Royce plc are compared to 2D CFD data from the present study.

Chapter 4 will discuss the other way in which NGV manufacturing introduces geometric variations that reduce capacity predictability, namely the machining of the trailing edge shape. The machining is designed to optimise the trailing edge's aerodynamics, and not necessarily to minimise variations in its shape. The chapter presents 2D CFD analyses of the effects of variable trailing edge cutback sizing on the 2D flow field and resulting flow capacity of the NGV. To address the variability of contemporary trailing edge designs and to examine the possibility of thicker trailing edges in the event of novel manufacturing methods, the chapter presents 2D CFD analyses of a design without a cutback. This design's loss performance is analysed, informed by a review of various definitions of loss from the literature, where a lack of consensus on a loss definition is demonstrated.

Chapter 5 will analyse the effects of film coolant injection location on both flow capacity and loss. The chapter discusses the possible requirement for an additional suction-side film cooling hole row to be added to NGVs. Given the variability inherent in the process of drilling film cooling holes, justification is given for a 2D CFD study of the effects of hole location on flow capacity and loss, analogous to the variable trailing edge study of Chapter 4. A correlation between hole location and flow capacity is analysed, as is the hole location's effect on loss.

1.4 Summary of findings

Chapter 3 shows that geometric throat width is a useful predictor of 2-dimensional nozzle guide vane flow capacity. However, the accuracy of the prediction is shown to be dependent on the feasibility of predicting the shape of the sonic line when the NGV is fully choked. If the sonic line is known to not vary significantly in shape within a given production standard of NGV, designers may have more confidence in using the geometric throat area to predict capacity without the use of CFD. In general, capacity predictability is challenged by the reduction of effective throat area by boundary layers whose thickness is difficult to define. Where a sonic line exists, its stability and its approach to the surface may be affected by the presence of the boundary layer. In 3 dimensions, capacity predictability is further challenged by the existence of secondary flows which migrate across the span.

Chapter 4 shows how changes to the NGV trailing edge geometry affect capacity differently at different pressure ratios. Changes to the NGV suction side trailing edge have little effect at fully-choked pressure ratios, whereas changes to the pressure side have a significant effect at the same pressure ratios. This is shown to result from the relative importance of the throat width when the flow is choked, compared to when it is not. At unchoked pressure ratios, it is possible for post-throat geometric changes to have a significant effect on capacity. The chapter also presents a detailed investigation of the aerodynamic penalties of altering the NGV trailing edge.

Chapter 5 shows that the introduction of film coolant on the NGV suction side has a significant effect on capacity. Coolant injection into locally slower regions is found to have a minimal penalty on both capacity and loss, and in extreme cases to even increase the capacity. Coolant injection into locally faster regions is found to cause a reduction in the capacity. The coolant injection is argued to be

equivalent to a change in the effective area at the point of injection, which is in agreement with the arguments about effective area presented in the earlier chapters.

The overall work thus provides insight into the necessary geometric parameters for an initial 2D aerofoil design, showing which parameters require iterative calculation and which may be changed without significant penalty to capacity or aerodynamics.

Chapter 2

Literature and scope

This chapter reviews the literature used to inform decisions about which flow phenomena require modelling in the present study, and which do not. The scope of the present analyses is thus defined. It is shown in Section 2.1 that certain analyses may be omitted without significant penalty to the usefulness of the study's findings, justifying the use of 2-dimensional, steady, adiabatic CFD, with air as the working gas. Section 2.2 reviews literature precedential to the present study's choice of turbulence model and to its definitions of loss.

2.1 Justification of effects not modelled in this study

2.1.1 3D effects

The present study is concerned with variations to the *profile* of NGVs, where a profile is a 2D aerofoil outline obtained by intersecting a 3D NGV shape with a plane perpendicular to the span. The NGV thus has a continuous set of profiles across its span. Through design intent or manufacturing variability, an NGV is likely to experience certain profile changes which are expressed across its whole span. Casting variations, discussed in Chapter 3, are expressed as smooth departures of the actual NGV surface from the design NGV surface, and are thus likely to affect the majority of the span. Changes to the design of the trailing edge shape, discussed in Chapter 4, affect the majority of the span over which the trailing edge extends.

These circumstances motivate the use of 2-dimensional CFD to study effects which are likely to occur throughout the NGV span and which are likely to be primarily coplanar with the NGV profile. This is only viable if these 2D effects are not overpowered by effects that appear in 3D, otherwise the 2D effects have no bearing on real engine performance.

GIVE EXAMPLES OF GOOD 2D CFD STUDIES WHICH HAVE ISOLATED THE KIND OF EFFECTS I'M TALKING ABOUT

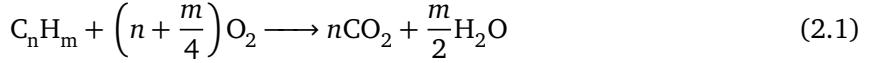
2.1.2 Unsteady effects

CITATION FOR WHY IT CAN BE STEADY, AND THUS WHY RANS IS OK TO DO as opposed to urans

2.1.3 Real gas transport properties

The present study simulates the flow of clean air through NGVs with an inlet total temperature of 300 K. Real NGV flows consist of a mixture of air and combustion products from jet fuel, the presence of which potentially alter the aerodynamics of the NGV compared to clean air. Simulation of purely air-based cases is justified by quantification of the combustion gas mixture constituents and evaluation of the mixture's properties. Simulation of cases at 300 K is justified by consideration of the properties of air at engine-representative total temperatures.

Lee et al [2] experimentally tested the combustion of Jet-A fuel under lean conditions with apparatus for measuring the chemical composition of the combustion products. Air/fuel ratios ranged from 1.67 to 2.13 times the stoichiometric air/fuel ratio. Molar fraction of CO₂ was measured to be approximately 6.8% downstream of combustion. This may be compared with exactly stoichiometric combustion which is, in this context, a worst case for the conversion of atmospheric O₂ into combustion products with properties dissimilar to air. Lee et al [2] provided a simplified mechanism for Jet-A combustion as



This may be further approximated as

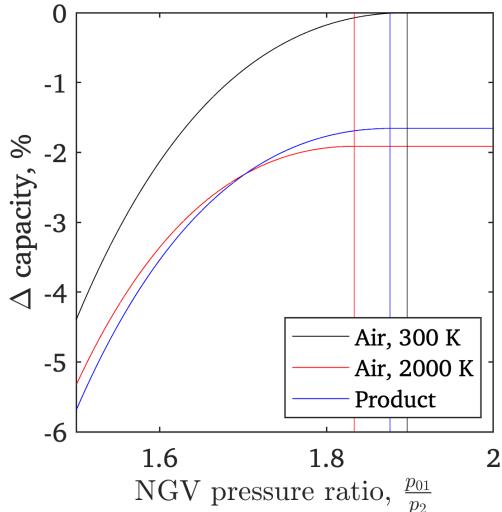


which, under stoichiometric conditions and not accounting for trace gases, would effect changes to the gas composition described in Table 2.1. Initial reagents are assumed to be 79 moles of N₂, 21 moles of O₂, and 14 moles of CH₂.

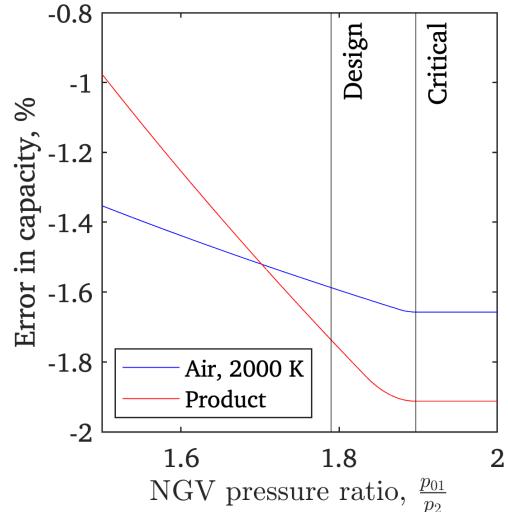
Table 2.1: Changes to the gas composition of air during stoichiometric combustion of Jet-A

Component	Before		After	
	Moles	% by mass	Moles	% by mass
N ₂	79	71.82	79	71.82
O ₂	21	21.82	0	0
CH ₂	14	6.36	0	0
CO ₂	0	0	14	20.00
H ₂ O	0	0	14	8.18

Matlab was used to compute the properties of the gas mixture described in Table 2.1 for comparison with the properties of air at 300 K as simulated by the present study. This comparison was made at a temperature of 300 K. The combustion product was computed to have a value of γ which was 2.43% less than air, and a value of R which was 1.65% greater than air. The same Matlab script was used to compute the properties of air at 2000 K, a typical contemporary combustor outlet temperature. The high-temperature air was computed to have a value of γ which was 7.48% less than cold air, and a value of R which was 1.54% less than cold air. These values were used with equation 1.12 to compare the 1-dimensional capacity trend of air at 300 K with that of air at 2000 K and with that of the combustion product. These trends are shown in Figure 2.1 for a range of inverse pressure ratios of interest to the present study.



(a) Computed capacity trends and critical inverse pressure ratios



(b) Errors due to air temperature or presence of combustion product

Figure 2.1: 1-dimensional capacity trends and relative errors for air at 300 K, air at 2000 K, and computed Jet-A stoichiometric combustion product

Figure 2.1a illustrates that the 3 dissimilar sets of gas properties resulted in significantly dissimilar predictions of 1D capacity as a function of pressure ratio, exhibiting qualitative differences, overall differences in capacity across the range of pressure ratios, and dissimilar critical pressure ratios. Figure 2.1b, which shows the relative errors in computed 1D capacity due to the working gas's temperature and due to its chemical composition, illustrates that these errors did not amount to a constant factor across the range of pressure ratios. Error due to gas temperature varied by approximately 0.30% across the range, and error due to chemical composition varied by approximately 0.93%.

Although these errors are significant, their mitigation would likely result in greater confusion. Concerning the non-air combustion product, it has been noted that lean burn conditions produce CO₂ concentrations significantly lower than the theoretical stoichiometric worst case considered by the above analysis. Precise air/fuel ratio, and thus combustion product composition, is a function of combustor design and engine operating conditions, the details of which are not available to the present study. Further, Marius and Grigore [3] demonstrated that the combustor exit temperature and pressure may vary significantly as a function of excess combustor air under lean burn conditions, proposing a mathematical formulation for this relationship.

NGV inlet conditions, combustor boundary conditions, and combustion product composition are interrelated in a non-trivial manner. Even with the assumption of air as the working gas, the relationship between NGV inlet total temperature and NGV pressure ratio is not readily available. It is concluded that it would be inappropriate to correct for either the properties of air at a constant hot temperature, or for the properties of an unchanging combustion product. Within the scope of the present study, it is instead justified to quantify the aerodynamic phenomena that affect capacity under known conditions. Future work may refer to analysis herein to correct for temperature or product composition if those variables are known as a function of pressure ratio.

2.1.4 Non-uniform and non-adiabatic boundary conditions

The present study assumes uniform profiles for total temperature and pressure at the NGV inlet boundary. The outlet total temperature and pressure profiles of a contemporary annular combustor were found to possess minimal non-uniformity in the circumferential direction by Singh et al [4], and any such non-uniformity was found by Ranjith et al [5] to have minimal effect on total pressure loss within the combustor.

Heat transfer between the working gas and the NGV metal is also determined to be a mechanism unsuitable for inclusion in the present study. Extensive 3D CFD investigation of NGV conjugate heat transfer has been performed by Jiang et al [6], who simulated an NGV with internal coolant flow, trailing edge slot ejection, and end-walls. 3D heat transfer between the NGV and the end-walls was found to result in highly dissimilar heat fluxes across the NGV internal and external surfaces. This would be impossible to model using the 2D CFD used by the present study, where the net heat fluxes across the NGV section boundaries would necessarily sum to 0. The authors further noted that “the Biot number at the NGV internal/external surfaces is only 0.006 in the present heat transfer case, much less than 1. This means that the resistance of the heat conduction in the NGV solid regions is much less than that of the heat convection through its surfaces. As a result, the temperature distribution in the NGV body is mainly determined by the complex heat convection among the NGV body, external main flow, and internal cooling flow”, and that “local variations and bumps of the heat flux profiles are observed, which are determined by the local flow conditions and geometry.” None of these phenomena are resolvable by the present simulations and it is deemed superfluous to model them in unrealistic 2-dimensional form.

2.2 Precedent for analytical techniques used in this study

2.2.1 Definitions of loss

Loss may refer to any process whereby the recoverable energy of a turbomachinery flow is reduced during transit through a turbine stage, other than by shaft work, with corresponding entropy creation. Minimisation of loss remains a primary objective of turbomachinery design, but there is not a universal consensus on how to quantify it. As subsequent sections of this thesis will evaluate the losses caused by changes to the trailing edge of nozzle guide vanes, the purpose of this section is to review various definitions of loss from the literature and to facilitate the use of appropriate definitions in the present study.

Trinidade et al [7] characterised sources of loss as shock loss, profile losses, tip leakage, end-wall losses, and cooling losses. Tip leakage results from flow through the clearance space between blade tips and their annular casing. It will not be considered by the present study, since in the present study NGVs are cast along with their end-walls. End-wall losses result from 3-dimensional secondary flows, and will not be considered in the present study which is of 2-dimensional phenomena.

Trinidade et al [7] characterised shock loss as resulting from entropy creation across the shock wave during supersonic flow. The present study will consider this mechanism during discussion of CFD results at choking pressure ratios.

Profile loss was characterised by entropy creation by viscosity in the boundary layer on the blade surface. Entropy generated near the blade’s trailing edge was considered as profile loss due to the high entropy creation in the wake region following flow separation at the trailing edge. The authors

extended this definition to include the entropy generated as the flow turns tightly around the trailing edge curvature and forms expansion waves.

The authors also defined the category of cooling losses to refer to the aerodynamic penalties incurred by cooling in general, namely “thicker blade profiles from coolant holes, interaction of coolant film with the blade boundary layer, mixing losses between coolant and main flow and endwall losses.” The present study seeks to isolate the mechanisms whereby film cooling causes boundary layer changes and mixing effects, discussing film cooling in Chapter 5.

The present study seeks to define a coefficient of NGV total pressure loss whose arguments are flow measurements or numerically predicted parameters. It is first useful to consider the motivation for quantifying loss in terms of total pressure. This approach treats the nozzle guide vane problem analogously to the problem of flow in a rough pipe, where frictional forces must be balanced by a negative total pressure gradient in the downstream direction. The greater the sum of frictional forces, the greater the loss of total pressure between the inlet and outlet. Total pressure loss can thus aggregate all aerodynamic drag forces acting on the nozzle guide vane or other component.

In an experimental or computational domain, the total pressure loss between inlet and outlet is $p_{01} - p_{02}$. It is intuitive to normalise this against the upstream total pressure p_{01} but it is more useful to normalise it against $p_{01} - p_2$, where p_2 is the outlet static pressure. p_{02} never assumes a value greater than p_{01} nor less than p_2 , so if a total pressure loss coefficient is quantified as

$$C_{pt} = \frac{p_{01} - p_{02}}{p_{01} - p_2} \quad (2.3)$$

then the coefficient will be 0 in the case of no total pressure loss, and 1 in the extreme case of $p_{02} = p_2$.

Giel et al [8], whose findings will be discussed in Section 4.2, surveyed the total pressure wake profiles of a blade at mid-span. They defined a total pressure loss coefficient as in equation 2.3, where p_{01} and p_{02} were the inlet and wake total pressures, and p_2 was the wake static pressure.

Gao et al [9], whose findings will be discussed in section 4.1, defined a total pressure loss coefficient as

$$C_{Gao} = \frac{p_{01} - p_{02}}{p_{02} - p_2} \quad (2.4)$$

This definition is equivalent to normalising the total pressure loss against the downstream dynamic pressure. In the case of simulations where the boundary conditions p_{01} and p_2 are set, NGV geometry is the independent variable and p_{02} is the dependent variable. It is thus less convenient for the present study to use Gao et al’s [9] loss coefficient formulation, since it does not scale linearly across a range of p_{02} . The definition in equation 2.3 will be used for this reason.

Where subsequent sections are to compare the findings of Giel et al [8], Gao et al [9], and other studies of loss, it is required to formulate the total pressure loss coefficient consistently. Gao’s [9] definition of C_{pt} may be expanded by Taylor series on the constant p_{01} and as a function of p_{02} as

$$f(p_{02}) = f(p_{01}) + f'(p_{01})(p_{02} - p_{01}) + \frac{1}{2!}f''(p_{01})(p_{02} - p_{01})^2 + \dots \quad (2.5)$$

where $f^n(p_{01})$ may be shown by differentiation to be

$$f^n(p_{01}) = \frac{(-1)^n n!}{(p_{01} - p_2)^n} \quad (2.6)$$

This results in the following mappings between the two definitions of total pressure loss coefficient.

$$C_{Gao} = \sum_{n=1}^{\infty} C_{pt}^n \quad (2.7)$$

$$C_{pt} = \sum_{n=1}^{\infty} (-1)^{n-1} C_{Gao}^n \quad (2.8)$$

Since the total pressure loss coefficient quantifies loss as a summation of all drag forces on the NGV, loss may also be quantified as the total amount of kinetic energy dissipated between inlet and outlet, of the form

$$\zeta = \frac{KE_1 - KE_2}{KE_1} = 1 - \frac{KE_2}{KE_1} \quad (2.9)$$

Kinetic energy may be formulated using conservation of energy as

$$u = \sqrt{2 \left(\frac{\gamma}{\gamma-1} \right) \left[\frac{p_0}{\rho_0} - \frac{p}{\rho} \right]} \quad (1.9)$$

$$u = \sqrt{2 \left(\frac{\gamma}{\gamma-1} \right) RT_0 \left[1 - \left(\frac{p_0}{p} \right)^{\frac{1-\gamma}{\gamma}} \right]} \quad (2.10)$$

The flow's kinetic energy at a given station is thus of the form

$$KE(p) \sim u^2 \sim 1 - \left(\frac{p_0}{p} \right)^{\frac{1-\gamma}{\gamma}} \quad (2.11)$$

allowing equation 2.9 to be written as

$$\zeta = 1 - \frac{1 - \left(\frac{p_{02}}{p_2} \right)^{\frac{1-\gamma}{\gamma}}}{1 - \left(\frac{p_{01}}{p_2} \right)^{\frac{1-\gamma}{\gamma}}} \quad (2.12)$$

$$\zeta = \frac{\left(\frac{p_{01}}{p_{02}} \right)^{\frac{\gamma-1}{\gamma}} - 1}{\left(\frac{p_{01}}{p_2} \right)^{\frac{\gamma-1}{\gamma}} - 1} \quad (2.13)$$

This definition of kinetic energy loss coefficient was used by Giel et al [8]. Like the total pressure loss coefficient, it takes a value of 0 in the case of no loss where $p_{02} = p_{01}$, and 1 in the extreme case of $p_{02} = p_2$.

Saha et al [10] experimentally investigated the loss effects of shower-head and trailing edge cooling in an annular sector. By defining kinetic energy loss in 3 alternative ways, the authors demonstrated the extent to which computed loss can vary depending on definition. Discrepancies were shown to result from how the coolant kinetic energy is accounted for. Where the ratio of coolant mass flow rate to mainstream mass flow rate was Y , the authors defined kinetic energy loss as

$$\zeta = 1 - \frac{(1+Y) \left[1 - \left(\frac{p_2}{p_{02}} \right)^{\frac{\gamma-1}{\gamma}} \right]}{\left[1 - \left(\frac{p_2}{p_{01}} \right)^{\frac{\gamma-1}{\gamma}} \right] + Y \left[1 - \left(\frac{p_2}{p_{0c}} \right)^{\frac{\gamma-1}{\gamma}} \right]} \quad (2.14)$$

In the case of no coolant flow ($Y = 0$) this is equivalent to the definition in equation 2.13. Equation 2.14 is equivalent to the loss definition defined by Deckers and Denton [11] in the case of no significant temperature difference between coolant and mainstream, as in a significant proportion of experimental studies.

Where coolant flow is present, equation 2.14 requires a local value of Y in order to obtain the loss at any particular point. Assuming that the coolant concentration is a function of the local total pressure loss compared to an uncooled vane, the authors redefined Y as a function of spanwise distance x as

$$\frac{Y(x)}{Y_{max}} = \frac{p_{02uc} - p_{02}(x)}{|p_{02uc} - p_{02}|_{max}} \quad (2.15)$$

where p_{02uc} was the total pressure downstream of the cascade with no cooling, p_{02} was the total pressure downstream of the cascade as a function of spanwise distance (with cooling), and $|p_{02uc} - p_{02}|_{max}$ denotes the maximum possible difference in downstream total pressure between the uncooled and the cooled cases. Reasoning that this total pressure difference is maximal when $p_{02} = p_{01}$ and $p_{02} = p_{wake}$ (the total pressure in the wake region), Saha et al [10] thus defined their function for local coolant/mainstream mass flux ratio as

$$\frac{Y(x)}{Y} = \frac{p_{02uc} - p_{02}(x)}{p_1 - p_{02wake}} \quad (2.16)$$

By substituting this definition of Y into equation 2.14, Saha et al [10] arrived at their novel definition of kinetic energy loss intended to solve the problem of unphysical loss in the free-stream where the previous definition erroneously assumed the presence of coolant. Their new definition is able to use the nominal values for shower-head and trailing edge coolant mass flow ratio and adjust the coolant profile according to the aforementioned function of spanwise distance. Using measurements from a downstream traverse in their linear cascade, the novel loss definition was found to produce loss profiles that were in good agreement with equation 2.13 and in disagreement with equation 2.14.

2.2.2 Choice of turbulence model

REFERENCES THAT ARGUE AS TO sst's EFFECTIVENESS

From Jiang heat transfer: The SST k- \tilde{L} model (the shear-stress transport model) is selected to model turbulent transfer items in the flow. Major improvements are observed in the prediction of separation and adverse pressure gradient flows in comparison with the standard k- \tilde{L} and k- $\tilde{\epsilon}$ models [9]. This model has been successfully used in the heat transfer simulation for the film cooling of a linear cascade, and the results are in good agreement with the experimental measurements [3].

REFERENCES THAT SHOW sst IS COMMONLY USED SUCCESSFULLY FOR TURBOMACHINERY

2.3 Chapter Conclusions

Chapter 3

Geometric throat area

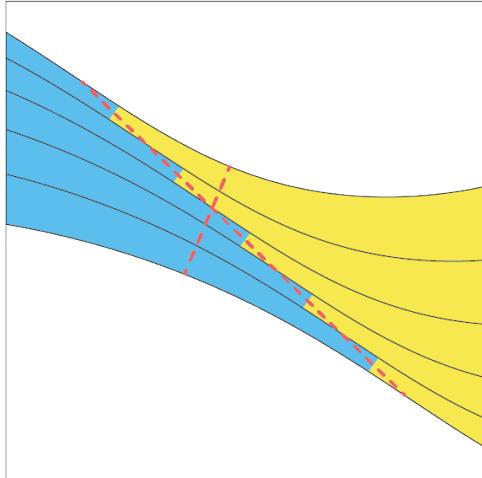
A 1-dimensional supersonic nozzle is equivalent to a single streamline of variable cross-sectional area. It is possible to solve for the flow conditions throughout the nozzle, provided area is specified as a function of position along the nozzle. The mass flow rate capacity is a function of only the flow's minimum area, as in equation 1.17.

A 2-dimensional isentropic fully choked nozzle may be modelled as a group of adjacent streamlines, each of which may have dissimilar area functions. It is notable that the streamlines' minimum areas may not correspond to a straight line across the narrowest part of the nozzle. This is illustrated in Figure 3.1a by supposing the division of a 2-dimensional flow into a finite number of streams of finite width. Each stream has an individual point of minimum width where sonic conditions exist, shown as the transition between subsonic flow in blue and supersonic flow in yellow. These sonic points are distributed on a line distinct from the overall passage line of minimum width. The resulting minimum area line is shown in red along with the geometric minimum area line, to illustrate their disparity.

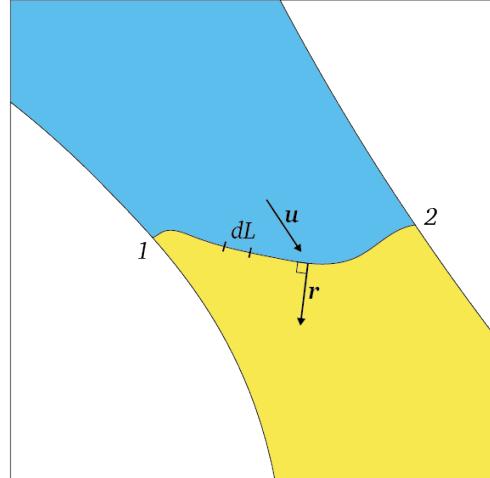
If this concept is extended to infinitesimal streamlines (and the flow is isentropic) each streamline will experience sonic conditions at its point of minimum area, coalescing to form the 2-dimensional sonic line. The effective throat area of a 2-dimensional nozzle is thus the sum of its streamlines' throat areas. This is distinct from the sonic line length, and may be expressed by the integral

$$A_{eff} = \int_1^2 \hat{u} \cdot \hat{r} dL \quad (3.1)$$

where \hat{u} is the unit vector of local flow velocity, \hat{r} is the unit vector perpendicular to the local sonic line, and the integral is performed on the scalar infinitesimal dL over the length of the sonic line, as illustrated in Figure 3.1b.



(a) Different minimum area points of dissimilar streams



(b) Integral for 2D nozzle equivalent throat area

Figure 3.1: Considerations for defining the minimum area of an arbitrarily shaped nozzle in choked compressible isentropic flow, where blue areas lie upstream of each stream tube throat and yellow downstream

In the case of 1-dimensional nozzle flow, Equation 3.1 collapses to the value of the throat area. In the case of 2D flow through an arbitrarily shaped nozzle such as a gas turbine nozzle guide vane, the integral describes the infinitesimal sum of the areas encountered by each streamline at the point of sonic conditions. It is proposed as a physically sensible 2D extension of the 1D concept of throat area, as opposed to finding the narrowest point across the passage to obtain a geometric throat area.

For a fully choked streamline, flow conditions upstream of the sonic line are independent of those downstream. This facilitates an analytical approach where the flow conditions immediately upstream of any choked streamline's sonic point are treated as a known state. That streamline's mass flow rate is wholly a function of that state, thus the mass flow rate of a fully choked 2D nozzle is wholly a function of its A_{eff} as derived from its sonic line. For an unchoked streamline, its mass flow rate is a function of the state of every point along the streamline, including points downstream of where sonic conditions would appear in choked cases. It is thus advantageous to supplement design-condition simulations with simulations at a pressure ratio where the nozzle guide vane is guaranteed fully choked, allowing for analysis of a fully-formed sonic line and computation of a corresponding A_{eff} .

The present study will nonetheless discuss the reasons for which geometric throat area remains a useful predictor of NGV flow capacity in many cases, as has been noted in the literature. Thirumurthy et al [12] discussed the challenges and uncertainties associated with the accurate matching of an aeroderivative gas generation turbine. The authors' focus was on various means of predicting capacity to facilitate proper matching. The authors noted that "the throat area of any blade or vane row has a strong influence on the overall capacity of the turbine. The vane or blade throat plane...is defined as the plane formed by the smallest passage area normal to the flow path. The effects are of first order when the throat area is changed for the first stage of the turbine." The prior discussion of effective area is in agreement with this statement. If 2D nozzle throat width is varied in a way that does not significantly affect the sonic line shape, effective area and thus choked mass flow rate would be expected to vary to first order. This hypothesis is tested in this chapter.

3.1 Nozzle guide vane capacity uncertainty in 2 dimensions

The immediate challenge in quantifying 2D nozzle flow capacity is that analytical approaches are incomplete. If any nozzle's A_{eff} could be inferred from its geometry, it would be possible to investigate the effects of the geometry on the flow capacity to a high degree of accuracy, but the only way to find A_{eff} is to solve the flow computationally to obtain the sonic line. Once a CFD solution has been obtained, the flow capacity is necessarily also obtained.

Those concerned with mapping NGV geometry onto flow capacity are thus presented with 2 options: either perform CFD on every conceivable shape of NGV and create a lookup table of arbitrary fidelity, or analyse a relatively small set of CFD solutions to create heuristics about what types of geometric changes cause what types of changes to the shape of the sonic line and local flow vectors. Furthermore, a typical starting point for a commercial engine designer is to conduct a 2D analysis based on a previous "successful" engine design, with some cooling features included. This has necessarily limited design changes, and has led to local optimisation within a very small design envelope.

3.1.1 Geometry, mesh, and boundary conditions

Rolls-Royce plc have provided the present study with a family of NGV geometries suitable for such an approach, all from the Trent 900 engine. Geometric variation among Trent 900 NGVs has been subject to extensive measurement by Rolls-Royce. In one such set of studies, Hall [13] and Zamboni [14] produced geometric definitions of 6 NGVs. These 6 NGVs are members of 2 slightly different production standards within the Trent 900 NGV family, which are referred to by the company as the M-skew standard and the EP1 standard. Rolls-Royce randomly selected three production NGVs from each standard and measured their surface geometries using the *white light/GOM* scanning method. This resulted in the 6 geometric definition files used by Hall [13] and Zamboni [14], which were provided to the present study. These files do not include film cooling holes or the trailing edge slot. The trailing edges are smoothly rounded.

Variations exist among the geometry of the 6 NGVs, even when cooling features are not accounted for. Although these variations are of the order of 0.5 mm, they are sufficiently large to significantly affect flow capacity. Zamboni [14] described the process for quantifying these variations in 3D, which will be discussed in Section 3.2. The present study defined an approach for deriving 2D geometries from the 3D files and quantifying the variations among them.

The 3D NGV surface shape was provided by Rolls-Royce as a set of co-ordinates which define 21 closed loops on the vane surface. Each loop consists of a pair of streamlines which diverge from a stagnation point on the vane's leading edge and converge at the trailing edge. The 11th loop was thus considered to be the closest approximation to a mid-span slice of the NGV. Matlab was used to process the 3D curve of the 11th loop, producing a 2D section via the following process.

1. Project the loop's coordinates onto a cylindrical surface whose radius is equal to the NGV annular radius at mid-span.
2. Periodically repeat the resulting shape in the circumferential direction to create an annulus of 2D vanes wrapped around the cylinder.
3. Transform the annulus into an infinite 2D linear cascade by taking the circumferential coordinate to be a vertical coordinate.

This process is illustrated in Figure 3.2.

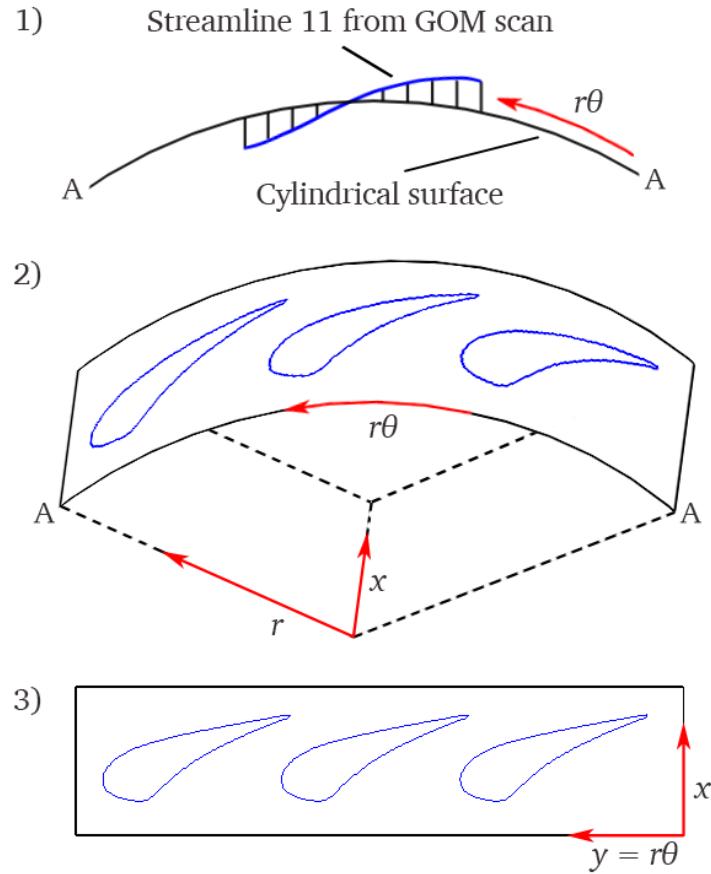


Figure 3.2: Creation of a 2D mid-span approximation of NGV geometry

The resulting coordinates were connected to form a closed body. This body was placed in a computational domain consisting of a straight inlet section, a curved turning section, and a straight outlet section inclined at the NGV turning angle. The domain was modelled in Ansys Fluent, where the inlet boundary was specified to have total pressure p_{01} and the outlet boundary was specified to have static pressure p_2 . The remaining domain boundaries were made periodic with one another to preserve the 2D linear cascade. The NGV surface boundary was specified as a solid wall with a no-slip boundary condition and no heat conduction. The resulting computational domain is illustrated in Figure 3.3. On the outlet boundary, labels 0 and 1 denote the start and end points for the wake surveys that will be presented in Chapter 4.

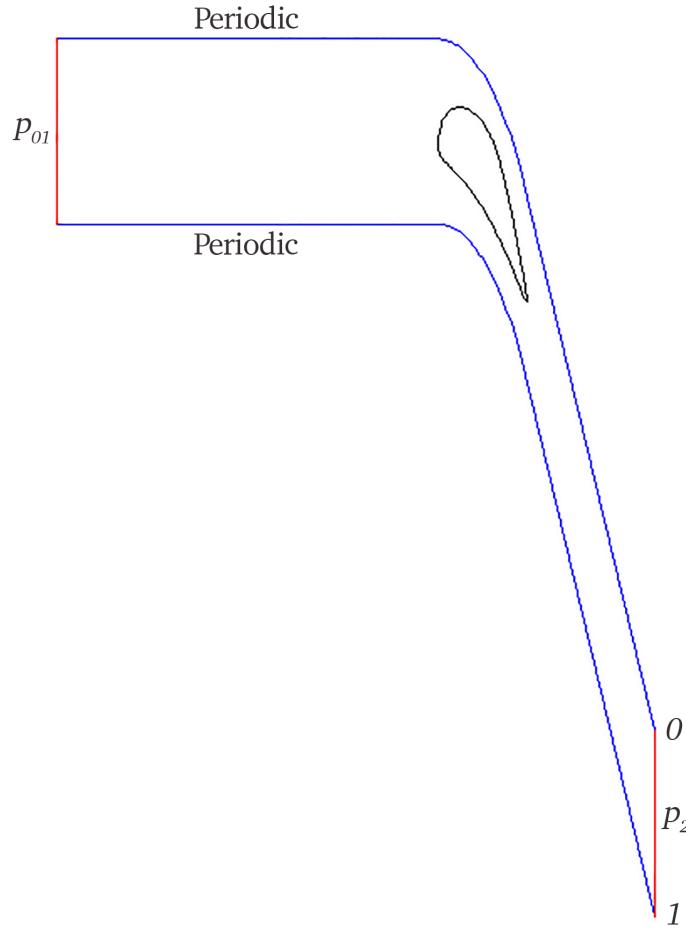


Figure 3.3: Domain and boundaries for the present 2D CFD study

This configuration has been the basis for all other 2D CFD analyses in this thesis, where additional boundaries are added to account for cooling features as required. Values for the simulation were set according to Table 3.1.

Table 3.1: Boundary conditions at design pressure ratio for Trent 900 multi-vane capacity study

Parameter	Value
NGV series	Rolls-Royce Trent 900
NGV turning (degrees)	76.89
Inverse pressure ratio $\frac{p_{01}}{p_2}$	1.79, 3.33
Inlet total pressure (Pa)	4.33×10^6
Inlet total temperature (K)	300
Outlet static pressure (design) (Pa)	2.42×10^6
Outlet static temperature (K)	300
Solver type	Density-based
Cell count	35,000

For turbomachinery flows of this type, the boundary layer thickness will be shown to be large enough to significantly affect the NGV throat area. The mesh must resolve the whole boundary layer within a

region of high resolution which is sufficiently large to cover the maximum boundary layer thickness. The maximum thickness of a turbulent boundary layer is approximated by the formula

$$\delta \approx 0.37 \frac{L}{Re^{\frac{1}{5}}} \quad (3.2)$$

where L is the characteristic length in the direction of the flow (the approximate NGV chord length) and Re is the Reynolds number. The Reynolds number is defined as

$$Re = \frac{uL\rho}{\mu} \quad (3.3)$$

where u is a representative value for flow velocity and μ is the dynamic viscosity of the fluid within the temperature range of the flow. For compressible flow, the velocity and density are substituted to give

$$Re = \frac{M \sqrt{\gamma RT} L \frac{p}{RT}}{\mu} \quad (3.4)$$

For isentropic flow, this may be expressed in terms of total temperature and pressure as

$$Re = \frac{L}{\mu} \sqrt{\frac{\gamma}{R}} \frac{p_0}{\sqrt{T_0}} M \left(1 + \frac{\gamma - 1}{2} M^2 \right)^{\frac{\gamma+1}{2(1-\gamma)}} \quad (3.5)$$

Equation 3.5 was used to compute a Reynolds number for the case of choked or near-choked NGV flow with the following values, based on the values specified in Table 3.1.

Table 3.2: Values for computing an approximate Reynolds number for an NGV passage

Parameter	Value
L	0.08 m
μ	19×10^{-6} Pas
p_0	4.33×10^6 Pa
T_0	300 K
γ	1.4
R	$287 \text{ Jkg}^{-1}\text{K}^{-1}$
M	1

This resulted in a value of $Re = 4.2 \times 10^7$. Maximum boundary layer thickness was thus estimated using equation 3.2 to be 1 mm. This is of the order of 10% of the NGV throat width, so full resolution of the boundary layer is required for any CFD study of the effects of NGV geometric changes.

The NGV surface was enclosed in a structured quadrilateral mesh which extended out by 2 mm. Compared to the estimated maximum boundary layer thickness, the factor of 2 ensured that the whole boundary layer was captured, reduced the gradient of cell size change within the boundary layer mesh, and provided additional resolution within the base region downstream of the trailing edge, where boundary layer separation and entropy generation occur amid high surface curvature.

Full resolution of the boundary layer required placement of mesh elements within the laminar sub-layer. Regions within the boundary layer were assumed to be divided according to the *universal law of the wall*. This boundary layer model is derived from experimental measurements and dimensional analysis performed by Nikuradse [15]. The author's motivation was the need to predict the velocity

profile and thickness of turbulent boundary layers, given the free-stream conditions. The work is of renewed importance in the context of contemporary CFD such as the present study, where knowledge of appropriate boundary layer mesh resolution is mandatory.

Nikuradse [15] showed that turbulent boundary layers in general exhibit a high degree of dimensional similarity if distance from the wall y is appropriately non-dimensionalised. The assumption was that qualitatively distinct regions of the boundary layer may be characterised by a dimensionless number that takes the place of y . Regions closer to the wall are expected to be dominated by viscous forces, and regions closer to the free-stream are expected to be dominated by inertial forces. The dimensionless wall distance parameter is thus expected to take similar form to the Reynolds number. It is defined as

$$y_+ = \frac{u_f y \rho}{\mu} \quad (3.6)$$

where u_f is the friction velocity, defined as

$$u_f = \sqrt{\frac{\tau_w}{\rho}} \quad (3.7)$$

where τ_w is the shear stress at the wall boundary. Equation 3.7 thus characterises the wall shear stress as a velocity which is used in the Reynolds-type formulation of Equation 3.6. τ_w is defined as

$$\tau_w = \frac{1}{2} C_f \rho u^2 \quad (3.8)$$

where C_f is a coefficient of skin friction and u is the free-stream velocity. C_f may be computed from the free-stream Reynolds number according to the correlation proposed by Schlichting [16]

$$C_f = (2 \log_{10} Re - 0.65)^{-2.3} \quad (3.9)$$

For isentropic compressible flows, equation 3.8 may be expressed as

$$\tau_w = \frac{1}{2} C_f \frac{p}{RT} M^2 \gamma RT \quad (3.10)$$

$$\tau_w = \frac{1}{2} C_f \gamma p_0 M^2 \left(1 + \frac{\gamma-1}{2} M^2\right)^{-\frac{\gamma}{\gamma-1}} \quad (3.11)$$

allowing a compressible expression of u_f as

$$u_f = \sqrt{\frac{\frac{1}{2} C_f \gamma p_0 M^2 \left(1 + \frac{\gamma-1}{2} M^2\right)^{-\frac{\gamma}{\gamma-1}}}{\rho_0 \left(1 + \frac{\gamma-1}{2} M^2\right)^{-\frac{1}{\gamma-1}}}} \quad (3.12)$$

$$u_f = \sqrt{\frac{C_f \gamma R T_0 M^2}{2 + (\gamma - 1) M^2}} \quad (3.13)$$

and allowing a compressible expression of y_+ as

$$y_+ = \sqrt{\frac{C_f \gamma R T_0 M^2}{2 + (\gamma - 1) M^2}} \frac{y}{\mu} \frac{p_0}{R T_0} \left(1 + \frac{\gamma-1}{2} M^2\right)^{-\frac{\gamma}{\gamma-1}} \quad (3.14)$$

$$y_+ = \frac{y}{\mu} \sqrt{\frac{\gamma}{R}} \frac{p_0}{\sqrt{T_0}} \sqrt{\frac{C_f}{2}} M \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (3.15)$$

This expression is of similar form to the expression for Reynolds number in equation 3.5. Both are shown to be a function of Mach number and of the upstream conditions $\frac{p_0}{\sqrt{T_0}}$. If these expressions are normalised against the upstream conditions in a similar way to flow capacity, it is shown that both the dimensionless speed Re and the dimensionless boundary layer thickness y_+ are purely functions of Mach number and of a geometric parameter – L and y respectively. This is subject to the assumptions that μ is approximately constant within the range of temperatures and $\sqrt{\frac{C_f}{2}}$ is approximately constant for sufficiently high Reynolds numbers.

Equation 3.15 may be rearranged to compute a real distance y from the wall given a value of y_+ . In the general case of turbulent boundary layers, the laminar sublayer occupies the region of $y_+ < 5$. The present study placed the first layer of mesh nodes at a wall distance of $0.3 \mu\text{m}$ corresponding to a y_+ value of 5. This is in accordance with a study of laminar sublayer resolution by Salim and Cheah [17]. The size of the first layer of mesh nodes was confirmed by measurement of the mesh after generation.

Within the structured boundary mesh, element size was grown so that the outermost elements had an aspect ratio of approximately $\frac{1}{2}$. Beyond this, the domain was populated with an unstructured quadrilateral-dominant mesh. Node distributions along the two periodic boundaries were made identical, and nodes adjacent to the structured boundary layer mesh were made to match its outermost node distributions. Within the general domain, unstructured mesh generation was automated using Ansys Fluent's built-in meshing feature. The resulting mesh formed the basis for all other 2-dimensional NGV meshes in the study. The mesh and periodic pattern are depicted in Figure 3.4 and details of the mesh, showing the structured boundary layer treatment, are depicted in Figure 3.5.

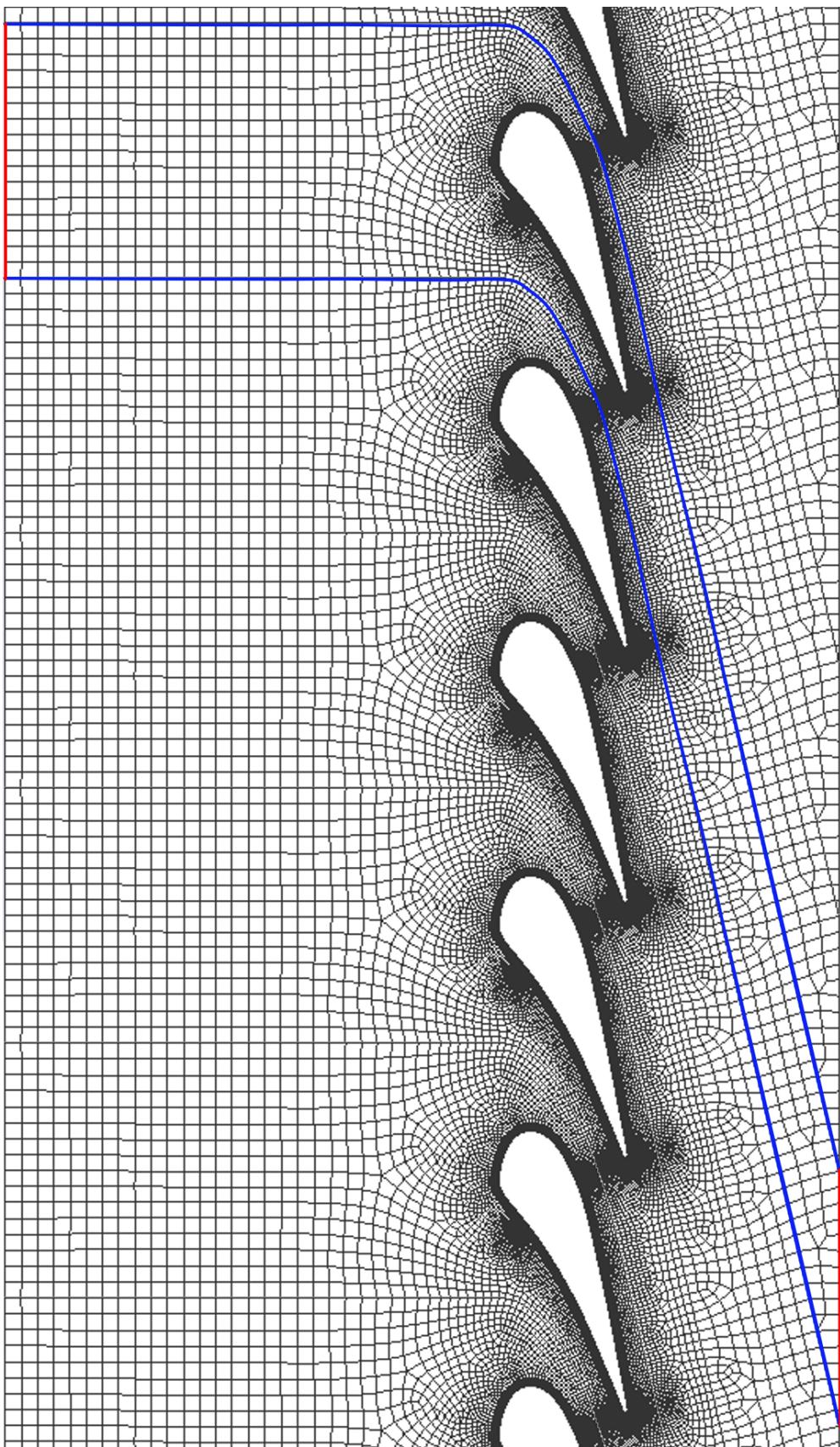


Figure 3.4: Mesh for Trent 900 throat width variation study, inlet and outlet boundaries shown in red, periodic boundary shown in blue

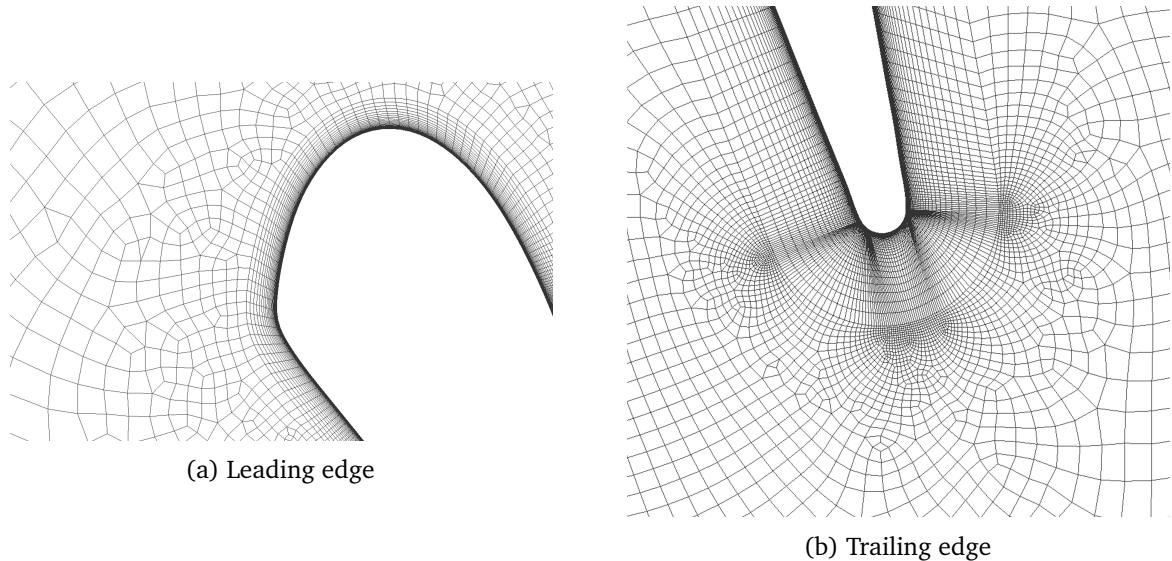


Figure 3.5: Details of mesh for Trent 900 throat width variation study

The described mesh and boundary condition specifications were used to perform a series of CFD simulations of each of the 6 2D NGVs in Ansys Fluent 2020 R2. Solutions were initialised using the solver's built-in FMG initialisation. This procedure automatically constructs a coarser version of the supplied mesh, on which an initial solution is converged before refinement to the final resolution. More detailed explanation of the scheme is provided by Ansys [18]. A script in the Fluent Journal language was used to produce solutions at incrementally increasing inverse pressure ratios of between 1.5 and a fully choked inverse pressure ratio of 3.33. NGV mass flow rate was saved at each pressure ratio. Full solution data were saved for the final fully choked pressure ratio to enable analysis of the shocks, expansions and sonic line at choked conditions. There were 32 increments of pressure ratio, and typical overall solution times were approximately 10 hours. The $k-\omega$ SST turbulence model was used. For these simulations and all others described in this thesis, convergence was determined by the outlet mass flow rate fluctuating by a factor of 10^{-6} or less. Mesh independence was verified by incrementally refining the mesh in Fluent and again confirming the outlet mass flow rate did not fluctuate significantly.

3.1.2 Effect on 2D capacity

Figure 3.6 shows contours of Mach number for one of the 6 solutions (vane KSZ03) at a fully choked pressure ratio. Streamlines released from the domain inlet illustrate the flow path through one of the vane passages. Figure 3.7 shown contours of Mach number for the same solution in the throat region.

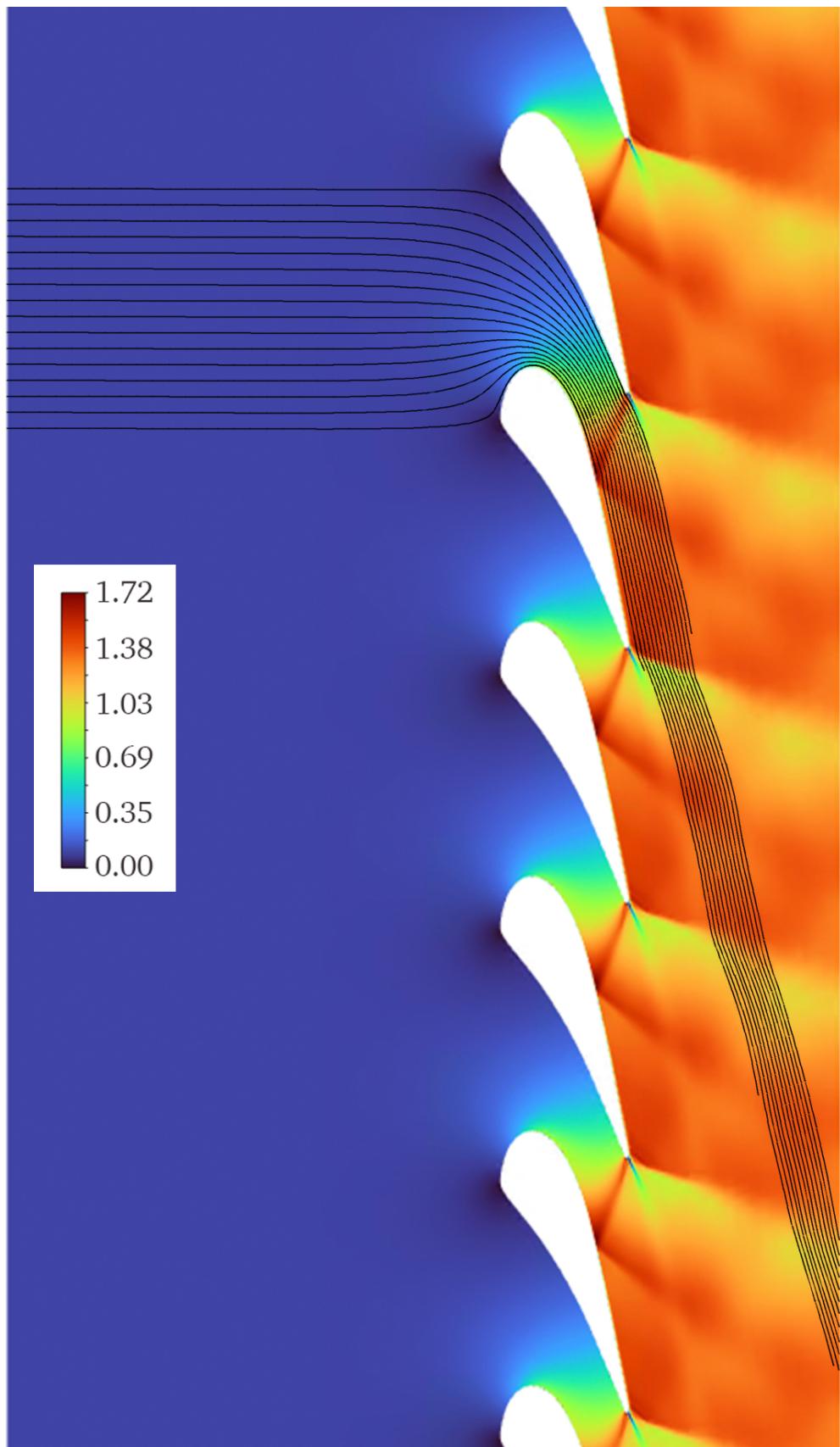


Figure 3.6: Contours of Mach number for whole solution on Trent 900 vane KSZ03 at $\frac{p_{01}}{p_2} = 3.33$ with streamlines illustrating flow through a single vane passage

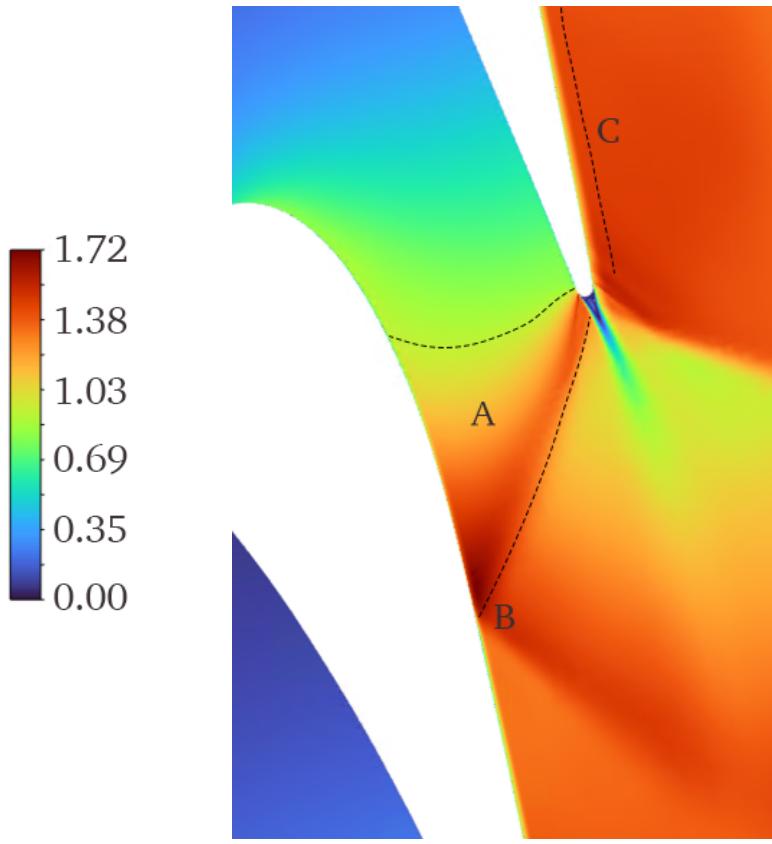


Figure 3.7: Contours of Mach number for solution near throat on Trent 900 vane KSZ03 at $\frac{p_{01}}{p_2} = 3.33$

Figures 3.6 and 3.7 illustrate the presence of developed supersonic flow phenomena downstream of the throat. Expansion fans are observed as the flow expands through the region labelled A around the NGV trailing edge (which is not shaped this way in reality). Shockwaves are subsequently induced as the effective passage narrows due to the presence of the trailing edge wake. The pressure side shockwave reflects off the suction side of the adjacent NGV at the point labelled B, in a similar fashion to supersonic nozzle shock diamonds. These phenomena are in agreement with commonly seen flow features of NGVs in the supersonic regime. Figure 3.7 also illustrates the growth of a boundary layer on the downstream suction side of the NGV, labelled C. This boundary layer's interaction with the sonic line will be subsequently discussed in the context of its effect on flow capacity.

Figure 3.8 plots percentage changes in the flow capacity of the 6 NGVs (defined by equation 1.12 and quantified by the upstream boundary conditions in Table 3.1) against inverse pressure ratio $\frac{p_{01}}{p_2}$. Capacity changes are normalised against the capacity of vane KSZ03 at the design pressure ratio.

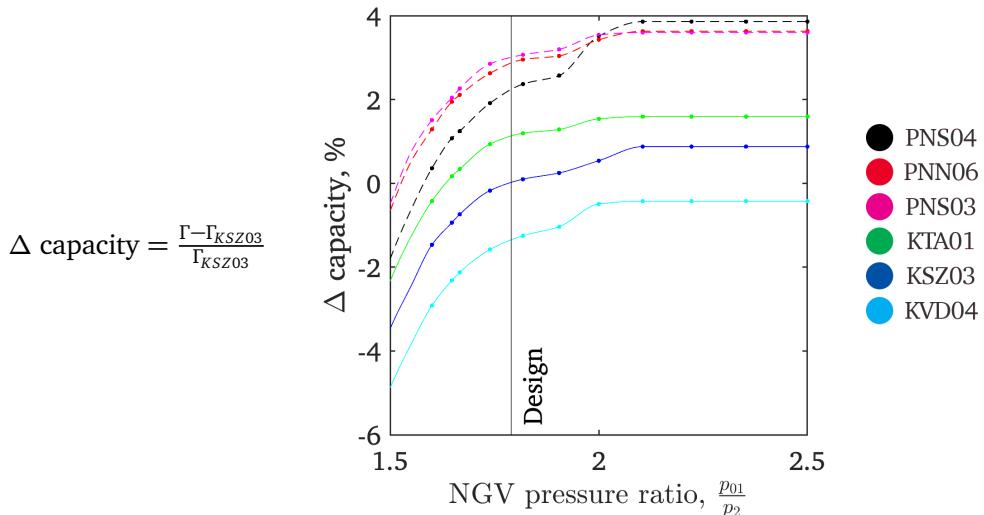


Figure 3.8: 2D normalised capacity as a function of pressure ratio for 6 Trent 900 NGVs

Differences are seen to exist between the capacity trends of the 6 NGVs. Across the range of pressure ratios, all 6 NGVs exhibited a range of approximately 4% capacity difference. Although the NGVs were all fully choked at the greatest inverse pressure ratio, separate NGVs became choked at significantly different pressure ratios, suggesting that the formation of transonic flow features occurred in different locations between the 6 NGVs. The capacity trends are seen to be broadly divided between the M-skew family (K- serial numbers) and the EP1 family (P- serial numbers). The 3 M-skew NGVs had comparatively lower flow capacities than the EP1 NGVs at all pressure ratios. The capacities of the EP1 NGVs had comparatively small variation from one another across pressure ratios, but their homogeneity was broken by vane PNS04, which had the lowest flow capacity of the family at low inverse pressure ratio, but switched to have the highest flow capacity at high inverse pressure ratio.

The differing capacity trends may be further discussed by inspecting the shape of the sonic lines formed in the throat regions of the 6 NGVs at a fully choked pressure ratio. These sonic lines are depicted in Figure 3.9 along with the lines of minimum length between the adjacent NGVs of each standard.

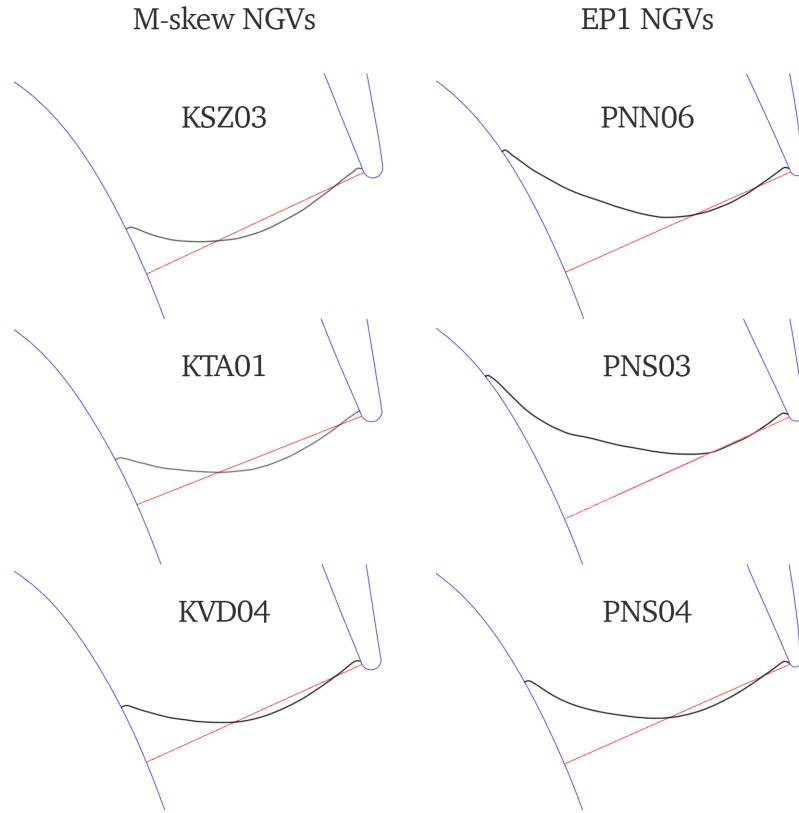


Figure 3.9: Sonic lines for 6 Trent 900 NGVs at $\frac{p_{01}}{p_2} = 3.33$

In Figure 3.9, a trend is visible of the M-skew sonic lines exhibiting smaller deviation from the line of minimum width, compared to the sonic lines of the EP1 NGVs. This suggests that a design choice resulted in a difference in the aerodynamics of the two families of NGV, such that upstream regions of the EP1 flow field reached sonic conditions significantly further upstream of the geometric throat compared to the M-skew flow field. Vane PNS04 presented a significantly different sonic line shape which is taken to correspond to its significantly different capacity trend compared to the other 2 vanes in its family. It is suggested that its relatively flow-orthogonal sonic line is caused by aerodynamic features that also cause its relatively sudden increase in capacity prior to choking. This cannot be confirmed in the absence of a statistically significant number of NGV geometries to compare.

It is further noted that significantly different capacity trends are exhibited by NGVs with similar sonic line shapes. For example vanes KVD04 and PNS04, whose sonic lines are similar in comparison to other vane pairings, exhibit the largest difference in their capacity across the range of pressure ratios. Although this is attributable to differences in geometric and effective throat area as subsequent analysis discusses, these 2 vanes' capacity trends also show significant qualitative differences. Their capacities are more different at fully choked pressure ratios than at lower pressure ratios. This suggests that the vanes possessed dissimilar passage areas in regions upstream and downstream of the throat, and that these dissimilarities acted to reduce their capacity difference at unchoked pressure ratios. Although most obvious when comparing these 2 vanes, this effect is concluded to be present to an extent among all 6 vanes.

Matlab was used to calculate the minimum throat width of each 2D NGV. The resulting values are given in Table 3.3.

Table 3.3: Throat widths of 6 Trent 900 NGVs

Production standard	Serial number	Throat width (mm)
M EP1	PNS04	12.7
	PNN06	12.7
	PNS03	12.7
M-skew	KTA01	12.5
	KSZ03	12.4
	KVD04	12.2

Discussion is warranted of the relationship between flow capacity and throat area. Consideration is to be made of both throat area in its pure geometric form A , and its effective form A_{eff} as defined in equation 3.1. Figure 3.10 plots the 6 NGVs' variations in capacity at design pressure ratio against their variations in geometric throat width. Capacity changes are normalised against the capacity of vane KSZ03 at the design pressure ratio. Throat width changes are normalised against the geometric throat width of vane KSZ03. The averages of the M-skew and EP1 families are plotted and lines of gradient 1 are plotted intersecting the average values, such that any deviations from 1-dimensional compressible flow correspond to deviations from the lines of gradient 1.

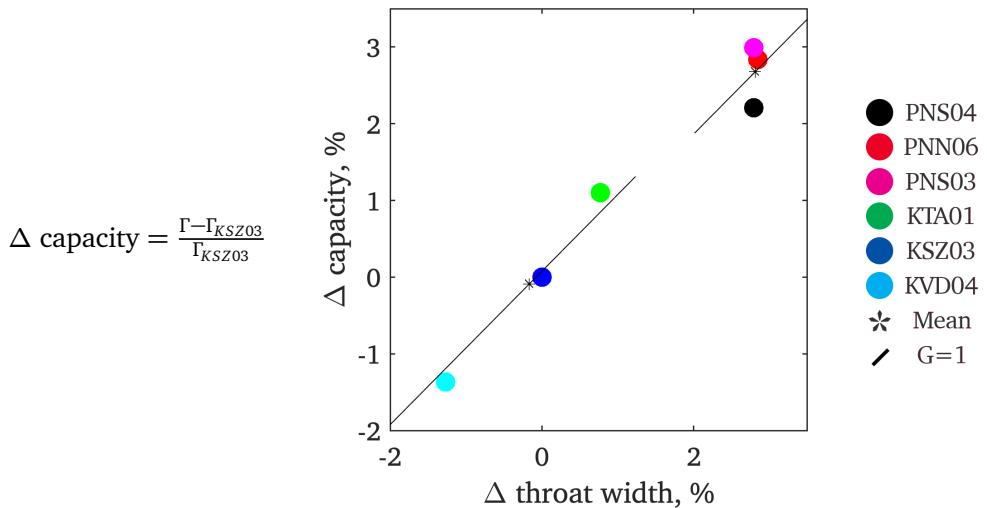


Figure 3.10: 2D capacity percentage delta as a function of 2D throat width for 6 Trent 900 NGVs at $\frac{p_{01}}{p_2} = 1.79$ (design)

The 6 NGVs are seen to approximately conform to a directly proportional relationship between geometric throat width and flow capacity, suggesting that geometric throat width is a good estimator of flow capacity among NGVs without significant differences in aerodynamic design. The M-skew vanes exhibited notable conformity to this trend. This is in agreement with the observed homogeneity between the M-skew sonic line shapes. It is suggested that, among the 3 vanes, the 2-dimensional sonic line shapes were scaling linearly with the shape of the geometric throat line, resulting in the observed linear relationship between geometric throat width and flow capacity despite the presence of a 2D flow field. 2D flow features appear to scale proportionately provided the sonic line scales proportionately.

In contrast, no correlation was observed between throat area and flow capacity among the EP1 NGVs.

Speculation may be limited to the observation that the qualitatively distinct PNS04 vane exhibited significantly lower flow capacity than the other 2 despite having almost identical geometric throat areas. This highlights the difficulty in developing an *a priori* understanding of the observed capacity changes, even with knowledge of the NGV geometries as manufactured.

Although NGV throat width is a good predictor of NGV flow capacity if aerodynamics do not vary significantly, it is not useful if the sonic line is subject to unpredictable changes in shape and location. The resulting heuristic fails to account for the fact that the majority of streamlines within the flow reach sonic conditions at a point other than their point of minimum width. This discrepancy may be investigated by quantifying the effective throat width of each case, instead of the geometric throat area. Matlab was used to implement the integral

$$A_{eff} = \int_1^2 \hat{u} \cdot \hat{r} dL \quad (3.1)$$

To achieve this, results for M and x and y velocity components were exported from each Fluent solution. These data were imported into Matlab and interpolated onto a structured quadrilateral grid which covered the region around the throat between 2 adjacent NGVs. Within this domain, data points corresponding to the sonic line were identified using an algorithm to detect the cross-over from $M < 1$ to $M > 1$. A subsequent algorithm was used to order and connect these points into a sonic line. It was then possible to compute the local velocity unit vector \hat{u} and local unit vector orthogonal to the sonic line \hat{r} at each point, and to perform the integral.

This resulted in Figure 3.11, which plots the 6 NGVs' variations in capacity at design pressure ratio against their variations in effective throat width. Capacity changes are normalised against the capacity of vane KSZ03 at the design pressure ratio. Effective throat width changes are normalised against the effective throat width of vane KSZ03. Because the concept of A_{eff} is designed to account for generalised variations between NGVs, Figure 3.11 does not group the NGVs into 2 separate families. A line of gradient 1 is plotted and positioned on the y axis to fit the data. It is notable that this line does not correspond to the line $y = x$, but instead corresponds to a negative offset in capacity. This suggests the presence of boundary layer effects which reduced the capacity compared to the values which effective throat area alone would predict.

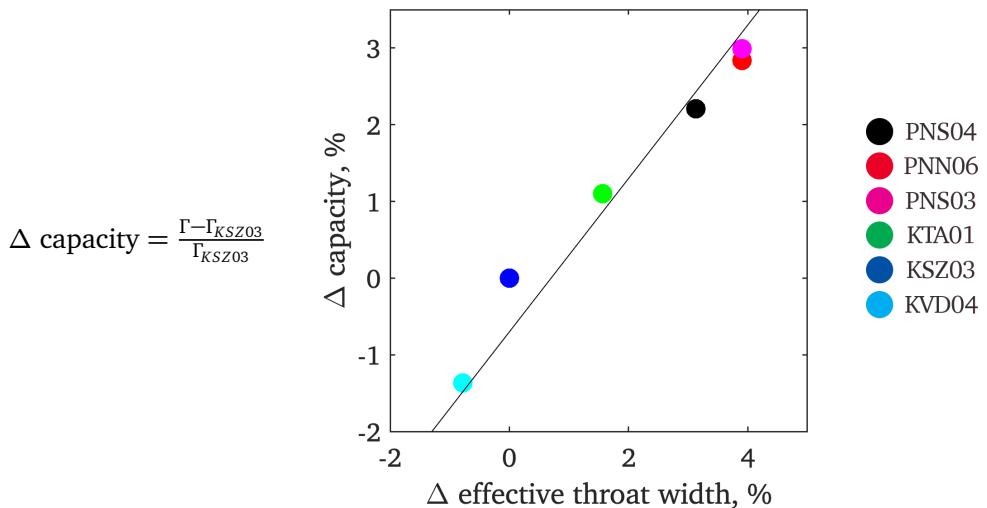


Figure 3.11: 2D capacity percentage delta as a function of effective throat width (as defined by equation 3.1) for 6 Trent 900 NGVs at $\frac{p_{01}}{p_2} = 1.79$ (design)

Figure 3.11 demonstrates the viability of the A_{eff} approach. All six vanes approximately show a directly proportional relationship between flow capacity and effective throat width. This is in agreement with the assumption that the integral definition of A_{eff} amounts to the summation of the 1-dimensional throat widths of every streamline in the flow. However, 3 of the NGVs exhibit significant deviation from direct proportionality, suggesting that the use of the sonic line fails to account for regions of the flow which remain subsonic given that the flow is largely unchoked. A possible refinement to the A_{eff} approach may be to combine it with a prediction of the boundary layer thicknesses at the points where the sonic line meets the suction side and pressure side of the NGVs. Heuristics may be developed to relate the touch-down points with the predicted boundary layer thicknesses and thus the degree of A_{eff} over-estimation caused by the inclusion of subsonic flow. This would result in a metric which is directly proportional to choked 2D capacity and closely correlated with 2D capacity at the design pressure ratio.

A_{eff} remains computable only in the event that a CFD solution has been obtained, by which point flow capacity is already predicted. The next goal is to find an aspect of NGV geometry which can be shown to have a reliable effect on the shape of the sonic line. In this way, the geometric change will have been shown to account for a known change in A_{eff} , which has itself been shown to account for known changes in flow capacity in 2 dimensions. Since the M-skew and EP1 families exhibit clear differences in the sonic conditions which are present upstream of the geometric throat, future studies may examine whether NGVs can be reliably designed to have sonic lines whose shape is predictable. If the sonic line is known by design to be approximately orthogonal to the flow and non-susceptible to fluctuation, it is safe to rely on just 2D geometric throat width to predict variations in NGV flow capacity in 2 dimensions.

3.2 Comparison of 2D capacity predictions with 3D data

The present study compared the 2D data presented in Section 3.1 with Rolls-Royce's 3D CFD predictions of the flow capacities of the same 6 NGVs. The motivation was to analyse the differences between the 2D throat length vs capacity relationship and the 3D throat area vs capacity relationship. The analytical techniques of Section 3.1 were translated to this 3D relationship where possible. As with the 2D study, the 3D vanes were uncooled, as were the vane platforms.

3.2.1 Effect on 2D capacity versus 3D capacity

Figure 3.12 plots percentage changes in the flow capacity of the 6 NGVs (defined by equation 1.12 and quantified by the upstream boundary conditions in Table 3.1) against inverse pressure ratio $\frac{p_{01}}{p_2}$. Capacity changes are normalised against the 3D capacity (as stated by Rolls-Royce) of vane KSZ03 at the design pressure ratio.

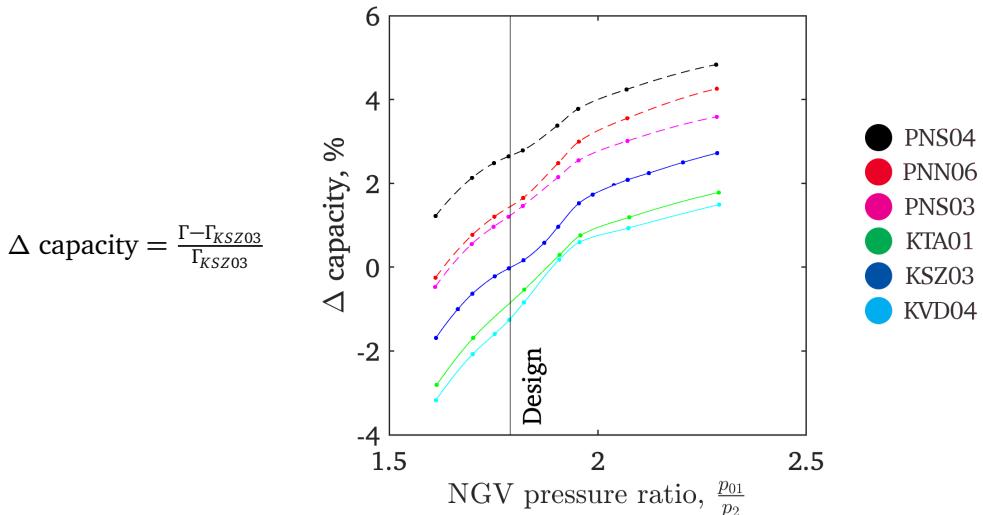


Figure 3.12: 3D normalised capacity as a function of pressure ratio for 6 Trent 900 NGVs

The predominant feature of Figure 3.12 is the continued rise in capacity with pressure ratio, in contrast to the 2D simulations where capacity plateaued between inverse pressure ratios of 2.0 and 2.2 for all 6 NGVs. This suggests that none of the NGVs reached a fully choked condition over the entire range of pressure ratios. While regions of the NGV span must be choked at these higher inverse pressure ratios, a 3D NGV passage will exhibit secondary flow structures leading to progressive choking. A sufficiently high inverse pressure ratio will result in a flattening of the capacity trend as choking cannot progress further, but this limiting condition is not reached by the range of pressure ratios in the data provided by Rolls-Royce. This alone is sufficient to preclude the present A_{eff} approach in these 3D cases, since it has been shown to be limited even by the presence of thin boundary layers in the 2D cases. In this case, a sonic surface may not exist as a flow-limiting condition, as there are unchoked alternative flow paths across the NGV span.

Zamboni [14] defined the Rolls-Royce process for calculating 3D throat area as follows: “Along each vane span section, the throat line is defined as that line which connects the trailing edge of one vane with the point of minimum distance on the suction surface of the nearby vane in the tangential direction. For a vane with a trailing edge slot, the trailing edge point is defined as the start of the cut back... The throat surface interpolates all the throat lines spanwise.” It is notable that the engine maker has defined the geometric throat by assuming the trailing edge point to be the start of the cutback. Results in Chapter 4 show this assumption to be inaccurate, as the 2D sonic line is observed to attach variously at this point or at the very end of the trailing edge, depending on precise cutback size.

The Rolls-Royce study produced values for throat area of the 6 NGVs in question. These values are listed in Table 3.4, where they are normalised against vane KSZ03 due to the sensitive nature of the data.

Table 3.4: Throat areas of 6 Trent 900 NGVs

Production standard	Serial number	Δ throat area, %
M EP1	PNS04	1.2924
	PNN06	0.8616
	PNS03	0.5575
M-skew	KTA01	0.3928
	KSZ03	0.0000
	KVD04	-0.4435

The viability of the geometric throat area approach to 3D data is illustrated in Figure 3.13, which plots the 6 NGVs' variations in capacity at design pressure ratio against their variations in geometric throat area. Capacity changes are normalised against the 3D capacity (as stated by Rolls-Royce) of vane KSZ03 at the design pressure ratio. Throat area changes are normalised against the 3D throat area (as stated by Rolls-Royce) of vane KSZ03. The averages of the M-skew and EP1 families are plotted and lines of gradient 1 are plotted intersecting the average values, such that any deviations from 1-dimensional compressible flow correspond to deviations from the lines of gradient 1.

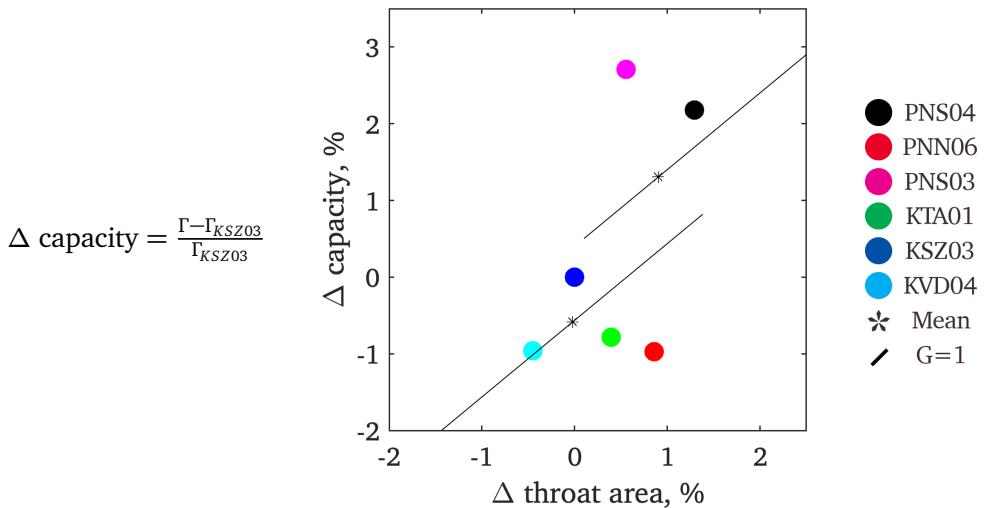


Figure 3.13: 3D capacity percentage delta as a function of 3D throat area for 6 Trent 900 NGVs at $\frac{p_{01}}{p_2} = 1.79$ (design)

Figure 3.13 shows that no correlation exists between geometric throat area and flow capacity for the 6 NGVs simulated by Rolls-Royce. This is in agreement with the hypothesis that highly 3-dimensional flow phenomena are present to a degree that predominates over any area-capacity relationship. Future study might divide focus between developing a 3D version of the A_{eff} technique and accessorising it with a model for the subsonic secondary flows that are hypothesised to be present even at the fully choked pressure ratio used to evaluate A_{eff} in the 2D cases. An overarching goal may be to confirm that secondary flows are indeed the confounding factor that is not captured by 2-dimensional CFD. In any case, motivation is presented to resolve the failure of present analytical techniques in understanding the sensitivity of nozzle guide vane flow capacity to geometric changes.

3.3 Chapter conclusions

Variations in the cast shape of nozzle guide vanes have been shown to cause variations in their predicted flow capacity. 2D CFD simulations have been performed on a family of 6 NGVs which were selected by Rolls-Royce to be representative of random variations in the shape of Trent 900 engine parts after they have been cast but before cooling features have been machined in.

At the NGVs' design inverse pressure ratio, the design flow capacity of the 6 vanes has been found to correlate to some extent with both the vanes' geometric throat area and with the effective throat width A_{eff} . 2D geometric throat width can be evaluated from the NGV design geometry without any further computational effort, but A_{eff} cannot be evaluated without obtaining a CFD solution at a fully choked pressure ratio. The A_{eff} approach is thus offered not as a means to predict the flow capacity of a given geometry, but rather as a means to quantify the shape of the 2-dimensional sonic line that forms at a fully choked pressure ratio, and to discuss this shape's effect on capacity.

Nozzle guide vane flow capacity correlates well with A_{eff} at the design pressure ratio despite the non-existence of a sonic line when the flow is not fully choked. This suggests that the sonic line shape is driven by the same geometric factors that drive the 2-dimensional flow field prior to choking. Thus for a given NGV production standard that outputs sets of vanes with casting variations, two conclusions can be drawn from simulating a representative sample of the vanes in 2D. Firstly any scanned vane's 2D capacity will be well-predicted by its 2D throat width if fully choked simulations have shown the sonic line to exhibit relatively small deviation from the geometric throat line. Secondly the whole production standard is likely to have reduced capacity predictability if fully choked simulations have shown the sonic line to vary significantly in shape between individual vanes.

Conclusions are more difficult to draw in the case of 3D capacity, where a 3D extension of the A_{eff} approach is rational but would require careful adjustment for the delayed onset of choking in 3D compared to 2D. Where Section 3.1 suggested a boundary-layer model as a future addition to the technique, Section 3.2 has presented data from 3D geometries for which the equivalent inverse pressure ratio of 3.33 would produce significant regions of secondary flow which are not choked. These regions may be accounted for by an appropriate model or negated by the use of an even higher inverse pressure ratio. The overall conclusion of this chapter is that future analyses of casting variations versus flow capacity should involve 3D simulation, should account for both boundary layers and secondary flows when conceptualising A_{eff} in 3D, and should use a statistically significant number of scanned vanes to produce two key metrics. Firstly the mean departure of the vanes' sonic surfaces from the surface of minimum area will reveal whether the minimum area is a useful capacity predictor for that production standard. Secondly the variance of the vanes' sonic line shapes will indicate that production standard's capacity uncertainty.

Chapter 4

Trailing edge shape

Nozzle guide vane flow capacity is known to be a function of effective throat area. Thus we must survey the practical reasons for which effective throat area might vary. In a real engine, NGV effective throat area may depart from its design value if the NGVs depart from the ideal aerodynamic design shape. This may occur through practical design choices for reasons such as cooling or blockage avoidance, because of the finite precision of manufacturing, or because of erosion while in service.

A goal of the present study is to help ascertain how much such design decisions and off-design conditions affect the predictability of NGV flow capacity, and to comment on ways to mitigate this limitation. The NGV trailing edge is an area of focus because it is particularly susceptible to both finite-precision and in-service departures from its design shape. It is also difficult to model small features accurately using CFD, so knowledge of which features may be neglected will enable faster and more extensive design calculations.

The trailing edge is susceptible to finite-precision departures from its design shape because of how it is manufactured. Vane pairs are cast to a finite precision as discussed in Section 3.1, where significant geometric variation appears even prior to the addition of cooling features. The vanes are then machined to finish off the trailing edge shape to a high tolerance. The finishing creates the aerodynamically best possible trailing edge.

The trailing edge's principal design feature is the difference between the amount of material left on the suction side of the coolant ejection slot and the amount left on the pressure side. This creates the thinnest possible final trailing edge for the vane with the intent of minimising separated wake area and thus loss. The resulting feature will be referred to as the end-edge in this thesis, and is illustrated in Figure 4.1. The end-edge depends on the slot coolant flow for protection against in-service erosion. The ideal coolant ejection slot width may be determined as the width through which the coolant would be ejected such that there is no difference in velocity between it and the mainstream flow.

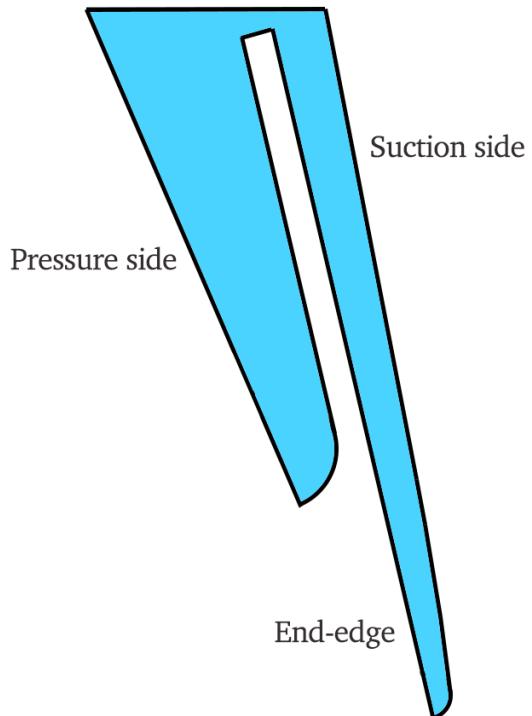


Figure 4.1: Main features of a contemporary nozzle guide vane trailing edge

The 3-dimensional design of contemporary nozzle guide vanes assumes they will be cast in pairs of vanes together with their inner and outer annulus end-walls. They feature a filleted transition to allow the end-edge to cleanly meet the end-walls, and an end-edge chord length that is consistent across its span. The creation of a repeatable minimum geometric area which provides the required turning and flow capacity is a primary objective, but so is generating a vane with minimal loss at the start of its service life. These design goals are not necessarily aligned, and it may be the case that a loss-optimised NGV trailing edge is suboptimal in terms of the design's repeatability or susceptibility to unintended changes while in service.

The trailing edge is the part of the vane most susceptible to in-service departures from its build design because it is vulnerable to both cooling and aerodynamic damage. The NGV remains largely intact over its lifetime despite the external gas temperature and high speed external flow. In contrast, the end-edge is subject to significant erosion. If there is a blockage in any of the plena which feed the trailing edge slot, part of its span will receive reduced coolant flow, accelerating the oxidation degradation of the end-edge in that region. Such cooling failures are not uncommon in sandy environments. In such environments, film cooling holes on the pressure side are particularly vulnerable to damage, and this has lead to the adoption of the “cut-back” trailing edge, where the trailing edge region is protected by coolant from the trailing edge slot that is shielded from the mainstream flow to prevent blockage. The pay-off is that the end-edge is now cooled by an external film which must remain attached and is subject to entrainment from the mainstream flow.

The nozzle guide vane must provide a repeatable setting for engine core flow capacity, correct flow turning, and minimal loss. This chapter will predict and analyse these metrics for cases where the shape of the trailing edge is subject to variation. Variations will include incremental reduction in the end-edge length associated with in-service erosion, and incremental reduction in the pressure-side cut-back length as a design variable. Definitions of loss in this chapter are as reviewed in Section 2.2.

4.1 Effects of suction-side trailing edge shape uncertainty

The end-edge, which forms the sharp tip of the trailing edge, is formed from material on the suction side of the NGV passage. This section will consider increasingly severe loss of material up to a potential worst case for in-service erosion of the end-edge, namely its complete deletion. Erosion has been assumed to take place at the NGV mid-span where flow speeds and temperatures are highest and there is previous anecdotal evidence of in-service damage. Here secondary flows across the blade are small and a 2-dimensional simulation of the mid-span flow should provide a physically realistic measure of performance.

4.1.1 Geometry, mesh, and boundary conditions

2D CFD has been used to model the effects of incremental removal of material from the suction-side end-edge of an NGV. The baseline geometry is vane KSZ03 from the 6 vanes provided by Rolls-Royce for the work discussed in Chapter 3. The 2D vane section was produced using the process illustrated in Figure 3.2. The overall computational domain was produced as in Figure 3.3. Unlike the section of vane KSZ03 studied in Chapter 3, the NGV trailing edge was not rounded but realistically shaped based on GOM scan analysis, and the domain was modified to include a flow inlet within the NGV's trailing edge slot, where the mass flow rate to be ejected was specified. The boundary conditions used for all simulations are as listed in Table 4.1.

Simulations were performed at a range of inverse pressure ratios between 1.5 and 3.33, and particular study was made at inverse pressure ratios of 1.5, 1.79 and 3.33. This permits comment on the NGV flow capacity as a function of only the sonic line shape, and eliminates the possibility of unchoked flow passing through the nozzle, with the exception of the boundary layers. $\frac{p_{01}}{p_2} = 3.33$ was considered to be a case where the nozzle guide vane is definitely fully choked. Although this particularly high inverse pressure ratio is possibly unachievable in the real engine, the simulated NGVs were observed to be fully choked at a substantially lower inverse pressure ratio of 2.5. $\frac{p_{01}}{p_2} = 1.79$ is the design cruise condition for the Trent 900 engine. $\frac{p_{01}}{p_2} = 1.5$ was considered to be a case where the nozzle guide vane is definitely not choked, and is possible to achieve in some very low-power operating conditions.

Table 4.1: Boundary conditions for Trent 900 end-edge and pressure-side cutback studies

Parameter	Value
NGV series	Rolls-Royce Trent 900
NGV turning (degrees)	76.89
Inverse pressure ratio $\frac{p_{01}}{p_2}$	1.5, 1.79, 3.33
Inlet total pressure (Pa)	4.33×10^6
Inlet total temperature (K)	300
Outlet static pressure (design) (Pa)	2.42×10^6
Outlet static temperature (K)	300
Coolant mass flow rate	3.00% of mainstream
Solver type	Density-based
Cell count	35,000

The strategy for geometry alteration and meshing was to divide the geometry into quadrilateral

regions of solid vane that were sequentially replaced by regions of fluid mesh. Each replacement incrementally eroded or cut back the NGV's end-edge. This required minor alteration of the trailing edge geometry provided by Rolls-Royce, as illustrated in Figure 4.2.

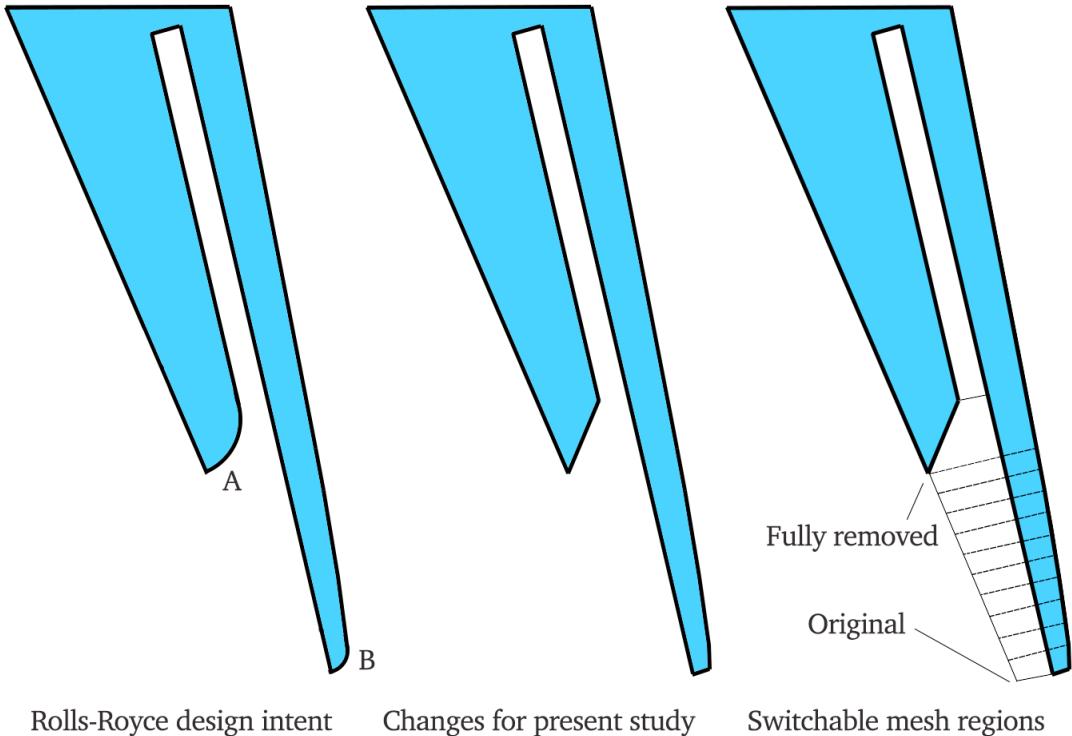


Figure 4.2: Geometry processing scheme for cutbacks to the end-edge of a Trent 900 NGV

The curved surface on the inside of the pressure side (labelled A) was changed to a straight line with an angular corner, and the curved tip of the suction side (labelled B) was changed to a square end. Comparison of the shape of manufactured NGVs with the shape of design-intent NGVs demonstrates that the present study's trailing edge treatment is more reflective of the manufactured NGVs, which have corners rather than smooth curves in the places in question. In any case the radius of curvature of the corner is too sharp to promote any attachment of the internal flow over its length, and so is aerodynamically irrelevant.

The resulting quadrilateral geometry allowed for the creation of a structured mesh that could be matched with a structured boundary layer mesh of the same design as that depicted in Figure 3.5b. Beyond this, an unstructured mesh was created to the same design as that depicted in Figure 3.4. Detail of the trailing edge mesh is shown in Figure 4.3 for a case where approximately 50% of the end-edge is removed and replaced with structured fluid mesh blocks.

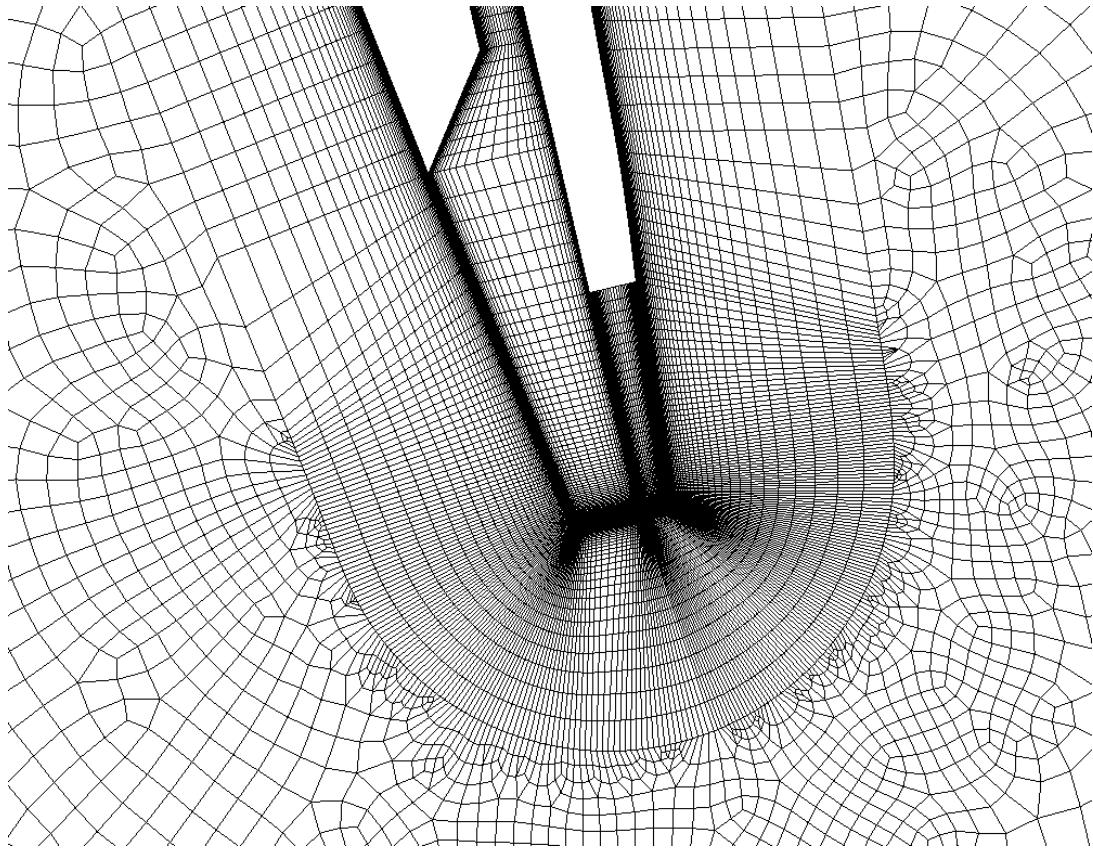


Figure 4.3: Example of mesh for cutbacks to the end-edge of a Trent 900 NGV

The described mesh, geometry alteration strategy, and boundary conditions were used to perform 11 CFD simulations which incrementally spanned the range of cutbacks between an unaltered trailing edge and a fully removed end-edge. Solutions were initialised using the solver's built-in FMG initialisation and Journal scripts as described in Section 3.1. NGV mass flow rate was saved at each pressure ratio. Full solution data were saved for the final fully choked pressure ratio to enable analysis of the shocks, expansions and sonic line at choked conditions. There were 32 increments of pressure ratio, and typical overall solution times were approximately 10 hours. The $k-\omega$ SST turbulence model was used.

4.1.2 Effect on capacity

Figure 4.4 shows contours of Mach number in the region of the trailing edge for the described study. The depicted range of cutbacks is between the unaltered baseline and the case of 30% removal of the overall length of the suction-side end-edge. Inverse pressure ratio is 3.3, fully choked.

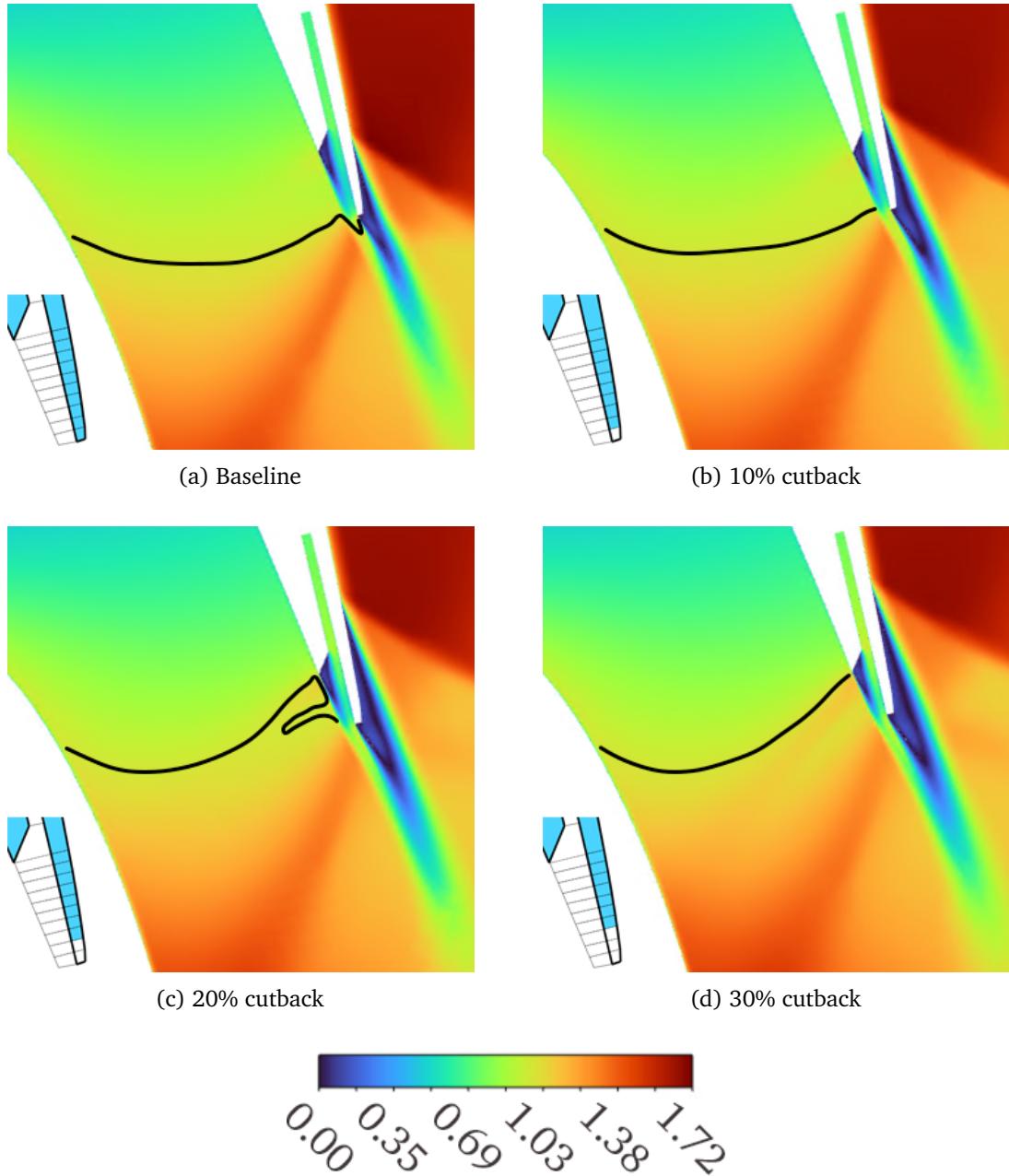


Figure 4.4: Contours of Mach number showing effects of small cutbacks on the sonic line shape for Trent 900 end-edge erosion study at $\frac{p_{01}}{p_2} = 3.33$

Figure 4.4 illustrates the subtle changes in the sonic line at the nozzle exit as the nozzle guide vane's end-edge is incrementally removed until 30% of its length is not present. The sonic line is shown to undergo a fundamental transition over this range of cutbacks, from initially impinging on the extremity of the end-edge in the baseline case, to impinging on the acute corner of the pressure side. It is notable that this is in direct contradiction to the commercial design philosophy which assumes the end of the cutback to define the throat in all cases. The simulated result for 20% cutback suggests a sonic line attachment point which may jump between the end-edge and cutback edge in unsteady conditions.

The geometric changes are also shown to alter the aerodynamics in the suction-side region upstream of the end-edge, where an attached shock moves incrementally upstream with each increment in

cutback. Shock-induced boundary layer separation is seen to be present in Figure 4.4, and moves upstream corresponding to the position of the shock. This results in an increasingly large separated wake region which is not in alignment with the NGV's turning angle.

Figure 4.5 shows further contours of Mach number. Again the range of cutbacks is between 40% and complete removal of the end-edge. Again the inverse pressure ratio is 3.3, fully choked.

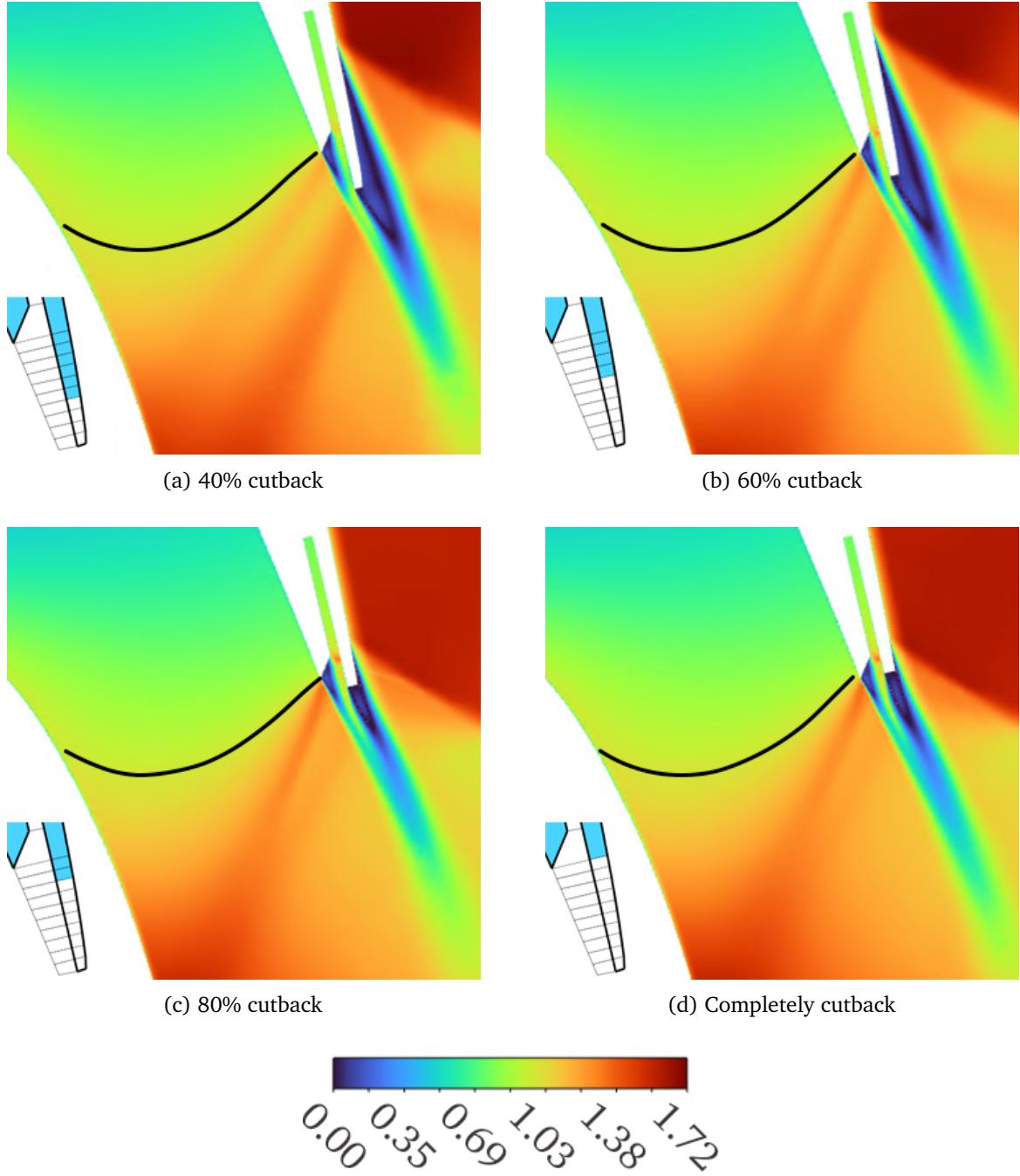


Figure 4.5: Contours of Mach number showing effects of large cutbacks on the sonic line shape for Trent 900 end-edge erosion study at $\frac{p_{01}}{p_2} = 3.33$

Figure 4.5 illustrates that the shape of the sonic line is not fundamentally altered in the range between 40% and 100% removal of the end-edge. The sonic line is shown to consistently attach to

the acute corner of the pressure side throughout this range of larger cutbacks. Upstream movement of the location of the suction-side attached shock continued to occur. This trend was reversed for the most extreme cases of 80% and complete cutbacks, where the shock transitioned to a downstream location close to the corner of the end-edge, resulting in a significantly smaller separated wake region compared to other cases.

The set of Mach number contours and sonic lines suggest that the greatest sensitivity of flow capacity to end-edge cutbacks is to occur for cutbacks of 30% of the end-edge or less. The sensitivity of the sonic line shape to the full range of cutbacks is illustrated in Figure 4.6, which superposes the sonic lines from all simulations. It is further suggested that the location of an attached suction-side shock and corresponding boundary layer separation near the trailing edge may be sensitive to cutbacks of 40% or more, but this may be imprecisely predicted by the present simulations. This is due to the lack of any observed correlation between the cutback amount and the variation in the shock location.

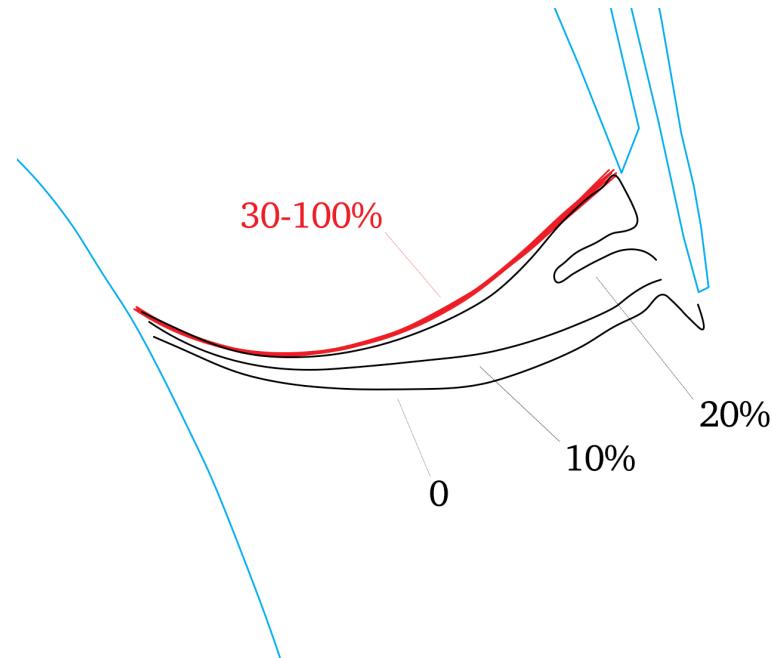


Figure 4.6: Variation in sonic line location over the full range of cutbacks for the Trent 900 end-edge erosion study, labelled by the percentage of the end-edge removed

Figure 4.6 shows that upstream movement of the location of the suction-side attached shock occurred between 0 and 30% removal of the end-edge. This trend did not continue for cutbacks greater than 30%. Within this range of cutbacks, the sonic line is attached to the NGV pressure side upstream of the cooling slot, as there is insufficient length over which reattachment can occur downstream. This is a useful result for the engine designer, as it provides a stable end-of-life capacity prediction for the NGV. The applicability of Section 3.1's A_{eff} to this result would require careful consideration. The present formulation of A_{eff} relies on the assumption that any stream tube can pass through the sonic line only once. This would result in mispredictions of effective area in cases such as 20% removal of the end edge, which is shown in Figure 4.6 to include stream tubes which pass though the sonic line more than once.

Figure 4.7 plots flow capacity change as a function of the amount of the end-edge that has been removed. The trend is plotted for 3 inverse pressure ratios: 1.50, the design value of 1.79, and a fully choked value of 3.33.

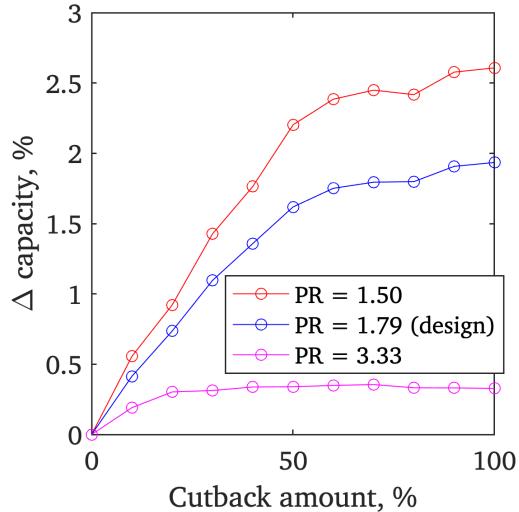


Figure 4.7: 2D capacity percentage delta as a function of end-edge cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.5, 1.79$

At an inverse pressure ratio of 3.33, Figure 4.7 shows a relationship between flow capacity and cutback amount which is in good agreement with the observations made from the corresponding sonic line visualisations. Capacity is shown to be sensitive to cutback amounts of 0, 10%, and 20%, and insensitive to cutbacks thereafter. The corresponding sonic lines are observed to vary in shape when capacity varies, and to remain similar in shape when capacity does not vary. The observed switching of the sonic line from the end-edge-attached mode (at baseline) to the pressure-side-attached mode (at cutbacks of 30% and greater) is associated with a 0.3 percentage point increase in capacity. For all cutbacks subsequent to the mode switch, there is no capacity change at this pressure ratio. This is in good agreement with the discussion in Chapter 3 which concluded that the effective throat area of a fully choked nozzle guide vane is predominantly a function of the shape of its sonic line.

At lower inverse pressure ratios where the flow is not fully choked, and thus a sonic line cannot be drawn, flow capacity varied over a significantly greater range of cutback percentage. This is to be expected by consideration of choked versus unchoked compressible flows as discussed earlier in this section. This discussion implies that, in the general case of compressible flow in 2D nozzles, the nozzle flow capacity will increase if the effective passage width is increased at any point along the nozzle. However, this is also a consequence of providing less turning in the flow. An entirely unturned flow would have maximum capacity in the annular cross-section that is the gas turbine.

This is in good agreement with the observed relationship between flow capacity and cutback amount at the unchoked pressure ratios. Removal of end-edge material increases the effective passage width in the region local to the end-edge, causing a local decrease in static pressure and increase in dynamic pressure. Because most streamlines are unchoked at the flow region and pressure ratios in question, this state change propagates along the entire streamline with a corresponding increase in mass flow rate.

The maximum change in capacity was 1.9 percentage points at the design inverse pressure ratio of 1.79, and 2.5 percentage points at an inverse pressure ratio of 1.50. The effect of increasing cutbacks became less pronounced at larger cutback amounts, suggesting that the size of the end-edge ceases to be the limiting factor on effective passage width for those geometries. Figure 4.8 shows contours of Mach number in the NGV wake region for the full range of cutbacks at the design inverse pressure

ratio of 1.79, labelled by the percentage of the end-edge removed.

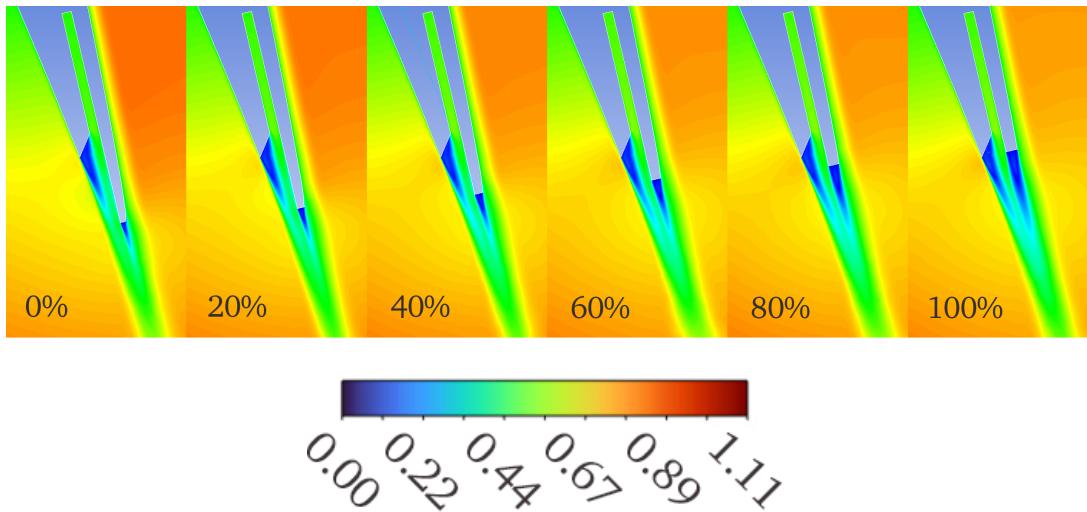


Figure 4.8: Contours of Mach number in the wake region of the Trent 900 end-edge erosion study at $\frac{p_{01}}{p_2} = 1.79$ (design), labelled by percent of the end-edge removed

Key features of Figure 4.8 include an outer wake region (rendered in green) and inner wake regions downstream of the pressure side and the end-edge (rendered in blue). No fundamental changes occurred to the trailing edge's aerodynamics over the range of cutbacks. Mach number is observed to continually increase in the region adjacent to the pressure side, and to continually decrease in the region adjacent to the end-edge. The trailing edge aerodynamics were sensitive to geometric changes across the full range of cutbacks. The reduced effect of greater cutbacks on flow capacity may result from two phenomena. Firstly, the local flow acceleration may be limited more by the position of the pressure side than by the end-edge at higher cutback values, where the end-edge tip is increasingly too far upstream to influence the pressure-side aerodynamics. Secondly, this upstream positioning of the end-edge tip is observed to cause a significant increase in outer wake thickness at higher cutback values. This likely reduced the effective passage width in this region and counteracted the predominant effect of flow capacity increasing.

Figure 4.9 plots trends of flow capacity change versus inverse pressure ratio at selected cutback amounts. The range of inverse pressure ratios includes the design value of 1.79. Capacity changes are normalised against the case of 0 cutback at the design pressure ratio.

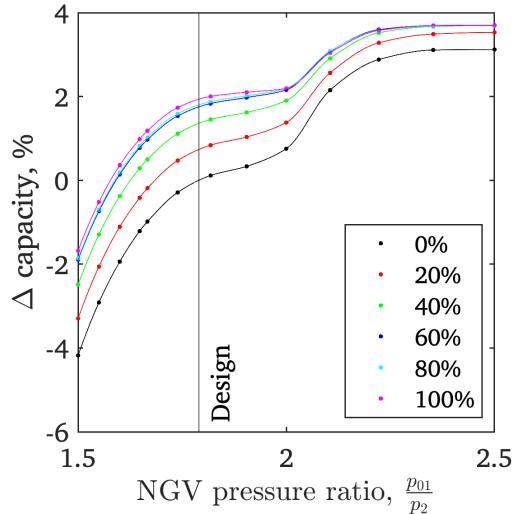


Figure 4.9: 2D normalised capacity as a function of pressure ratio for a Trent 900 NGV over the full range of end-edge cutbacks

In terms of the effects of cutbacks on flow capacity, Figure 4.9 is in good agreement with Figure 4.7. The capacity delta produced by full end-edge removal continuously decreased with increasing inverse pressure ratio, and the capacity trends remained qualitatively similar for all cutback amounts. These observations suggest that the cutback-induced capacity changes and the onset of choking are 2 independent phenomena which do not influence each other. It is concluded that, as inverse pressure ratio increased, more streamlines became choked and ceased to be affected by cutbacks downstream of those streamlines' sonic points.

It is further concluded that the capacity trend shapes and onsets of choking were unaffected by variable cutbacks, but remained a function of only inverse pressure ratio. This is likely due to the relevant geometric changes taking place downstream of the throat region. This is complementary to the results of Chapter 3, where geometric changes upstream of the throat resulted in qualitatively distinct capacity trends and dissimilar onsets of choking.

4.1.3 Effect on performance

Simulation data were also used to evaluate the aerodynamic penalties associated with the incremental cutbacks to the end-edge at the design inverse pressure ratio of 1.79. These penalties include the change to the NGV's ability to turn the flow by the correct angle, and the effect of the cutbacks on the NGV loss.

Velocity components at the domain outlet were surveyed and mass-averaged over the length of the outlet. This resulted in a value for mean NGV turning angle for each incremental cutback. Figure 4.10 plots turning angle deviation in degrees versus end-edge cutback amount.

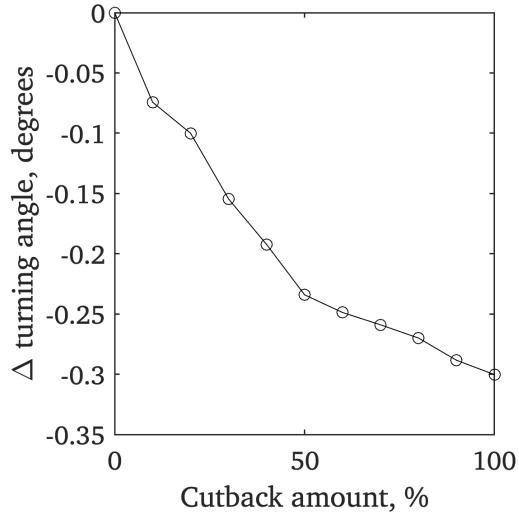


Figure 4.10: NGV turning angle delta as a function of end-edge cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.10 shows that the NGV's ability to turn the flow was significantly reduced as cutbacks increased. Complete removal of the end-edge resulted in a turning angle reduction of 0.3 degrees, with increased sensitivity to cutbacks at smaller cutback amounts. This trend is unsurprising. If no vane were present, this would equate to no turning. For the high-pressure turbine downstream of the NGV, reduced turning equates to less available work and additional loss at entry to the rotor.

Overall flow turning angle was surveyed along the length of the domain outlet plane. Figure 4.11 plots this distribution of turning angles at selected cutback amounts. On the outlet plane, $0 \rightarrow 1$ denotes travel in the negative y direction, which is the direction the flow turns. Stations 0 and 1 are labelled on the illustration of the computational domain in Chapter 3, Figure 3.3. Station 0.5 corresponds to the geometric extrapolation of the NGV trailing edge to the outlet plane.

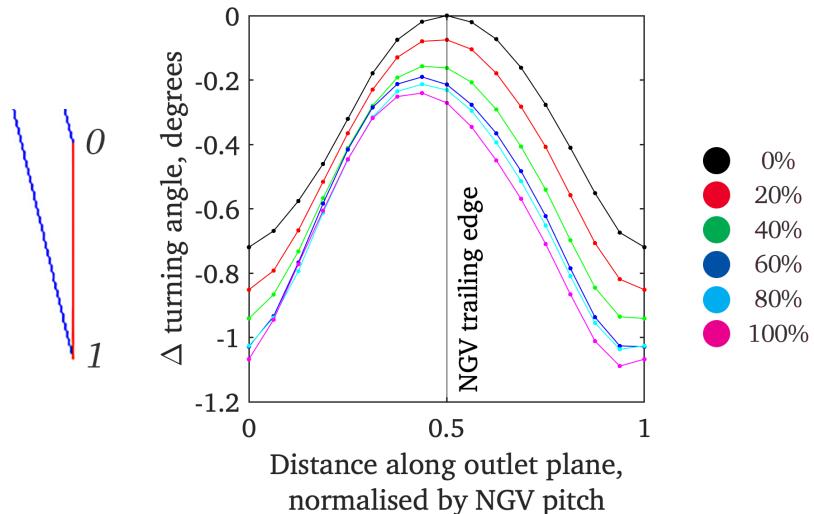


Figure 4.11: Outlet plane turning angle surveys over the full range of cutbacks for the Trent 900 end-edge erosion study at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.11 further illustrates the trend of reducing turning angles present in Figure 4.10. It is also

apparent that the incremental cutbacks caused a shift in the location of maximum turning angle. In the case of no cutback, maximum turning occurred exactly halfway across the domain exit plane, at a location immediately downstream of the NGV end-edge. Subsequent cutbacks caused both a reduction in maximum turning and a shift of the maximum turning location in the opposite direction to which turning occurs. This suggests that the NGV wake continued to extend downstream of the NGV at an angle which decreased with increasing cutbacks, arriving at the domain outlet at an incrementally increasing y -coordinate. Assuming that the downstream turning angle distribution is indicative of the NGV wake profile, the wake did not appear to become significantly more diffuse as cutbacks increased.

Figure 4.12 plots loss as a function of end-edge cutback amount at the design pressure ratio of 1.79, where total pressure loss and kinetic energy loss are defined as in Section 2.2. Total pressure values were surveyed at the domain outlet plane and averaged to produce the loss values.

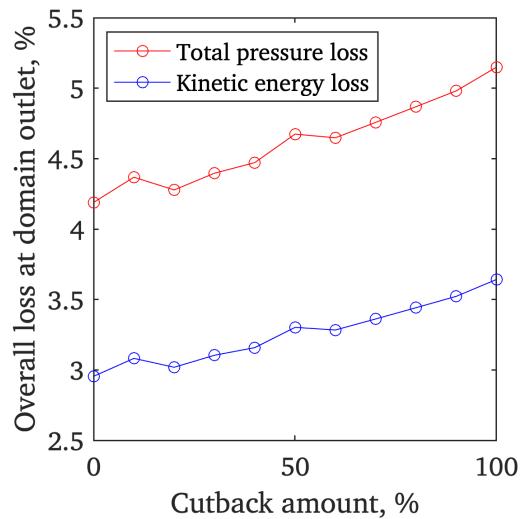


Figure 4.12: Loss as a function of end-edge cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.12 shows that both types of loss increased with incremental cutbacks. Total pressure loss was observed to increase by approximately 1% over the range of cutbacks, and kinetic energy loss by approximately 0.7%. This is in agreement with the discussion of figure 4.8 which suggested that loss would likely be incurred by the increasing area of separated wake that occurs as cutbacks increase. This effect may be exacerbated by the deviation from the design turning angle that also occurs, whereby the NGV wake is deflected in the positive x -coordinate with corresponding increase in its area.

Loss delta is plotted as a function of capacity delta in Figure 4.13. This plot covers the range of incremental cutbacks and is for the design inverse pressure ratio of 1.79.

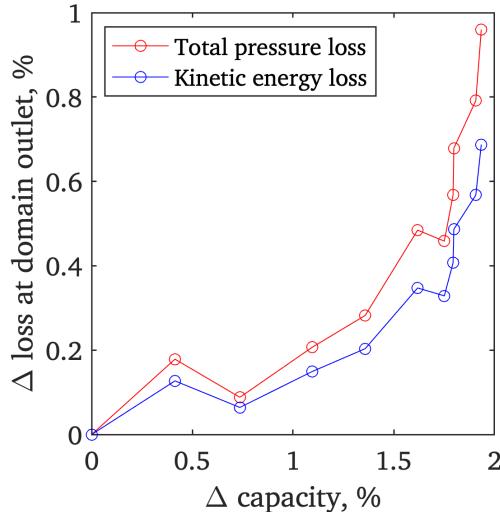


Figure 4.13: Loss delta as a function of capacity delta over the full range of cutbacks for the Trent 900 end-edge erosion study at $\frac{P_{01}}{P_2} = 1.79$

Figure 4.13 shows that, as the end-edge is incrementally removed, capacity and loss do not change in direct proportion to each other. Although overall capacity sensitivity was greater than overall loss sensitivity, at higher cutback amounts a relatively small increase in capacity corresponded to a sharp increase in loss by both definitions. In agreement with this section's previous analysis of the capacity and loss mechanisms present across the range of cutbacks, it is concluded that capacity sensitivity is of greatest concern in cases of relatively small erosion of the NGV end-edge, and loss sensitivity is of concern in all cases but especially in cases of relatively large erosion.

4.2 Effects of pressure-side trailing edge sizing

This section considers the location of the pressure-side cutback that is present on the NGV. This feature is required to prevent blockage of the coolant supply to the end-edge, which would be damaged very rapidly by oxidation erosion if the slot coolant flow were not present. Although the pressure side could be extended further downstream into a thinner feature with a smaller wake, the cutback prevents blockage of the slot coolant flow by causing it to form an external film attached to the pressure side of the end-edge. If a coolant blockage is present upstream inside the vane, the end-edge coolant film will remain relatively unchanged after mixing with itself.

Improved materials and manufacturing techniques may necessitate alternative trailing edge geometries. Giel et al [8] noted that “in the pursuit of higher turbine inlet temperatures for reduced fuel burn and emissions consistent with NASA’s goals [19], Ceramic Matrix Composite (CMC) materials are now being implemented in gas turbine engines...They enable higher turbine inlet temperatures, thus enabling higher overall pressure ratios (OPRs) for the engine and higher thermal efficiency.”

The authors used a linear cascade to measure the aerodynamic performance of a set of blades representing the geometric constraints of the CMC manufacturing method. Of main concern was the constraint that “the trailing edge thicknesses of CMC blades are anticipated to be significantly larger than those of current state-of-the-art metallic blades,” which may be expected to cause increased loss.

4.2.1 Geometry, mesh, and boundary conditions

The larger the pressure-side cutback, the less the likelihood of coolant blockage, and the easier it is to perform the machining of the trailing edge. However, a bigger cutback is expected to cause increased loss due to increased wake area, although the limiting design factor is the reduction in film cooling effectiveness on the end-edge as the coolant becomes mixed out. With enough mixing, there would eventually be no cooling potential in the film cooling flow. This section presents a 2D CFD study on varying the size of the pressure-side cutback, using the types of analyses presented for end-edge cutbacks in Section 4.1. The baseline geometry included a partially eroded end-edge to be representative of the full lifetime of the component, for which a cutback amount of approximately 50% was chosen. The baseline pressure-side cutback was such that the pressure side and the suction side extended by the same amount, with no end-edge. Cutbacks were then made to move the end of the pressure side upstream in increments of 25%, where 100% is equivalent to the existing location of the pressure side of the trailing edge. The process of geometry refinement is illustrated in Figure 4.14.

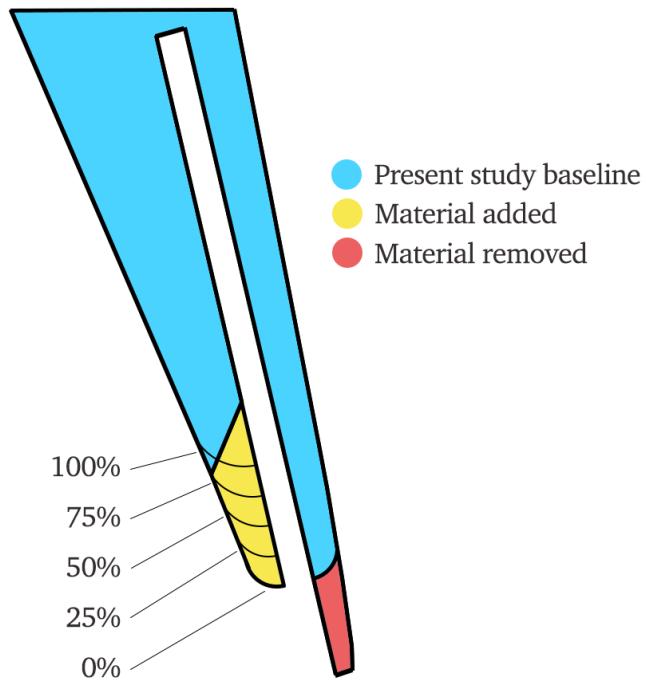


Figure 4.14: Geometry processing scheme for cutbacks to the pressure side of a Trent 900 NGV

As in Section 4.1, simulations were performed at a range of inverse pressure ratios between 1.5 and 3.33, and particular study was made at inverse pressure ratios of 1.5, 1.79 and 3.33. 1.79 is the design cruise condition for the Trent 900 engine. Boundary conditions were as described in Table 4.1.

This geometry did not allow for the approach of Section 4.1 where material was replaced with structured fluid mesh. For this geometry, an additional structured quadrilateral mesh block was created for cutback sizes greater than 0. This block deformed as cutbacks were increased, maintaining element spacing on the outer edge of the structured boundary layer mesh region. The sizing of this region was consistent with that used in Section 4.1, as was the design of the unstructured quadrilateral mesh for the overall domain. Figure 4.15 depicts the meshes used for the cases of 0%, 25%, 50%, and 75% cutbacks.

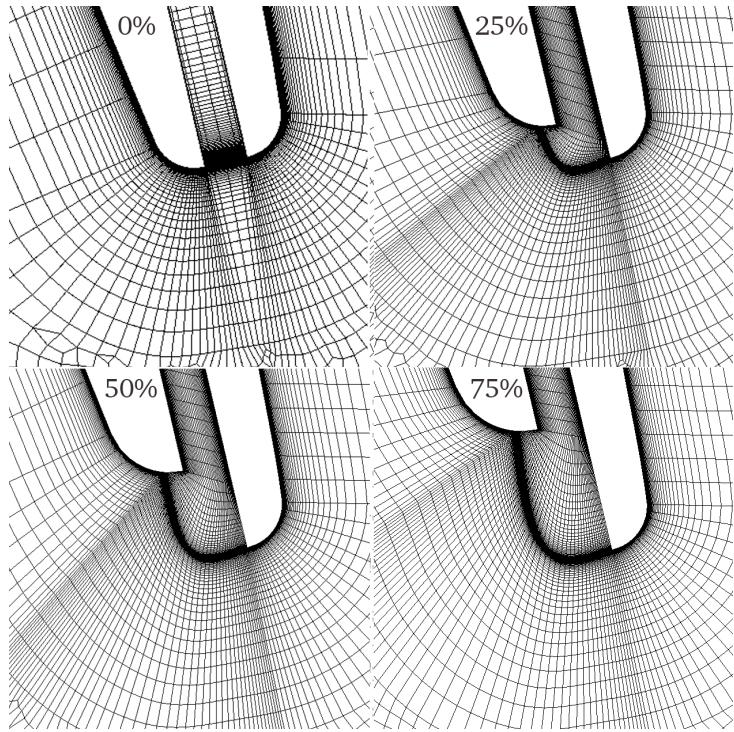


Figure 4.15: Examples of meshes for cutbacks to the pressure side of a Trent 900 NGV

In Figure 4.15, deformation of the bottom edge of the aforementioned mesh block is prominently visible due to the continuation of the laminar sublayer resolution around the circumference of the vane, which requires it to bridge the gap across the trailing edge slot. The described mesh, geometry alteration strategy, and boundary conditions were used to perform 5 CFD simulations which incrementally spanned the range of cutbacks between the described baseline and a fully cut back pressure side. Solutions were initialised using the solver's built-in FMG initialisation and Journal scripts as described in Section 3.1. NGV mass flow rate was saved at each pressure ratio. Full solution data were saved for the final fully choked pressure ratio to enable analysis of the shocks, expansions and sonic line at choked conditions. There were 32 increments of pressure ratio, and typical overall solution times were approximately 10 hours. The $k-\omega$ SST turbulence model was used.

4.2.2 Effect on capacity

Figure 4.16 shows contours of Mach number in the region of the trailing edge for the described study. The depicted range of cutbacks is between 0% and 100%. Inverse pressure ratio is 3.33, fully choked.

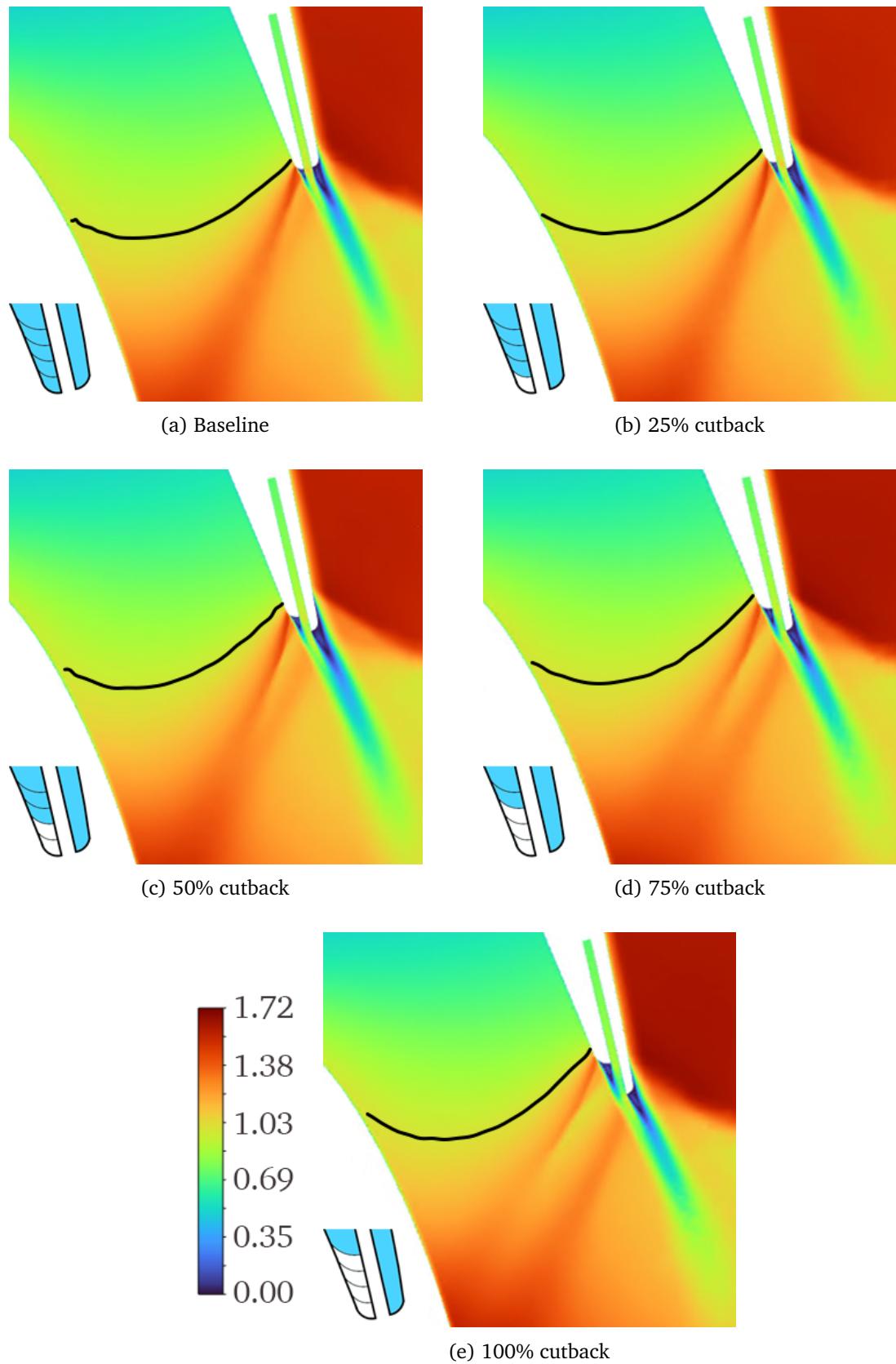


Figure 4.16: Contours of Mach number in the wake region of the Trent 900 pressure-side cutback study at $\frac{p_{01}}{p_2} = 3.33$, labelled by percent of the pressure side removed

Figure 4.16 illustrates that the sonic line moved incrementally upstream with increasing pressure-side

cutbacks. The sonic line remained attached to the pressure side of the trailing edge at a point just upstream of where boundary layer separation occurred, and this remained true as both the pressure side and the sonic line progressed upstream as cutbacks increased. On the suction side of the adjacent vane, the sonic line attached at a point that also moved incrementally upstream. In all cases, a shock was present immediately upstream of the point of pressure-side boundary layer separation, which was in a region of high convex curvature on the vane surface. Shock-induced boundary layer separation also occurred on the suction side of the trailing edge at a location that was not affected by the incremental changes to the pressure side. In cases of 25% cutback or more, an additional shock appeared downstream of the pressure-side trailing edge, and appeared stronger as cutbacks increased. The overall trend observed is that increasing cutbacks caused the line of geometric minimum width to move upstream, and that the sonic line moved upstream correspondingly. This observation is supported by the relationship between the cutback amount and the nozzle's geometric throat width, which is plotted in Figure 4.17. The sensitivity of the sonic line shape to the full range of cutbacks is illustrated in Figure 4.18.

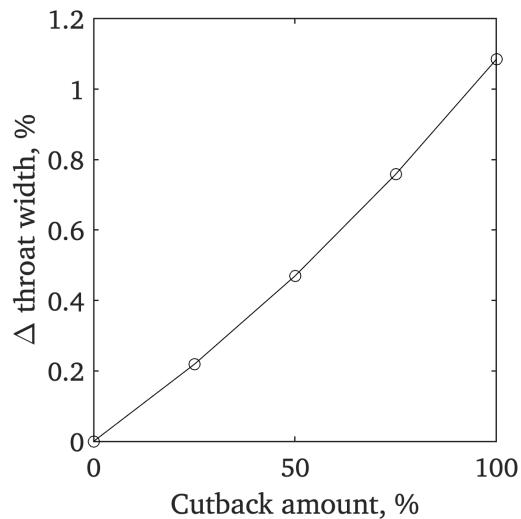


Figure 4.17: NGV geometric throat width as a function of cutback amount over the full range of cutbacks for the Trent 900 pressure-side cutback study

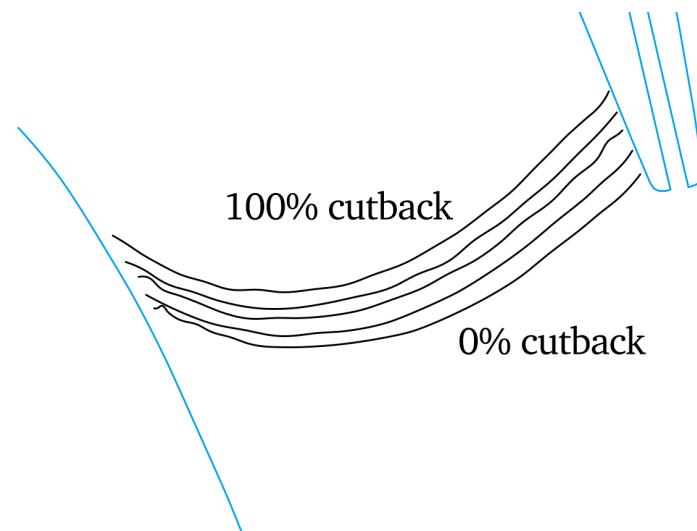


Figure 4.18: Variation in sonic line location over the full range of cutbacks for the Trent 900 pressure-side cutback study, labelled by percentage of the pressure side removed

Figures 4.17 and 4.18 are in good agreement with the hypothesis that increasing the pressure-side cutbacks resulted in an upstream movement of the NGV's geometric throat line, with a corresponding increase in throat width that was approximately linearly related to the size of the cutback.

Figure 4.19 plots flow capacity change as a function of the amount of pressure-side cutback. The trend is plotted for 3 inverse pressure ratios: 1.50, the design value of 1.79, and a fully choked value of 3.33.

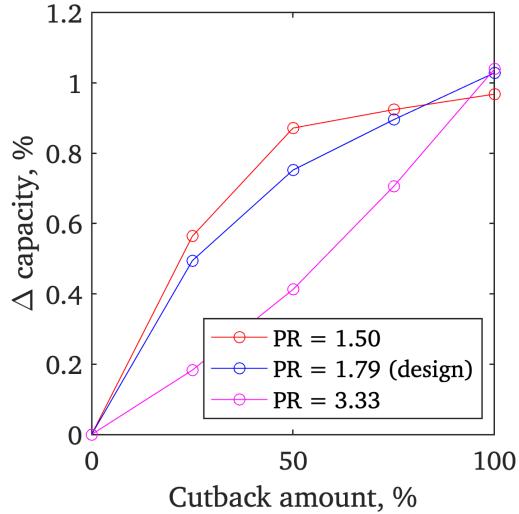


Figure 4.19: 2D capacity percentage delta as a function of pressure-side cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.5, 1.79$ (design), and 3.33

At an inverse pressure ratio of 3.33, Figure 4.19 shows a relationship between cutback amount and capacity delta that is in agreement with the hypothesis that the present changes are driven by an incremental increase in throat area. The graph of capacity versus cutback amount is similar in shape to the graph of throat width versus cutback amount in Figure 4.17. At the design inverse pressure ratio, capacity initially increased sharply with cutback amount but became less sensitive for greater cutbacks. At both the fully choked and the design inverse pressure ratios, 100% cutback resulted in a 1% increase in flow capacity. At the unchoked inverse pressure ratio of 1.5, the change in capacity was slightly smaller at 0.97%.

Overall it was apparent that only the fully choked cases were changing in direct proportion to changes to the nozzle throat width, with 100% cutback increasing both throat width and flow capacity by 1%. The design-condition cases and fully unchoked cases were evidently subject to aerodynamic changes downstream of the trailing edge region which allowed for greater sensitivity to smaller cutbacks and lesser sensitivity to larger cutbacks. To illustrate some of the relevant aerodynamic effects, Figure 4.20 shows contours of Mach number in the region of the trailing edge for the described study. The depicted range of cutbacks is between 0% and 100%. Inverse pressure ratio is 1.79, the design cruise condition.

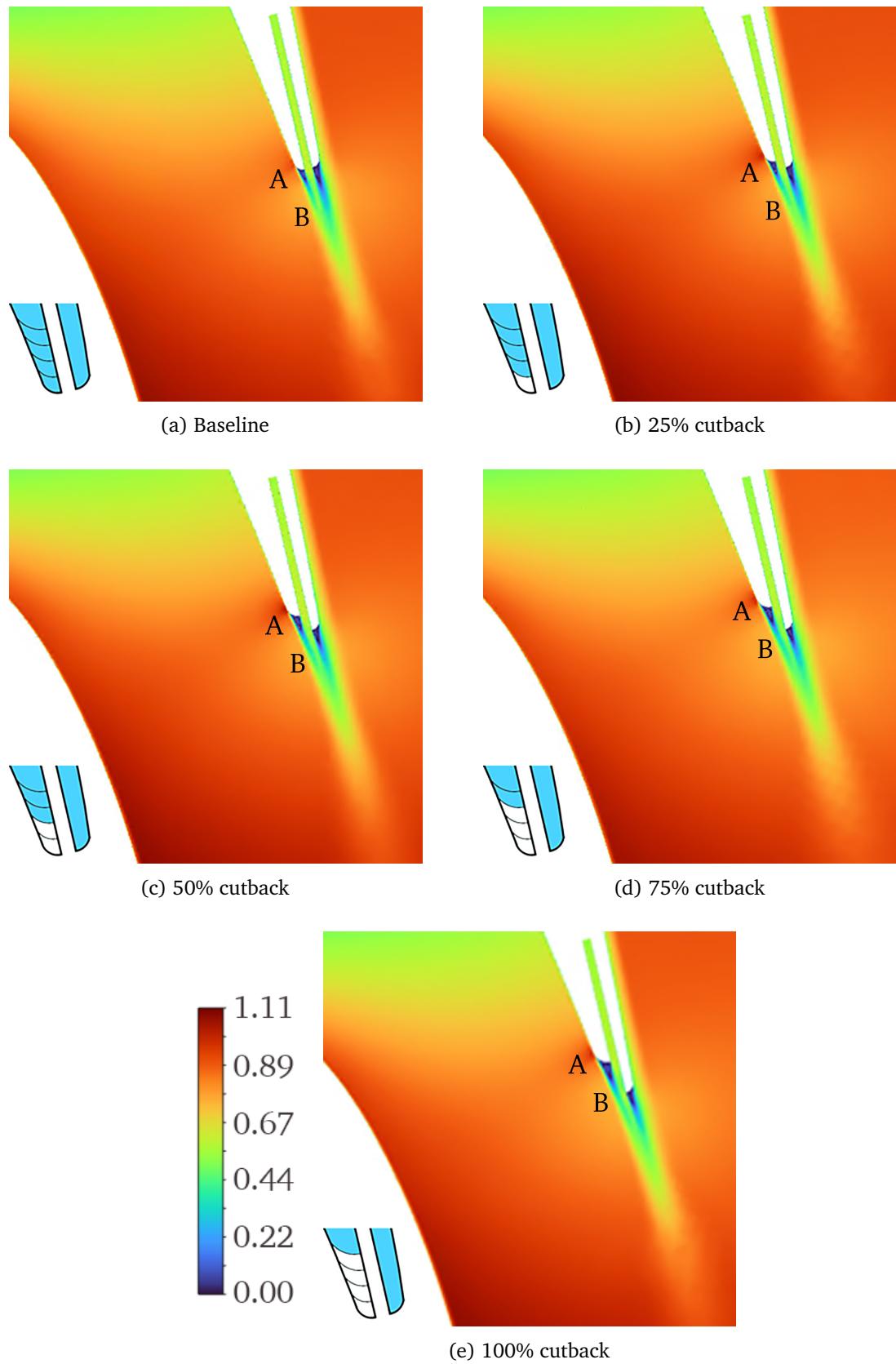


Figure 4.20: Contours of Mach number in the wake region of the Trent 900 pressure-side cutback study at $\frac{p_{01}}{p_2} = 1.79$ (design), labelled by percent of the pressure side removed

Figure 4.20 shows that the trailing edge region aerodynamics remained fundamentally unchanged

in the case of incremental pressure-side cutbacks at the design pressure ratio. An exception to this was the presence of a region of accelerated flow, labelled A, adjacent to the area near the end of the pressure side where the vane surface has high convex curvature. This feature became more pronounced as cutbacks increased, suggesting that it contributed to the non-linear relationship between cutback amount and flow capacity delta at the design inverse pressure ratio.

Another significantly changing feature, labelled B, occurred directly downstream of this region, where the flow remained attached along part of the convex surface. The high-momentum mainstream is observed to turn towards the positive x -direction more as cutback increased, impinging on the low-momentum outer wake region. This resulted in reduced flow turning overall, which will be discussed subsequently. This downstream flow straightening corresponds to an expansion in the effective flow width downstream of the vane, a change which is likely a primary cause of the observed trend of capacity increasing sharply with smaller cutbacks. In the extreme, the transformation of outer wake area into mainstream area is limited by the momentum of the slow coolant flow, which prevents the mainstream from completely overwhelming the wake. This is likely the reason why both unchoked cases exhibited reduced sensitivity of capacity to cutbacks at larger cutback amounts.

Figure 4.21 plots trends of flow capacity change versus inverse pressure ratio at selected cutback amounts. The range of inverse pressure ratios includes the design value of 1.79. Capacity changes are normalised against the case of 0 cutback at the design pressure ratio.

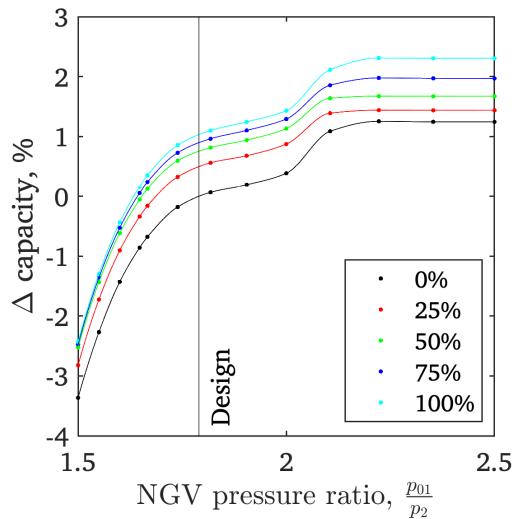


Figure 4.21: 2D normalised capacity as a function of pressure ratio for a Trent 900 NGV over the full range of pressure-side cutbacks

Figure 4.21 is in good agreement with Figure 4.19. The capacity delta produced by a 100% pressure-side cutback continuously increased with increasing inverse pressure ratio. It is concluded that, as inverse pressure ratio increased, more streamlines became choked, causing effects such as downstream flow straightening and expansion to have a reduced effect on flow capacity. When the flow was fully choked, capacity changes were almost directly proportional to the throat width changes that corresponded to the incremental cutbacks. This is complementary to the conclusions of Section 4.1, where capacity changes were primarily driven by effects other than a changing throat area, and were thus more sensitive at lower inverse pressure ratios rather than higher ones.

Capacity trends remained qualitatively similar for all cutback amounts. It is thus further concluded that the capacity trend shapes and onsets of choking were unaffected by pressure-side cutbacks, but remained a function of only inverse pressure ratio. This is likely due to the relevant geometric

changes taking place downstream of the throat region. Both the conclusions of Section 4.1 and this section are complementary to the results of Chapter 3.

4.2.3 Effect on performance

Simulation data were also used to evaluate the aerodynamic penalties associated with the incremental cutbacks to the pressure side at the design inverse pressure ratio of 1.79. These penalties include the change to the NGV's ability to turn the flow by the correct angle, and the effect of the cutbacks on the NGV loss.

Velocity components at the domain outlet were surveyed and mass-averaged over the length of the outlet. This resulted in a value for mean NGV turning angle for each incremental cutback. Figure 4.22 plots turning angle deviation in degrees versus pressure-side cutback amount.

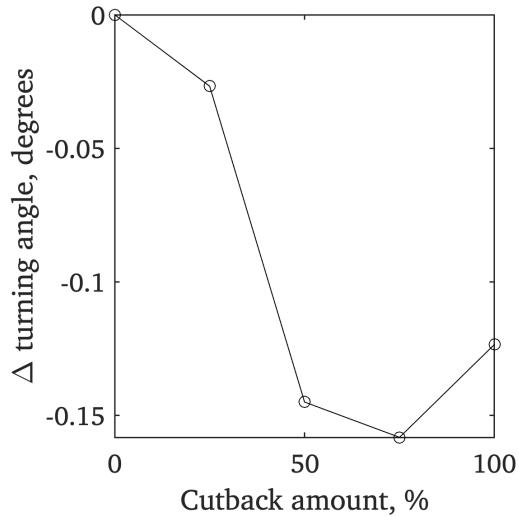


Figure 4.22: NGV turning angle delta as a function of pressure-side cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.22 shows that the NGV's ability to turn the flow was slightly reduced as cutbacks increased. Complete removal of the end-edge resulted in a turning angle reduction of 0.12 degrees. This is approximately half the sensitivity to end-edge cutbacks shown to be present in Section 4.1, which was 0.30 degrees. It is notable that between 75% and 100% cutback, the turning angle trend was actually reversed, with the most severe turning angle reduction being 0.16% at 75% cutback. This suggests that at 75% the turning angle sensitivity resulted from the removal of pressure side material reducing turning in the whirl direction, but at 100% the flow could impact on the coolant jet and suction side material, causing whirl velocity to be imparted once again. Due to the overall small effect of these pressure side cutbacks on turning angle, it is suggested that the correct end-edge length is more essential for proper flow turning than the position of the trailing edge's pressure side.

Overall flow turning angle was surveyed along the length of the domain outlet plane. Figure 4.23 plots this distribution of turning angles throughout the range of cutback amounts. On the outlet plane, 0→1 denotes travel in the negative y direction, which is the direction the flow turns. Stations 0 and 1 are labelled on the illustration of the computational domain in Chapter 3, Figure 3.3.

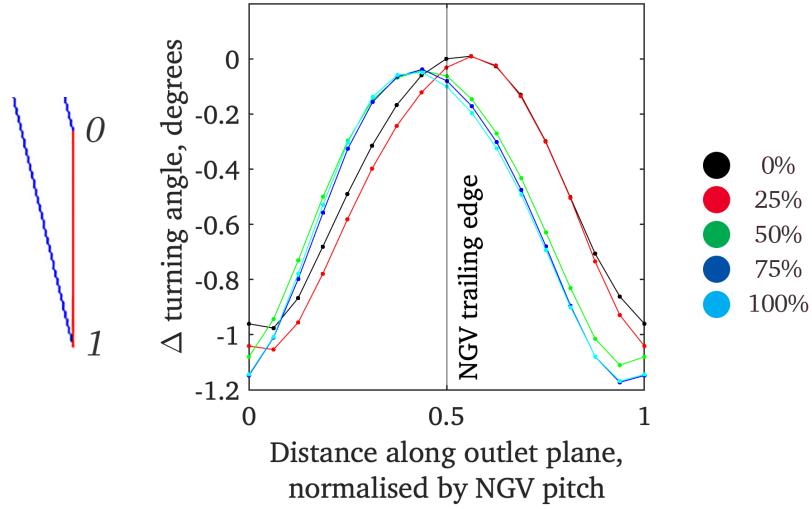


Figure 4.23: Outlet plane turning angle surveys over the full range of cutbacks for the Trent 900 pressure-side cutback study at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.23 indicates that there is not an obvious pattern to describe the changes that occurred to the flow turning angle downstream of the NGV. Overall, the location of maximum turning was observed to move in the positive y direction. This is both intuitive given that material is being removed from the vane, and in agreement with the similar observation from Section 4.1. It is interesting to note that the first pressure-side cutback of 25% produced a small change in the location of maximum turning in the opposite direction to the general trend, although mean turning angle was slightly reduced even by this cutback amount. Subsequent cutbacks resulted in an apparent mode switch where the maximum turning location was shifted in the positive y direction but was only negligibly affected by changes to cutback size between 50% and 100%. This behaviour was likely related to the observed post-throat flow straightening at smaller cutback sizes. At larger cutback sizes this behaviour was limited by interaction between the mainstream and the slot coolant flow momentum, and by the presence of the potential field from the end-edge, which re-establishes flow turning.

Figure 4.24 plots loss as a function of pressure-side cutback amount at the design pressure ratio of 1.79, where total pressure loss and kinetic energy loss are defined as in Section 3.1. Total pressure values were surveyed at the domain outlet plane and averaged to produce the loss values.

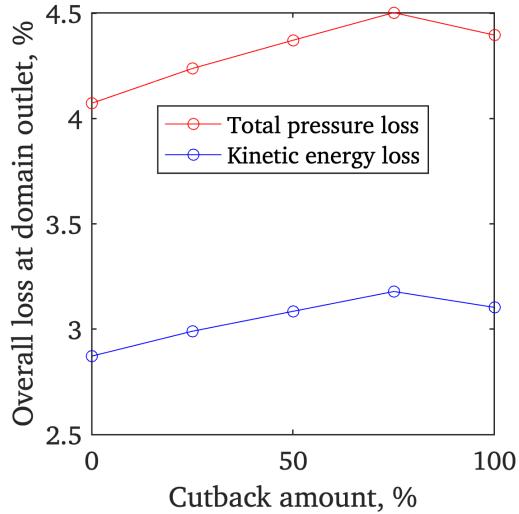


Figure 4.24: Loss as a function of pressure-side cutback amount for a Trent 900 NGV at $\frac{p_{01}}{p_2} = 1.79$

Figure 4.24 shows that both types of loss initially increased with increasing cutbacks, but were decreasing at the final and largest cutback size. This is largely in agreement with the hypothesis that larger cutbacks produce larger wake areas which produce more loss, but the final data points suggest that a counteractive mechanism is also present and becomes dominant at the largest cutback size. This mechanism may involve the aforementioned impingement onto the pressure-side wake from the mainstream at the largest cutback size, reducing the area of this wake region and reversing the trend of increasing loss. Total pressure loss was observed to increase by approximately 0.32% over the range of cutbacks, and kinetic energy loss by approximately 0.23%.

Loss delta is plotted as a function of capacity delta in Figure 4.25. This plot covers the range of incremental cutbacks and is for the design inverse pressure ratio of 1.79.

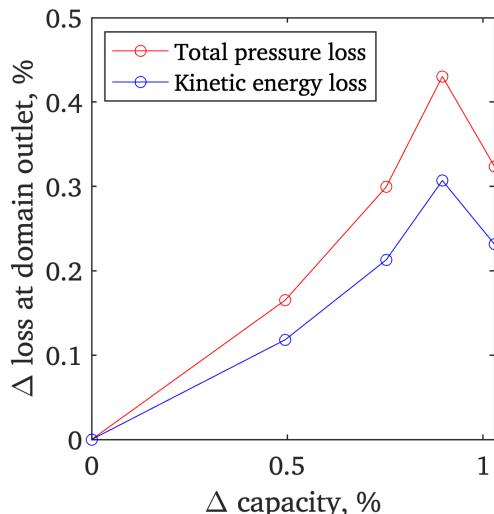


Figure 4.25: Loss delta as a function of capacity delta over the full range of cutbacks for the Trent 900 pressure-side cutback study at $PR = 1.79$

Figure 4.25 shows that, as the pressure side is incrementally removed, capacity and loss do not change in direct proportion to each other. Overall capacity sensitivity was greater than overall loss

sensitivity by approximately a factor of two, which is similar to the equivalent result in Section 4.1. At higher cutback amounts a relatively small increase in capacity corresponded to a sharp increase in loss by both definitions, except for the case of 100% cutback where loss was observed to decrease as discussed.

4.3 Chapter conclusions

Changes to the suction-side end-edge of the simulated NGV and changes to its pressure side cutback have both been shown to cause changes to the vane's flow capacity and aerodynamic performance.

Although capacity consistently increases when material is removed from either side of the trailing edge, the suction-side changes and the pressure-side changes are dominated by different mechanisms. Removal of suction-side end-edge material allowed for greater flow expansion downstream of the geometric throat, and consequently the flow capacity was more affected at unchoked pressure ratios. In contrast, the pressure-side cutbacks directly affected the width and location of the geometric throat, and the flow capacity was more affected at more choked pressure ratios where capacity is wholly set by the conditions on the sonic line as shown in Chapter 3.

Aerodynamic performance evaluations have included total pressure loss, kinetic energy loss, and flow turning angle deviation. All of these are shown to be affected by changes to either side of the trailing edge, although all were less severely affected by the pressure-side changes than by the suction-side ones. In all cases, loss increases are shown to result from increases in wake area caused by earlier boundary layer separation and improper shaping of the flow by the altered trailing edge. Improper flow shaping is also shown to cause the flow to excessively expand downstream of the NGV and experience improper turning. Turning errors are found to follow a simple trend in the case of suction-side changes, where end-edge material removal causes an incremental reduction in the vane's turning without fundamentally changing the wake profile. Pressure-side changes are shown to cause an interaction between the mainstream and the slot coolant flow, leading to a relationship between pressure-side cutbacks and turning angle surveys which is more difficult to categorise.

Chapter 5

Film cooling location

Chapter 3 has discussed how variations in the nozzle guide vane's overall cast shape affect flow capacity and performance, developing analytical techniques to draw conclusions about the relevance of throat width versus other factors at different pressure ratios. Chapter 4 has focused these analytical techniques on the NGV trailing edge, whose proximity to the throat region causes it to significantly affect capacity if its geometry is subject to small changes. This chapter will complete the present study's evaluation of near-throat variations by considering the effects of film coolant injection on the NGV suction side.

If a film cooling row is required on this part of the vane, small variations in the row's placement will cause the film coolant to be injected at various locations throughout the throat region. At choking pressure ratios, injection locations immediately upstream of the sonic line are expected to cause distinctly different effects compared to injection locations downstream of the sonic line. At all pressure ratios, varying the film coolant injection location is expected to cause variations in capacity and performance. This is due to the exchange of momentum between film coolant and mainstream, and due to the resulting variation in downstream boundary layer thickness which directly affects the effective throat width.

5.1 Sensitivity of capacity to cooling holes on the suction side

This section will consider the effects of varying the location of a single row of film cooling holes on the suction side of an otherwise uncooled nozzle guide vane. Real NGVs have a full showerhead of cooling holes on their leading edge, whose capacity and aerodynamic effects are far greater than those caused by the addition of a single row. These cooling holes are known to be necessary to prevent rapid failure of the NGV. The present study's goal is to control for the effects of the showerhead by simulating only a single film cooling row on the NGV suction side. Conventionally, film cooling has been avoided in this area to minimise loss, but newer engine combustor outlet temperatures are more likely to require suction side films in future. It is thus timely to understand their effects on flow capacity and aerodynamic performance.

The introduction of film coolant in this region is shown to affect the NGV flow capacity, and this effect is shown to be sensitive to the precise location of the film cooling hole row. This section uses the Rolls-Royce Trent XWB 84K nozzle guide vane as its baseline geometry. This has been selected because it represents one of the latest iterations of contemporary large civil aero engines, introduced into service in 2015 to power the Airbus A350 XWB. Successive generations of aero engines such as

the Trent XWB 97K have used increasingly high pressure ratios and combustor outlet temperatures, and thus the latest engine design is considered to be the most representative of designs most likely to require additional film cooling in future.

5.1.1 Geometry, mesh, and boundary conditions

A series of 2D CFD simulations were performed with a single cooling hole at a range of locations throughout the nozzle guide vane throat region. The blade profile geometry is the Rolls-Royce Trent XWB 84K nozzle guide vane. A 2D vane section was produced using the process illustrated in Figure 3.2. The overall computational domain was produced as in Figure 3.3. The NGV trailing edge was smoothly rounded as this section of study is not concerned with trailing edge effects. The NGV surface was modified to include a single cooling hole consisting of a slot and plenum with its total pressure inlet boundary condition described above.

Matlab was used to parametrically generate 7 geometries by moving the single cooling hole between 0% and 100% of its possible range of physical locations on the NGV suction side in increments of approximately 16%, although spacing of simulated hole locations was closer in the throat region of the nozzle. The angle between the cooling hole passage and the NGV surface remained constant throughout. In practice the exit angle of each film coolant row is varied according to location, with injection into higher-velocity flow performed at a smaller angle to the surface. The objective of this is to maintain a more constant coolant film thickness in leading edge regions closer to the NGV's stagnation point, where surface static pressure is greatest. The present study controls for ejection angle with a constant value of 60 degrees between coolant passage and NGV surface. Increased ejection angles would introduce coolant with a lower component of momentum in the mainstream flow direction. This would be expected to result in reduced capacity as momentum would be transferred from the mainstream to accelerate this coolant.

The range of hole locations is illustrated in Figure 5.1.

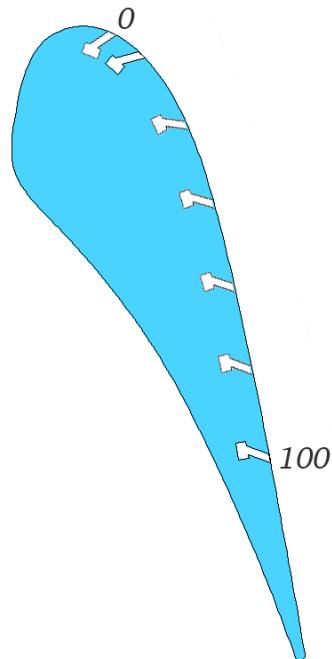


Figure 5.1: Range of locations for a single suction-side film cooling hole on a Trent XWB NGV

Simulations were performed at the design inverse pressure ratio of 1.65 but not at a fully choked inverse pressure ratio. This decision was made because the majority of the range of hole locations lie downstream of the nozzle's sonic line. In accordance with the other findings of this study, these locations are expected to have minimal effect on the NGV capacity.

If a film cooling row is to be modelled using 2-dimensional CFD, several considerations must be made to ensure the simulation is representative of real engine conditions. These considerations fall into 2 categories, namely the correct setting of boundary conditions at the coolant inlet, and the mitigation of 3-dimensional flow phenomena that affect coolant mixing but are not captured by 2-dimensional simulations.

The coolant inlet boundary exists to model the network of passageways that feeds compressor bleed air to the film cooling holes in a real engine. The present study represents this as a small plenum connected to the coolant hole. The coolant hole is specified as a narrow rectangular passage of engine-representative diameter, with no-slip walls. Total pressure is specified on the coolant plenum walls. An example of a 2D CFD domain for a single cooling row and its plenum is shown in Figure 5.2.

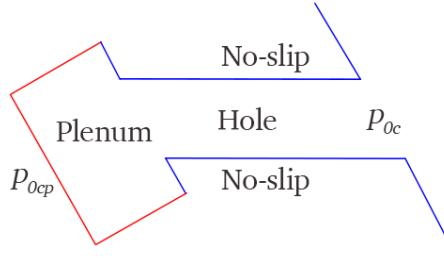


Figure 5.2: Computational domain and boundaries for simulating a film cooling hole and plenum on the suction side of a Trent XWB NGV

The present study aims to simulate an engine-representative ratio of coolant-to-mainstream mass flow rate. A typical value has been obtained from the technical memoranda provided by Rolls-Royce, and has been rounded to a value of 1% of the mainstream mass flow rate due to the sensitive nature of the data. Although it is optional to specify a desired mass flow rate on an inlet boundary in CFD, this is not a realistic simulation of the physics of a nozzle guide vane, where the designer has instead targeted a total pressure within each film coolant plenum. The coolant flow through the plenum and hole is then subject to a degree of total pressure loss. The resulting ideal isentropic mass flow rate from the film cooling hole is related to the total pressure and temperature at the hole exit p_{0c} and T_{0c} , the local mainstream static pressure p_m , and the hole cross-sectional area A_h by an adapted form of equation 1.11, as

$$\dot{m}_c = \frac{p_{0c}}{\sqrt{T_{0c}}} A_h \sqrt{\frac{\gamma}{R}} \left(\frac{p_m}{p_{0c}} \right)^{\frac{1}{\gamma}} \sqrt{\left(\frac{2}{\gamma-1} \right) \left[1 - \left(\frac{p_m}{p_{0c}} \right)^{\frac{\gamma-1}{\gamma}} \right]} \quad (5.1)$$

For a desired value of \dot{m}_c and a value of p_m calculated at a benchmark cooling hole location, it is thus possible to compute a required minimum value of p_{0c} . This may be achieved iteratively by rearranging equation 5.1 as

$$\lambda_n = p_m \left[1 - \frac{R(\gamma-1)}{2\gamma} T_{0c} \left(\frac{\dot{m}_c \lambda_{n-1}^{\frac{1-\gamma}{\gamma}}}{A_h p_w^{\frac{1}{\gamma}}} \right)^2 \right]^{\frac{\gamma}{1-\gamma}} \quad (5.2)$$

where $\lambda = p_{0c}$. T_{0c} is assumed to be 300K as the present study assumes adiabatic conditions.

Isentropic conditions may not be assumed, since losses in the plena of a real NGV cause the mass flow rate \dot{m} to be significantly lower than that predicted by equation 5.2, which assumes isentropic flow driven by the ratio $\frac{p_m}{p_{0c}}$. This loss may be quantified by applying a loss coefficient of a form similar to the general total pressure loss coefficient in equation 2.3, as

$$\zeta_c = \frac{p_{0cp} - p_{0c}}{p_{0cp} - p_m} \quad (5.3)$$

Typical values for p_{0cp} and ζ_c may be referenced from the literature. However, the present study sought to use 2D CFD to model a film cooling hole row as a slot, while achieving mass flow rates representative of those expected in a fully 3D vane with discrete hole locations. Such a 2D case will have inherently lower loss than the 3D case.

The differences in aerodynamic performance between film cooling holes and slots has long been a subject of research, with flow mechanisms downstream of hole rows being more complex than those formed by slots. A discrete hole is likely to have a pair of counter-rotating secondary flow vortices formed as the coolant enters the hole, with an unsteady process of vortex stripping and entrainment into the mainstream as the coolant exits the hole. In contrast, a slot tends to form a steady contiguous film on the external surface, with a separation bubble present under some conditions. To obtain boundary conditions likely to achieve coolant mass flow rates on the desired magnitude, coolant plenum boundary conditions were computed via the following process.

1. Converge a baseline CFD solution with no cooling holes. Use this case to report a baseline mainstream mass flow rate \dot{m} and a baseline NGV surface static pressure distribution. Use the surface static pressure distribution to report a value of p_m at each cooling hole location.
2. Converge a CFD solution with the cooling hole at position 0 and the cooling hole plenum specified as a mass flow inlet providing the benchmark coolant mass flow rate $\dot{m}_c = 1\%$ of \dot{m} (the rounded value obtained from Rolls-Royce). Report values for p_{0cp} and p_{0c} area-averaged across the plenum inlet boundary and the cooling hole exit.
3. Use this p_{0cp} as the specified total pressure on the coolant plenum inlet for all cases in the study.
4. Use this p_{0cp} and p_{0c} to validate ζ_c for the purpose of further discussion.

The resulting boundary conditions were used for all simulations and are listed in Table 5.1.

Table 5.1: Boundary conditions for Trent XWB suction-side cooling hole position study

Parameter	Value
NGV series	Rolls-Royce Trent XWB 84K
NGV turning (degrees)	73.97
Design inverse pressure ratio $\frac{p_{01}}{p_2}$	1.65
Inlet total pressure (Pa)	4.33×10^6
Inlet total temperature (K)	300
Outlet static pressure (Pa)	2.63×10^6
Outlet static temperature (K)	300
Benchmark coolant mass flow rate	1.00% of mainstream
Coolant ejection angle (degrees)	60
Film coolant loss coefficient ζ_c	0.8
Coolant plenum total pressure p_{0cp}	79.91% of mainstream
Solver type	Density-based
Cell count	40,000

The computed value for ζ_c of 0.8 corresponds to a high degree of total pressure loss within the coolant plenum and hole, which is to be expected both in simulation and in real engine parts. This suggests that the mass flow rate of coolant predicted by the present CFD study is likely to depart significantly from that predicted by isentropic flow alone. The computed value for p_{0cp} of 79.91% of mainstream is used as the coolant plenum total pressure in all subsequent CFD simulations.

Figure 5.1 depicts a range of geometries which allows the introduction of film coolant at various locations both upstream and downstream of the NGV geometric throat (and its sonic line in the case of fully choked flow). As the cooling hole and plenum consist of 2 rectangles, each was assigned a structured quadrilateral mesh that could be matched with a structured boundary layer mesh of the same design as that depicted in Figure 3.5a. Beyond this, an unstructured mesh was created to the same design as that depicted in Figure 3.4. Details of the resulting mesh are shown in Figure 5.3.

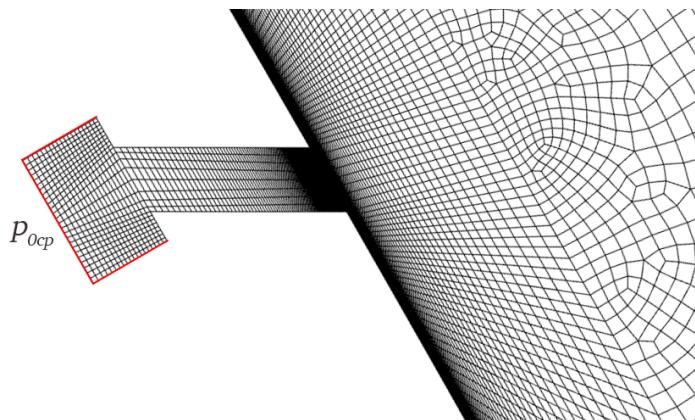


Figure 5.3: Detail of mesh for XWB single cooling hole study

5.1.2 Effect on capacity

Figures 5.4, 5.5, 5.6, and 5.7 show contours of Mach number in the region of the nozzle guide vane for the described study. Inverse pressure ratio is 1.65, the design cruise condition.

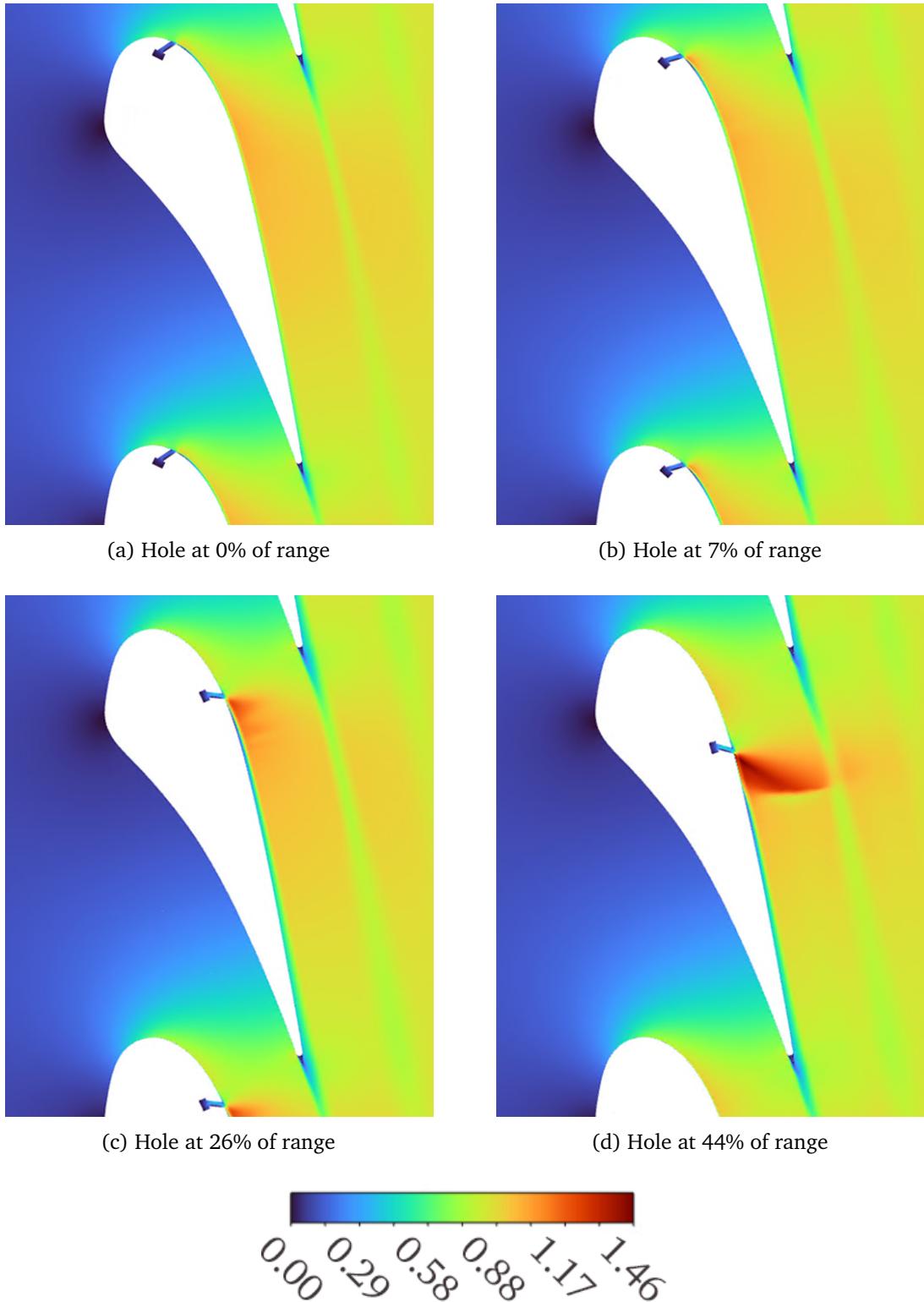
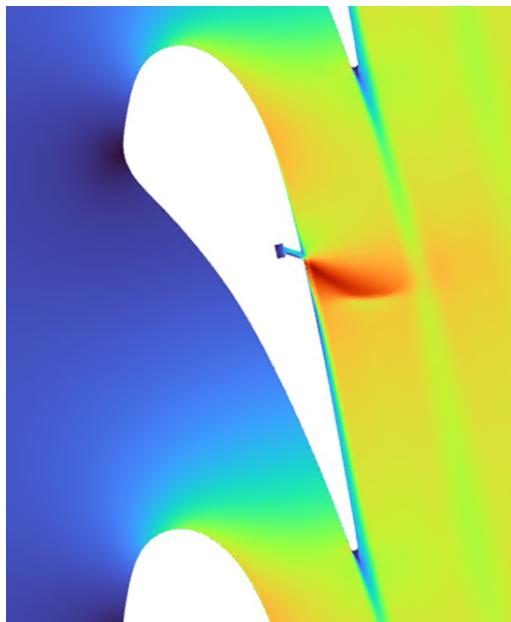
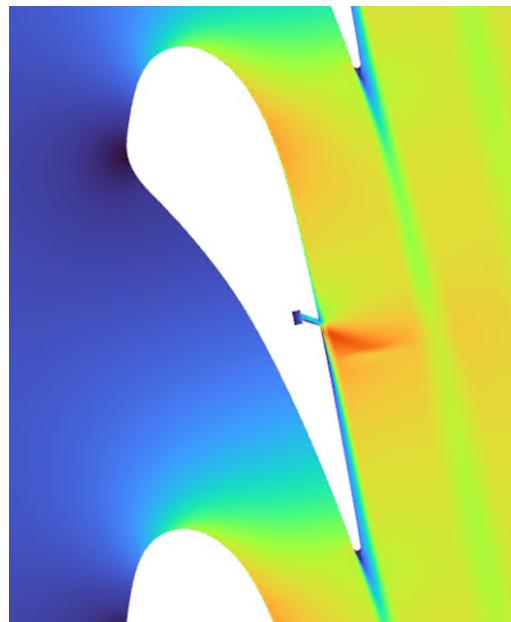


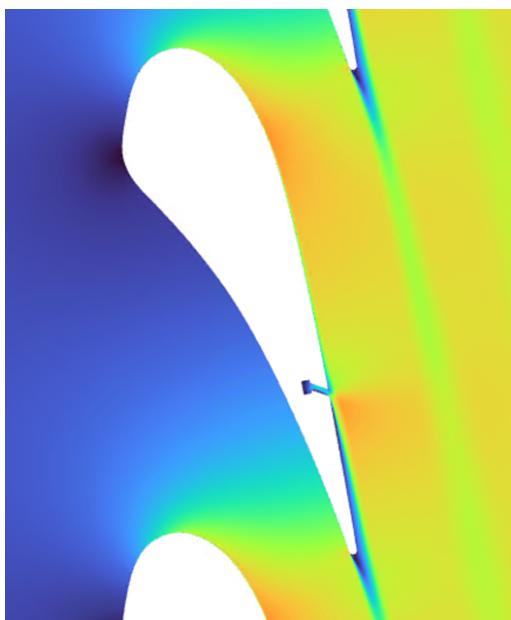
Figure 5.4: Mach contours for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$, labelled by position of single suction-side film cooling hole - part 1 of 2



(a) Hole at 63% of range



(b) Hole at 81% of range



(c) Hole at 100% of range

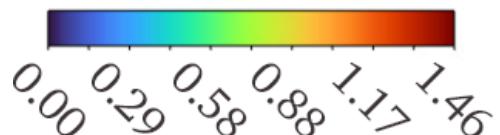


Figure 5.5: Mach contours for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$, labelled by position of single suction-side film cooling hole - part 2 of 2

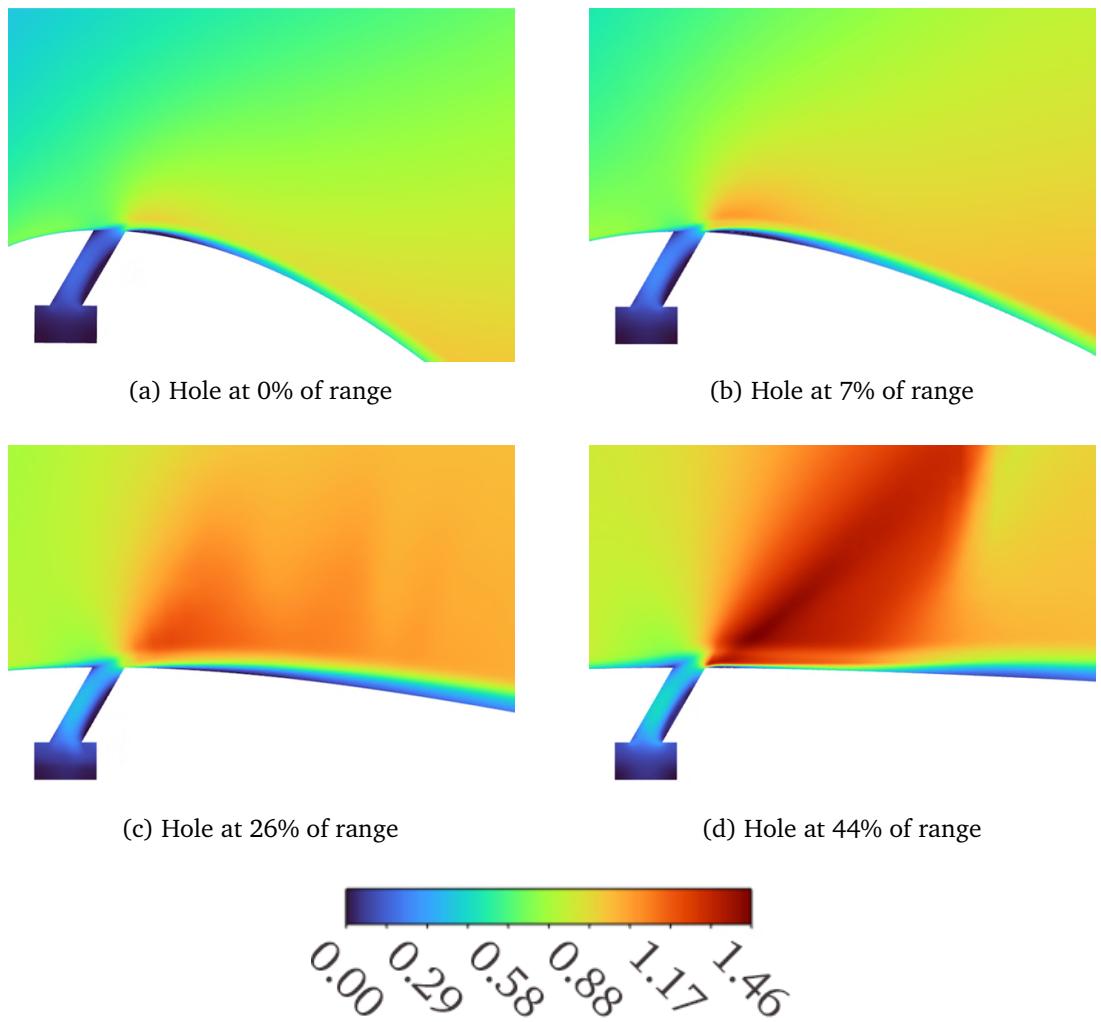


Figure 5.6: Mach contours near single cooling hole for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$, labelled by position of single suction-side film cooling hole - part 1 of 2

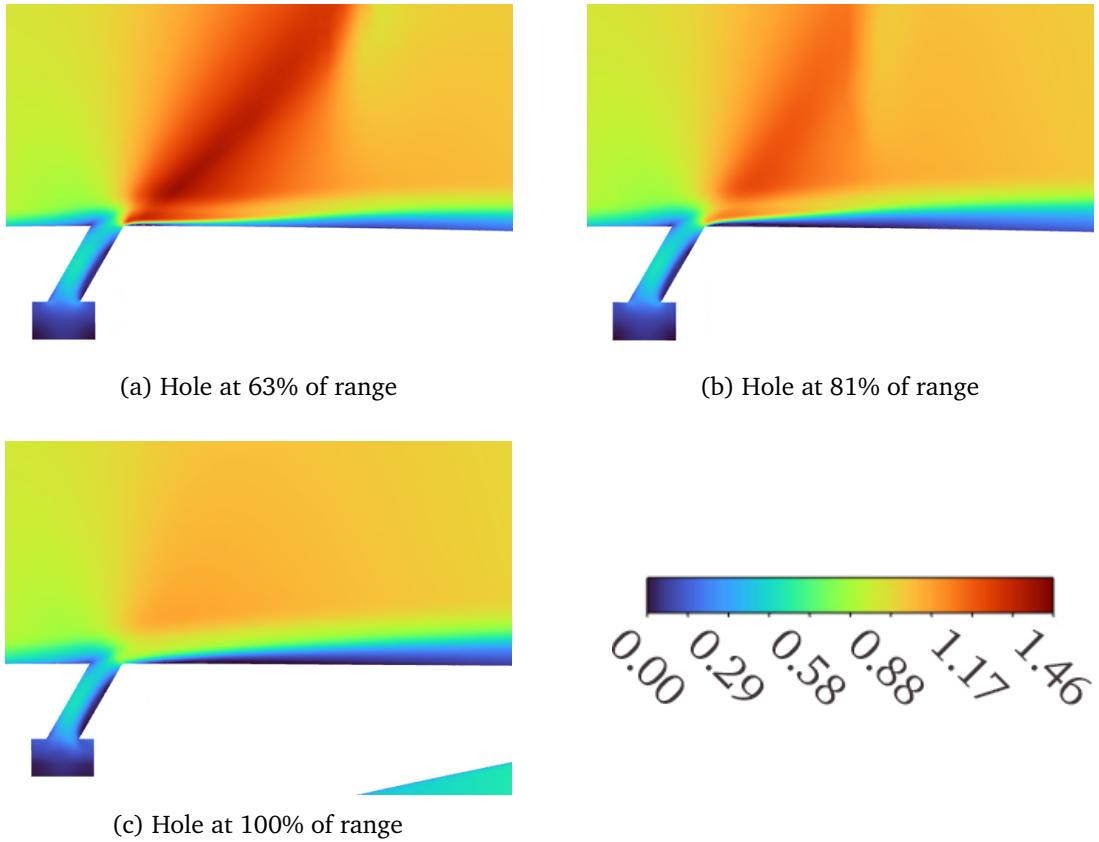


Figure 5.7: Mach contours near single cooling hole for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$, labelled by position of single suction-side film cooling hole - part 2 of 2

Figures 5.4, 5.5, 5.6, and 5.7 illustrate the presence of transonic flow phenomena that varied significantly with the variations to the location of film coolant injection. Injection locations upstream and far downstream of the throat region caused localised flow acceleration as the potential field of the coolant jet caused a narrowing of the effective throat area. At injection locations immediately downstream of the throat, where the mainstream flow velocity was greatest, this effect was significantly stronger. Here the local acceleration resulted in regions of supersonic flow within the mainstream, followed by deceleration through a shock attached to the suction side of the nozzle guide vane.

In all cases, the suction side boundary layer thickness increased immediately downstream of the film cooling hole, due to the mainstream flow being displaced by the momentum of the coolant jet in the direction perpendicular to the NGV surface. In the cases with the hole at 0% and 7% of the range of travel, where the injection location was upstream of the geometric throat, this increase in boundary layer thickness amounted to a local bubble after which the boundary layer became thinner again and experienced conventional growth further downstream. In the case with the hole at 26% of the range of travel, the coolant injection appeared to initiate a growth of the boundary layer which began immediately downstream of the hole and continued throughout the suction side of the NGV, resulting in a distinctly thicker boundary layer at the suction side trailing edge compared to the cases of pre-throat coolant injection.

In the cases with the hole at 44% and 63% of the range of travel, where the coolant-induced acceleration and shock were strongest, the coolant-induced boundary layer growth appeared to be delayed until the point of shock attachment on the NGV suction side. Downstream of this, an uninterrupted boundary layer growth again resulted in a thick boundary layer at the suction side trailing edge. In the cases with the hole at 81% and 100% of the range of travel, boundary layer growth was

reminiscent of the case of 26%, initiating immediately downstream of the film cooling hole despite the presence of supersonic regions and shocks. All of these observations suggest that shock loss is an important factor in evaluating the performance effects of the cooling hole location. This will be discussed subsequently.

Figures 5.6 and 5.7 show that coolant flow separation occurred within the plenum and hole passage. This is not considered to significantly affect the accuracy of the conclusions drawn from the present study, as the flow is seen to reattach before exiting the coolant hole. Furthermore, the boundary conditions set at the coolant plenum boundary have been shown to result in the correct coolant mass flow rate, and thus phenomena such as in-passage separation are accounted for. Furthermore, as shown in Figures 5.6 and 5.7, within the coolant hole and plenum, the flow structures remained highly similar regardless of location on the NGV suction side.

Figure 5.8 plots the percentage change in the NGV flow capacity as a function of the cooling hole location.

For this analysis, two definitions of capacity are provided. The first, Γ_{in} , is defined as

$$\Gamma_{in} = \frac{\sqrt{T_{01}}}{p_{01}} \dot{m} \quad (5.4)$$

where T_{01} and p_{01} are the upstream total conditions and \dot{m} is the mainstream mass flow rate measured at the domain inlet. The second definition, Γ_{out} , represents the capacity of the flow leaving the domain, and is defined as

$$\Gamma_{out} = \frac{\sqrt{T_{01}}}{p_{01}} (\dot{m} + \dot{m}_c) \quad (5.5)$$

where \dot{m}_c is the coolant mass flow rate which may vary with injection location as the coolant plenum is specified by total pressure instead of mass flow rate.

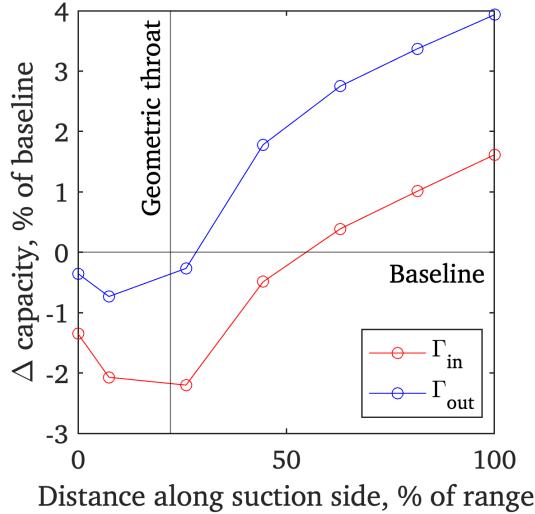


Figure 5.8: Total capacity percentage delta as a function of single cooling hole position on the Trent XWB suction side surface at $\frac{p_{01}}{p_2} = 1.65$

Figure 5.8 shows a general trend of flow capacity increasing as the film coolant is injected. The maximum range of Γ_{in} was 3.82% over the range of hole locations, and the maximum range of Γ_{out} was 4.67%. This trend is uniformly true for the cases where coolant is injected downstream of the geometric throat. It is hypothesised that this capacity increase is primarily driven by the introduction

of the coolant into regions of progressively lower mainstream flow velocity as the hole location moves downstream and away from the throat region. This decrease in mainstream flow velocity is observable in Figures 5.4 and 5.5 and is to be expected of unchoked flow downstream of the throat of a nozzle guide vane. Assuming that, in general, film coolant affects NGV capacity via the exchange of momentum between the fast mainstream and the slower coolant, it is concluded that this deficit to mainstream flow momentum is less severe as the coolant is injected into slower regions further downstream.

This hypothesis is supported by the capacity predictions for the cases where coolant is injected upstream of, or very near, the NGV geometric throat. Compared to the furthest location upstream, the 2 subsequent downstream locations resulted in a deficit to flow capacity which was most severe in the region local to the throat. Here the mainstream flow velocity was highest and thus the coolant injection would be expected to cause the greatest deficit to mainstream momentum and thus mass flow rate. This hypothesis may be further tested by considering the isentropic Mach number on the NGV surface, which may be defined as

$$M_{isent} = \sqrt{\frac{2}{\gamma-1} \left[\left(\frac{p_{01}}{p_m} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \quad (5.6)$$

Figure 5.9 plots the percentage change in the NGV flow capacity as a function of the surface isentropic Mach number at each cooling hole location. Data points are connected to convey the sequence of incremental changes to the hole location.

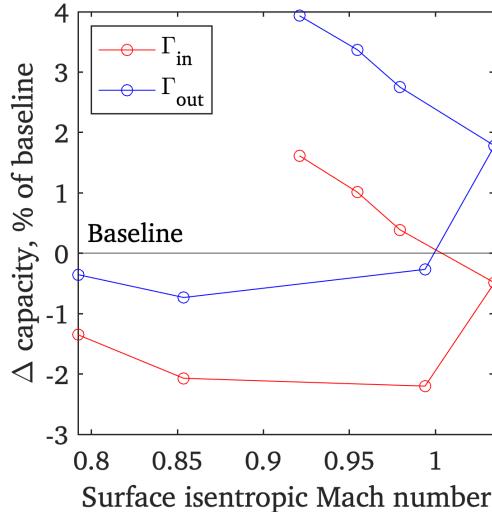


Figure 5.9: Total capacity percentage delta as a function of surface isentropic Mach number for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$

Figure 5.9 shows a relationship between surface isentropic Mach number and flow capacity which is in agreement with the prior discussion for cases downstream of the geometric throat, as capacity decreased as the coolant was injected into locations having a higher Mach number. The 3 data points furthest upstream are less clearly interpretable. A trend of capacity decreasing with local Mach number was arguably present, however these data were not in alignment with those downstream of the throat. This suggests that a consideration of the local flow velocity or Mach number does not entirely explain the observed relationship between hole location and capacity.

We may also examine the variation in the capacity of the coolant itself as it is injected at various

locations at a constant plenum total pressure. The coolant capacity is defined as

$$\Gamma_c = \frac{\sqrt{T_{0cp}}}{p_{0cp}} \dot{m}_c \quad (5.7)$$

where T_{0cp} and p_{0cp} are the coolant plenum inlet total conditions. Figure 5.10 plots the coolant capacity as a function of the cooling hole location.

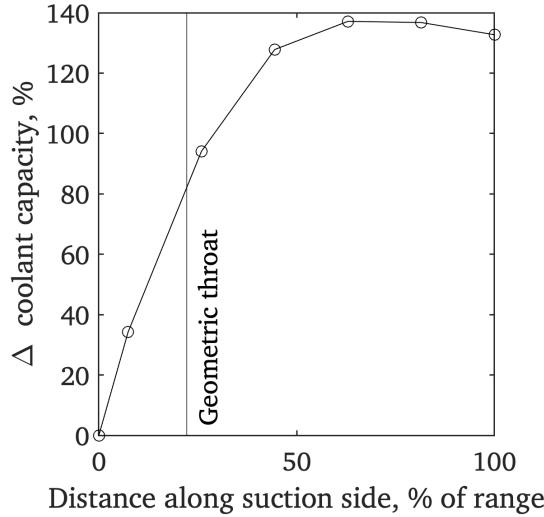


Figure 5.10: Coolant capacity percentage delta as a function of single cooling hole position for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$

Figure 5.10 shows that the coolant capacity varied significantly with the hole location, with the maximum range being approximately 137.10%, or a factor of 2.37. This variation is hypothesised to be the result of different hole locations causing the coolant to be injected into regions of different static pressure p_m , with correspondingly different pressure ratios as defined in equation 5.2. If this is the case, the predicted coolant capacity would be expected to correlate closely with the coolant isentropic mass flow rate given by equation 5.1 using the local p_m and p_{0c} as inputs. The predicted coolant capacity is plotted as a function of the coolant isentropic capacity (defined as in equation 5.7) in Figure 5.11.

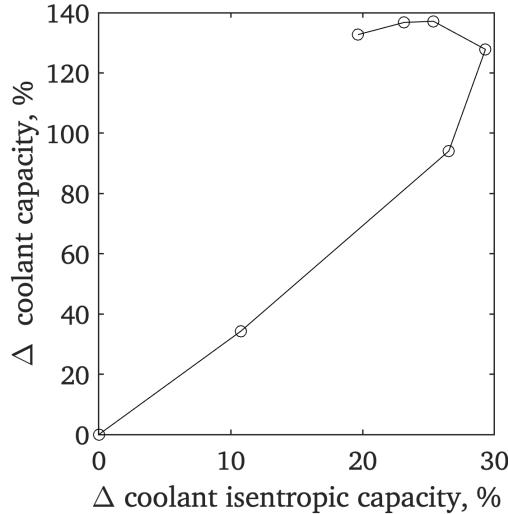


Figure 5.11: Coolant capacity percentage delta as a function of coolant isentropic capacity percentage delta for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$

Figure 5.11 shows a trend of the predicted coolant capacity increasing in moderate correlation with the coolant isentropic capacity for the range of injection locations between 0% and 44% of range. At locations further downstream, the coolant isentropic capacity decreases but the predicted capacity does not also decrease as expected. This is likely to result from the interaction between the coolant and the shock that forms immediately downstream of the injection location at mid-range positions. This shock formation is visible in detail in the Mach number contours in Figures 5.6 and 5.7.

At locations between 0% and 44%, coolant capacity increased as a result of decreasing local static pressure, although this mechanism of increase is assumed to be partly attenuated by the appearance of the shocks. At locations incrementally further downstream, the local static pressure was increasing, with a corresponding decrease in the coolant isentropic capacity. However, mainstream flow velocity was decreasing, with a corresponding decrease in shock formation downstream of the single cooling hole. These opposing effects are hypothesised to cause the trend of approximately constant predicted coolant capacity for hole locations downstream of 44% of range.

5.1.3 Effect on performance

Shock loss has been hypothesised to be a significant influence on the aerodynamic performance of the present configuration at different cooling hole locations. Figure 5.12 plots loss (as defined by equation 2.3) as a function of single cooling hole position.

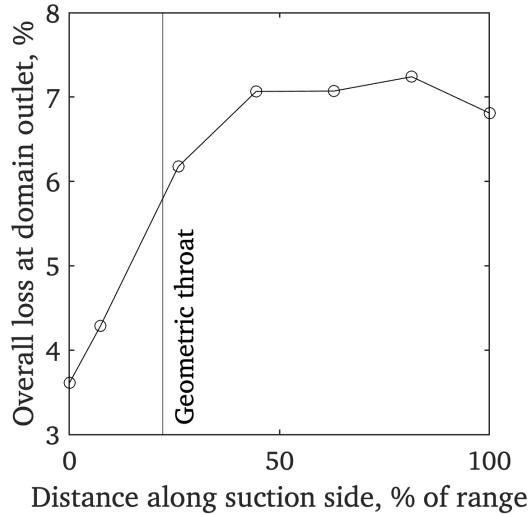


Figure 5.12: Loss as a function of single cooling hole position for Trent XWB film cooling study at $\frac{p_{01}}{p_2} = 1.65$

The trend exhibited in Figure 5.12 is in good agreement with the prior discussion of Figures 5.4 and 5.5 which suggests that the degree of aerodynamic loss incurred will correlate strongly with the strength of shocks precipitated by the injection of film coolant. The Mach contours show the increasing appearance of shocks as the coolant is introduced further downstream, with shocks most apparent when the coolant hole is at 44%, 63%, and 81% of its range of positions. Correspondingly these positions resulted in the greatest amount of total pressure loss. It is concluded that shock loss is the primary loss mechanism driving the observed trend.

5.2 Chapter conclusions

This chapter has investigated the effects of injecting film coolant at a constant plenum total pressure, but at varying locations, on the suction side of a nozzle guide vane. This investigation has been justified by the movement in industry towards higher combustor outlet temperatures leading to NGVs that are likely to require additional film cooling rows.

Where, historically, film coolant rows have been grouped in a shower-head at the NGV leading edge, novel designs are likely to need the additional row at some location on the suction side. The capacity and aerodynamic penalties associated with this change are best understood by considering the reasons for which film coolant is currently only dispersed from the leading edge shower-head.

Section 5.1 has demonstrated how the injection of coolant into regions of high mainstream flow velocity causes both reduced flow capacity and increased loss. The CFD-derived trends of flow capacity as a function of cooling hole location have illustrated that injection near the NGV throat region causes a minimum flow capacity compared to the rest of the trend. Elsewhere injection into locally slower regions results in capacity predictions that match or even exceed the baseline capacity derived from applying the same CFD boundary conditions to an uncooled and unfeatured NGV. Loss has also been considered, with the conclusion that the present cases experienced a significant degree of shock loss due to the formation of shocks immediately downstream of the single cooling hole.

It is concluded that, depending on the ratio of coolant-to-mainstream momentum, film coolant

injection is capable of either energising a low-velocity mainstream or of de-energising a high-velocity mainstream. This is particularly interesting when considered alongside the other conclusions of this thesis. All previous chapters have sought to characterise nozzle guide vane flow capacity in 2 simple ways: it is a function of the effective areas throughout the nozzle, and if the flow is choked then it is a function of only the effective throat area. The suction side film cooling problem may be characterised similarly. Injection of film coolant into a high-velocity mainstream is, in the limiting case, equivalent to the placement of a stationary obstacle to the flow, and is therefore characteristic of a reduction in the effective area of the flow at that location along the nozzle. At the other extreme is the case of introducing film coolant into a nozzle with 0 mainstream velocity. Assuming the film coolant has a momentum component along the direction of the nozzle, this is characteristic of creating an effective area of flow velocity where before there was none. Since the suction side film cooling investigation has been entirely at non-choked pressure ratios, it is to be expected that the film coolant injection location continues to have an effect throughout the suction side and beyond the NGV geometric throat.

This chapter's conclusions are in good agreement with those of the other chapters, in particular where the relationship between flow capacity and effective area is concerned.

Chapter 6

Conclusion

6.1 Summary of findings

This thesis demonstrates that nozzle guide vane capacity, although a highly complex problem, benefits from a simplified approach whereby the principal mechanisms can be identified and modelled separately from one another in a 2-dimensional environment. All the effects seen result from nozzle guide vane geometry changes. Small geometric changes are magnified into larger changes in capacity resulting from the differences between the effective throat area and the geometric throat.

Chapter 1 outlined the importance of flow capacity as the scalable pseudo-dimensionless variable describing the mass flow rate through the engine. Chapter 3 linked this to an effective throat area, and investigated its variance in response to small changes in manufacturing tolerance introduced in the first stage of manufacturing, namely casting. Chapter 4 introduced design-led NGV geometry features in the trailing edge, and investigated how capacity changes in response to these. Here, changes in the pressure side and suction side features are decided primarily by cutback design and wear respectively. Notably, the industrial assumption of a geometric throat attached to the pressure side cutback is seen to be challenged in the early service life of the blade when a thin trailing edge is maintained. Chapter 5 introduced coolant flows ejected from the suction side surface of the blade. High operating temperatures may require such features, which are always somewhat undesirable in terms of loss. The injection into the high-velocity suction side flow is discussed, and the sensitivity of capacity and loss to varying the injection location is established. In combination, these chapters seek to present a clarification of the main challenges to our understanding and prediction of nozzle guide vane flow capacity and loss.

6.2 Suggestions for future work

With only 6 blade geometries available, the current work has established that modern CFD techniques can reliably predict significant capacity changes at typical manufacturing tolerances. Further work and commercial exploitation may be achieved by post-manufacture characterisation of finished cast engine components prior to assembly, to generate annular sets of nozzle guide vanes with similar vane-to-vane capacity, limiting the forcing function on the downstream rotor assembly. Additionally, the modelling of many such passages will allow the development of surrogate models for a given engine architecture, allowing the accurate mapping of any scanned NGV passage onto a predicted capacity characteristic without further use of CFD or testing. This has the potential to greatly increase

the yield of cast components, improving cost and sustainability in manufacture.

The problem of additional film cooling is less conducive to speculation. Additional film cooling is highly likely to occur as a result of inevitably increasing operating temperatures. It is uncertain which strategy will be employed: manufacturers may choose to inject film coolant into the low-velocity region upstream of the NGV throat, which would be loss-optimal in theory but would require a high coolant mass flow rate to ensure coolant presence along the full NGV chord. Manufacturers may instead choose to inject less coolant at this location and to refresh the coolant film with additional rows downstream. Such design choices are expected to be a topic of interest in the near future.

Finally, in the event that novel material choices, such as CMC, require a thicker trailing edge, it is likely that the cutback design will be retained for the purpose of preventing blockage. In this case there would be relatively little information about the lifetime of the end-edge with a novel material. This would strongly motivate further study of end-edge in-service changes. The benefits of this would include validation of the present study's findings on end-edge cutbacks, and valuable service life information on the use of novel materials in the most extreme environment within a gas turbine.

Bibliography

- [1] A. Guiffre' and M. Pini, "Design guidelines for axial turbines operating with non-ideal compressible flows," *Proceedings of ASME Turbo Expo*, 2020.
- [2] C.-M. Lee, K. Kundu, and W. Acosta, "Jet-a reaction mechanism study for combustion application," Tech. Rep. 04441, NASA and US Army Aviation Systems Command, Lewis Research Center, Cleveland, Ohio, June 1991.
- [3] C. R. Marius and C. Grigore, "Study of air excess in relation with engine parameters for a generalized reaction based on jet-a fuel," *Applied Mechanics and Materials*, vol. 772, no. 395, pp. 395–400, 2015.
- [4] S. N. Singh, V. Seshadri, R. K. Singh, and T. Mishra, "Flow characteristics of an annular gas turbine combustor model for reacting flows using cfd," *NISCAIR Journal of Scientific and Industrial Research*, vol. 65, pp. 921–934, 2006.
- [5] P. V. Ranjith, M. Shivashankar, G. Sivaramakrishna, and V. Narayanan, "Reduction of gas turbine combustor pattern factors using cfd," *International Journal of Engineering Research and Technology*, vol. 3, no. 6, 2014.
- [6] L. Jiang, X. Wu, and Z. Zhang, "Conjugate heat transfer of an internally air-cooled nozzle guide vane and shrouds," *Advances in Mechanical Engineering*, vol. 6, 2014.
- [7] D. B. da Trinidade, P. Bugala, and D. Simone, "Review of loss models for high pressure turbines," *Journal of KONES Powertrain and Transport*, vol. 25, no. 2, pp. 37–44, 2018.
- [8] P. W. Giel, V. Shyam, P. Juangphanich, and J. P. Clark, "Effects of trailing edge thickness and blade loading distribution on the aerodynamic performance of simulated cmc turbine blades," *Proceedings of ASME Turbo Expo*, 2020.
- [9] J. Gau, M. Wei, W. Fu, Q. Zheng, and G. Yue, "Experimental and numerical investigations of trailing edge injection in a transonic turbine cascade," *Elsevier Journal of Aerospace Science and Technology*, vol. 92, pp. 258–268, 2019.
- [10] R. Saha, J. Fridh, and T. H. Fransson, "Shower head and trailing edge cooling influence on transonic vane aero performance," *Proceedings of ASME Turbo Expo*, 2014.
- [11] M. Deckers and J. D. Denton, "The aerodynamics of trailing-edge-cooled transonic turbine blades: Part 1 - experimental approach," *Proceedings of ASME Turbo Expo*, 1997.
- [12] D. Thirumurthy, J. C. C. Coca, and K. Suraweera, "Capacity matching of aeroderivative gas generator with free power turbine: Challenges, uncertainties, and opportunities," *Proceedings of ASME Turbo Expo*, 2019.
- [13] T. Hall, "Trent 900 CFD investigation of HPNGV capacity sensitivity to trailing edge geometry," Tech. Rep. DNS 170140, Rolls-Royce plc, Gipsy Patch Lane, Filton, Bristol, March 2011.

- [14] G. Zamboni, “HYDRA CFD of the trent 900 EP1 turbine high pressure nozzle guide vane: analysis of the trailing edge slot geometry influence on capacity predictions using gom scanned data,” Tech. Rep. DNS 181981, Rolls-Royce plc, Gipsy Patch Lane, Filton, Bristol, July 2012.
- [15] J. Nikuradse, “Laws of flow in rough pipes,” *VDI Verlag research booklet; “supplement to Research in the field of engineering”*, vol. 361, no. B4, 1933.
- [16] H. Schlichting, *Boundary Layer Theory*. New York, NY, USA: McGraw-Hill, 1979.
- [17] S. M. Salim and S.-C. Cheah, “Wall $y+$ strategy for dealing with wall-bounded turbulent flows,” *Proceedings of the International MultiConference of Engineers and Computer Scientists*, vol. II, 2009.
- [18] ANSYS Inc., “Overview of FMG initialization.” <https://www.afs.enea.it/project/neptunius/docs/fluent/html/th/node388.htm>, 2009. Accessed: 2021/06/23.
- [19] S. M. Jones, W. J. Haller, and M. T. Tong, “An n+3 technology level reference propulsion system,” *NASA technical memorandum*, 2017.

Appendix A

Matlab post-processing codes

A.1 Geometric throat width calculator

```
close all;
clear variables;
load workspaces/T900_RThX_all_ver08;

%the spacing in metres between each NGV at mid-span radius
periodic_spacing = 0.05881;

%input which vane
vane_xy = KSZ03_streamline_11_xyz(:,1:2);
vane_section = vane_xy(20:50,:);

%apply the periodic spacing
%vane_xyz_2 = vane_xyz;
%vane_xyz_2(:,2) = vane_xyz(:,2) + periodic_spacing;

% OVERSAMPLING THE VANE COORDINATES %

n = size(vane_section);
q = n(2);
n = n(1);

range = vane_section(n,1) - vane_section(1,1);
resolution = 10000;

interp_vector = vane_section(1,1):range/resolution:vane_section(n,1);
interp_vector = interp_vector';

p = size(interp_vector);
p = p(1);
vane_section_oversampled = zeros(p,q);
```

```

for i2 = 1:q
    vane_section_oversampled(:,i2) = interp1(vane_section(:,1),...
        vane_section(:,i2), interp_vector, 'pchip');
end

% CALCULATING THE DISTANCES %

%for PS cutbacks
vane_section_2 = [-0.01005, 0.001008];
vane_section_2(:,2) = vane_section_2(:,2) + 0.0588106;

iterations = size(vane_section_oversampled);
iterations = iterations(1);
distances = zeros(iterations, 1);

%turn on this bit for PS cutbacks
for m = 1:iterations
    local_vector = vane_section_oversampled(m,:) - vane_section_2;
    distances(m) = norm(local_vector,2);
end

throat_width = min(distances(:,1));
throat_width = min(throat_width)
distances = distances(:,1);
[row] = find(distances <= throat_width);

%for smooth vanes
%throat_line = [vane_sectionz(row,:); vane_section_2(column,:)] ;

%for PS cutbacks
throat_line = [vane_section_oversampled(row,1:2); vane_section_2(1,1:2)] ;

%calculate the throat width differently to confirm the value
throat_width_alt = sqrt((throat_line(1,1) - throat_line(2,1))^2 + ...
    (throat_line(1,2) - throat_line(2,2))^2);

% PLOTS %

figure(1)
plot(vane_xy(:,1), vane_xy(:,2), 'b')
hold on
plot(vane_xy(:,1), vane_xy(:,2) + 0.0588106, 'b')
plot(throat_line(:,1), throat_line(:,2), 'r')
plot(vane_section_2(:,1), vane_section_2(:,2), 'ko')
axis equal

figure(2)
plot(PS_cutback_throat_widths(:,1),...
    100*PS_cutback_throat_widths(:,2)/PS_cutback_throat_widths(1,2)-100,...
```

```

'ko-')
xlabel('Cutback amount')
ylabel('Change in throat width, %')
title('2D throat width vs. PS cutbacks')

figure(3)
plot(100*PS_cutback_throat_widths(:,2)/PS_cutback_throat_widths(1,2)-100, ...
    100*cutback_capacities_design(:,3)/cutback_capacities_design(1,2), ...
    'ko-')
hold on
plot(100*PS_cutback_throat_widths(:,2)/PS_cutback_throat_widths(1,2)-100, ...
    100*cutback_capacities_design(:,2)/cutback_capacities_design(1,2), ...
    'k^-')
plot(100*PS_cutback_throat_widths(:,2)/PS_cutback_throat_widths(1,2)-100, ...
    100*cutback_capacities_design(:,1)/cutback_capacities_design(1,2), ...
    'kh-')
xlabel('Change in throat width, %')
ylabel('\Delta Capacity, %')
title('2D Capacities vs. 2D throat widths')
legend('PR = 3.33', 'PR = 1.79 (design)', 'PR = 1.5')
ylim([95 104])

figure(4)
plot(0:1:4, ...
    100*cutback_capacities_design(:,3)/cutback_capacities_design(1,2), ...
    'ko-')
hold on
plot(0:1:4, ...
    100*cutback_capacities_design(:,2)/cutback_capacities_design(1,2), ...
    'k^-')
plot(0:1:4, ...
    100*cutback_capacities_design(:,1)/cutback_capacities_design(1,2), ...
    'kh-')
xlabel('Cutback amount')
ylabel('\Delta Capacity, %')
title('2D Capacities vs. PS Cutback Amount')
legend('PR = 3.33', 'PR = 1.79 (design)', 'PR = 1.5')
ylim([95 104])

```

A.2 Effective throat width calculator

```

close all;
clear variables;
load workspaces/T900_2021.mat;

%the spacing in metres between each NGV at mid-span radius
periodic_spacing = 0.05881;

```

```

%load data from the imported workspace
x = KSZ03_xvel_yvel_mach(:,2);
y = KSZ03_xvel_yvel_mach(:,3);
xvel = KSZ03_xvel_yvel_mach(:,4);
yvel = KSZ03_xvel_yvel_mach(:,5);
M = KSZ03_xvel_yvel_mach(:,6);

%make it 2 vanes instead of 1
x_repeated = x;
y_repeated = y;
for n = 1:length(y)
    y_repeated(n) = y(n) + periodic_spacing;
end
x = cat(1,x,x_repeated);
y = cat(1,y,y_repeated);
M = cat(1,M,M);
xvel = cat(1,xvel,xvel);
yvel = cat(1,yvel,yvel);

%create a uniform quadrilateral mesh onto which the existing data will be
%interpolated
[x_grid,y_grid] = meshgrid(-0.03:0.0001:-0.009,0.050:0.0001:0.070);
mach_grid = griddata(x, y, M, x_grid, y_grid);
xvel_grid = griddata(x, y, xvel, x_grid, y_grid);
yvel_grid = griddata(x, y, yvel, x_grid, y_grid);
mach_grid_size = size(mach_grid);
height = mach_grid_size(1);
width = mach_grid_size(2);

%replace NaN values with 0
for i = 1:height
    for j = 1:width
        if isnan(mach_grid(i,j))
            mach_grid(i,j) = 0;
        end
    end
end

%find the M=1 line
M1_positions_and_velocities = zeros(1,4);
for j = 1:width
    %go along a vertical strip until M > 1
    for i = 2:height
        if (mach_grid(i-1,j) > 1 && mach_grid(i,j) < 1) ||...
            (mach_grid(i-1,j) < 1 && mach_grid(i,j) > 1)
            M1_position_and_velocity = [x_grid(i,j),y_grid(i,j),...
                xvel_grid(i,j),yvel_grid(i,j)];
            M1_positions_and_velocities =...
                cat(1,M1_positions_and_velocities,...);
            M1_position_and_velocity);
    end
end

```

```

    end
end
M1_positions_and_velocities = M1_positions_and_velocities(2:end,:);

%add two columns to M1_positions which is are x and y coordinates tilted at
%an angle approximately orthogonal to the sonic line so they can be sorted
%along this direction
theta = 2*pi*-30/360;
R = [cos(theta) -sin(theta) ; sin(theta) cos(theta)];
M1_positions_and_velocities = cat(2,M1_positions_and_velocities,... 
    zeros(size(M1_positions_and_velocities,1),2));
for i = 1:size(M1_positions_and_velocities,1)
    outputVector = R*[M1_positions_and_velocities(i,1),...
        M1_positions_and_velocities(i,2)]';
    M1_positions_and_velocities(i,5) = outputVector(1);
    M1_positions_and_velocities(i,6) = outputVector(2);
end
M1_positions_and_velocities = sortrows(M1_positions_and_velocities,5);

%trim the ends so spurious bits aren't included
M1_positions_and_velocities = M1_positions_and_velocities(1:end,:);

%integrate along the M1 line
theta = 2*pi*90/360;
R = [cos(theta) -sin(theta) ; sin(theta) cos(theta)];
integral = 0;
for i = 2:size(M1_positions_and_velocities,1)
    localVector = [M1_positions_and_velocities(i,1),...
        M1_positions_and_velocities(i,2)]-...
        [M1_positions_and_velocities(i-1,1),...
        M1_positions_and_velocities(i-1,2)];
    localUnitVector = localVector/norm(localVector);
    localOrthogonalUnitVector = R*localUnitVector';
    %find the velocity vector local to this point on the line
    localVelocity = [M1_positions_and_velocities(i,3),...
        M1_positions_and_velocities(i,4)];
    localVelocityUnitVector = localVelocity/norm(localVelocity);
    integrand = dot(localOrthogonalUnitVector, ...
        localVelocityUnitVector)*norm(localVector);
    if isnan(integrand)
    else
        integral = integral + integrand;
    end
end

%plot the sonic line shape over the mesh nodes
figure(1)
plot(x,y,'k.')
hold on
plot(M1_positions_and_velocities(:,1),...
    M1_positions_and_velocities(:,2),'r-')

```

```

axis equal
xlim([-0.03 -0.009])
ylim([0.050 0.070])

```

A.3 Film cooling plenum loss calculator

```

close all;
clear variables;
load workspaces/sch_data.mat;

%find the plenum total pressure from a given mass flow rate fraction

%physical properties
R = 287.058; %[Joules/(kg.K)]
cp = 1121; %[Joules/(kg.K)]
cv = 834; %[Joules/(kg.K)]
gamma = cp/cv;

fluent_operating_pressure = 4285900;
p_m_benchmark = -1e6 + fluent_operating_pressure;

%coolant/mainstream mass flow ratio
coolant_ratio = 0.01;

%2D hole width
A_h = 7.4993e-4;

%inlet total pressure
p_0m = 4325590;

%total temperatures
T_0m = 300;
T_0c = 300;

%correction between 2D and Q3D
q3d_strip_width = 0.0029;
ratio_of_slot_to_hole = (4/pi)*q3d_strip_width/A_h;

%use the benchmark coolant MFR to work out the plenum total pressure,
%iteratively

%benchmark values
m_m_benchmark = 121;
m_c_benchmark = m_m_benchmark*coolant_ratio;
zeta_c = 0.8;

%array to store and plot the convergence for both possible methods

```

```

number_of_iterations = 10;
array = zeros(number_of_iterations,1);

%initial guess
p_0c_benchmark = p_m_benchmark;

for i = 1:number_of_iterations
    p_0c_benchmark = p_m_benchmark*( 1 - ( R*(gamma-1)*T_0c*m_c_benchmark^2*...
        p_0c_benchmark^((2-2*gamma)/gamma) )/( 2*gamma*...
        A_h^2*p_m_benchmark^(2/gamma) ) )^(gamma/(1-gamma));
    array(i,1) = p_0c_benchmark;
end

ratio_of_coolant_to_main_tp = p_0c_benchmark/p_0m;

resulting_coolant_mass_flow_rate = (p_0c_benchmark/sqrt(T_0c))*A_h*...
    sqrt(gamma/R)*(p_m_benchmark/p_0c_benchmark)^(1/gamma)*...
    sqrt( (2/(gamma-1))*( 1 - (p_m_benchmark/p_0c_benchmark)^...
        ((gamma-1)/gamma) ) );
resulting_coolant_ratio = resulting_coolant_mass_flow_rate/m_m_benchmark;

%find the correct plenum total pressure
p_0cp = ( p_0c_benchmark - zeta_c*p_m_benchmark )/( 1 - zeta_c );
ratio_of_plenum_to_main_tp = p_0cp/p_0m;
p_0cp_gauge = p_0cp - fluent_operating_pressure;

%plot the CFD data

%mass_flow_rates columns:
%1) hole position (not normalised)
%2) inlet MFR
%3) outlet MFR
%4) plenum MFR
%5) local surface static pressure (gauge in Fluent)

%outlet_total_pressures_averages columns:
%1) hole position (not normalised)
%2) area-averaged outlet total pressure (gauge in Fluent)

%normalise the hole positions
hole_positions = (50/27)*(mass_flow_rates(:,1) - 26);

%work out the theoretical hole exit total pressures and thus capacities
m_c = mass_flow_rates(:,4);
p_m = mass_flow_rates(:,5) + fluent_operating_pressure;
p_0c = zeta_c.*p_m(:) + (1-zeta_c)*p_0cp;
G_c = ( sqrt(T_0c)/p_0cp ).*m_c;

%work out the capacities
m_in = mass_flow_rates(:,2);

```

```

G_in = ( sqrt(T_0m)/p_0m ).*m_in;
G_out = ( sqrt(T_0m)/p_0m ).*( m_in + m_c );
G_baseline = ( sqrt(T_0m)/p_0m )*baseline;

%define a surface pressure coefficient
C_p = (p_m-min(p_m))/(max(p_m)-min(p_m));
%C_p = p_m;
%C_p = p_0cp./p_m;

%define the critical pressure ratio
r_crit = ((gamma+1)/2)^(gamma/(1-gamma));

%define a coolant isentropic capacity
G_c_isent = (sqrt(T_0c)/p_0cp).*(p_0c/sqrt(T_0c))*A_h.*sqrt(gamma/R).*...
(p_m./p_0c).^((1/gamma).*sqrt( (2/(gamma-1)).*( 1 - (p_m./p_0c).^...
((gamma-1)/gamma) ) ) );

%define a surface isentropic Mach number
M_surf = sqrt( (2/(gamma-1))*( (p_0m./p_m).^((gamma-1)/gamma) - 1 ) );
p_2 = 2625200; %outlet static pressure

%define a loss for each hole position
total_pressures = outlet_total_pressure_averages(:,2);
total_pressures_absolute = total_pressures + fluent_operating_pressure;
loss = (p_0m - total_pressures_absolute)/(p_0m - p_2);

% Default figure settings
figure_width = 4;      % Width in inches
figure_height = 4;      % Height in inches
axes_line_width = 0.75;  % AxesLineWidth
font_size = 14;         % Fontsize
line_width = 1.5;        % LineWidth
marker_size = 8;         % MarkerSize

geometric_throat_location = 38;
geometric_throat_normalised = (50/27)*(geometric_throat_location - 26);

figure(1)
plot(hole_positions,100*(G_in/G_baseline - 1), 'r-o')
hold on
plot(hole_positions,100*(G_out/G_baseline - 1), 'b-o')
xlabel('Distance along suction side, % of range')
ylabel('\Delta capacity, % of baseline')
throat_line = xline(geometric_throat_normalised,'-k',{'Geometric throat'},...
'FontName','Charter','FontSize',font_size);
throat_line.LabelVerticalAlignment = 'top';
throat_line.LabelHorizontalAlignment = 'left';
baseline_line = yline(100*(G_baseline/G_baseline - 1),'-k',{'Baseline'},...
'FontName','Charter','FontSize',font_size);
baseline_line.LabelVerticalAlignment = 'bottom';

```

```

baseline_line.LabelHorizontalAlignment = 'right';
legend('\Gamma_{in}', '\Gamma_{out}', 'Location', 'southeast')
%set up the axes
pos = get(gcf, 'Position');
set(gcf, 'Position', [pos(1) pos(2) figure_width*100, figure_height*100]);
set(gca, 'FontSize', font_size, 'LineWidth', axes_line_width);
set(gca, 'FontName', 'Charter', 'FontSize', font_size)
%preserve the size of the image when it's saved
set(gcf, 'InvertHardcopy', 'on');
set(gcf, 'PaperUnits', 'inches');
papersize = get(gcf, 'PaperSize');
left = (pagesize(1)- figure_width)/2;
bottom = (pagesize(2)- figure_height)/2;
myfiguresize = [left, bottom, figure_width, figure_height];
set(gcf, 'PaperPosition', myfiguresize);
print('..../figs/sch_hole_location_vs_capacity', '-dpng', '-r300');

figure(2)
plot(hole_positions, 100*(G_c/G_c(1,1) - 1), 'k-o')
xlabel('Distance along suction side, % of range')
ylabel('\Delta coolant capacity, %')
throat_line = xline(geometric_throat_normalised, '-k', {'Geometric throat'}, ...
    'FontName', 'Charter', 'FontSize', font_size);
throat_line.LabelVerticalAlignment = 'bottom';
%set up the axes
pos = get(gcf, 'Position');
set(gcf, 'Position', [pos(1) pos(2) figure_width*100, figure_height*100]);
set(gca, 'FontSize', font_size, 'LineWidth', axes_line_width);
set(gca, 'FontName', 'Charter', 'FontSize', font_size)
%preserve the size of the image when it's saved
set(gcf, 'InvertHardcopy', 'on');
set(gcf, 'PaperUnits', 'inches');
pagesize = get(gcf, 'PaperSize');
left = (pagesize(1)- figure_width)/2;
bottom = (pagesize(2)- figure_height)/2;
myfiguresize = [left, bottom, figure_width, figure_height];
set(gcf, 'PaperPosition', myfiguresize);
print('..../figs/sch_hole_location_vs_coolant_capacity', '-dpng', '-r300');

figure(3)
plot( M_surf, 100*(G_in/G_baseline - 1), 'r-o')
hold on
plot( M_surf, 100*(G_out/G_baseline - 1), 'b-o')
xlabel('Surface isentropic Mach number')
ylabel('\Delta capacity, % of baseline')
baseline_line = yline(100*(G_baseline/G_baseline - 1), '-k', {'Baseline'}, ...
    'FontName', 'Charter', 'FontSize', font_size);
baseline_line.LabelVerticalAlignment = 'top';
baseline_line.LabelHorizontalAlignment = 'left';
legend('\Gamma_{in}', '\Gamma_{out}', 'Location', 'northwest')
%set up the axes

```

```

pos = get(gcf, 'Position');
set(gcf, 'Position', [pos(1) pos(2) figure_width*100, figure_height*100]);
set(gca, 'FontSize', font_size, 'LineWidth', axes_line_width);
set(gca, 'FontName', 'Charter', 'FontSize', font_size)
%preserve the size of the image when it's saved
set(gcf, 'InvertHardcopy', 'on');
set(gcf, 'PaperUnits', 'inches');
papersize = get(gcf, 'PaperSize');
left = (pagesize(1)- figure_width)/2;
bottom = (pagesize(2)- figure_height)/2;
myfiguresize = [left, bottom, figure_width, figure_height];
set(gcf, 'PaperPosition', myfiguresize);
print('../..../figs/sch_surface_isentropic_mach_number_vs_capacity', '-dpng',...
    '-r300');

figure(4)
plot( 100*(G_c_isent/G_c_isent(1,1) - 1), 100*(G_c/G_c(1,1) - 1), 'k-o')
xlabel('\Delta coolant isentropic capacity, %')
ylabel('\Delta coolant capacity, %')
%set up the axes
pos = get(gcf, 'Position');
set(gcf, 'Position', [pos(1) pos(2) figure_width*100, figure_height*100]);
set(gca, 'FontSize', font_size, 'LineWidth', axes_line_width);
set(gca, 'FontName', 'Charter', 'FontSize', font_size)
%preserve the size of the image when it's saved
set(gcf, 'InvertHardcopy', 'on');
set(gcf, 'PaperUnits', 'inches');
papersize = get(gcf, 'PaperSize');
left = (pagesize(1)- figure_width)/2;
bottom = (pagesize(2)- figure_height)/2;
myfiguresize = [left, bottom, figure_width, figure_height];
set(gcf, 'PaperPosition', myfiguresize);
print('../..../figs/sch_coolant_isentropic_capacity_vs_coolant_capacity',...
    '-dpng', '-r300');

figure(5)
plot(hole_positions,100*loss, 'k-o')
xlabel('Distance along suction side, % of range')
ylabel('Overall loss at domain outlet, %')
throat_line = xline(geometric_throat_normalised,'-k',{'Geometric throat'},...
    'FontName', 'Charter', 'FontSize', font_size);
throat_line.LabelVerticalAlignment = 'bottom';
%set up the axes
pos = get(gcf, 'Position');
set(gcf, 'Position', [pos(1) pos(2) figure_width*100, figure_height*100]);
set(gca, 'FontSize', font_size, 'LineWidth', axes_line_width);
set(gca, 'FontName', 'Charter', 'FontSize', font_size)
%preserve the size of the image when it's saved
set(gcf, 'InvertHardcopy', 'on');
set(gcf, 'PaperUnits', 'inches');
papersize = get(gcf, 'PaperSize');

```

```
left = (papersize(1)- figure_width)/2;
bottom = (papersize(2)- figure_height)/2;
myfiguresize = [left, bottom, figure_width, figure_height];
set(gcf, 'PaperPosition', myfiguresize);
print('.../.../figs/sch_hole_location_vs_loss', '-dpng', '-r300');
```

Appendix B

NGV mid-span profile coordinates

The coordinates given here correspond to the 2-dimensional mid-span profile generated by the NGV coordinate processing scheme described in Section 3.1.

B.1 Trent 900

B.1.1 Vane PNS04 (M EP1 standard)

Point	x	y			
1	-0.0384113	0.05177516	26	-0.0282007	0.06347288
2	-0.0384573	0.05197567	27	-0.0274718	0.06300822
3	-0.0384945	0.05217805	28	-0.0267865	0.06247375
4	-0.0385228	0.05238188	29	-0.0261505	0.06189097
5	-0.0385421	0.05258678	30	-0.0255661	0.06127622
6	-0.0384894	0.05366169	31	-0.025027	0.06063382
7	-0.0383709	0.05451211	32	-0.0245259	0.05996645
8	-0.0382084	0.05535448	33	-0.0240553	0.0592768
9	-0.0380128	0.0561902	34	-0.0236078	0.05856756
10	-0.0377951	0.05701373	35	-0.0231789	0.05784148
11	-0.0375587	0.05782143	36	-0.022767	0.05710149
12	-0.0372928	0.05861392	37	-0.022371	0.05635047
13	-0.0369846	0.05939235	38	-0.0219896	0.05559132
14	-0.0366212	0.06015783	39	-0.0216217	0.05482676
15	-0.0361902	0.06091103	40	-0.0212668	0.05405759
16	-0.0356872	0.06164067	41	-0.0209252	0.05328333
17	-0.0351116	0.06232271	42	-0.0205972	0.05250346
18	-0.0344808	0.06293249	43	-0.020283	0.05171751
19	-0.0337854	0.06344539	44	-0.0199827	0.05092511
20	-0.0330341	0.06383818	45	-0.0196957	0.05012667
21	-0.0322392	0.06410176	46	-0.019421	0.04932284
22	-0.0314181	0.06423504	47	-0.0191579	0.04851426
23	-0.0305879	0.064237	48	-0.0189055	0.04770159
24	-0.0297658	0.06410666	49	-0.0186627	0.04688544
25	-0.0289674	0.0638462	50	-0.0184284	0.04606628
			51	-0.0182015	0.04524461
			52	-0.0179806	0.04442087

53	-0.0177646	0.04359556		104	-0.0086374	0.00071367
54	-0.0175527	0.04276894		105	-0.0085425	-0.0001705
55	-0.0173446	0.04194109		106	-0.008544	-0.0002054
56	-0.0171401	0.041112		107	-0.0085485	-0.0002401
57	-0.0169388	0.04028174		108	-0.0085561	-0.0002742
58	-0.0167406	0.03945032		109	-0.0085666	-0.0003076
59	-0.0165452	0.03861786		110	-0.00858	-0.0003399
60	-0.0163521	0.03778446		111	-0.0085961	-0.000371
61	-0.0161611	0.0369503		112	-0.0086148	-0.0004005
62	-0.0159716	0.03611551		113	-0.0086361	-0.0004282
63	-0.0157834	0.03528021		114	-0.0086597	-0.0004541
64	-0.0155962	0.03444446		115	-0.0086855	-0.0004777
65	-0.0154098	0.03360827		116	-0.0087132	-0.000499
66	-0.0152241	0.03277169		117	-0.0087426	-0.0005179
67	-0.0150387	0.03193471		118	-0.0087736	-0.0005341
68	-0.0148536	0.03109736		119	-0.0088059	-0.0005475
69	-0.0146689	0.03025966		120	-0.0088392	-0.0005581
70	-0.0144845	0.02942161		121	-0.0088734	-0.0005658
71	-0.0143005	0.02858323		122	-0.008908	-0.0005704
72	-0.0141171	0.02774449		123	-0.008943	-0.000572
73	-0.0139343	0.02690541		124	-0.0089779	-0.0005706
74	-0.0137523	0.02606589		125	-0.0090126	-0.0005661
75	-0.0135712	0.02522589		126	-0.0090467	-0.0005586
76	-0.0133911	0.02438534		127	-0.0090801	-0.0005482
77	-0.0132122	0.02354418		128	-0.0091125	-0.0005349
78	-0.0130345	0.02270242		129	-0.0091435	-0.0005188
79	-0.0128579	0.02186016		130	-0.0091731	-0.0005001
80	-0.0126824	0.02101746		131	-0.0092009	-0.0004789
81	-0.0125079	0.02017443		132	-0.0092268	-0.0004554
82	-0.0123344	0.01933113		133	-0.0092505	-0.0004297
83	-0.0121613	0.01848764		134	-0.0092719	-0.000402
84	-0.011988	0.01764394		135	-0.0092908	-0.0003726
85	-0.0118139	0.01680008		136	-0.0095434	0.00018639
86	-0.0116385	0.01595608		137	-0.0097897	0.00072377
87	-0.0114611	0.01511202		138	-0.0100425	0.00126644
88	-0.0112818	0.01426809		139	-0.0102985	0.00181031
89	-0.0111004	0.01342454		140	-0.0105545	0.00235181
90	-0.010917	0.01258164		141	-0.0108093	0.00289071
91	-0.0107315	0.01173962		142	-0.0110627	0.0034282
92	-0.0105446	0.01089838		143	-0.0113142	0.00396546
93	-0.0103575	0.01005727		144	-0.0115634	0.0045036
94	-0.0101718	0.00921553		145	-0.0118102	0.00504298
95	-0.0099891	0.00837243		146	-0.0120547	0.00558351
96	-0.0098108	0.00752727		147	-0.0122969	0.00612505
97	-0.0096382	0.00667992		148	-0.0125368	0.0066675
98	-0.0094722	0.00583082		149	-0.0127745	0.00721073
99	-0.0093137	0.00498042		150	-0.0130099	0.00775462
100	-0.0091636	0.00412916		151	-0.0132432	0.00829906
101	-0.0090223	0.00327748		152	-0.0134744	0.00884392
102	-0.008886	0.00242549		153	-0.0137036	0.00938911
103	-0.0087494	0.00157303		154	-0.0139311	0.00993455

155	-0.0141572	0.01048017		198	-0.0252454	0.03324888
156	-0.0143824	0.0110259		199	-0.0255571	0.03375392
157	-0.0146068	0.01157166		200	-0.025871	0.03425779
158	-0.014831	0.01211738		201	-0.0261871	0.03476056
159	-0.0150551	0.01266298		202	-0.0265051	0.03526225
160	-0.0152794	0.0132084		203	-0.0268253	0.0357628
161	-0.0155044	0.01375357		204	-0.0271478	0.03626188
162	-0.0157301	0.01429843		205	-0.0274731	0.03675915
163	-0.0159564	0.01484295		206	-0.0278015	0.03725429
164	-0.0161834	0.01538707		207	-0.0281333	0.03774697
165	-0.0164111	0.01593073		208	-0.0284689	0.0382369
166	-0.0166396	0.01647394		209	-0.0288084	0.03872385
167	-0.0168688	0.01701659		210	-0.0291522	0.0392075
168	-0.0170988	0.01755868		211	-0.0295003	0.03968767
169	-0.0173297	0.01810013		212	-0.0298523	0.04016448
170	-0.0175619	0.01864068		213	-0.0302078	0.04063809
171	-0.0177965	0.01917996		214	-0.0305659	0.04110869
172	-0.0180343	0.01971759		215	-0.0309266	0.04157647
173	-0.0182762	0.02025321		216	-0.0312889	0.0420416
174	-0.0185225	0.02078674		217	-0.0316526	0.04250427
175	-0.0187728	0.02131841		218	-0.0320169	0.04296468
176	-0.0190267	0.02184848		219	-0.0323815	0.04342299
177	-0.019284	0.02237718		220	-0.032746	0.04387949
178	-0.0195442	0.02290471		221	-0.0331108	0.04433453
179	-0.0198074	0.02343112		222	-0.0334755	0.04478842
180	-0.0200732	0.02395647		223	-0.0338404	0.04524151
181	-0.0203415	0.02448083		224	-0.0342056	0.04569412
182	-0.0206122	0.02500425		225	-0.0345712	0.04614659
183	-0.0208851	0.02552679		226	-0.0349374	0.04659925
184	-0.02116	0.02604851		227	-0.0353042	0.04705245
185	-0.0214368	0.0265695		228	-0.0356713	0.04750649
186	-0.0217153	0.02708976		229	-0.036037	0.04796176
187	-0.0219957	0.02760923		230	-0.0363997	0.04841856
188	-0.0222781	0.02812782		231	-0.0367574	0.04887726
189	-0.0225627	0.02864547		232	-0.0371075	0.04933986
190	-0.0228497	0.02916207		233	-0.0374442	0.04981245
191	-0.0231392	0.02967753		234	-0.0377613	0.05030169
192	-0.0234314	0.03019177		235	-0.0381413	0.05099947
193	-0.0237265	0.03070471		236	-0.0382215	0.05118867
194	-0.0240246	0.03121623		237	-0.0382933	0.05138127
195	-0.0243257	0.03172637		238	-0.0383566	0.0515769
196	-0.0246296	0.03223516		239	-0.0384113	0.05177516
197	-0.0249363	0.03274265				

B.1.2 Vane PNN06 (M EP1 standard)

Point	x	y
1	-0.0383765	0.05178918
2	-0.0384276	0.05198641
3	-0.0384696	0.05218582

4	-0.0385024	0.05238699
5	-0.0385259	0.05258947
6	-0.0384822	0.05365377
7	-0.0383693	0.05449352

8	-0.0382112	0.05533087		59	-0.0165039	0.03858055
9	-0.0380177	0.05616577		60	-0.0163091	0.03774922
10	-0.0377983	0.05699796		61	-0.0161159	0.03691725
11	-0.0375565	0.05782546		62	-0.0159242	0.03608473
12	-0.0372834	0.05864269		63	-0.0157336	0.0352518
13	-0.0369689	0.05944367		64	-0.0155442	0.0344184
14	-0.0366028	0.0602224		65	-0.015356	0.03358449
15	-0.0361751	0.06097273		66	-0.0151691	0.03275
16	-0.0356805	0.06168356		67	-0.0149833	0.03191486
17	-0.0351187	0.06233864		68	-0.0147989	0.03107905
18	-0.0344895	0.06292143		69	-0.0146157	0.03024258
19	-0.0337924	0.06341542		70	-0.0144338	0.02940547
20	-0.0330277	0.06380462		71	-0.0142532	0.02856778
21	-0.0322104	0.06407835		72	-0.0140737	0.02772951
22	-0.0313639	0.06422892		73	-0.0138955	0.02689072
23	-0.0305112	0.06424933		74	-0.0137184	0.02605137
24	-0.0296747	0.06413369		75	-0.0135423	0.02521148
25	-0.0288737	0.06388044		76	-0.013367	0.024371
26	-0.0281138	0.0635075		77	-0.0131926	0.02352996
27	-0.0273965	0.06303841		78	-0.013019	0.02268834
28	-0.026723	0.06249679		79	-0.0128463	0.0218462
29	-0.0260946	0.06190615		80	-0.0126747	0.02100355
30	-0.0255108	0.06128426		81	-0.0125042	0.0201604
31	-0.0249671	0.06063564		82	-0.0123349	0.0193168
32	-0.0244585	0.0599629		83	-0.012166	0.01847287
33	-0.0239802	0.05926869		84	-0.0119966	0.01762875
34	-0.0235271	0.05855567		85	-0.0118257	0.01678461
35	-0.0230957	0.05782644		86	-0.0116524	0.01594058
36	-0.022684	0.05708358		87	-0.0114759	0.01509681
37	-0.0222902	0.05632968		88	-0.0112966	0.01425329
38	-0.0219124	0.05556728		89	-0.0111154	0.01341004
39	-0.0215488	0.05479882		90	-0.0109328	0.01256705
40	-0.0211987	0.05402522		91	-0.0107495	0.01172433
41	-0.0208623	0.05324636		92	-0.0105663	0.01088175
42	-0.0205394	0.05246211		93	-0.0103839	0.01003898
43	-0.0202302	0.05167238		94	-0.0102032	0.00919565
44	-0.0199345	0.05087708		95	-0.0100249	0.00835142
45	-0.0196516	0.05007664		96	-0.0098498	0.00750594
46	-0.0193803	0.0492716		97	-0.0096787	0.00665904
47	-0.0191196	0.04846253		98	-0.0095124	0.00581075
48	-0.0188683	0.04764995		99	-0.0093515	0.00496112
49	-0.0186255	0.04683436		100	-0.0091967	0.00411016
50	-0.0183905	0.04601615		101	-0.0090493	0.00325814
51	-0.0181623	0.04519566		102	-0.0089131	0.00240712
52	-0.0179404	0.04437326		103	-0.0087935	0.00155976
53	-0.0177239	0.04354925		104	-0.0086795	0.00070455
54	-0.0175121	0.04272392		105	-0.0085469	-0.0002052
55	-0.0173044	0.04189735		106	-0.0085483	-0.0002377
56	-0.0171003	0.04106963		107	-0.0085526	-0.00027
57	-0.0168992	0.04024087		108	-0.0085596	-0.0003018
58	-0.0167005	0.03941114		109	-0.0085695	-0.0003328

110	-0.008582	-0.0003629		161	-0.0153647	0.01372841
111	-0.0085971	-0.0003918		162	-0.015595	0.01426779
112	-0.0086146	-0.0004192		163	-0.0158271	0.01480614
113	-0.0086345	-0.000445		164	-0.0160608	0.01534361
114	-0.0086566	-0.000469		165	-0.0162959	0.01588034
115	-0.0086807	-0.0004909		166	-0.0165322	0.01641651
116	-0.0087066	-0.0005106		167	-0.0167696	0.01695225
117	-0.0087341	-0.000528		168	-0.0170077	0.01748773
118	-0.008763	-0.0005429		169	-0.0172464	0.01802308
119	-0.0087932	-0.0005553		170	-0.0174858	0.0185583
120	-0.0088243	-0.0005649		171	-0.0177262	0.0190933
121	-0.0088561	-0.0005718		172	-0.0179676	0.01962797
122	-0.0088884	-0.0005758		173	-0.0182105	0.02016222
123	-0.008921	-0.0005771		174	-0.0184549	0.02069596
124	-0.0089535	-0.0005754		175	-0.0187011	0.02122908
125	-0.0089858	-0.000571		176	-0.0189494	0.02176148
126	-0.0090175	-0.0005637		177	-0.0192	0.02229308
127	-0.0090485	-0.0005537		178	-0.019453	0.0228238
128	-0.0090785	-0.000541		179	-0.0197085	0.02335368
129	-0.0091072	-0.0005257		180	-0.0199666	0.0238827
130	-0.0091345	-0.000508		181	-0.0202274	0.02441089
131	-0.0091602	-0.0004879		182	-0.0204911	0.02493825
132	-0.009184	-0.0004657		183	-0.0207576	0.02546473
133	-0.0092058	-0.0004415		184	-0.0210271	0.02599034
134	-0.0092254	-0.0004154		185	-0.0212998	0.02651505
135	-0.0092426	-0.0003878		186	-0.0215758	0.02703879
136	-0.0094986	0.00020787		187	-0.021855	0.02756151
137	-0.0097368	0.00075662		188	-0.0221375	0.02808309
138	-0.0099743	0.00129424		189	-0.0224231	0.02860342
139	-0.0102135	0.0018275		190	-0.0227119	0.02912241
140	-0.0104566	0.00236242		191	-0.0230039	0.02963997
141	-0.010703	0.00289988		192	-0.0232989	0.03015597
142	-0.0109516	0.00343871		193	-0.0235971	0.03067034
143	-0.0112009	0.00397773		194	-0.0238983	0.03118298
144	-0.0114498	0.00451584		195	-0.0242024	0.03169397
145	-0.0116972	0.00505305		196	-0.0245091	0.03220354
146	-0.0119424	0.00559011		197	-0.0248183	0.03271192
147	-0.0121847	0.00612776		198	-0.0251295	0.03321933
148	-0.0124234	0.00666673		199	-0.0254428	0.03372595
149	-0.0126585	0.00720727		200	-0.0257577	0.03423205
150	-0.0128903	0.00774916		201	-0.026074	0.0347378
151	-0.0131193	0.00829214		202	-0.0263917	0.03524344
152	-0.013346	0.00883597		203	-0.0267105	0.03574887
153	-0.0135709	0.0093804		204	-0.0270312	0.03625356
154	-0.0137945	0.00992519		205	-0.0273542	0.0367569
155	-0.0140173	0.01047009		206	-0.0276801	0.0372583
156	-0.0142397	0.01101487		207	-0.0280093	0.03775721
157	-0.0144623	0.01155927		208	-0.0283425	0.03825303
158	-0.0146856	0.01210307		209	-0.02868	0.03874521
159	-0.0149102	0.012646		210	-0.0290224	0.03923316
160	-0.0151364	0.01318785		211	-0.0293701	0.03971648

212	-0.0297224	0.04019539		226	-0.0348483	0.04663843
213	-0.0300789	0.04067026		227	-0.0352166	0.04709249
214	-0.0304387	0.04114147		228	-0.0355843	0.04754725
215	-0.0308016	0.0416094		229	-0.0359504	0.04800314
216	-0.0311667	0.04207441		230	-0.0363133	0.04846057
217	-0.0315334	0.04253687		231	-0.0366715	0.04892
218	-0.0319012	0.04299717		232	-0.0370229	0.04938325
219	-0.0322695	0.04345566		233	-0.0373627	0.04985559
220	-0.0326379	0.04391268		234	-0.0376863	0.05034282
221	-0.0330064	0.04436848		235	-0.0380836	0.05103051
222	-0.033375	0.04482331		236	-0.0381698	0.05121482
223	-0.0337434	0.04527746		237	-0.0382475	0.05140297
224	-0.0341118	0.04573118		238	-0.0383164	0.05159456
225	-0.03448	0.04618476		239	-0.0383765	0.05178918

B.1.3 Vane PNS03 (M EP1 standard)

Point	x	y		32	-0.0245259	0.05996645
1	-0.0384113	0.05177516		33	-0.0240553	0.0592768
2	-0.0384573	0.05197567		34	-0.0236078	0.05856756
3	-0.0384945	0.05217805		35	-0.0231789	0.05784148
4	-0.0385228	0.05238188		36	-0.022767	0.05710149
5	-0.0385421	0.05258678		37	-0.022371	0.05635047
6	-0.0384894	0.05366169		38	-0.0219896	0.05559132
7	-0.0383709	0.05451211		39	-0.0216217	0.05482676
8	-0.0382084	0.05535448		40	-0.0212668	0.05405759
9	-0.0380128	0.0561902		41	-0.0209252	0.05328333
10	-0.0377951	0.05701373		42	-0.0205972	0.05250346
11	-0.0375587	0.05782143		43	-0.020283	0.05171751
12	-0.0372928	0.05861392		44	-0.0199827	0.05092511
13	-0.0369846	0.05939235		45	-0.0196957	0.05012667
14	-0.0366212	0.06015783		46	-0.019421	0.04932284
15	-0.0361902	0.06091103		47	-0.0191579	0.04851426
16	-0.0356872	0.06164067		48	-0.0189055	0.04770159
17	-0.035116	0.06232271		49	-0.0186627	0.04688544
18	-0.0344808	0.06293249		50	-0.0184284	0.04606628
19	-0.0337854	0.06344539		51	-0.0182015	0.04524461
20	-0.0330341	0.06383818		52	-0.0179806	0.04442087
21	-0.0322392	0.06410176		53	-0.0177646	0.04359556
22	-0.0314181	0.06423504		54	-0.0175527	0.04276894
23	-0.0305879	0.064237		55	-0.0173446	0.04194109
24	-0.0297658	0.06410666		56	-0.0171401	0.041112
25	-0.0289674	0.0638462		57	-0.0169388	0.04028174
26	-0.0282007	0.06347288		58	-0.0167406	0.03945032
27	-0.0274718	0.06300822		59	-0.0165452	0.03861786
28	-0.0267865	0.06247375		60	-0.0163521	0.03778446
29	-0.0261505	0.06189097		61	-0.0161611	0.0369503
30	-0.0255661	0.06127622		62	-0.0159716	0.03611551
31	-0.025027	0.06063382		63	-0.0157834	0.03528021
				64	-0.0155962	0.03444446

65	-0.0154098	0.03360827		116	-0.0087132	-0.000499
66	-0.0152241	0.03277169		117	-0.0087426	-0.0005179
67	-0.0150387	0.03193471		118	-0.0087736	-0.0005341
68	-0.0148536	0.03109736		119	-0.0088059	-0.0005475
69	-0.0146689	0.03025966		120	-0.0088392	-0.0005581
70	-0.0144845	0.02942161		121	-0.0088734	-0.0005658
71	-0.0143005	0.02858323		122	-0.008908	-0.0005704
72	-0.0141171	0.02774449		123	-0.008943	-0.000572
73	-0.0139343	0.02690541		124	-0.0089779	-0.0005706
74	-0.0137523	0.02606589		125	-0.0090126	-0.0005661
75	-0.0135712	0.02522589		126	-0.0090467	-0.0005586
76	-0.0133911	0.02438534		127	-0.0090801	-0.0005482
77	-0.0132122	0.02354418		128	-0.0091125	-0.0005349
78	-0.0130345	0.02270242		129	-0.0091435	-0.0005188
79	-0.0128579	0.02186016		130	-0.0091731	-0.0005001
80	-0.0126824	0.02101746		131	-0.0092009	-0.0004789
81	-0.0125079	0.02017443		132	-0.0092268	-0.0004554
82	-0.0123344	0.01933113		133	-0.0092505	-0.0004297
83	-0.0121613	0.01848764		134	-0.0092719	-0.000402
84	-0.011988	0.01764394		135	-0.0092908	-0.0003726
85	-0.0118139	0.01680008		136	-0.0095434	0.00018639
86	-0.0116385	0.01595608		137	-0.0097897	0.00072377
87	-0.0114611	0.01511202		138	-0.0100425	0.00126644
88	-0.0112818	0.01426809		139	-0.0102985	0.00181031
89	-0.0111004	0.01342454		140	-0.0105545	0.00235181
90	-0.010917	0.01258164		141	-0.0108093	0.00289071
91	-0.0107315	0.01173962		142	-0.0110627	0.0034282
92	-0.0105446	0.01089838		143	-0.0113142	0.00396546
93	-0.0103575	0.01005727		144	-0.0115634	0.0045036
94	-0.0101718	0.00921553		145	-0.0118102	0.00504298
95	-0.0099891	0.00837243		146	-0.0120547	0.00558351
96	-0.0098108	0.00752727		147	-0.0122969	0.00612505
97	-0.0096382	0.00667992		148	-0.0125368	0.0066675
98	-0.0094722	0.00583082		149	-0.0127745	0.00721073
99	-0.0093137	0.00498042		150	-0.0130099	0.00775462
100	-0.0091636	0.00412916		151	-0.0132432	0.00829906
101	-0.0090223	0.00327748		152	-0.0134744	0.00884392
102	-0.008886	0.00242549		153	-0.0137036	0.00938911
103	-0.0087494	0.00157303		154	-0.0139311	0.00993455
104	-0.0086374	0.00071367		155	-0.0141572	0.01048017
105	-0.0085425	-0.0001705		156	-0.0143824	0.0110259
106	-0.008544	-0.0002054		157	-0.0146068	0.01157166
107	-0.0085485	-0.0002401		158	-0.014831	0.01211738
108	-0.0085561	-0.0002742		159	-0.0150551	0.01266298
109	-0.0085666	-0.0003076		160	-0.0152794	0.0132084
110	-0.00858	-0.0003399		161	-0.0155044	0.01375357
111	-0.0085961	-0.000371		162	-0.0157301	0.01429843
112	-0.0086148	-0.0004005		163	-0.0159564	0.01484295
113	-0.0086361	-0.0004282		164	-0.0161834	0.01538707
114	-0.0086597	-0.0004541		165	-0.0164111	0.01593073
115	-0.0086855	-0.0004777		166	-0.0166396	0.01647394

167	-0.0168688	0.01701659		204	-0.0271478	0.03626188
168	-0.0170988	0.01755868		205	-0.0274731	0.03675915
169	-0.0173297	0.01810013		206	-0.0278015	0.03725429
170	-0.0175619	0.01864068		207	-0.0281333	0.03774697
171	-0.0177965	0.01917996		208	-0.0284689	0.0382369
172	-0.0180343	0.01971759		209	-0.0288084	0.03872385
173	-0.0182762	0.02025321		210	-0.0291522	0.0392075
174	-0.0185225	0.02078674		211	-0.0295003	0.03968767
175	-0.0187728	0.02131841		212	-0.0298523	0.04016448
176	-0.0190267	0.02184848		213	-0.0302078	0.04063809
177	-0.019284	0.02237718		214	-0.0305659	0.04110869
178	-0.0195442	0.02290471		215	-0.0309266	0.04157647
179	-0.0198074	0.02343112		216	-0.0312889	0.0420416
180	-0.0200732	0.02395647		217	-0.0316526	0.04250427
181	-0.0203415	0.02448083		218	-0.0320169	0.04296468
182	-0.0206122	0.02500425		219	-0.0323815	0.04342299
183	-0.0208851	0.02552679		220	-0.032746	0.04387949
184	-0.02116	0.02604851		221	-0.0331108	0.04433453
185	-0.0214368	0.0265695		222	-0.0334755	0.04478842
186	-0.0217153	0.02708976		223	-0.0338404	0.04524151
187	-0.0219957	0.02760923		224	-0.0342056	0.04569412
188	-0.0222781	0.02812782		225	-0.0345712	0.04614659
189	-0.0225627	0.02864547		226	-0.0349374	0.04659925
190	-0.0228497	0.02916207		227	-0.0353042	0.04705245
191	-0.0231392	0.02967753		228	-0.0356713	0.04750649
192	-0.0234314	0.03019177		229	-0.036037	0.04796176
193	-0.0237265	0.03070471		230	-0.0363997	0.04841856
194	-0.0240246	0.03121623		231	-0.0367574	0.04887726
195	-0.0243257	0.03172637		232	-0.0371075	0.04933986
196	-0.0246296	0.03223516		233	-0.0374442	0.04981245
197	-0.0249363	0.03274265		234	-0.0377613	0.05030169
198	-0.0252454	0.03324888		235	-0.0381413	0.05099947
199	-0.0255571	0.03375392		236	-0.0382215	0.05118867
200	-0.025871	0.03425779		237	-0.0382933	0.05138127
201	-0.0261871	0.03476056		238	-0.0383566	0.0515769
202	-0.0265051	0.03526225		239	-0.0384113	0.05177516
203	-0.0268253	0.0357628				

B.1.4 Vane KTA01 (M-skew standard)

Point	x	y
1	-0.0382162	0.05182894
2	-0.038268	0.05207091
3	-0.0383079	0.05231519
4	-0.038336	0.05256112
5	-0.0383308	0.0536641
6	-0.0382208	0.05449107
7	-0.0380384	0.05531149
8	-0.0378243	0.05612872
9	-0.0375915	0.05694268

10	-0.0373448	0.05775217
11	-0.0370739	0.05855386
12	-0.0367665	0.05934416
13	-0.0364104	0.0601195
14	-0.0359936	0.06087592
15	-0.03551	0.06160072
16	-0.0349597	0.06227173
17	-0.0343431	0.06286637
18	-0.0336599	0.06336205
19	-0.0329113	0.06373753

20	-0.0321111	0.0639846		71	-0.0140157	0.02774849
21	-0.031281	0.06410243		72	-0.0138343	0.02691327
22	-0.0304424	0.06409062		73	-0.0136543	0.02607749
23	-0.0296159	0.06394962		74	-0.0134755	0.02524114
24	-0.0288197	0.06368345		75	-0.013298	0.02440422
25	-0.0280608	0.06330843		76	-0.0131216	0.02356672
26	-0.0273432	0.06284441		77	-0.0129464	0.02272868
27	-0.0266705	0.06231123		78	-0.0127721	0.0218902
28	-0.0260465	0.06172872		79	-0.0125985	0.02105135
29	-0.0254716	0.06111229		80	-0.0124254	0.02021221
30	-0.0249392	0.06046734		81	-0.0122526	0.01937285
31	-0.0244419	0.05979782		82	-0.0120797	0.01853334
32	-0.023972	0.0591077		83	-0.0119065	0.01769375
33	-0.0235221	0.05840094		84	-0.0117325	0.01685411
34	-0.0230882	0.05768037		85	-0.0115572	0.0160145
35	-0.0226704	0.05694763		86	-0.0113806	0.01517496
36	-0.0222694	0.0562042		87	-0.0112031	0.01433539
37	-0.0218855	0.05545162		88	-0.0110256	0.01349573
38	-0.0215191	0.05469134		89	-0.0108487	0.01265587
39	-0.0211696	0.05392416		90	-0.0106731	0.01181575
40	-0.0208358	0.05315047		91	-0.0104995	0.01097525
41	-0.0205163	0.05237058		92	-0.0103284	0.01013427
42	-0.02021	0.05158488		93	-0.0101601	0.00929268
43	-0.0199157	0.05079376		94	-0.0099951	0.00845037
44	-0.0196325	0.04999767		95	-0.0098338	0.00760721
45	-0.0193599	0.04919713		96	-0.0096766	0.00676311
46	-0.0190973	0.04839265		97	-0.0095235	0.005918
47	-0.0188441	0.04758475		98	-0.0093748	0.00507179
48	-0.0185997	0.04677386		99	-0.0092305	0.0042244
49	-0.0183631	0.04596027		100	-0.0090906	0.00337569
50	-0.0181338	0.04514429		101	-0.0089533	0.00252483
51	-0.0179107	0.04432615		102	-0.0088157	0.00167063
52	-0.0176932	0.04350614		103	-0.0086749	0.00081178
53	-0.0174805	0.04268448		104	-0.0085334	-5.25E-05
54	-0.017272	0.04186134		105	-0.0085356	-0.0001014
55	-0.0170672	0.04103689		106	-0.008542	-0.0001499
56	-0.0168656	0.0402113		107	-0.0085527	-0.0001976
57	-0.0166664	0.03938476		108	-0.0085676	-0.0002442
58	-0.0164694	0.03855735		109	-0.0085866	-0.0002893
59	-0.0162742	0.03772919		110	-0.0086095	-0.0003326
60	-0.0160806	0.03690035		111	-0.008636	-0.0003736
61	-0.0158882	0.03607094		112	-0.0086661	-0.0004122
62	-0.0156969	0.03524103		113	-0.0086995	-0.000448
63	-0.0155065	0.03441063		114	-0.008736	-0.0004806
64	-0.015317	0.03357973		115	-0.0087751	-0.0005099
65	-0.0151283	0.03274832		116	-0.0088167	-0.0005357
66	-0.0149405	0.03191637		117	-0.0088604	-0.0005577
67	-0.0147535	0.03108389		118	-0.0089059	-0.0005757
68	-0.0145674	0.03025086		119	-0.0089528	-0.0005896
69	-0.0143823	0.0294173		120	-0.0090007	-0.0005994
70	-0.0141984	0.02858317		121	-0.0090493	-0.0006049

122	-0.0090982	-0.000606		173	-0.0184498	0.02098148
123	-0.009147	-0.0006029		174	-0.0186996	0.02151288
124	-0.0091954	-0.0005954		175	-0.0189507	0.02204361
125	-0.0092429	-0.0005837		176	-0.0192028	0.02257379
126	-0.0092892	-0.0005678		177	-0.0194562	0.02310335
127	-0.0093339	-0.000548		178	-0.0197113	0.02363213
128	-0.0093766	-0.0005242		179	-0.0199685	0.02415989
129	-0.0094171	-0.0004968		180	-0.0202283	0.02468645
130	-0.0094551	-0.0004659		181	-0.0204912	0.02521158
131	-0.0094901	-0.0004318		182	-0.0207577	0.02573507
132	-0.009522	-0.0003947		183	-0.0210283	0.02625672
133	-0.0095505	-0.0003549		184	-0.0213035	0.0267763
134	-0.0095754	-0.0003128		185	-0.0215835	0.02729367
135	-0.0098105	0.00024869		186	-0.0218681	0.02780893
136	-0.010042	0.00078499		187	-0.0221569	0.02832225
137	-0.0102829	0.00133374		188	-0.0224494	0.02883376
138	-0.0105247	0.00188807		189	-0.0227451	0.02934363
139	-0.0107599	0.00244185		190	-0.0230436	0.02985203
140	-0.0109879	0.0029938		191	-0.0233445	0.03035911
141	-0.0112109	0.00354461		192	-0.0236473	0.03086503
142	-0.011431	0.00409496		193	-0.0239515	0.03136994
143	-0.0116504	0.00464553		194	-0.024257	0.03187397
144	-0.0118699	0.0051965		195	-0.0245639	0.03237723
145	-0.0120893	0.00574775		196	-0.0248719	0.03287984
146	-0.0123086	0.00629918		197	-0.0251813	0.03338194
147	-0.0125279	0.00685065		198	-0.0254919	0.03388361
148	-0.0127469	0.00740206		199	-0.0258037	0.03438498
149	-0.0129658	0.00795328		200	-0.0261168	0.03488617
150	-0.0131844	0.0085042		201	-0.0264311	0.03538726
151	-0.0134027	0.0090547		202	-0.0267469	0.03588813
152	-0.0136207	0.0096047		203	-0.0270647	0.03638819
153	-0.0138386	0.01015417		204	-0.027385	0.03688685
154	-0.0140566	0.01070309		205	-0.0277083	0.0373835
155	-0.0142749	0.01125143		206	-0.0280351	0.03787755
156	-0.0144938	0.01179917		207	-0.0283661	0.03836845
157	-0.0147134	0.01234629		208	-0.0287016	0.03885562
158	-0.0149339	0.01289276		209	-0.0290421	0.03933853
159	-0.0151556	0.01343856		210	-0.029388	0.03981675
160	-0.0153786	0.01398366		211	-0.0297386	0.04029049
161	-0.015603	0.014528		212	-0.0300934	0.04076013
162	-0.0158291	0.01507151		213	-0.0304515	0.04122601
163	-0.0160569	0.01561413		214	-0.0308125	0.04168851
164	-0.0162865	0.01615579		215	-0.0311755	0.04214797
165	-0.0165182	0.01669643		216	-0.0315401	0.04260474
166	-0.016752	0.01723599		217	-0.0319054	0.04305917
167	-0.016988	0.01777439		218	-0.0322711	0.04351159
168	-0.0172264	0.01831158		219	-0.0326366	0.0439625
169	-0.0174671	0.01884758		220	-0.0330021	0.0444124
170	-0.01771	0.01938248		221	-0.033367	0.04486183
171	-0.0179549	0.01991638		222	-0.0337317	0.0453113
172	-0.0182015	0.02044934		223	-0.0340958	0.04576136

224	-0.0344596	0.04621254		231	-0.0369712	0.0494152
225	-0.0348229	0.04666535		232	-0.0373061	0.04988548
226	-0.0351857	0.04712032		233	-0.0376168	0.05037569
227	-0.0355478	0.04757751		234	-0.0379914	0.05112246
228	-0.0359083	0.04803632		235	-0.0380778	0.05135413
229	-0.0362665	0.04849588		236	-0.0381528	0.05158982
230	-0.0366217	0.04895495		237	-0.0382162	0.05182894

B.1.5 Vane KSZ03 (M-skew standard)

Point	x	y		39	-0.0200657	0.05161497
1	-0.0381768	0.05259344		40	-0.0197687	0.05082581
2	-0.0381043	0.05365238		41	-0.019484	0.05003065
3	-0.0379962	0.0545012		42	-0.019211	0.04923022
4	-0.0378516	0.05534338		43	-0.018949	0.04842514
5	-0.0376753	0.05618013		44	-0.0186972	0.04761612
6	-0.0374725	0.05700642		45	-0.0184548	0.04680374
7	-0.0372435	0.05781867		46	-0.0182209	0.0459884
8	-0.0369794	0.05861665		47	-0.0179944	0.04517046
9	-0.0366698	0.0594005		48	-0.0177744	0.04435028
10	-0.0363045	0.06017036		49	-0.0175599	0.04352821
11	-0.0358737	0.06092592		50	-0.01735	0.0427045
12	-0.0353734	0.06165552		51	-0.0171443	0.0418793
13	-0.0348067	0.06233536		52	-0.0169425	0.04105271
14	-0.0341767	0.06294108		53	-0.0167441	0.04022484
15	-0.033486	0.06344832		54	-0.0165487	0.03939579
16	-0.032738	0.06383389		55	-0.0163559	0.03856573
17	-0.0319449	0.06408624		56	-0.0161653	0.03773474
18	-0.0311242	0.06420045		57	-0.0159764	0.03690301
19	-0.0302942	0.06417581		58	-0.0157889	0.03607066
20	-0.0294736	0.064018		59	-0.0156025	0.0352378
21	-0.0286792	0.06373532		60	-0.0154169	0.03440448
22	-0.0279188	0.06334581		61	-0.0152322	0.03357065
23	-0.0271973	0.06287027		62	-0.0150485	0.03273629
24	-0.0265195	0.06232951		63	-0.0148657	0.03190138
25	-0.0258901	0.06174436		64	-0.0146839	0.03106593
26	-0.0253106	0.06113031		65	-0.0145029	0.03022995
27	-0.024775	0.06049086		66	-0.0143226	0.02939352
28	-0.0242763	0.05982782		67	-0.014143	0.02855667
29	-0.0238073	0.05914298		68	-0.013964	0.02771946
30	-0.0233611	0.05843816		69	-0.0137856	0.02688192
31	-0.0229334	0.05771575		70	-0.0136078	0.02604398
32	-0.0225229	0.05697883		71	-0.0134307	0.0252056
33	-0.0221289	0.05623054		72	-0.0132544	0.02436674
34	-0.0217501	0.05547399		73	-0.0130789	0.02352737
35	-0.0213859	0.05471214		74	-0.0129045	0.02268744
36	-0.0210355	0.05394582		75	-0.0127315	0.02184696
37	-0.0206989	0.05317452		76	-0.0125603	0.02100591
38	-0.0203757	0.05239775		77	-0.0123911	0.02016429
				78	-0.0122243	0.0193221

79	-0.0120593	0.0184794		130	-0.0094765	-0.0004279
80	-0.0118954	0.01763631		131	-0.0094993	-0.0003878
81	-0.0117317	0.01679292		132	-0.0097441	0.00024068
82	-0.0115675	0.01594933		133	-0.0099672	0.00079909
83	-0.0114021	0.01510566		134	-0.0101883	0.00134086
84	-0.0112359	0.01426197		135	-0.0104078	0.0018776
85	-0.0110691	0.01341834		136	-0.0106265	0.00241955
86	-0.010902	0.01257485		137	-0.0108449	0.00296783
87	-0.0107352	0.01173159		138	-0.0110638	0.00351983
88	-0.0105686	0.01088853		139	-0.011284	0.00407295
89	-0.010402	0.01004545		140	-0.011506	0.00462471
90	-0.0102348	0.00920211		141	-0.01173	0.00517433
91	-0.0100667	0.00835826		142	-0.0119557	0.00572211
92	-0.0098974	0.0075137		143	-0.0121829	0.00626836
93	-0.0097276	0.0066685		144	-0.0124111	0.0068134
94	-0.0095591	0.00582306		145	-0.0126402	0.00735755
95	-0.0093939	0.00497777		146	-0.0128699	0.00790111
96	-0.0092337	0.00413303		147	-0.0130999	0.00844443
97	-0.0090799	0.00328922		148	-0.0133299	0.00898779
98	-0.0089282	0.00244652		149	-0.0135596	0.00953138
99	-0.0087722	0.00160513		150	-0.0137892	0.01007513
100	-0.0086404	0.00076941		151	-0.0140187	0.01061897
101	-0.0085203	-0.0001524		152	-0.014248	0.01116281
102	-0.0085224	-0.0001984		153	-0.0144771	0.01170657
103	-0.0085285	-0.0002441		154	-0.0147061	0.01225017
104	-0.0085387	-2.89E-04		155	-0.0149351	0.01279354
105	-0.0085528	-0.0003329		156	-0.0151639	0.01333659
106	-0.0085707	-0.0003753		157	-0.0153926	0.01387927
107	-0.0085924	-0.000416		158	-0.0156214	0.01442153
108	-0.0086176	-0.0004545		159	-0.0158504	0.0149634
109	-0.0086461	-0.0004907		160	-0.0160796	0.01550483
110	-0.0086777	-0.0005242		161	-0.0163093	0.01604585
111	-0.0087122	-0.0005548		162	-0.0165395	0.01658643
112	-0.0087492	-0.0005822		163	-0.0167704	0.01712657
113	-0.0087885	-0.0006062		164	-0.017002	0.01766628
114	-0.0088298	-0.0006265		165	-0.0172346	0.0182055
115	-0.0088728	-0.0006432		166	-0.0174683	0.01874416
116	-0.0089171	-0.0006559		167	-0.0177036	0.01928206
117	-0.0089623	-0.0006647		168	-0.0179407	0.019819
118	-0.0090081	-0.0006694		169	-0.0181801	0.02035482
119	-0.0090542	-0.00067		170	-0.0184219	0.02088931
120	-0.0091001	-0.0006666		171	-0.0186667	0.02142231
121	-0.0091455	-0.000659		172	-0.0189147	0.02195363
122	-0.0091901	-0.0006475		173	-0.0191662	0.02248307
123	-0.0092335	-0.000632		174	-0.0194214	0.0230106
124	-0.0092753	-0.0006127		175	-0.0196801	0.02353638
125	-0.0093153	-0.0005898		176	-0.019942	0.02406057
126	-0.0093531	-0.0005634		177	-0.0202069	0.02458334
127	-0.0093883	-0.0005338		178	-0.0204745	0.02510489
128	-0.0094208	-0.0005012		179	-0.0207446	0.02562538
129	-0.0094503	-0.0004657		180	-0.021017	0.02614498

181	-0.0212913	0.02666387		211	-0.0307213	0.04165815
182	-0.0215675	0.02718217		212	-0.0310829	0.04212403
183	-0.0218457	0.02769981		213	-0.0314466	0.04258734
184	-0.0221259	0.02821663		214	-0.0318114	0.04304825
185	-0.0224085	0.02873251		215	-0.0321774	0.043507
186	-0.0226936	0.02924729		216	-0.0325437	0.04396388
187	-0.0229814	0.02976086		217	-0.0329108	0.04441917
188	-0.023272	0.03027308		218	-0.0332778	0.04487324
189	-0.0235656	0.03078382		219	-0.0336452	0.04532637
190	-0.0238624	0.03129298		220	-0.0340125	0.0457789
191	-0.0241623	0.03180059		221	-0.03438	0.04623111
192	-0.0244651	0.03230682		222	-0.0347473	0.04668336
193	-0.0247706	0.03281183		223	-0.0351147	0.04713595
194	-0.0250786	0.03331578		224	-0.0354809	0.04758954
195	-0.025389	0.03381884		225	-0.0358437	0.04804533
196	-0.0257015	0.03432115		226	-0.0362003	0.04850455
197	-0.0260159	0.03482289		227	-0.0365484	0.04896841
198	-0.0263321	0.0353242		228	-0.0368852	0.04943895
199	-0.0266501	0.03582505		229	-0.0372081	0.04992014
200	-0.0269703	0.036325		230	-0.0375145	0.05041622
201	-0.027293	0.03682366		231	-0.0378721	0.05108781
202	-0.0276186	0.03732058		232	-0.0379353	0.05124738
203	-0.0279474	0.03781537		233	-0.0379915	0.05140964
204	-0.0282799	0.03830756		234	-0.0380403	0.0515743
205	-0.0286163	0.03879674		235	-0.0380818	0.051741
206	-0.0289571	0.03928248		236	-0.0381159	0.05190942
207	-0.0293025	0.0397645		237	-0.0381425	0.05207922
208	-0.029652	0.04024285		238	-0.0381615	0.05225005
209	-0.0300053	0.04071777		239	-0.038173	0.05242157
210	-0.0303619	0.04118946		240	-0.0381768	0.05259344

B.1.6 Vane KVD04 (M-skew standard)

Point	x	y		16	-0.0348842	0.06232668
1	-0.0381493	0.05184285		17	-0.0342617	0.06293574
2	-0.0382009	0.05208029		18	-0.033577	0.06344695
3	-0.0382407	0.05232004		19	-0.0328331	0.06383801
4	-0.0382686	0.05256151		20	-0.0320425	0.0641
5	-0.0382586	0.05366364		21	-0.0312229	0.06423169
6	-0.038139	0.05449767		22	-0.0303922	0.06423185
7	-0.0379504	0.05532557		23	-0.0295682	0.06409933
8	-0.0377383	0.05615108		24	-0.0287669	0.06383637
9	-0.0375117	0.0569709		25	-0.0279967	0.06346131
10	-0.0372722	0.05778215		26	-0.027264	0.062997
11	-0.0370078	0.05858323		27	-0.0265753	0.06246516
12	-0.0367052	0.05937258		28	-0.0259374	0.06188661
13	-0.0363508	0.06014872		29	-0.0253531	0.06127694
14	-0.0359316	0.06090975		30	-0.0248148	0.06064007
15	-0.0354418	0.06164345		31	-0.0243139	0.05997821
				32	-0.0238418	0.05929362

33	-0.0233898	0.05858855		84	-0.0115836	0.01681496
34	-0.0229536	0.0578655		85	-0.0114153	0.0159692
35	-0.0225339	0.05712744		86	-0.0112467	0.01512333
36	-0.0221318	0.0563772		87	-0.0110784	0.01427726
37	-0.0217483	0.05561775		88	-0.010911	0.01343092
38	-0.0213844	0.05485184		89	-0.0107452	0.01258422
39	-0.0210391	0.05408043		90	-0.0105817	0.01173708
40	-0.0207104	0.05330329		91	-0.0104211	0.01088939
41	-0.0203961	0.0525202		92	-0.0102639	0.01004105
42	-0.0200942	0.05173093		93	-0.0101107	0.00919194
43	-0.0198028	0.05093542		94	-0.0099619	0.00834196
44	-0.0195213	0.05013429		95	-0.009818	0.00749098
45	-0.0192494	0.04932846		96	-0.0096788	0.00663908
46	-0.0189867	0.04851883		97	-0.0095433	0.00578647
47	-0.0187332	0.04770629		98	-0.0094108	0.00493335
48	-0.0184883	0.04689154		99	-0.0092804	0.00407996
49	-0.0182513	0.0460746		100	-0.0091511	0.00322651
50	-0.0180215	0.04525544		101	-0.0090214	0.00237324
51	-0.0177981	0.044434		102	-0.0088895	0.00152041
52	-0.0175803	0.04361025		103	-0.0087536	0.00066852
53	-0.0173674	0.04278433		104	-0.0086102	-2.20E-04
54	-0.0171587	0.04195658		105	-0.0086122	-0.0002658
55	-0.0169535	0.04112741		106	-0.0086184	-0.0003117
56	-0.0167511	0.04029717		107	-0.0086286	-0.0003568
57	-0.0165509	0.03946625		108	-0.0086428	-0.0004008
58	-0.0163525	0.03863476		109	-0.0086608	-0.0004434
59	-0.0161557	0.03780266		110	-0.0086826	-0.0004843
60	-0.0159604	0.03696992		111	-0.0087079	-0.000523
61	-0.0157664	0.03613649		112	-0.0087365	-0.0005593
62	-0.0155735	0.03530235		113	-0.0087683	-0.000593
63	-0.0153817	0.03446751		114	-0.0088029	-0.0006237
64	-0.0151908	0.03363203		115	-0.0088401	-0.0006511
65	-0.0150009	0.032796		116	-0.0088796	-0.0006752
66	-0.0148117	0.03195947		117	-0.0089211	-0.0006957
67	-0.0146232	0.03112248		118	-0.0089643	-0.0007123
68	-0.0144355	0.03028504		119	-0.0090087	-0.0007251
69	-0.0142486	0.02944712		120	-0.0090542	-0.0007339
70	-0.0140624	0.02860874		121	-0.0091002	-0.0007386
71	-0.013877	0.02776987		122	-0.0091464	-0.0007392
72	-0.0136924	0.0269305		123	-0.0091926	-0.0007356
73	-0.0135088	0.0260906		124	-0.0092382	-0.000728
74	-0.0133263	0.02525015		125	-0.009283	-0.0007163
75	-0.0131451	0.02440914		126	-0.0093265	-0.0007008
76	-0.0129652	0.02356752		127	-0.0093685	-0.0006814
77	-0.0127869	0.0227253		128	-0.0094086	-0.0006583
78	-0.0126101	0.02188251		129	-0.0094465	-0.0006318
79	-0.0124351	0.02103913		130	-0.0094819	-0.000602
80	-0.0122619	0.0201952		131	-0.0095145	-0.0005691
81	-0.0120906	0.01935075		132	-0.0095441	-0.0005335
82	-0.0119207	0.01850581		133	-0.0095703	-0.0004955
83	-0.0117519	0.01766053		134	-0.0095931	-0.0004552

135	-0.0098263	0.00013894		187	-0.0220895	0.02830361
136	-0.0100486	0.00069023		188	-0.0223791	0.02881668
137	-0.010275	0.00124142		189	-0.0226712	0.02932858
138	-0.0105013	0.0017931		190	-0.0229657	0.02983933
139	-0.010724	0.00234579		191	-0.0232626	0.0303489
140	-0.010943	0.00289935		192	-0.023562	0.03085726
141	-0.0111597	0.00345336		193	-0.0238637	0.03136442
142	-0.0113756	0.00400742		194	-0.0241677	0.03187038
143	-0.0115922	0.00456113		195	-0.0244739	0.03237524
144	-0.0118097	0.00511438		196	-0.0247823	0.03287902
145	-0.0120282	0.00566717		197	-0.0250928	0.03338179
146	-0.0122473	0.00621956		198	-0.0254054	0.03388362
147	-0.0124671	0.00677157		199	-0.0257199	0.03438453
148	-0.0126873	0.00732323		200	-0.0260363	0.03488462
149	-0.0129078	0.00787458		201	-0.0263545	0.03538394
150	-0.0131285	0.00842565		202	-0.0266746	0.03588237
151	-0.0133491	0.00897647		203	-0.0269969	0.03637963
152	-0.0135696	0.00952706		204	-0.0273217	0.0368754
153	-0.0137901	0.0100774		205	-0.0276493	0.03736934
154	-0.0140106	0.01062748		206	-0.0279799	0.03786111
155	-0.0142312	0.01117727		207	-0.0283139	0.0383504
156	-0.0144518	0.01172676		208	-0.0286515	0.03883688
157	-0.0146726	0.01227593		209	-0.0289931	0.03932022
158	-0.0148937	0.01282477		210	-0.0293387	0.03980018
159	-0.0151115	0.01337326		211	-0.0296881	0.0402768
160	-0.0153367	0.01392136		212	-0.0300408	0.04075022
161	-0.0155589	0.01446903		213	-0.0303962	0.04122057
162	-0.0157817	0.01501616		214	-0.0307541	0.04168798
163	-0.0160055	0.0155627		215	-0.0311137	0.04215259
164	-0.0162304	0.01610856		216	-0.0314749	0.0426145
165	-0.0164565	0.01665367		217	-0.0318369	0.04307388
166	-0.016684	0.01719794		218	-0.0321995	0.04353085
167	-0.0169133	0.01774132		219	-0.0325622	0.04398577
168	-0.0171443	0.01828369		220	-0.0329255	0.0444391
169	-0.0173774	0.01882499		221	-0.0332887	0.04489133
170	-0.0176127	0.01936509		222	-0.0336525	0.04534293
171	-0.0178505	0.01990388		223	-0.0340164	0.04579437
172	-0.0180911	0.02044124		224	-0.0343808	0.04624612
173	-0.0183345	0.02097708		225	-0.0347457	0.04669866
174	-0.0185812	0.02151126		226	-0.0351112	0.04715246
175	-0.0188312	0.0220437		227	-0.0354769	0.0476078
176	-0.0190848	0.02257425		228	-0.0358413	0.04806459
177	-0.0193421	0.0231029		229	-0.036203	0.04852278
178	-0.019603	0.02362971		230	-0.0365603	0.04898229
179	-0.0198673	0.02415481		231	-0.03691	0.04944513
180	-0.020135	0.02467825		232	-0.0372437	0.04991849
181	-0.0204057	0.02520015		233	-0.0375523	0.05041029
182	-0.0206795	0.02572057		234	-0.0379247	0.05115043
183	-0.0209562	0.02623964		235	-0.038011	0.05137734
184	-0.0212357	0.02675741		236	-0.0380859	0.05160834
185	-0.0215177	0.02727399		237	-0.0381493	0.05184285

B.2 Trent XWB 84K

B.2.1 Vane with undisclosed serial number

Point	x	y			
1	-0.0317541	0.04918229	46	-0.0133752	0.04895685
2	-0.031812	0.04945261	47	-0.013122	0.04817164
3	-0.0318572	0.04972522	48	-0.0128792	0.04738358
4	-0.0318896	0.04999953	49	-0.0126458	0.04659302
5	-0.0319086	0.05109252	50	-0.0124206	0.04580003
6	-0.0318444	0.05192324	51	-0.0122025	0.04500497
7	-0.0317409	0.05275106	52	-0.0119907	0.04420815
8	-0.031615	0.05357445	53	-0.0117841	0.04340967
9	-0.0314773	0.05439445	54	-0.011582	0.04260979
10	-0.031332	0.05521118	55	-0.011384	0.04180891
11	-0.0311707	0.05602272	56	-0.0111894	0.04100718
12	-0.0309834	0.05682686	57	-0.0109975	0.04020478
13	-0.0307601	0.0576215	58	-0.010808	0.03940185
14	-0.0304907	0.05840422	59	-0.0106212	0.03859849
15	-0.0301654	0.05916561	60	-0.0104366	0.03779452
16	-0.0297743	0.05988928	61	-0.0102544	0.03698992
17	-0.0293076	0.0605582	62	-0.0100744	0.03618465
18	-0.0287554	0.06115541	63	-0.0098967	0.03537892
19	-0.0281101	0.06166447	64	-0.0097209	0.03457267
20	-0.0273837	0.06207445	65	-0.0095467	0.03376595
21	-0.0265996	0.06237763	66	-0.0093741	0.03295886
22	-0.0257817	0.06256571	67	-0.009203	0.03215155
23	-0.0249538	0.06263062	68	-0.0090333	0.03134393
24	-0.0241366	0.06256838	69	-0.0088649	0.03053596
25	-0.0233389	0.06239031	70	-0.0086978	0.02972764
26	-0.0225655	0.06211281	71	-0.0085321	0.028919
27	-0.0218211	0.06175282	72	-0.0083678	0.02811003
28	-0.0211108	0.06132696	73	-0.0082049	0.02730069
29	-0.0204382	0.06084788	74	-0.0080433	0.02649103
30	-0.0198029	0.06032177	75	-0.0078831	0.02568107
31	-0.0192041	0.0597541	76	-0.0077245	0.02487086
32	-0.0186407	0.05915086	77	-0.0075672	0.02406033
33	-0.0181116	0.0585181	78	-0.0074111	0.02324951
34	-0.0176153	0.05786037	79	-0.0072563	0.02243838
35	-0.0171485	0.05718049	80	-0.0071028	0.02162696
36	-0.0167088	0.05648211	81	-0.0069505	0.02081525
37	-0.0162932	0.05576845	82	-0.0067991	0.02000325
38	-0.0158993	0.05504318	83	-0.0066487	0.01919102
39	-0.0155253	0.05430826	84	-0.0064992	0.01837859
40	-0.0151703	0.05356461	85	-0.0063507	0.01756614
41	-0.0148331	0.05281292	86	-0.006203	0.01675363
42	-0.0145124	0.05205359	87	-0.0060557	0.01594099
43	-0.0142074	0.05128771	88	-0.0059086	0.0151282
44	-0.0139169	0.05051568	89	-0.0057616	0.01431523
45	-0.0136398	0.04973838	90	-0.0056146	0.01350211
			91	-0.0054674	0.01268877
			92	-0.0053202	0.01187529

93	-0.0051732	0.01106177		144	-0.0056213	0.0048832
94	-0.0050268	0.01024829		145	-0.0058093	0.00539125
95	-0.0048816	0.00943499		146	-0.0059985	0.00589875
96	-0.004737	0.00862171		147	-0.0061893	0.00640534
97	-0.0045926	0.00780821		148	-0.0063817	0.00691094
98	-0.0044475	0.00699423		149	-0.0065762	0.00741568
99	-0.0043013	0.0061795		150	-0.0067724	0.00791963
100	-0.0041545	0.00536372		151	-0.0069701	0.00842286
101	-0.0040139	0.00454597		152	-0.0071693	0.00892546
102	-0.0038896	0.00372521		153	-0.0073702	0.00942754
103	-0.0037693	0.00290481		154	-0.0075723	0.00992918
104	-0.0036036	2.07E-03		155	-0.0077757	0.01043043
105	-0.0035996	0.00204569		156	-0.0079803	0.01093135
106	-0.0035967	0.00202183		157	-0.0081862	0.0114319
107	-0.003595	0.00199785		158	-0.0083933	0.01193199
108	-0.0035944	0.00197382		159	-0.0086017	0.01243156
109	-0.0035964	0.00192937		160	-0.0088114	0.01293058
110	-0.0036023	0.00188528		161	-0.0090224	0.01342896
111	-0.0036122	0.00184193		162	-0.0092347	0.01392664
112	-0.0036258	0.00179968		163	-0.0094485	0.01442358
113	-0.0036432	0.00175888		164	-0.0096637	0.01491976
114	-0.0036641	0.00171987		165	-0.0098802	0.01541516
115	-0.0036884	0.00168297		166	-0.0100981	0.01590985
116	-0.0037159	0.0016485		167	-0.0103174	0.01640395
117	-0.0037463	0.00161673		168	-0.010538	0.01689744
118	-0.0037795	0.00158794		169	-0.0107597	0.01739037
119	-0.0038151	0.00156236		170	-0.0109828	0.01788286
120	-0.0038528	0.0015402		171	-0.0112071	0.01837491
121	-0.0038923	0.00152166		172	-0.0114325	0.01886654
122	-0.0039333	0.00150687		173	-0.0116591	0.01935778
123	-0.0039755	0.00149598		174	-0.011887	0.01984851
124	-0.0040184	0.00148906		175	-0.0121163	0.02033862
125	-0.0040618	0.00148618		176	-0.0123471	0.02082804
126	-0.0041053	0.00148735		177	-0.0125795	0.02131673
127	-0.0041484	0.00149258		178	-0.0128135	0.02180452
128	-0.004191	0.00150181		179	-0.0130493	0.02229135
129	-0.0042325	0.00151496		180	-0.013287	0.02277721
130	-0.0042727	0.00153193		181	-0.0135267	0.02326194
131	-0.0043112	0.00155258		182	-0.0137683	0.02374557
132	-0.0043478	0.00157674		183	-0.014012	0.02422821
133	-0.0043821	0.00160419		184	-0.0142578	0.02470972
134	-0.0044138	0.00163472		185	-0.0145057	0.02519014
135	-0.0044427	0.00166807		186	-0.0147559	0.0256696
136	-0.0044684	0.00170397		187	-0.0150082	0.02614792
137	-0.0044909	0.0017421		188	-0.0152627	0.02662512
138	-0.0045098	0.00178217		189	-0.0155195	0.02710119
139	-0.0046952	0.00233941		190	-0.0157788	0.02757598
140	-0.0048738	0.00285007		191	-0.0160407	0.02804935
141	-0.0050583	0.00335872		192	-0.0163053	0.02852109
142	-0.005246	0.00386675		193	-0.0165728	0.02899108
143	-0.0054338	0.00437492		194	-0.0168434	0.0294591

195	-0.0171173	0.0299251		219	-0.0247866	0.04036929
196	-0.0173948	0.03038901		220	-0.0251434	0.04077452
197	-0.0176759	0.03085064		221	-0.0255033	0.0411768
198	-0.017961	0.03130992		222	-0.0258663	0.04157614
199	-0.01825	0.03176687		223	-0.0262322	0.04197259
200	-0.0185431	0.03222136		224	-0.0266009	0.04236663
201	-0.0188401	0.03267316		225	-0.0269717	0.04275873
202	-0.0191413	0.03312267		226	-0.0273444	0.04314939
203	-0.0194465	0.03356926		227	-0.0277186	0.04353901
204	-0.0197558	0.03401302		228	-0.0280939	0.04392807
205	-0.0200693	0.03445377		229	-0.0284701	0.04431689
206	-0.0203867	0.03489149		230	-0.0288467	0.04470595
207	-0.0207079	0.03532646		231	-0.0292218	0.0450967
208	-0.0210328	0.03575859		232	-0.0295903	0.04549256
209	-0.0213609	0.0361885		233	-0.0299472	0.04589711
210	-0.0216922	0.0366158		234	-0.0302872	0.04631388
211	-0.0220263	0.03704123		235	-0.0306059	0.04674582
212	-0.022363	0.03746444		236	-0.0308998	0.04719439
213	-0.022702	0.03788583		237	-0.0311655	0.04765934
214	-0.0230433	0.0383053		238	-0.0315054	0.04839112
215	-0.0233869	0.03872278		239	-0.0316006	0.04865094
216	-0.0237328	0.03913807		240	-0.0316836	0.04891486
217	-0.0240814	0.039551		241	-0.0317541	0.04918229
218	-0.0244326	0.03996144				