

Problem 1

Assignment *4 Soln's

Approach:

Use a system of 3 eqns composed of E and M bals to solve for 3 unk's

- Well insulated \Rightarrow essentially adiabatic
- \rightarrow How much steam enters?
- \rightarrow How much liquid water at 75°C

$$U_i = (x) U_{i,vap} + (1-x) U_{i,liquid}$$

$$U_i = (x)(2476 \text{ kJ/kg}) + (1-x)(317 \text{ kJ/kg})$$

Volume of Vapor: $65000 \text{ L} - 220 \text{ L} = 64780 \text{ L}$
 Vapor density = $0.24 \frac{\text{kg}}{\text{m}^3} \times \frac{1\text{m}^3}{1000\text{L}} = 15.547 \text{ kg}_{\text{vapor}}$

Liquid = $974 \frac{\text{kg}}{\text{m}^3} \times \frac{1\text{m}^3}{1000\text{L}} \times 220\text{L} = 214 \text{ kg}_{\text{liquid}}$

$$x = \frac{15.547 \text{ kg}_{\text{vap}}}{15.547 \text{ kg}_{\text{vap}} + 214 \text{ kg}_{\text{l}}} = 0.0677$$

$$U_i = (0.0677)2476 \text{ kJ/kg} + (1-0.0677)(317 \text{ kJ/kg})$$

$$= 463.2 \text{ kJ/kg}$$

$$\Delta U = m \Delta u = m [0.91 \cdot 2712.7 \text{ kJ/kg} + 0.9 \cdot 523.9 \text{ kJ/kg}] = m (2518.37 \text{ kJ/kg} = U_f - U_i)$$

$$U_f = m (2518.37 \text{ kJ/kg}) + (463.2 \text{ kJ/kg})(230 \text{ kg})$$

$P_f = 2.3 \text{ bar}$, sat temp = 124.69°C after equilibrium is reached in the tank

3 eqn
3 unk.

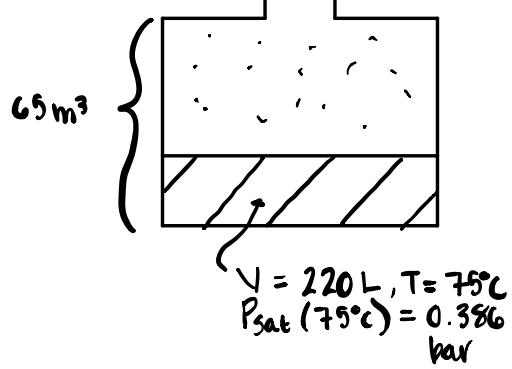
$$\left\{ \begin{array}{l} U_f = [q_f (2534 \text{ kJ/kg}) + (1-q_f) 524 \text{ kJ/kg}] \\ 65 = q_f (0.775 \text{ kJ/kg})(m + 230 \text{ kg}) + (1-q_f)(0.0011 \text{ kJ/kg})(m + 230 \text{ kg}) \\ U_f = \frac{m(2518.37 \text{ kJ/kg}) + (463.2 \text{ kJ/kg})(230 \text{ kg})}{m + 230} \end{array} \right.$$

using Mathematica or other solver tool : $U_f = 1048 \text{ kJ/kg}$, $q_f = 0.26$, $m = 91.6 \text{ kg}$

$$q_f = 0.26 = \frac{m_{vap}}{m_{tot}} = \frac{m_{vap} \cdot 83 \text{ kg}}{91.6 \text{ kg} + 230 \text{ kg}} \Rightarrow \frac{m_{vap}}{230 \text{ kg} - 91.6 \text{ kg} - 83 \text{ kg}} = \boxed{240 \text{ kg liquid}}$$

$m = 92 \text{ kg}$ steam enter the tank

2.3 bar 91% quality



Problem 2

$$M_{\text{kg}} = 1 \text{ kg} = 0.01 \text{ kg}$$

$$T = 60^\circ\text{C} = 333\text{K}$$

$$V_F = 0.0010 \text{ m}^3$$

1 kg H ₂ O	Vacuum
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$$\Delta U = q + \dot{w}_0, \quad U_F = U_I - 251.16 \text{ kJ/kg}$$

$$\hat{V}_F = \frac{0.0010 \text{ m}^3}{0.01 \text{ kg}} = 0.1 \text{ m}^3/\text{kg} = x \hat{V}_V + (1-x) \hat{V}_L$$

$$U_F = 251.16 \text{ kJ/kg} = x U_V + (1-x) U_L$$

APPROACH

Must iteratively find solution that satisfies Volume balance

Try $T_1 \rightarrow$ find $q_1(T)$

$$\text{use } V = m(qV_V + (1-q)V_L) = 0.001 \text{ m}^3$$

Check q by solving for U_F to see if = 251.16 kJ/kg

Guess 45°C $\Rightarrow U_V = 2436 \text{ kJ/kg}$

$$U_L = 188.43 \text{ "} \Rightarrow 0.1 \text{ m}^3/\text{kg} = q(15.29 \text{ m}^3/\text{kg}) + (1-q)(0.00101 \frac{\text{m}^3}{\text{kg}})$$

$$V_V = 15.2921 \text{ m}^3/\text{kg}$$

$$V_L = 0.00101 \text{ "}$$

$$q = 0.0065$$

$$\text{Check: } U_F = (0.0065)(2436 \text{ kJ/kg}) + 0.9935(188.43 \text{ kJ/kg}) = 203 \text{ kJ/kg} \neq 251 \text{ kJ/kg}$$

Guess 55°C $\Rightarrow U_V = 2499.34 \text{ kJ/kg}$

$$U_L = 230.24 \text{ "} \Rightarrow 0.1 \text{ m}^3/\text{kg} = q(9.56 \text{ m}^3/\text{kg}) + (1-q)(0.001 \frac{\text{m}^3}{\text{kg}})$$

$$V_V = 9.5643 \text{ m}^3/\text{kg}$$

$$V_L = 0.001015 \text{ "}$$

$$q = 0.0104$$

$$\text{Check: } U_F = (0.0104)(2436.08 \frac{\text{kJ}}{\text{kg}}) + 0.9896(230.24 \text{ kJ/kg}) = 253 \text{ kJ/kg} \approx 251 \text{ kJ/kg}$$

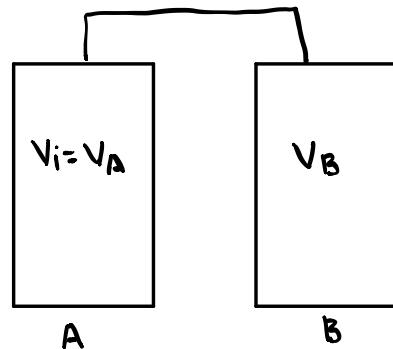
$T = 55^\circ\text{C}$ $P \approx 0.16 \text{ bar}$ $M_{\text{vap}} = 0.10 \text{ g}$ $M_{\text{Liq}} = 9.9 \text{ g}$ $M_{\text{tot}} = 0 \text{ g}$

Problem 3

adiabatic, reversible expansion

$$P_i = 12 \text{ bar}$$

$$T_i = 35^\circ\text{C} = 308 \text{ K}$$



Approach: CANNOT assume $V_B = 2V_A$

use 4 governing equations:

$$\rightarrow \text{Mball: } n_i = n_A + n_B$$

$$\rightarrow \text{Eball: } n_i u_i = n_A u_A + n_B u_B$$

$$\rightarrow \text{Ideal gas: } PV = nRT$$

$$\rightarrow \text{reversible adiabatic expansion: } \frac{T_A}{T_i} = \left(\frac{P_A}{P_i}\right)^{R/C_p}$$

$$n_i = n_A + n_B$$

$$\frac{P_i V_i}{R T_i} = \frac{P_A V_A}{R T_A} + \frac{P_B V_B}{R T_B} \Rightarrow \frac{P_i}{T_i} = \frac{P_A}{T_A} + \frac{P_B}{T_B}$$

$$n_i u_i = n_A u_A + n_B u_B$$

$$\frac{P_i V_i}{R T_i} (C_v T_i - C_p T_r) = \frac{P_A V_A}{R T_A} (C_v T_A - C_p T_r) + \frac{P_B V_B}{R T_B} (C_v T_B - C_p T_r)$$

$$\frac{P_i C_v - P_i C_p T_r}{T_i} = P_A C_v - \frac{P_A C_p T_r}{T_A} + P_B C_v - \frac{P_B C_p T_r}{T_B}$$

$$P_i C_v - P_A C_v - P_B C_v - \left(\frac{P_i}{T_i} - \frac{P_A}{T_A} - \frac{P_B}{T_B} \right) C_p T_r = 0$$

$$C_v (P_i - P_A - P_B) = 0$$

$$P_i = P_A + P_B$$

$$P_A = P_B$$

$$P_i = 2P_A$$

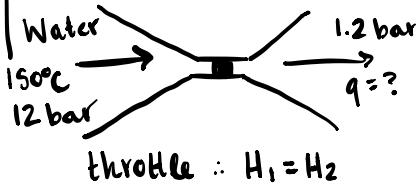
$$P_A = \frac{12}{6} = 2 \text{ bar}$$

$$\frac{T_A}{T_i} = \left(\frac{P_A}{P_i}\right)^{R/C_p}$$

$$T_A = T_i \left(\frac{P_A}{P_i}\right)^{R/C_p} = 308 \left(\frac{6 \text{ bar}}{12 \text{ bar}}\right)^{8.314/28}$$

$$\boxed{T_A = 251 \text{ K}}$$

Problem 4



Approach:

$$\text{use } \Delta H = 0 \Rightarrow q \\ \text{steam tables} \Rightarrow T$$

$$H_1 = 632.698 \text{ kJ/kg} = H_2$$

@ 1.2 bar, $H_{\text{sat}}^l = 439.4 \text{ kJ/kg}$, $H_{\text{sat}}^v = 2683 \text{ kJ/kg}$; $H_{\text{sat}}^l < H_2 < H_{\text{sat}}^v \therefore 2 \text{ phases}$

Outlet saturated so $T_f = 104^\circ \text{C} \approx 100^\circ \text{C}$

$$H_f = H_{\text{sat}}^l(1-x) + xH_{\text{sat}}^v \Rightarrow 632.698 = 439.4 \text{ kJ/kg} (1-x) + 2683 \text{ kJ/kg} (x)$$

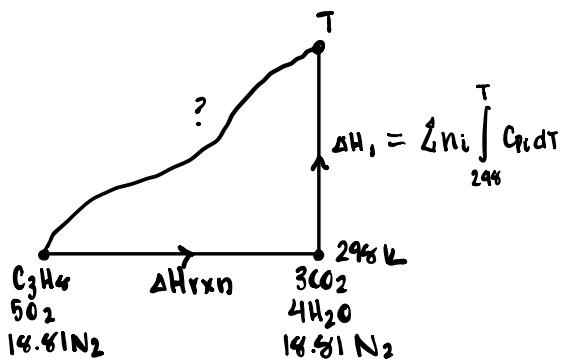
$$x = 0.086$$

$\therefore [9\% \text{ vapor}, 91\% \text{ liquid}]$

Problem 5



Adiabatic, $\Delta H = 0$



Approach:

Use $\Delta H_{rxn} + \Delta H_1 = 0$
to find T

$$\text{Calculate } \Delta H_{rxn}: \Delta H_{rxn} = \sum \Delta H_f^\circ, \text{prod} - \sum \Delta H_f^\circ, \text{rxns} = 3 \Delta H_f^\circ, CO_2 + 4 \Delta H_f^\circ, H_2O - \Delta H_f^\circ, C_3H_8$$

$$\Delta H_{rxn} = (3 \text{ mol})(-393.51 \frac{\text{kJ}}{\text{mol}}) + 4 \text{ mol}(-241.835 \frac{\text{kJ/mol}}{\text{mol}}) - (1 \text{ mol})(-107.64 \frac{\text{kJ}}{\text{mol}})$$

$$\Delta H_{rxn} = -2049.19 \text{ kJ}$$

$$\begin{aligned} C_p, CO_2 &= 19.98 + 0.07344T - 5.602 \times 10^{-5}T^2 + 1.715 \times 10^{-8}T^3 \\ C_p, H_2O &= 32.24 + 0.001924T + 1.055 \times 10^{-6}T^2 - 3.596 \times 10^{-9}T^3 \\ C_p, N_2 &= 31.15 - 0.001357T + 2.680 \times 10^{-5}T^2 - 1.168 \times 10^{-8}T^3 \end{aligned} \quad \text{From Textbook}$$

$$\sum_i n_i C_p = 3C_p, CO_2 + 4C_p, H_2O + 16.81 C_p, N_2 = 773.98 - 2.7E-2T + 3.78E-4T^2 - 1.425E-7T^3$$

$$\int_{298}^T \sum_i n_i C_p dT = 773.98 \left[T - \frac{2.7E-2}{2} T^2 \right]_{298}^T + \frac{3.78E-4}{3} \left[T^3 \right]_{298}^T - \frac{1.425E-7}{4} \left[T^4 \right]_{298}^T$$

$$\int_{298}^T \sum_i n_i C_p dT = -4.65E-8T^4 + 0.000126T^3 - 0.0135T^2 + 773.98T - 232641 \text{ J}$$

$$0 = \Delta H_{rxn} + \int_{298}^T \sum_i n_i C_p dT$$

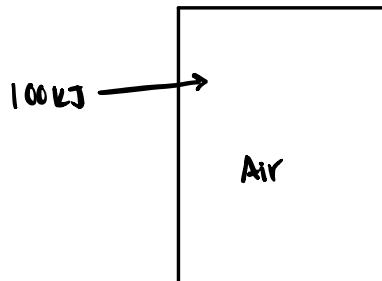
$$0 = -2041.190 \frac{\text{J/mol}}{\text{mol}} - 4.56E-8T^4 + 0.000126T^3 - 0.0135T^2 + 773.98T - 232641 \text{ J}$$

Solve for T \Rightarrow imaginary solutions b/c the heat capacity of nitrogen $\rightarrow \infty$ as T ↑.

Recommend Cp expressions from Perry's handbook.
If you use other source, T will range from 1000K to 3000K.

Problem 6 $H_f > < \neq 100 \text{ kJ}$?

$$\begin{aligned} dH &= dU + PdV + VdP \\ dU &= dQ + VdP = 100 \\ dH &= (100 \text{ kJ}) + (VdP) \\ \therefore dH &> dU \quad \boxed{H_f > 100 \text{ kJ}} \end{aligned}$$



$$V = \text{constant}, P = 2 \text{ bar}$$

The change in internal energy = 100 kJ because there is no work. By adding heat, $T \uparrow$ so $P \uparrow$. So, H is going to be dependent on the internal energy and the change in pressure. So H must be $> Q$

Problem 7

Second Law

$$\Delta S_{\text{eng}} = 0$$

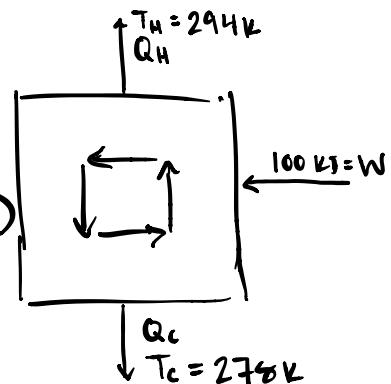
$$\frac{Q_c}{T_c} + \frac{Q_H}{T_H} = 0$$

$$\frac{Q_c}{278 \text{ K}} + \frac{Q_H}{294 \text{ K}} = 0$$

First Law

$$Q_H + Q_C + W = 0$$

$$Q_H = -(Q_C + W)$$



$$\text{Combine: } \frac{Q_c}{278 \text{ K}} + \frac{(-Q_c + W)}{294 \text{ K}} = 0 \Rightarrow 294Q_c = 278(Q_c + W)$$

$$1.06Q_c = Q_c + 100 \text{ kJ}$$

$$0.06Q_c = 1738 \text{ kJ}$$

$$Q_c = 1738 \text{ kJ}$$

$$Q_H = -1838 \text{ kJ}$$

$$\boxed{Q_H = 1838 \text{ kJ} \text{ heat added}}$$

The Carnot cycle achieves maximum efficiency, which implies maximum heat

Problem 8] if $P_{N_2} \downarrow, P_{Ar}, T_{Ar} = ?$

$$dU = Q + W \quad \text{insulated} \therefore \text{adiabatic}$$

$$dU = W = \int P dV$$

$$\Delta U \uparrow \therefore T \uparrow$$

Work is being done on the Ar as $P_{N_2} \uparrow$.
Therefore $dU \uparrow$. U is proportional to T so $\frac{T_{Ar} \uparrow}{\cancel{s}}$.

$P_{Ar} \uparrow$ because $T_{Ar} \uparrow$ as $V_{Ar} \downarrow$.

PISTON
(2kg, insulator)



equilibrium