



## Complex



# **AY-2025-2026 ODD SEM**

# Department of ECE

# **ANALOG ELECTRONIC CIRCUIT DESIGN**

## **23EC2|04**

## Topic:

# HYBRID MODEL FOR BJT CONFIGURATIONS-CE, CB, CC

# Session - 09

# SESSION CONTENT

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- Hybrid Model for BJT Configurations-CE, CB, CC

## AIM OF THE SESSION

To analyze and understand the Hybrid- $\pi$  model for the Common Emitter (CE), CB, CC configuration of a BJT and apply it in small-signal amplifier circuit analysis.



## INSTRUCTIONAL OBJECTIVES

The Session is designed to:



1. Explain the concept of the Hybrid- $\pi$  model for BJTs.
2. Identify the key elements of the Hybrid- $\pi$  equivalent circuit.
3. Describe the role of each parameter ( $r_{\pi}$ ,  $g_m$ ,  $r_o$ ) in CE, CB, CC configuration.
4. Apply the model to analyze small-signal behavior of CE, CB, CC amplifiers.

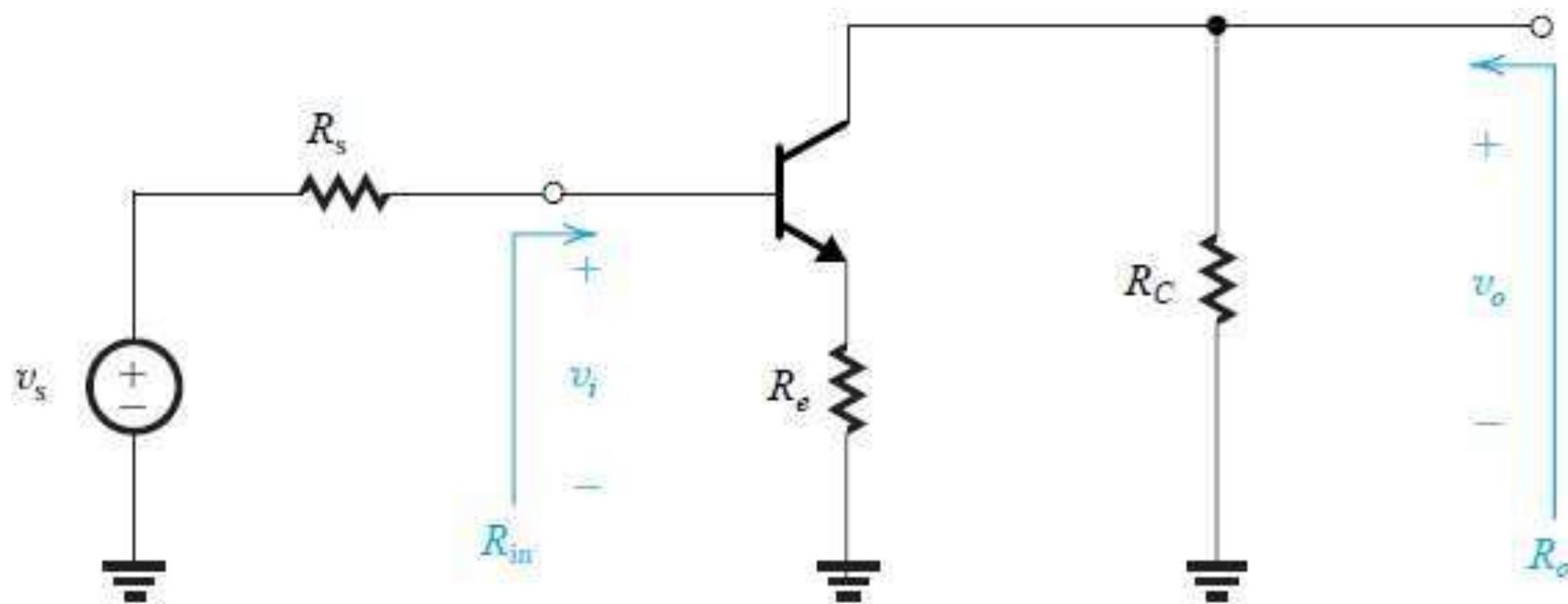
## LEARNING OUTCOMES



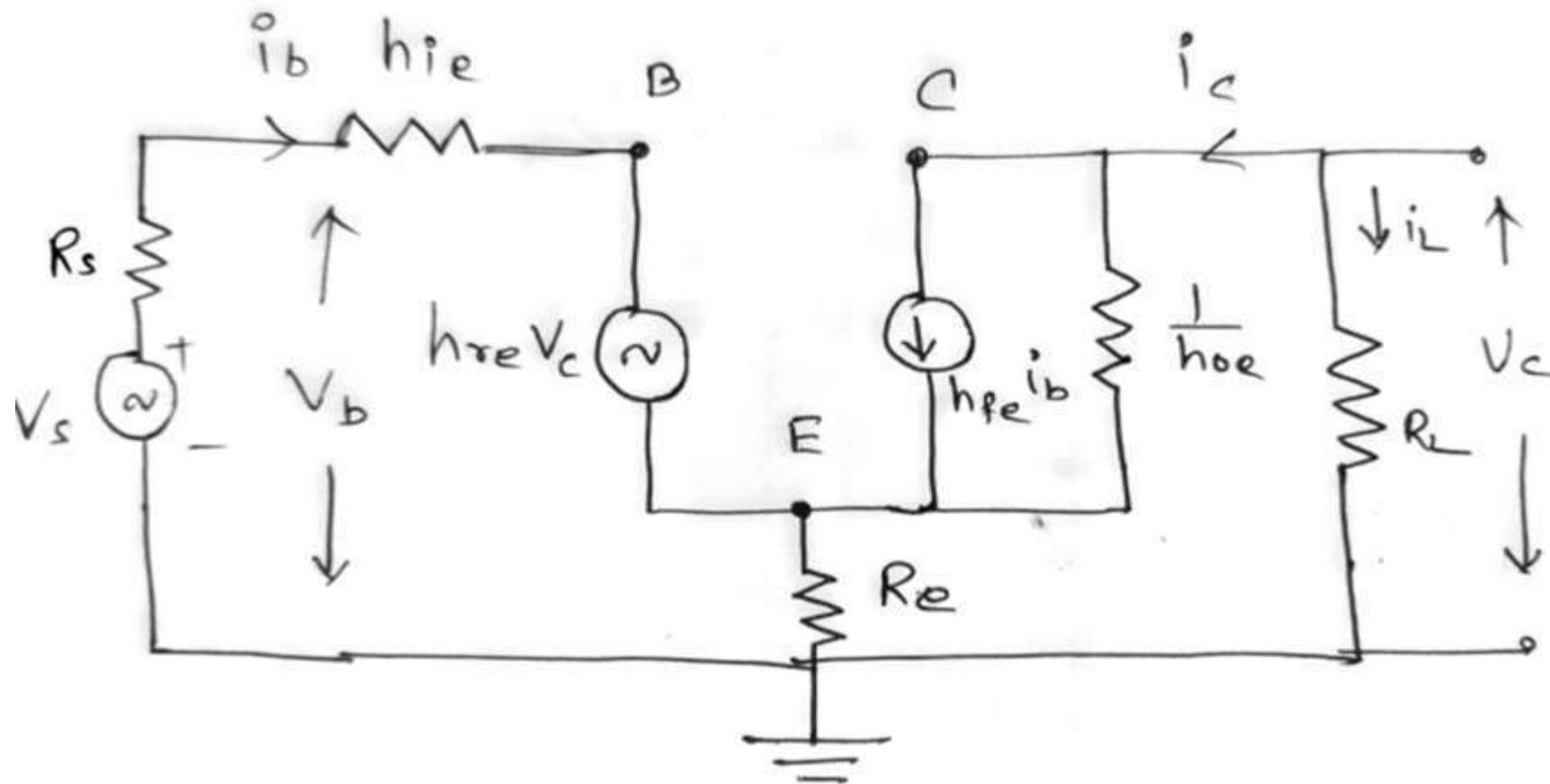
At the end of this session, learners will be able to:

1. Construct the Hybrid- $\pi$  equivalent circuit for a given BJT CE, CB, CC configuration.
2. Use the model to calculate small-signal parameters and performance metrics.
3. Understand how the base-emitter resistance ( $r_{\pi}$ ) and transconductance ( $g_m$ ) influence signal gain.

# CE Amplifier With Emitter Resistance



# CE Amplifier With Emitter Resistance (Using Hybrid Model)



# CE Amplifier With Emitter Resistance (Using Hybrid Model)

$$A_i = -\frac{h_{fe}}{1 + h_{oe}R_L}$$

$$R_i = \frac{V_b}{I_b} = h_{ie} + h_{re} A_i R_L$$

$$A_v = \frac{A_i R_L}{R_i}$$

$$Y_0 = h_{oe} - \frac{h_{fe}h_{re}}{R_s + h_{ie}} \text{ and } R_0 = \frac{1}{Y_0}$$

$$A_i = \frac{h_{oe}R_e - h_{fe}}{1 + h_{oe}(R_L + R_e)}$$

$$R_i = h_{ie} + h_{re} A_i (R_L + R_e) + R_e (1 - A_i) - R_e h_{re}$$

$$A_v = \frac{A_i R_L}{R_i}$$

$$R_0 = \frac{1 + h_{fe}}{h_{oe}} + \frac{(R_s + h_{ie})(1 + h_{oe}R_e)}{h_{oe}R_e} \text{ and } Y_0 = \frac{1}{R_0}$$

## Hybrid model

$$A_i = -\frac{h_{fe}}{1+h_{oe}R_L}$$

$$R_i = \frac{V_b}{I_b} = h_{ie} + h_{re} A_i R_L$$

$$A_v = \frac{A_i R_L}{R_i}$$

$$Y_0 = h_{oe} - \frac{h_{fe} h_{re}}{R_s + h_{ie}} \text{ and } R_0 = \frac{1}{Y_0}$$

## Approximate Hybrid model

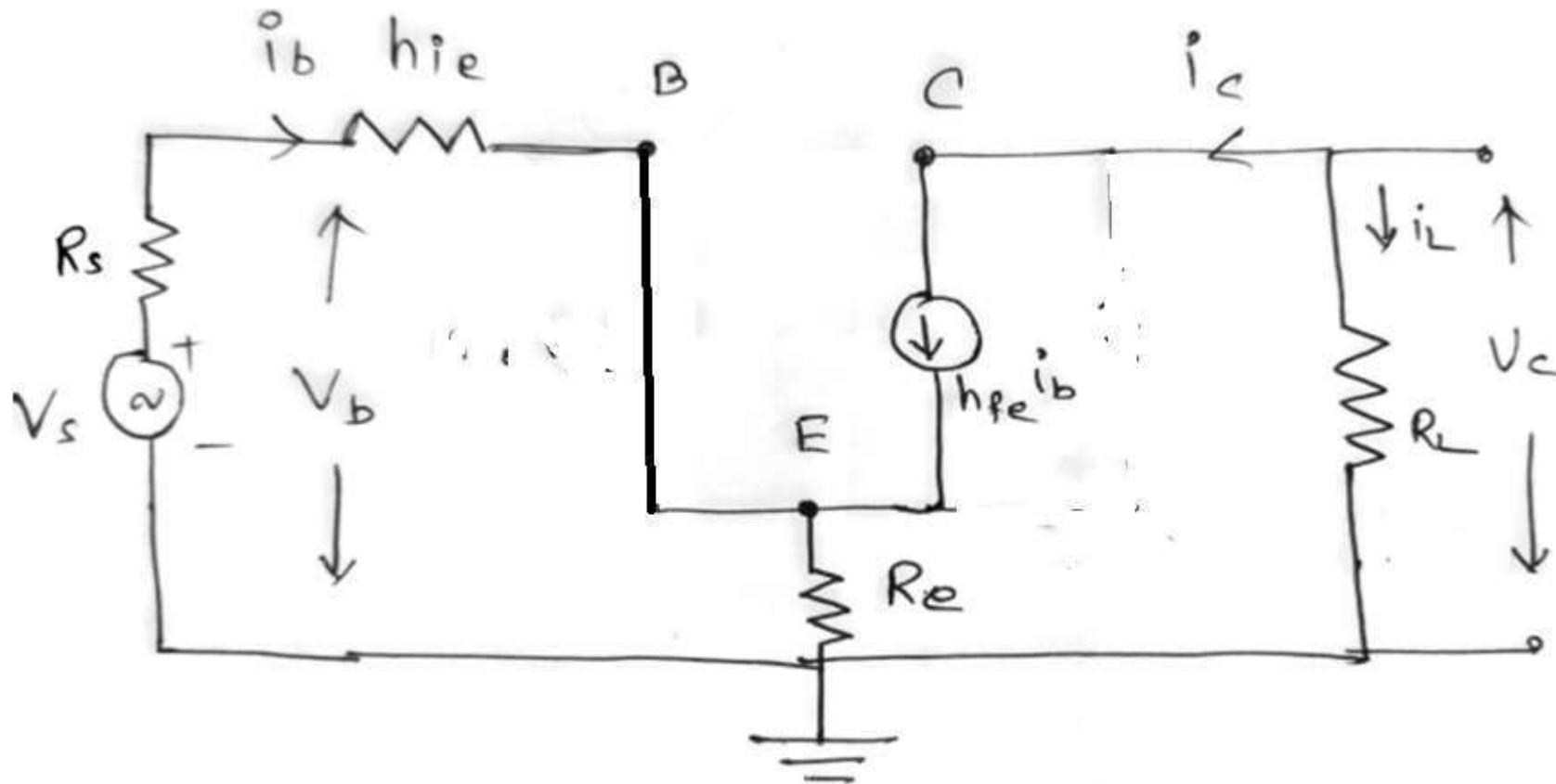
$$A_i = -h_{fe}$$

$$R_i = h_{ie} + (1+h_{fe})R_e$$

$$A_v = \frac{A_i R_L}{R_i} = \frac{-h_{fe} R_L}{h_{ie} + (1+h_{fe})R_e}$$

$$Y_0 = 0, \text{ and } R_0 = \infty$$

# CE Amplifier With Emitter Resistance (Using Approximate Hybrid Model)



# CE Amplifier With Emitter Resistance (Using Approximate Hybrid Model)

$$A_i = \frac{h_{oe}R_e - h_{fe}}{1 + h_{oe}(R_L + R_e)}$$

$$R_i = h_{ie} + h_{re}A_i(R_L + R_e) + R_e(1 - A_i) - R_e h_{re}$$

$$A_v = \frac{A_i R_L}{R_i}$$

$$R_0 = \frac{1 + h_{fe}}{h_{oe}} + \frac{(R_s + h_{ie})(1 + h_{oe}R_e)}{h_{oe}R_e} \text{ and } Y_0 = \frac{1}{R_0}$$

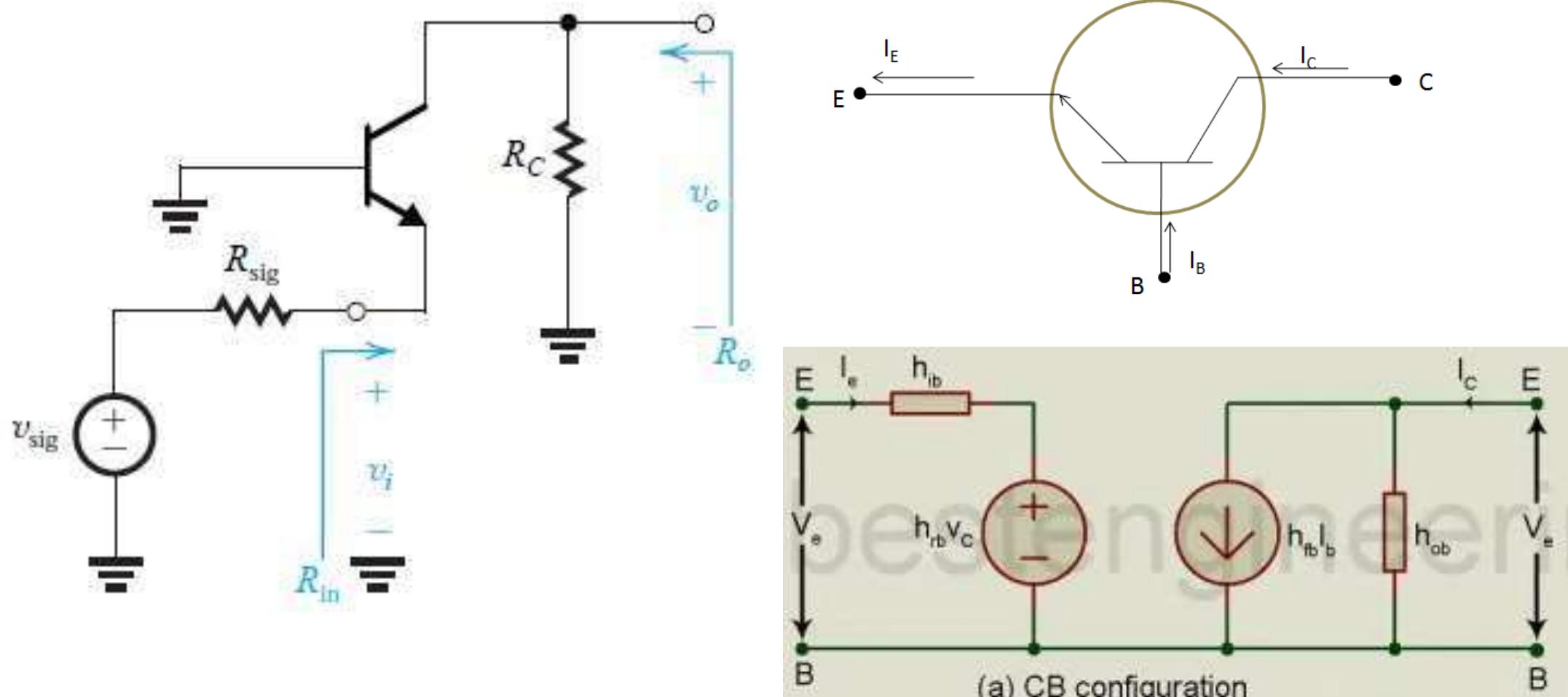
$$A_i = -h_{fe}$$

$$R_i = h_{ie} + (1 + h_{fe})R_e$$

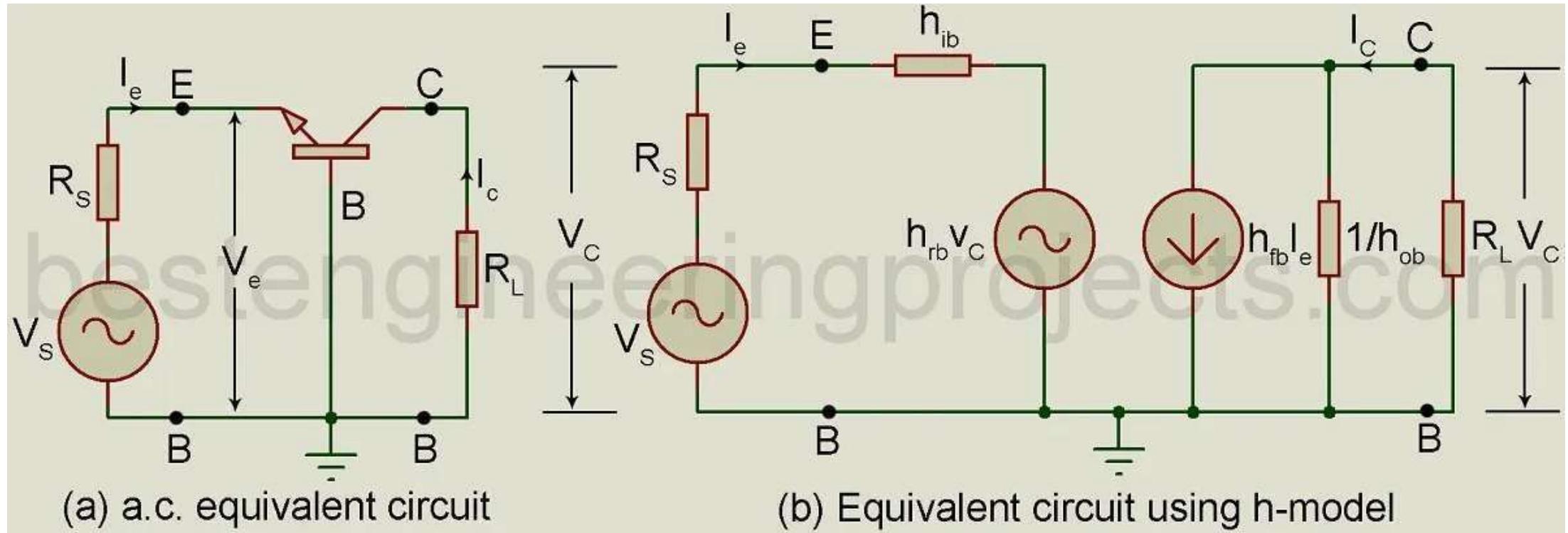
$$A_v = \frac{A_i R_L}{R_i} = \frac{-h_{fe} R_L}{h_{ie} + (1 + h_{fe})R_e}$$

$$Y_0 = 0, \text{ and } R_0 = \infty$$

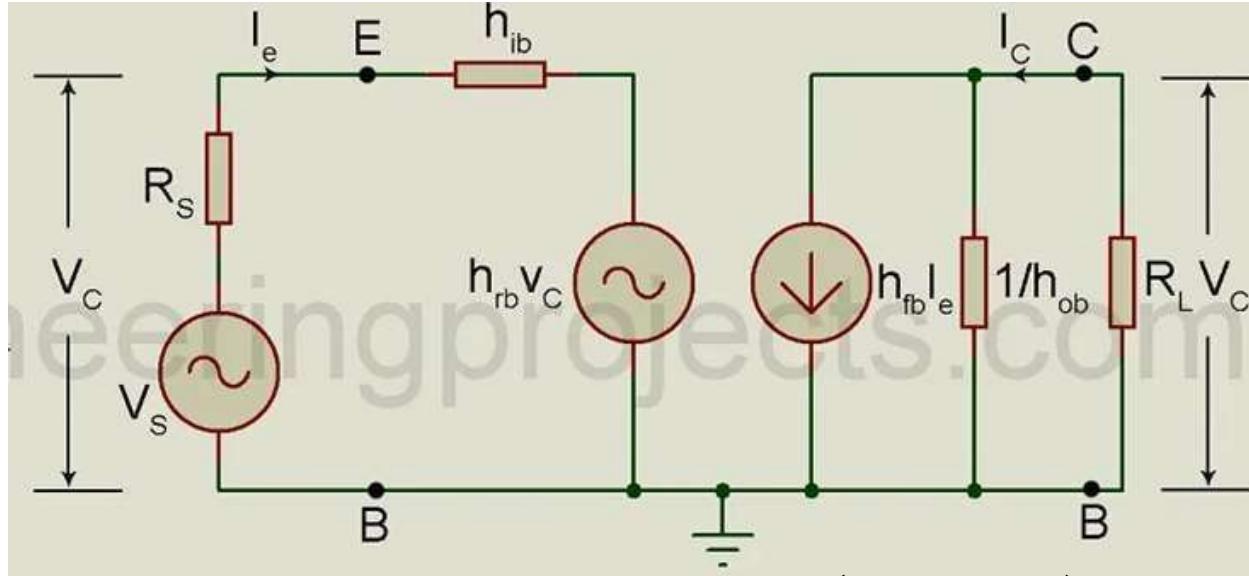
# CB Amplifier(Using Hybrid Model)



# CB Amplifier(Using Hybrid Model)



# CB Amplifier (Using Hybrid Model)



$$A_i = \frac{\dot{i}_L}{\dot{i}_e} = -\frac{\dot{i}_c}{\dot{i}_e}$$

$$\dot{i}_c = h_{fb}\dot{i}_e + h_{ob}V_c$$

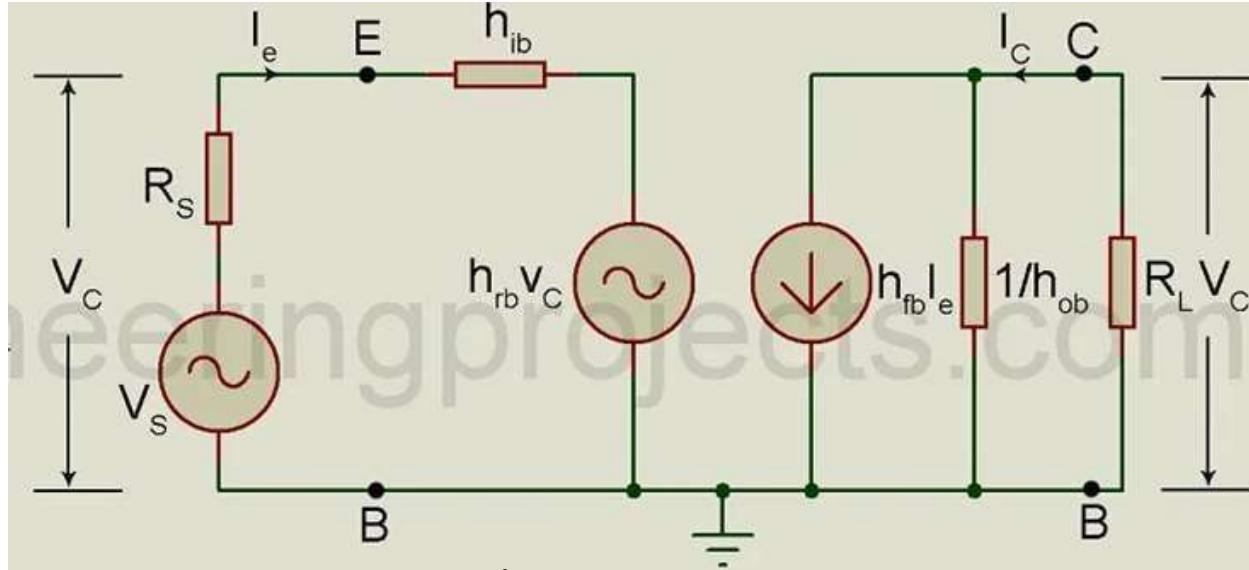
$$V_c = \dot{i}_L R_L = -\dot{i}_c R_L$$

$$\dot{i}_c = h_{fb}\dot{i}_e + h_{ob}(-\dot{i}_c R_L)$$

$$\dot{i}_c(1 + h_{ob}R_L) = h_{fb}\dot{i}_e$$

$$A_i = \frac{\dot{i}_c}{\dot{i}_e} = -\frac{h_{fb}}{1 + h_{ob}R_L}$$

# CB Amplifier (Using Hybrid Model)



$$R_i = \frac{V_e}{i_e}$$

$$V_e = h_{ib} i_e + h_{rb} V_c$$

But,  $A_i = -\frac{i_c}{i_e} \Rightarrow i_c = -A_i i_e$

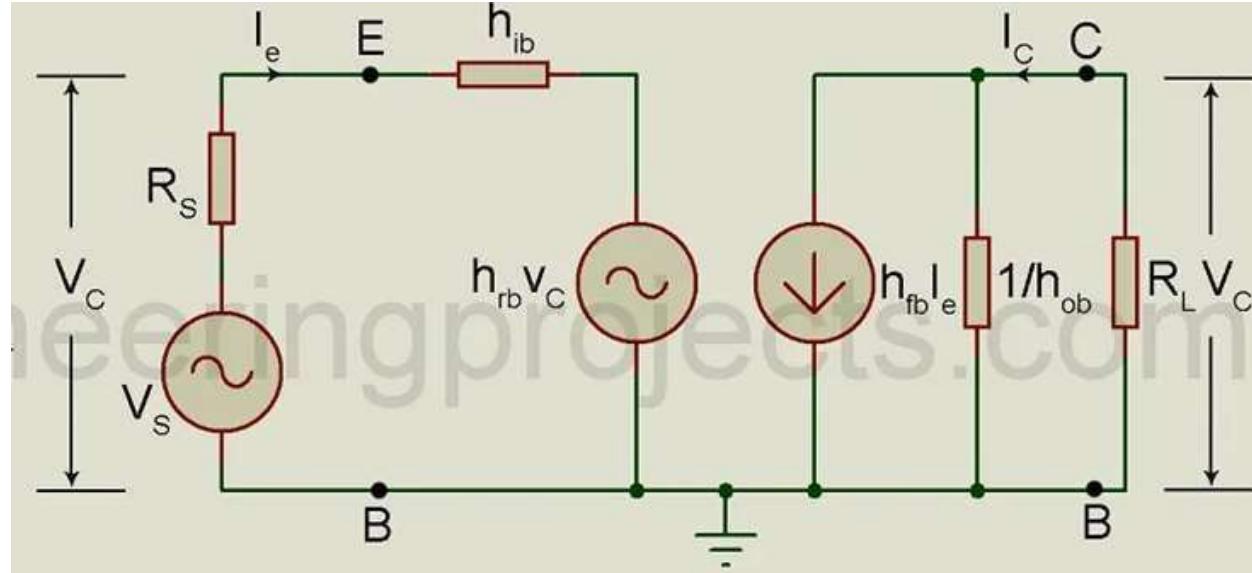
$$V_c = i_c R_L = -i_c R_L = A_i i_e R_L$$

$$V_e = h_{ib} i_e + h_{rb} (A_i i_e R_L)$$

$$V_e = i_e (h_{ib} + h_{rb} A_i R_L)$$

$$\Rightarrow R_i = \frac{V_e}{i_e} = h_{ib} + h_{rb} A_i R_L$$

# CB Amplifier (Using Hybrid Model)



$$A_v = \frac{V_c}{V_e}$$

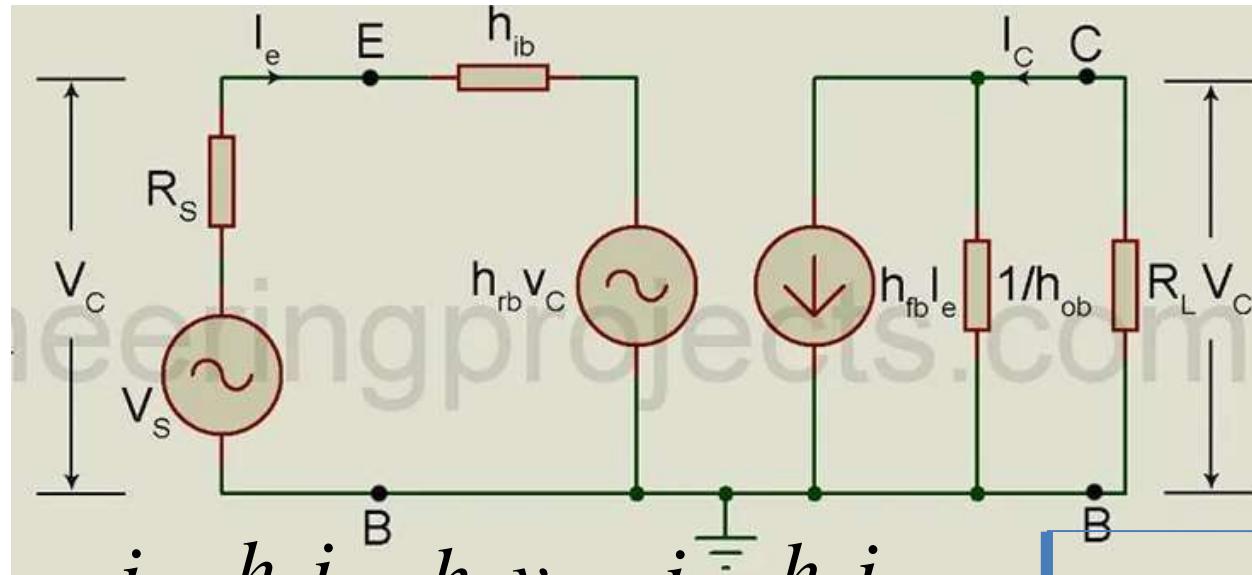
But,  $A_i = -\frac{i_c}{i_e} \Rightarrow i_c = -A_i i_e$

$$V_c = i_c R_L = -i_c R_L = A_i i_e R_L$$

$$\frac{1}{R_i} = \frac{i_e}{V_e}$$

$$\Rightarrow A_v = \frac{V_c}{V_e} = \frac{A_i i_e R_L}{V_e} = \frac{A_i R_L}{R_i}$$

# CB Amplifier (Using Hybrid Model)



$$\frac{i_c}{V_c} = \frac{h_{fb}i_e}{V_c} + \frac{h_{ob}V_c}{V_c} \Rightarrow \frac{i_c}{V_c} = \frac{h_{fb}i_e}{V_c} + h_{ob}$$

$$V_s = 0, R_s i_e + h_{ib} i_e + h_{rb} V_c = 0$$

$$(R_s + h_{ib}) i_e = -h_{rb} V_c$$

**Output Admittance  $Y_o$**

$$Y_o = \frac{i_c}{V_c}$$

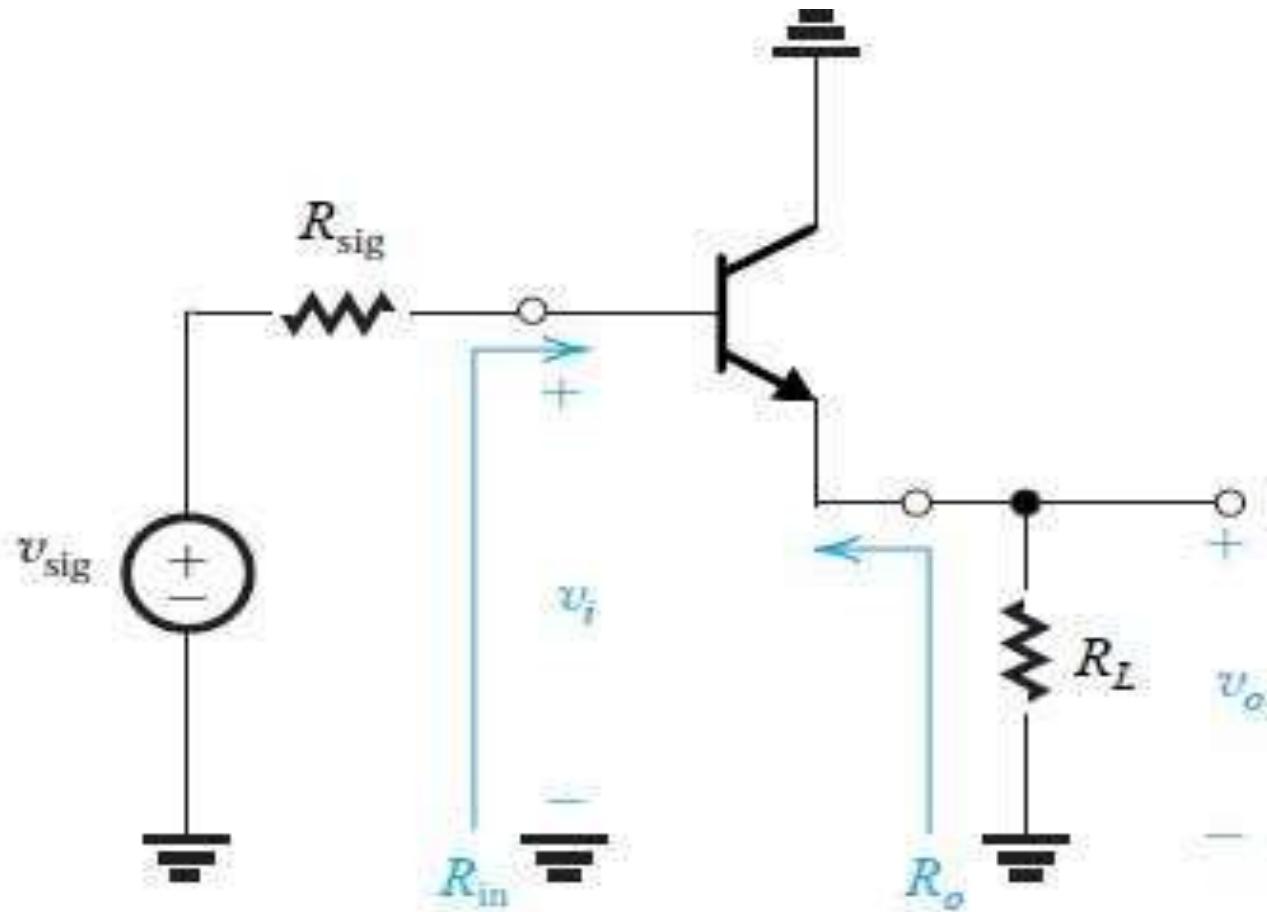
$$i_c = h_{fb}i_e + h_{ob}V_c$$

**Dividing By  $V_c$**

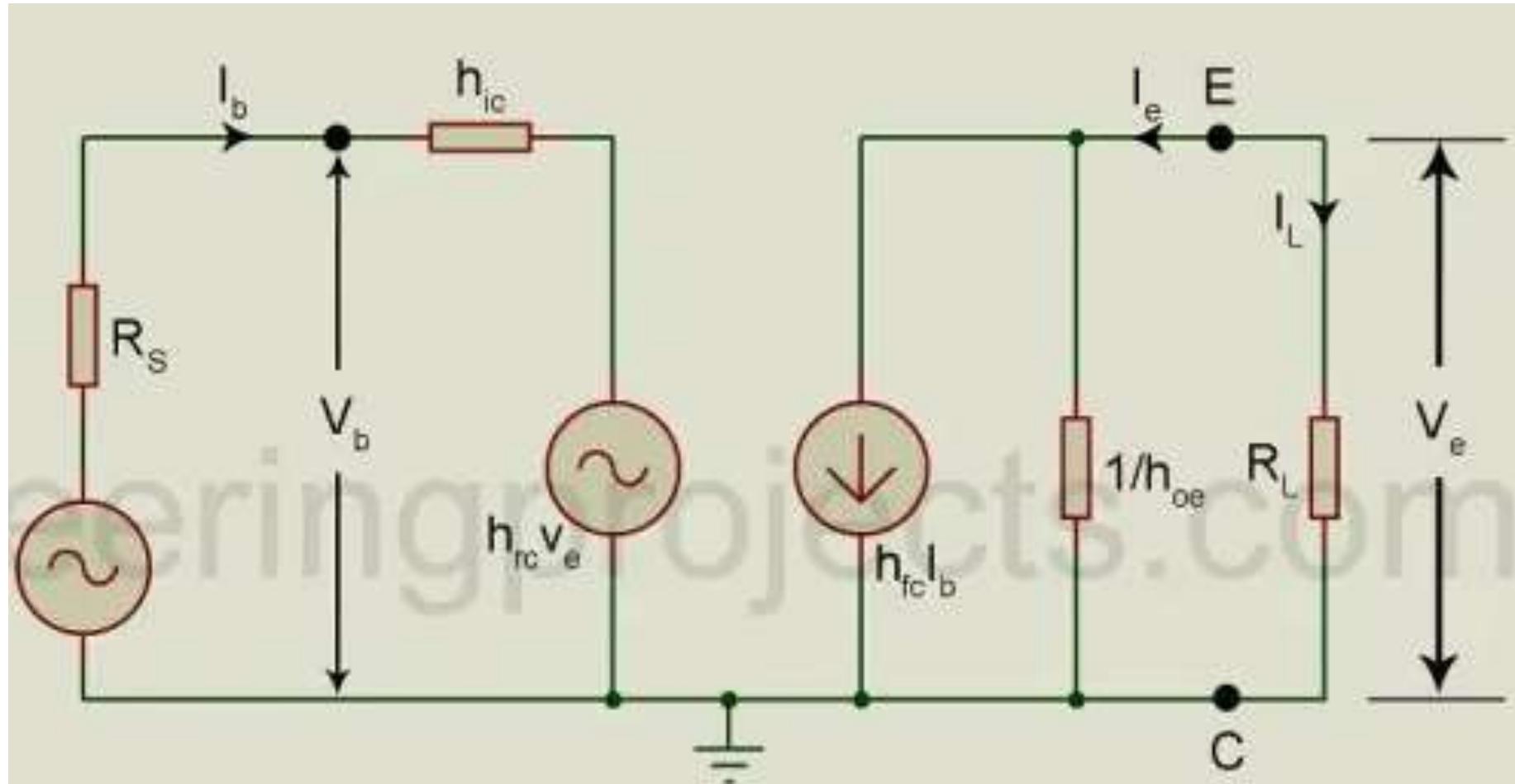
$$\Rightarrow \frac{i_e}{V_c} = -\frac{h_{rb}}{R_s + h_{ib}}$$

$$\Rightarrow Y_o = h_{ob} - \frac{h_{fb}h_{rb}}{R_s + h_{ib}} \text{ and } R_o = \frac{1}{Y_o}$$

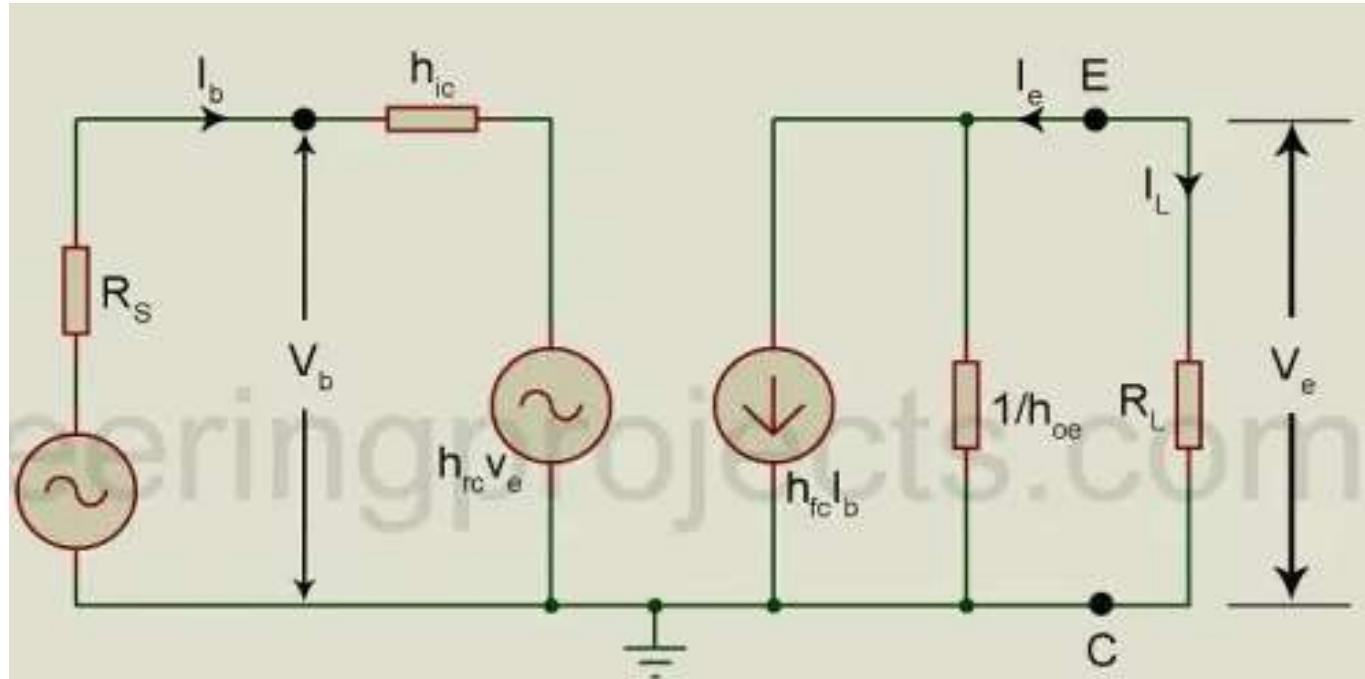
# CC Amplifier(Using Hybrid Model)



# CB Amplifier(Using Hybrid Model)



# CB Amplifier (Using Hybrid Model)



$$A_i = \frac{\dot{i}_L}{\dot{i}_b} = -\frac{\dot{i}_e}{\dot{i}_b}$$

$$\dot{i}_e = h_{fc} \dot{i}_b + h_{oc} v_e$$

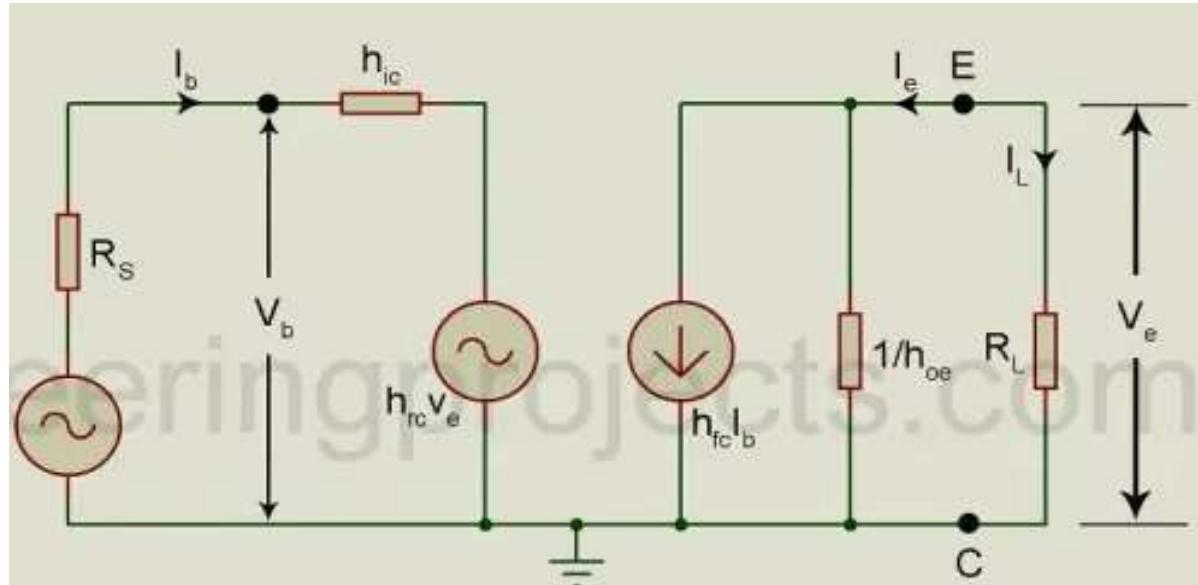
$$v_c = \dot{i}_L R_L = -\dot{i}_e R_L$$

$$\dot{i}_e = h_{fc} \dot{i}_b + h_{oc} (-\dot{i}_e R_L)$$

$$\dot{i}_e (1 + h_{oc} R_L) = h_{fc} \dot{i}_b$$

$$A_i = \frac{\dot{i}_e}{\dot{i}_b} = -\frac{h_{fc}}{1 + h_{oc} R_L}$$

# CB Amplifier (Using Hybrid Model)



$$R_i = \frac{V_b}{i_b}$$

$$V_b = h_{ic} i_b + h_{rc} V_e$$

But,  $A_i = -\frac{i_e}{i_b} \Rightarrow i_e = -A_i i_b$

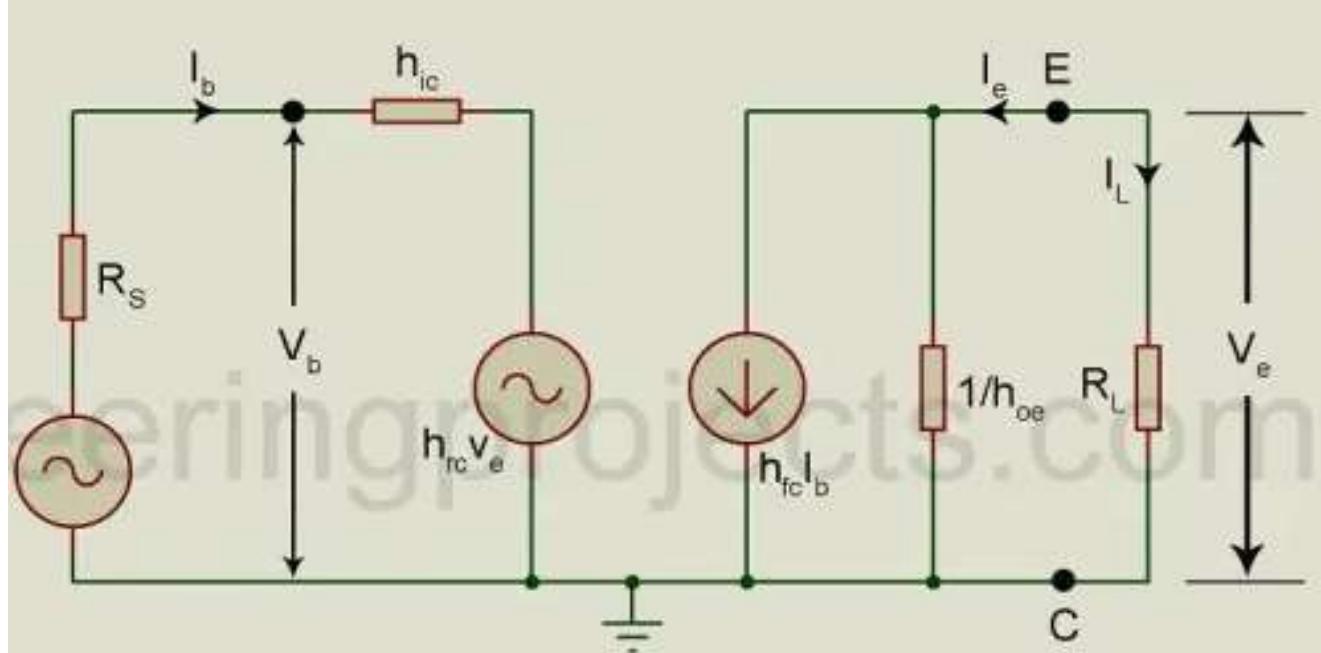
$$V_e = i_e R_L = -i_e R_L = A_i i_b R_L$$

$$V_b = h_{ic} i_b + h_{rc} (A_i i_b R_L)$$

$$V_b = i_b (h_{ic} + h_{rc} A_i R_L)$$

$$\Rightarrow R_i = \frac{V_b}{i_b} = h_{ic} + h_{rc} A_i R_L$$

# CB Amplifier (Using Hybrid Model)



$$A_v = \frac{V_e}{V_b}$$

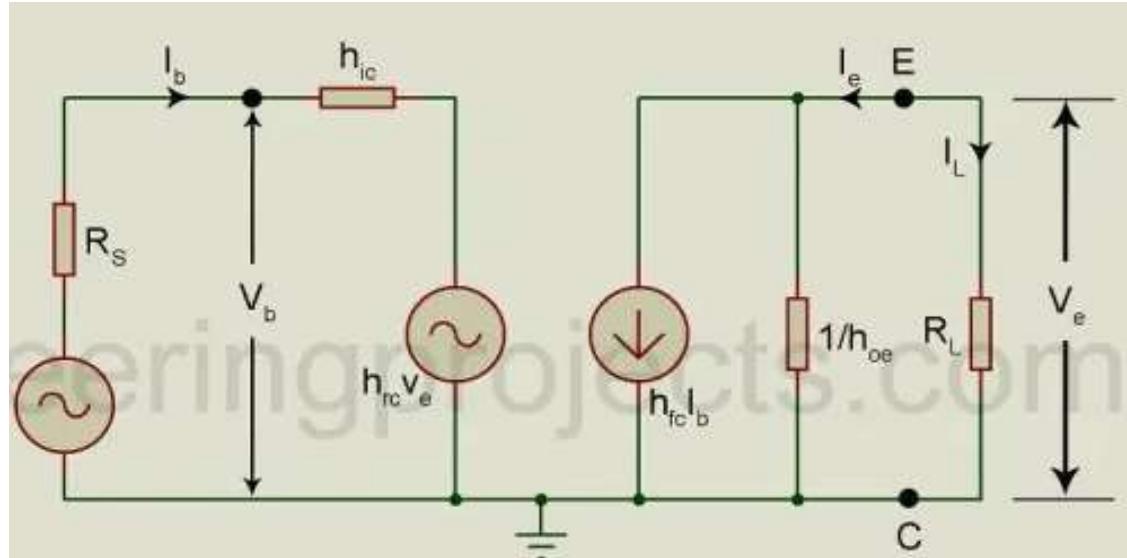
But,  $A_i = -\frac{i_e}{i_b} \Rightarrow i_e = -A_i i_b$

$$V_e = i_L R_L = -i_e R_L = A_i i_b R_L$$

$$\frac{1}{R_i} = \frac{i_b}{V_b}$$

$$\Rightarrow A_v = \frac{V_e}{V_b} = \frac{A_i i_b R_L}{V_b} = \frac{A_i R_L}{R_i}$$

# CB Amplifier (Using Hybrid Model)



$$\frac{i_e}{v_e} = \frac{h_{fc} i_b}{v_e} + \frac{h_{oc} v_e}{v_e} \Rightarrow \frac{i_e}{v_e} = \frac{h_{fc} i_b}{v_e} + h_{oc}$$

$$v_s = 0, R_s i_b + h_{ic} i_b + h_{rc} v_e = 0$$

$$(R_s + h_{ic}) i_b = -h_{rc} v_e$$

**Output Admittance  $Y_o$**

$$Y_o = \frac{i_e}{v_e}$$

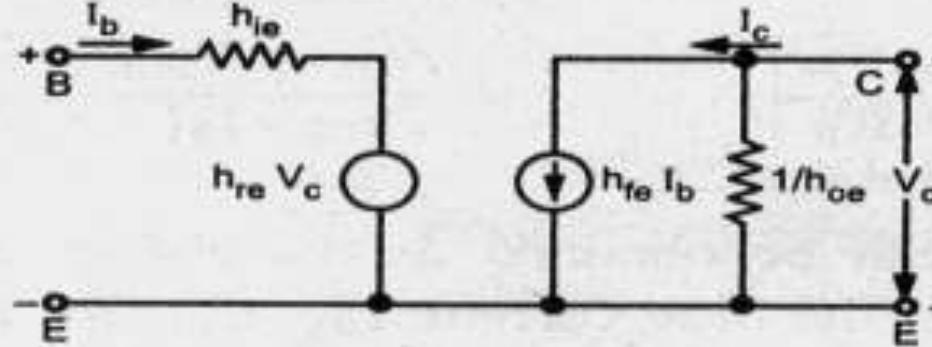
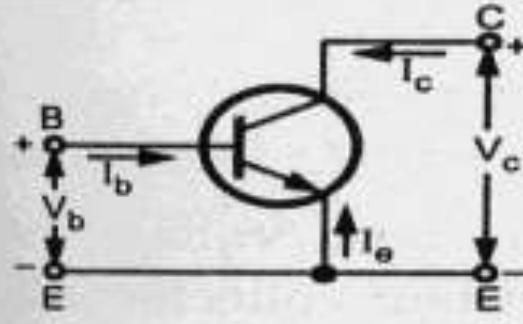
$$i_e = h_{fc} i_b + h_{oc} v_e$$

**Dividing By  $V_e$**

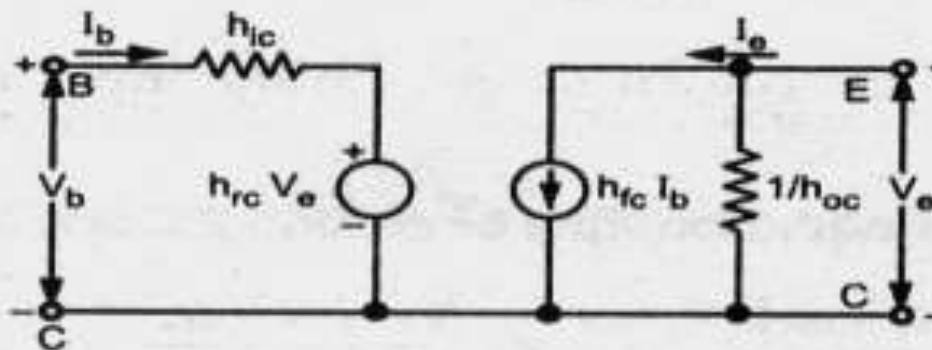
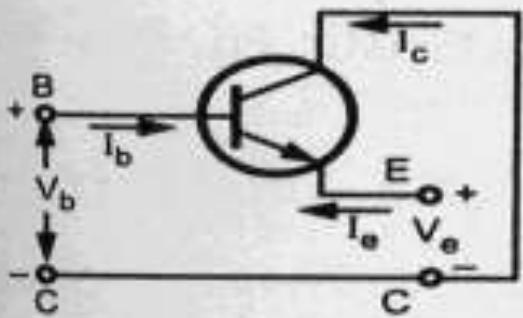
$$\Rightarrow \frac{i_b}{v_e} = -\frac{h_{rc}}{R_s + h_{ic}}$$

$$\Rightarrow Y_o = h_{oc} - \frac{h_{fc} h_{rc}}{R_s + h_{ic}} \text{ and } R_o = \frac{1}{Y_o}$$

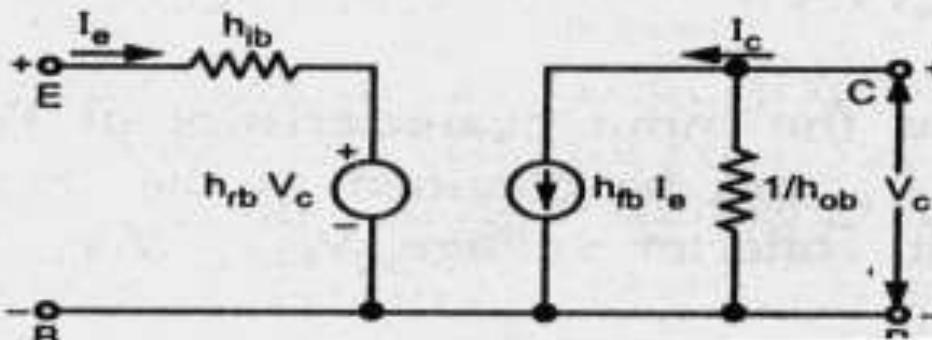
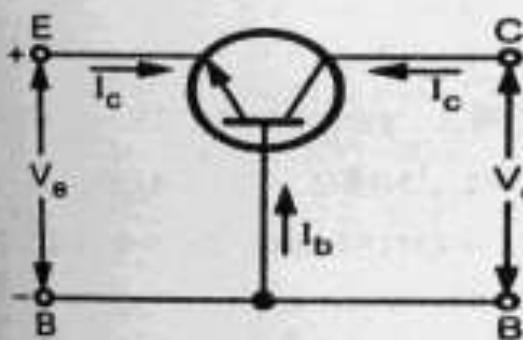
Hybrid Model and Equations for the transistor in three different configurations are given below.



$$\begin{aligned} & \text{CE} \\ & V_b = h_{ie} I_b + h_{re} V_c \\ & I_c = h_{fe} I_b + h_{oe} V_c \end{aligned}$$



$$\begin{aligned} & \text{CC} \\ & V_b = h_{ic} I_b + h_{rc} V_e \\ & I_e = h_{fc} I_b + h_{oc} V_e \end{aligned}$$



$$\begin{aligned} & \text{CB} \\ & V_e = h_{ib} I_e + h_{rb} V_c \\ & I_c = h_{fb} I_e + h_{ob} V_c \end{aligned}$$

# Conversion Formulae for Hybrid Parameters

CE to CB h-parameters	CE to CC h-parameters	CE h-parameters to r-parameters
$h_{ib} \approx \frac{h_{ie}}{1 + h_{fe}}$	$h_{ic} = h_{ie}$	$\alpha \approx \frac{h_{fe}}{1 + h_{fe}}$
$h_{rb} \approx \frac{h_{ie} h_{oe}}{1 + h_{fe}} \cdot h_{re}$	$h_{rc} = 1 - h_{re}$	$r_c = \frac{1 + h_{fe}}{h_{oe}}$
$h_{fb} \approx \frac{h_{fe}}{1 + h_{fe}}$	$h_{fc} = 1 + h_{fe}$	$r_e = \frac{h_{ie}}{1 + h_{fe}} \approx r'_e$
$h_{ob} \approx \frac{h_{oe}}{1 + h_{fe}}$	$h_{oc} = h_{oe}$	$r_b = h_{ie} - \frac{h_{re}(1 + h_{fe})}{h_{oe}}$
		$r_n = h_{ie}$
		$\beta = h_{fe}$

TABLE 11.4

<i>Configuration Parameter</i>	<i>Common Emitter, CE</i>	<i>Common Base, CB</i>	<i>Common Collector, CC</i>	<i>Equivalent T-Circuit</i>
$h_{ie}$	1.1 k $\Omega$	$\frac{h_{ib}}{1+h_{fb}}$	$h_{ic}^*$	$r_b + \frac{r_e}{1-a}$
$h_{re}$	$2.5 \times 10^{-4}$	$\frac{h_{ib} h_{ob}}{1+h_{fb}} - h_{rb}$	$1-h_{rc}^*$	$\frac{r_e}{r_c(1-a)}$
$h_{fe}$	50	$-\frac{h_{fb}}{1+h_{fb}}$	$-(1+h_{fe})^*$	$\frac{a}{1-a}$
$h_{oe}$	$25 \mu\text{S}$ ( $\mu\text{A/V}$ )	$\frac{h_{ob}}{1+h_{fb}}$	$h_{oc}^*$	$\frac{1}{r_c(1-a)}$
$h_{ib}$	$\frac{h_{ie}}{1+h_{fe}}$	21.6 $\Omega$	$-h_{ie}/h_{fe}$	$r_e + (1-a) r_b$
$h_{rb}$	$\frac{h_{ie} h_{oe}}{1+h_{fe}} - h_{re}$	$2.9 \times 10^{-4}$	$h_{rc} - \frac{h_{ic} h_{oc}}{h_{fe}} - 1$	$r_b/r_c$
$h_{fb}$	$-\frac{h_{fe}}{1+h_{fe}}$	-0.98	$-\frac{1+h_{fe}}{h_{fe}}$	$-a$
$h_{ob}$	$\frac{h_{oe}}{1+h_{fe}}$	0.49 $\mu\text{S}$ ( $\mu\text{A/V}$ )	$-\frac{h_{oc}}{h_{fe}}$	$1/r_c$
$h_{ic}$	$h_{ie}^*$	$\frac{h_{ib}}{1+h_{fb}}$	1.1 k $\Omega$	$r_b + \frac{r_e}{1-a}$
$h_{rc}$	$1-h_{re}=1^*$	1	1	$1 - \frac{r_e}{r_c(1-a)}$
$h_{fc}$	$-(1+h_{fe})^*$	$-\frac{1}{1+h_{fb}}$	-51	$-\frac{1}{1-a}$
$h_{oc}$	$h_{oe}^*$	$\frac{h_{ob}}{1+h_{fb}}$	25 $\mu\text{S}$ ( $\mu\text{A/V}$ )	$\frac{1}{r_c(1-a)}$
$a$	$\frac{h_{fe}}{1+h_{fe}}$	$-h_{fb}$	$\frac{1+h_{fe}}{h_{fe}}$	0.98
$r_c$	$\frac{1+h_{fe}}{h_{oe}}^*$	$\frac{1}{h_{ob}}$	$-\frac{h_{fc}}{h_{oc}}^*$	2.04 M $\Omega$
$r_e$	$\frac{h_{re}}{h_{oe}}^*$	$h_{ib} - \frac{h_{ib}}{h_{ob}} (1+h_{fb})^*$	$\frac{1-h_{rc}}{h_{oc}}^*$	10 $\Omega$
$r_b$	$h_{ie} - \frac{h_{re}}{h_{oe}} (1+h_{fe})^*$	$\frac{h_{rb}}{h_{ob}}^*$	$h_{ic} + \frac{h_{fc}}{h_{oc}} (1-h_{rc})^*$	590 $\Omega$

\* Stands for exact.