

# Smart Switching Regulator

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Link to code: <https://github.com/vladniculescu/GSOC>

# 1 Prerequisites

In order to realize or develop this project, you will need:

1. Populated development board
2. Digilent Nexys Video FPGA board
3. Oscilloscope
4. Power Source (1.5A current capability)
5. Logic analyser (not mandatory, but useful)

## 2 Introduction

The main goal of this project is to design an adjustable converter for the Aper-tus AXIOM Beta camera system. The AXIOM requires multiple voltages, so an adjustable solution is preferred over having multiple converters. Multiple instances of this converter will be utilized in the Beta, each one working at a different output voltage, but with identical hardware components. The performance criteria of the converter are efficiency, accuracy and ripple. The whole converter will represent an individual block, which will communicate with the central processing through I2C. The input supply voltage is 5V.

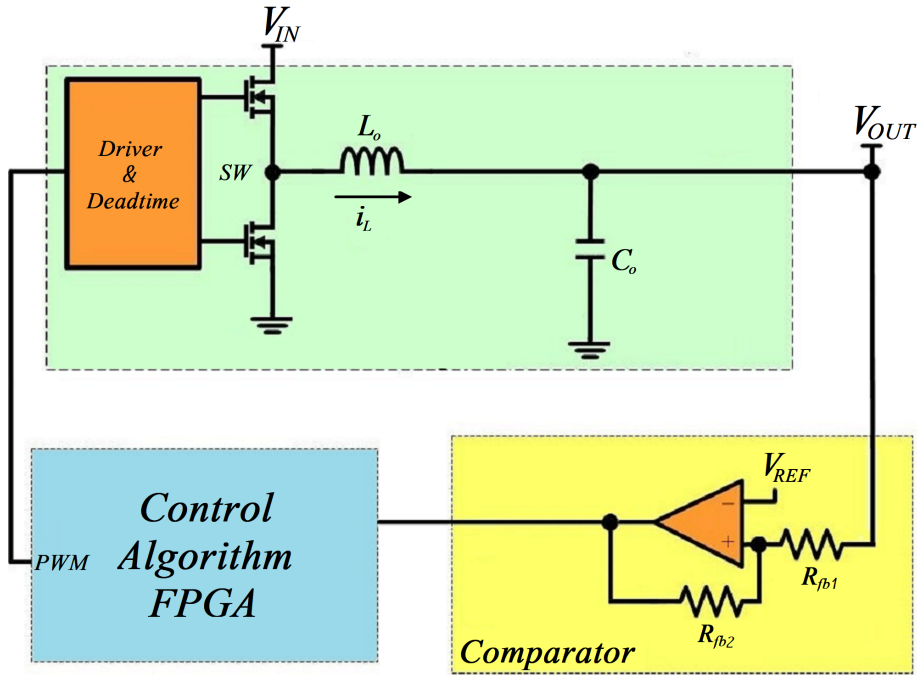


Figure 1: The Block Schematic

The synchronous configuration was preferred because of efficiency considerations. The chosen driver is controlled by a single PWM signal and process it in order to properly drive the two transistors – it generates two complementary signals and also adds deadtime. The output voltage is maintained constant due to the feedback mechanism, which This consists of a hysteresis comparator that indicates if the actual voltage is above or below a reference voltage. The control algorithm runs on an FPGA and controls the converter according to the information received from the comparator. Its main purpose is to maintain the output voltage as close as possible to the reference. This reference is generated by a 12-bit DAC and thus can be easily adjusted. The output voltage follows the

reference voltage regardless of the drawn current. Both the DAC and the control algorithm act as I2C slaves which allow the I2C master to modify essential parameters. While the DAC's I2C allows for a reference change, the converter's I2C gives control over the converter's parameters, like switching frequency or the speed of the feedback loop. Both slaves will be connected to the global I2C bus of the AXIOM system.

### 3 Designing the Converter

The first step in realizing this project was to design a schematic for a test setup as well as building a prototype to test with. A rendering of the designed prototype board can be seen in figure 2.

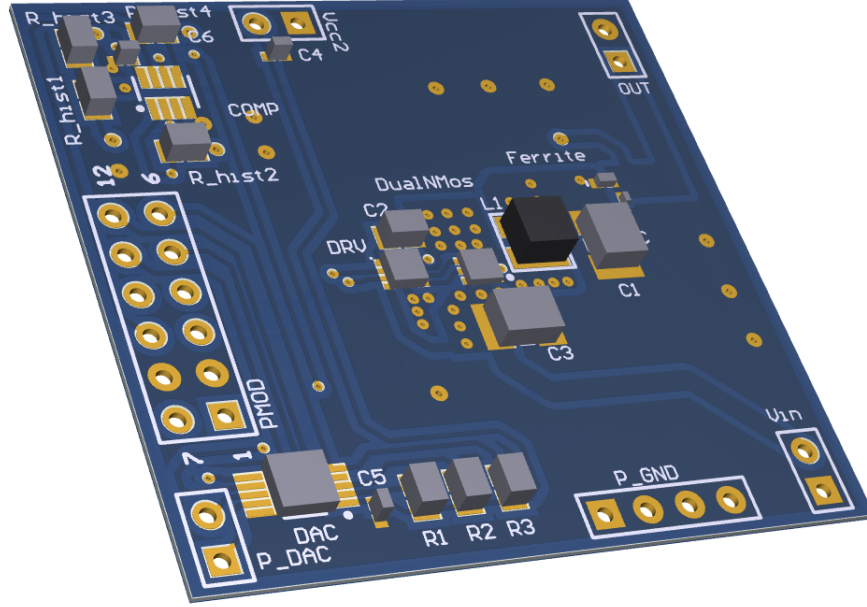


Figure 2: The PCB

Based on the design files, the PCB was fabricated at OSH Park and manually populated. The board was equipped using the “hot plite”, because this was a good way to solder the parts in QFN packages.

After the board was populated, I started testing each module individually. The converter placed in the center of the board was tested using a fixed duty cycle pwm signal. Applying such a signal, it was observed that the output varies according to the duty cycle of this pwm signal. This assured the proper functionality of the converter.

The DAC converter that uses a I2C interface was the next tested module. Using a USB to I2C Master board from Microchip Technology, certain configuration bytes were sent through I2C to configure the internal registers of the DAC. I searched in the datasheet for the command that changes the output voltage and sent the commands that set certain output voltages. I also measured the actual value at the DAC's output to check if this voltage has the expected value. Finally, I came to the conclusion that the DAC block works good, too.

Testing the comparator was the next stage of guaranteeing the right functionality of the board. If this one had worked good, the functionality of the board would have been validated. However, during this test, I discovered an electrical error in the schematic. The positive feedback of the comparator was wrongly connected, so the comparator didn't like as a hysteresis one anymore. Consequently, I modified the board and I managed do it without damaging the traces. by soldering two resistors on the pads of one. Anyway, this problem was fixed in the final iteration of the board, which is currently available on github (Layout Files/PCB\_Project).

The hysteresis comparator acts like a feedback mechanism which gives the input for the control algorithm. The hysteresis was introduced to reduce the switching frequency of its output. However, the hysteresis width was set to 80mV. A higher value would generate a higher ripple, too.

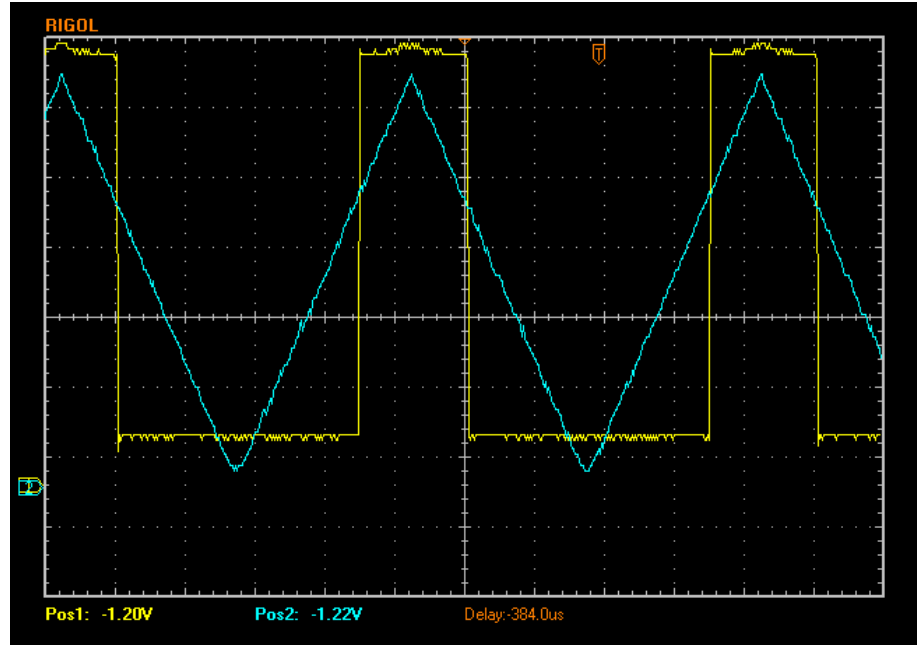


Figure 3: The comparator's output

The comparator's output In order to obtain the desired value, a 62 ratio of the resistors was needed – in theory. To test if this value is also obtained

in practice, a triangular signal was applied at the non-inverting input of the comparator, while a fixed voltage was applied at the inverting input. Figure 3 illustrates the triangular signal and also the comparator's output where the two thresholds are obvious.

## 4 The UART to I2C Bridge:

To simplify the hardware testing, an USB to I2C bridge was designed to command the system from a PC via serial port. This bridge allows real-time communication between computer and the converter which means that the converter's parameters as well as the DACs output voltage can be adjusted from the serial console of the computer. The FPGA development board used for this purpose was a Digilent Nexys Video, equipped with a Xilinx Artix 7.

The first step was to establish communication between computer and FPGA. The USB to I2C bridge was splitted in two components:

1. The USB to UART component: This half is used to adjust the converter's settings
2. The UART to I2C Master: In order to configure the DAC, both components are required

Therefore, the first developed component was a UART module. This one was consisted of a receiver and a transmitted module. The transmitter was tested using the leds on the development board. Basically, I sent different characters from the serial console and the eight leds lighted according to the 8 bit ASCII number that corresponds to the sent character.

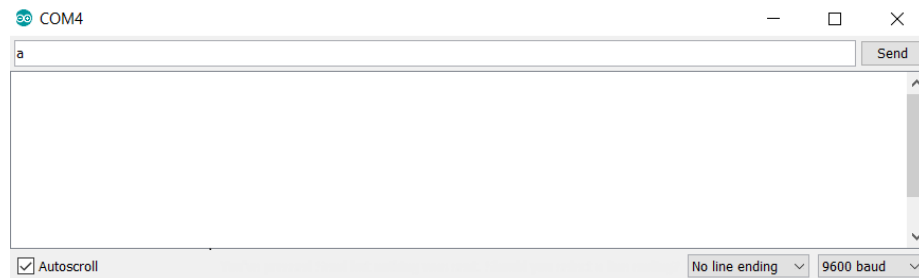


Figure 4: The Serial Console

Figure 4 shows how characters are sent from the serial console.

The second step was to develop a I2C Master module. This one takes the information received from the UART Receiver module, and sends it through I2C to the DAC to configure it. The received command is firstly decoded and sent to the I2C bus, controlling the DAC. Both UART and I2C Master are implemented as Verilog modules. The communication protocol consists of a

string of characters that represents hexadecimal numbers. The I2C Master sends 8 bit packages, so, the command string is consisted of pairs of two bytes followed by a read/write flag.

**For example**, I used a discrete slave I2C device to figure out if the Master works properly. I sent a sequence like “S49W71W00Rs”, which reads the value in register 0x71 for a device with the address equal to 24. “S” represents that a command for DAC is going to be sent and “s” marks the final character in this command. After a command was successfully executed, the bridge responds with a “D” character as acknowledge. The “00”sequence behind the “R” doesn’t have any significance and it just signals that a byte is going to be received. The hexadecimal number “49” represents the concatenation of the hexadecimal “24” in binary with “1”, which corresponds to a read operation. The waveforms involved in this process are highlighted in Figure 5. A Saleae logic analyzer was used to test and debug the functionality of the I2C Master.



Figure 5: The I2C waveforms

In this way I separately tested the functionality of the two components of the bridge. After I was sure that both UART module and I2C Master worked, I integrated these two modules to obtain the desired bridge. Finally, I sent a string from the serial console to configure the DAC.

I wanted to obtain 2.05V at all of the four outputs of the DAC.

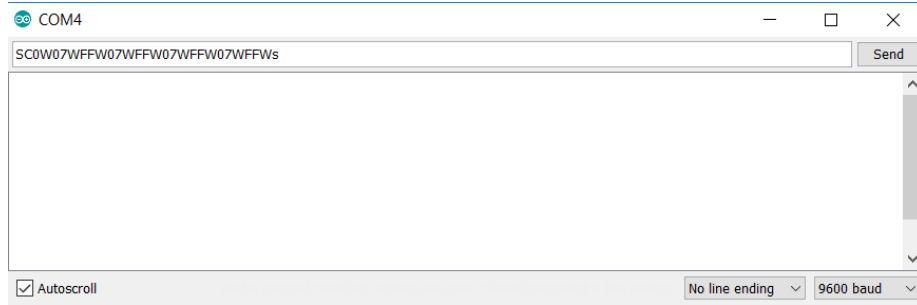


Figure 6: The I2C waveforms

Consequently, I sent the package in Figure6.

Table 1 the structure of the package that has to be sent in order to configure the DAC.

Where the MSb and LSb mean most significant, respectively least significant bit. There are four channels because the DAC is a 12-bit four channel type. The

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Address	Ch1_MSb	Ch1_LSb	Ch2_MSb	Ch2_LSb	Ch3_MSb	Ch3_LSb	Ch4_MSb	Ch4_LSb
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Table 1: The Package Structure for DAC configuration

ChX\_MSbyte is a 4-bit number and ChX\_LSbyte is an 8 bit one. Concatenating those two, the 12-bit value is obtained for each channel. So, returning to the example, “SC0W07WFFW07WFFW07WFFW07WFFWs” is sent from the serial console. S represents the start command, C0 the device address and W written after each two-number group says that the number has to be written (R is for read). The numbers are sent in hexadecimal format. Concatenating 07 and FF for each channel, 2047 is obtained. This is 2.05V for a 4.096V reference.

The Bridge can also adjust the converter’s parameters. The structure of the command is very similar, but this time the first letter of the string command will not be “S”.

Command	Effect	Length
S	Adjusts the DAC’s settings	Variable
X	Modifies the switching frequency	16 bit
T	Adjusts the loop speed	16 bit

Table 2: The commands of the Bridge

Table 2Shows the adjustments that can be made using the Bridge. Those adjustments are done from the serial console. The “X”and “T” characters signal that a command towards converter is going to be made. This one will only use the UART module.

The switching frequency can vary be adjusted between 0 and 780kHz with a 16 bit resolution. In order to modify it, a command like “Xxxxxs” should be sent from serial console, where “xxxx” represents a 16 bit number in hexadecimal format. Consequently, “XFFFFs” will set the frequency to its maximum value. The same mechanism works for the loop speed. A command like “Txxxxs” tells the algorithm how often to read the comparator. For a higher value of “xxxx” the loop will be slow.

As a conclusion, the bridge can adjust the DAC’s settings, the switching frequency and the feedback loop speed. However, for the last two, only half of bridge is necessary, as the controller is a verilog module, not a separate I2C slave device.

This I2C Master module was designed just for development. Because it allowed me to control the converter and DAC in real time, I didn’t need to re-synthetize the project at every parameter change. It won’t be necessary when the converter will be integrated in the AXIOM System, because it will be driven by this one through the I2C Slave module. So the next step I did was to implement the Slave I2C for converter. This allowed the converter to be configured by modifying some cells in the register file of a I2C Slave module. I tested this Slave module using an Arduino Uno board. Firstly, I wrote a certain



value in the first cell of the file register. Then, I read that cell to be sure that I receive the value I wrote. For the actual converter, register 0 and register 1 store the LSB and MSB of the frequency division variable and register 2 and register 3 store the LSB and MSB of the feedback loop speed variable. Example, if the register 0 equals “FF” and register 1 equals “AB”, the switching frequency will be:

$$f_{sw} = \frac{register[1] \cdot 256 + register[0]}{65536} \cdot 50Mhz = \quad (1)$$

$$= \frac{171 \cdot 256 + 255}{65536} \cdot 50Mhz = 0.67 \cdot 50Mhz = 33.5Mhz \quad (2)$$

“171” and “255” are the decimal values of the hexadecimal “AB” and “FF”.

## 5 The control algorithm

The control algorithm uses a fixed switching frequency and varies only the duty cycle of the PWM control signal. The parameters of this algorithm are the interval at which the duty cycle is updated and the switching frequency. The switching frequency was experimentally determined to be 780kHz. A counter is incremented whenever the output voltage is higher than the reference and decremented when this is smaller than the reference. When the update time comes, the counter is evaluated and the duty cycle is increased or decreased by 1, according to the value of this counter.

```
always @(posedge clock) begin
    ramp_prev <= ramp;

    if (ramp == 0 && ramp_prev == 63) begin
        test <= !test;
        if (fb) begin
            if (decimal == 65000 - fb_interval) begin
                decimal <= 65000;
                if (duty > 0)
                    duty <= duty - 1;
            end
        else
            decimal <= decimal - 1;
        end
    else begin
        if (decimal == 65000 + fb_interval) begin
            decimal <= 65000;
            if (duty < 63)
```

```

                                duty <= duty + 1;
                            end
                        else
                            decimal <= decimal + 1;
                        end
                    end
                end
            end
        end
    end
end

```

Tuning the algorithm:

Finding this way to control the transistor was by far the most challenging stage of this project. In the beginning I didn't even thought about including a variable that sets the feedback loop speed. Despite the fact that a high efficiency (over 85%) was obtained even from the first iterations of the algorithm, the biggest challenge was reducing the output ripple. I used the oscilloscope to measure this ripple, by evaluating the peak to peak amplitude of the AC component. It basically has a high frequency component, which comes from the switching frequency and a lower frequency component generated by the action of the control loop. This is usually between 1 and 30 kHz. If the feedback loop actions too slow, the ripple will be higher, because a low frequency component won't be rejected by the LC filter.



Figure 7: The output ripple for a slow feedback loop

Figure 7 highlights the output signal when such situation occurs. The transitions between levels present a quite square form, which indicates a poor filtering effect. In this case, the feedback loop speed should be increased, because a low pass filter does not have any effect on a very low frequency signal. This was a mistake I made and I hardly figured out the cause.

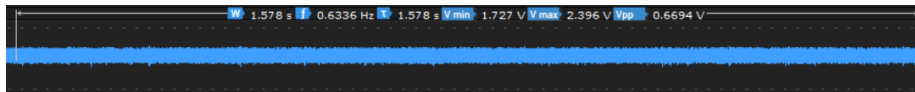


Figure 8: The output ripple for a fast feedback loop

However, if the feedback loop speed is set to a high value, its effect will be harmful, too. Because the algorithm uses only a proportional component, if this one is too aggressive will determine an increase in the output voltage at every iteration. Consequently, it will somehow oscillate around the average position with a high amplitude. This was the first problem I encountered in developing the algorithm. In the beginning, I evaluated the comparator and adjusted the duty cycle at the start of every pwm cycle. This proved to be too fast and triggered this kind of problem. In the end, an equilibrium was found, and I determined that the best value of the interval variable is 96. This means that the feedback loop is read every 96 cycles. Figure 8 highlights the improvement in ripple value.

Because the comparator's output turned out to be a little noisy, an averaging filter was introduced to reduce the noise.

```
always @(posedge clock) begin
    if (cnt == filter_length) begin
        cnt <= 0;
        cnt1 <= 0;
        cnt0 <= 0;
        comp_out_f <= fb_filtered;
    end
    else
        cnt <= cnt + 1;

    if (comp_out)
        cnt1 <= cnt1 + 1;
    else
        cnt0 <= cnt0 + 1;

    if (cnt1 > cnt0)
        fb_filtered <= 1;
    else
        fb_filtered <= 0;
end
```

This filter has two counters. During a fixed interval, it counts how many ones and how many zeros are encountered. At the end of the interval, it outputs the most dominant value. "cnt1" and "cnt0" are the two counters. The averaging interval can be modified. However, it is not recommended to choose high values for it, because it will cause a big delay. This averaging filter has the same impulse response as a finite impulse response low pass filter. Consequently, a higher order will cause a higher delay, which is not helpful when it comes to real time processes.

In Figure 9, the effect of the filter is obvious, because the narrow high frequency spikes are rejected.

Finally, adjusting the switching frequency at 780kHz for the found speed of the feedback loop, it was obtained the waveform in Figure 10,.



Figure 9: Filtered vs unfiltered comparator

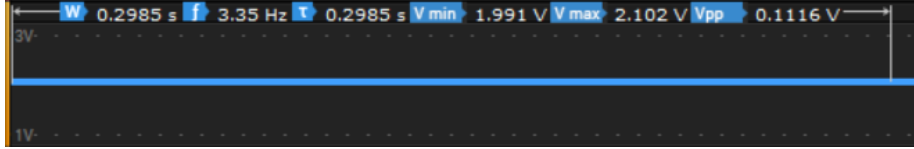


Figure 10: The output signal – 110mV ripple

The obtained ripple is around 110mV. This value is still poor for the requirements of this project. In order to reduce this ripple, an additional hardware filter was introduced. This one is consisted of a ferrite bead and an 1uF capacitor. Figure 11 presents the output ripple after this additional circuit was added. The ripple was reduced to 30mV.

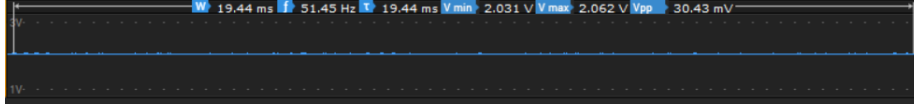


Figure 11: The output ripple after the second filter was added

Figure 12 displays the same waveform exported from a Rigol DS1102E oscilloscope set to 50mV/div.

## 6 Measuring the efficiency

After I managed to achieve the most important objective (obtaining a low ripple), I went on to determine its efficiency. The efficiency was measured as the ratio between the output power and the input one. All the efficiency measurements were done for a 2V output voltage. An ampere meter was put in series with the power supply and another one was put in series with the load. For different load resistances, the input current, input voltage, output current and output voltage were measured. The efficiency was calculated with the formula:

$$e = \frac{U_{out} \cdot I_{out}}{U_{in} \cdot I_{in}} \quad (3)$$

What is important to notice in Figure 13, is that for load currents over 100mA, the efficiency goes over 70%. Moreover, for output currents higher than 250mA the efficiency exceeds 90%.

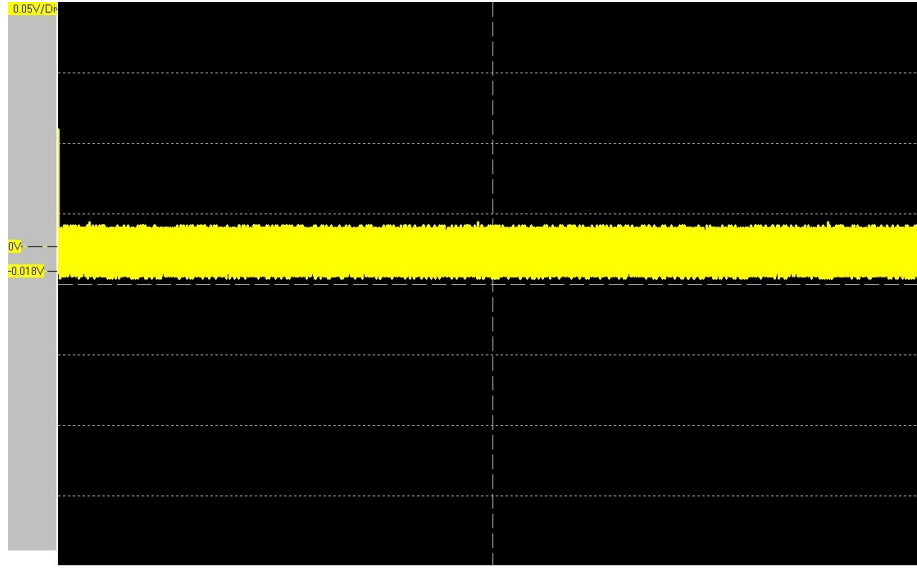


Figure 12: The output voltage measured with an oscilloscope

## 7 Measuring the accuracy

DAC voltage [V]	Output voltage [V]
1.5	1.47
1.753	1.749
2.05	2.08
2.249	2.229
2.49	2.53
2.99	3.03
3.49	3.53
3.99	3.988

Table 3: Reference Voltage vs Output Voltage

Table 3 shows that the difference between reference voltage and output voltage is more than 40mV.

## 8 Area occupied

The area occupied by each functional block is described below:

Table 4 shows the area occupied by each element of the buck converter.

Important: These parts were chosen for prototyping. For a final solution, the capacitors in a 1210 package can be replaced with a 0805 one.

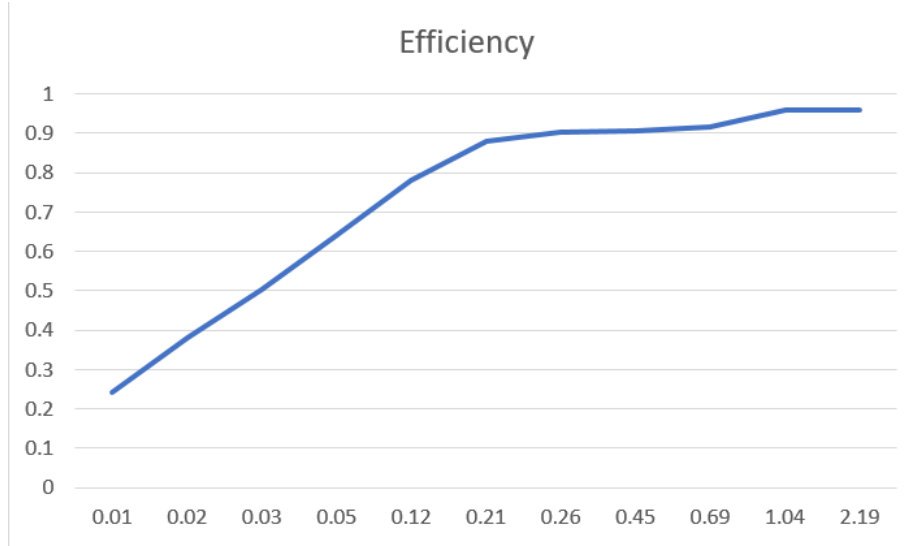


Figure 13: Variation of efficiency with current

Table 5 shows the area occupied by each element of the DAC's circuit.

Important: The 0805 resistances can be resistances can be replaced with some in 0402.

Table 6 shows the area occupied by each element of the Comparator's circuit.

Important: The 0805 resistances can be resistances can be replaced with some in 0402.

Part type	Area [mm2]	Code
Driver	4.6	NCP81151B
Dual MOS	4.6	NTLUD4C26N
2 x Capacitors 1210	25.2	
Capacitor 0805	4.05	
Inductor	12.21	
Ferrite bead	1.3	742792023
Capacitor 0603	1.3	
Total	53.2	
Total are on PCB	148.0	

Table 4: Area Occupied by Buck Converter

Part type	Area [mm2]	Code
DAC	11.1	MCP4728
3 x Resistance 0805	12.1	
1 x Capacitor 0402	0.3	
Total	23.5	
Total are on PCB	60.0	

Table 5: Area Occupied by DAC's circuit

Part type	Area [mm2]	Code
Comparator	9.0	MAX9107
4 x Resistance 0805	16.1	
1 x Capacitor 0402	0.3	
Total	25.4	
Total are on PCB	73.5	

Table 6: Area Occupied by Comparator's circuit

## 9 Future improvements

When it comes to future improvements, I think there are still many other things to be improved, especially for ripple and efficiency: Replacing the comparator with an ADC might bring some advantages. Basically, the comparator is a 1-bit ADC and the information provided by it is very poor. Consequently, the complexity of the control algorithm is limited due to the poor feedback information. By knowing exactly the value of the output voltage, a more precise control can be achieved. However, a research should be done here, because those advantages might not justify the additional price and space occupied by an ADC

Integrating a current measurement circuit. The output ripple and efficiency are powerfully dependent on the load current. By knowing the value of the instantaneous current, the algorithm's parameters can be adapted even during running. A look-up table can be developed inside the FPGA, so the algorithm will know what parameters to use depending on the load current.

## 10 Building the project

In order to test the project, several steps should be followed. If you want to test the converter through the USB to I2C bridge, you should:

1. Get the board and equip it
2. Download the files in the **UART to I2C Bridge** folder
3. Create a new project in your HDL synthetise tool (I used Xilinx Vivado)
4. Import all the ".v" files from the just downloaded folder as design sources

5. Import "constr.xdc" as constraints file (only if you use Digilent Nexys Video board). If you have other FPGA you would define your own constraints
6. Generate the bitfile and upload it
7. Connect the board to the JB PMOD connector of the board
8. Connect the computer to the UART port of your FPGA. If your FPGA board does not have a UART port, you should define your own UART pins and use a USB to UART bridge (like FTDI)
9. Open the serial console and configure the DAC. Example: send "SC0W07WFFW07WFFW07WFFW07WFFWs" to set the output voltage to 2.05V

If you want to test the converter through the I2C Slave module, you first have to know that you will need a separate I2C Master to command the converter and the DAC (which are two slave devices on the same bus). For instance, you can use Arduino Uno, because it allows you to send custom I2C commands. You should:

1. Get the board and equip it
2. Download the files in the **Converter I2C Slave** folder
3. Create a new project in your HDL synthetise tool (I used Xilinx Vivado)
4. Import all the ".v" files from the just downloaded folder as design sources
5. Import "constr.xdc" as constraints file (only if you use Digilent Nexys Video board). If you have other FPGA you would define your own constraints. This will assure the communication between converter's slave and board.
6. Manually connect the SDA and SCL of the DAC and converter's slave to your I2C bus.
7. Generate the bitfile and upload it
8. Connect the board to the JB PMOD connector of the board (only if you use Digilent Nexys Video board). If you have other FPGA you have to manually connect the FPGA I/Os to the board pins. Use the schematic and layout from "*Layout Files/PCB\_Project.pdf*" to identify the function of each pin of the board
9. Configure the DAC and converter from your I2C Master.

Note: If you have other FPGA board, you can also realize the setup. You have to manually connect the FPGA I/Os to the board pins. Use the schematic and layout from "*Layout Files/PCB\_Project.pdf*" to identify the function of each pin of the board.



## References

- [1] Texas Instruments, *Application Report SLVA477B–December 2011–Revised August 2015*, “Basic Calculation of a Buck Converter’s Power Stage”.
- [2] Texas Instruments, *Application Report SLVA390–February 2010*, “Calculating Efficiency”.
- [3] Texas Instruments, *Application Report SLVA630A–January 2014–Revised October 2014*, “Output Ripple Voltage for Buck Switching Regulator”.
- [4] Analog Devices, *Application Note AN-1144*, “Measuring Output Ripple and Switching Transients in Switching Regulators”.
- [5] [https://e2e.ti.com/support/power\\_management/simple\\_switcher/w/simple\\_switcher\\_wiki/2243.understanding-measuring-and-reducing-output-voltage-ripple](https://e2e.ti.com/support/power_management/simple_switcher/w/simple_switcher_wiki/2243.understanding-measuring-and-reducing-output-voltage-ripple)