

filters ~ an implementation either in software or hardware to reduce noise or unwanted response from a system's input. (@ RTG)

→ filters for rangefinders → Rolling average (Moving Average), Kalman filter, Standard Deviation, Median Filter, Distance filter??

* Moving Average: smooths out the irregularity occurring in data

↳ main types → Simple Moving Average (SMA) → Cumulative Moving Average (CMA)
↳ Exponential Moving Average (EMA)
↳ Weighted Moving Average (WMA)

↳ time series constructed by taking averages of several sequential values of another time series.

→ type of mathematical convolution

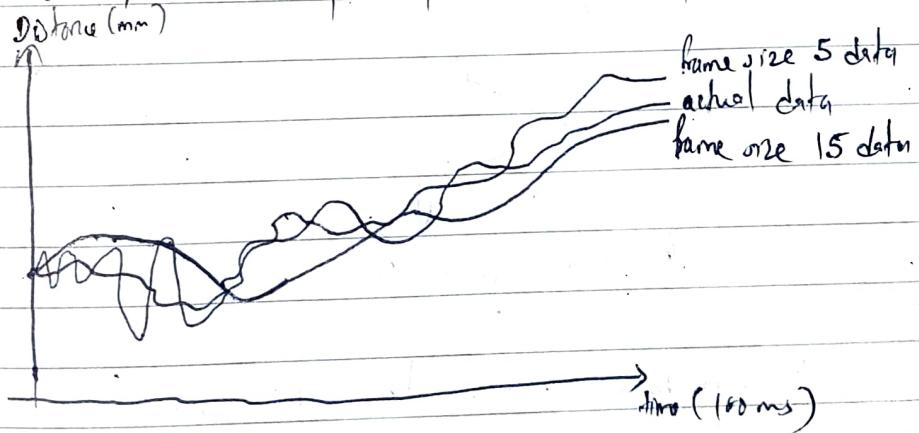
→ finite impulse response filter / low pass filter

→ typical for 1D signal model ??

→

* Algorithm:

→ select frame size (no. of elements in an array i.e. no. of data to be averaged)
less the frame size, more responsive the output is, bigger the frame size, less resp. responsive the output is.



→ save the values in an array and average them

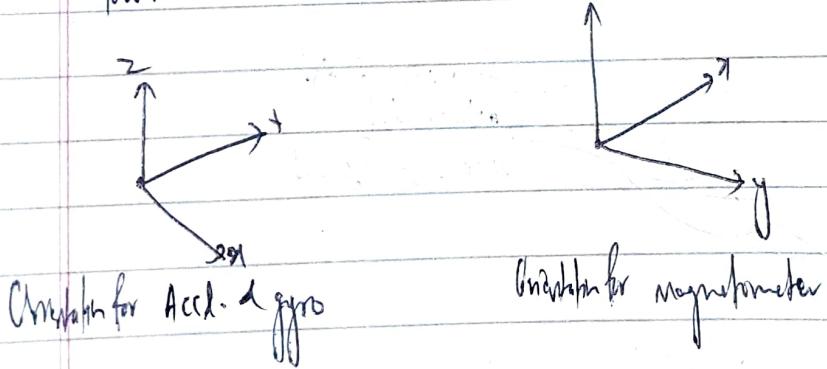
→ take next input as the last element move the other elements down the array.

→ output average and continue the last step.

MPU9250 :

- motion tracking device
- 3-axis gyroscope / 3-axis accelerometer / 3-axis magnetometer
- two dies in a single package → 1 die has gyro + accelerometer
→ 1 die has magnetometer (AK8963)
- Thus, 9-dof sensor (10-dof if barometer is added to auxiliary I₂C bus.)
- 3 16-bit ADCs for each output ~ total 9 ADCs of 16 bits
- Gyro range : ±250, ±500, ±1000, ±2000 dps
- Acc. range : ±2g, ±4g, ±8g and ±16g
- Mag. range : ±4800 uT
- Inbuilt digital filters with 10% drift from -40° to 85°C
- embedded temp. sensor
- support both I₂C & SPI interfaces
- I₂C at 400 kHz & SPI at 1MHz { (1-20) MHz over 8bit }

Note : typically, motion processing algorithms should be run at a higher rate; often around 200Hz in order to provide accurate results with low latency. This is required even if the application updates at a much lower rate



- * Selection of gyro scale: → should be able to handle the rotational speed of micromotor
→ (Rpm of motor is 650 rpm)

scale !: ±250 dps $\Rightarrow \frac{250}{360} \times 60 = 41.6 \text{ rpm}$

! ±500 dps $\frac{500}{3600} \times 60 = 83.3 \text{ rpm}$

$$\text{Scale 8: } \pm 1000 \text{ dPS} = \frac{1000}{310} \times 60 = 166.4 \text{ rpm}$$

$$\frac{1}{2} 2\pi n \text{dps} = \frac{2000}{360} \times 60 = 332.8 \text{ rpm}$$

Rotational speed of the micromixer stir: 100 to 300 rpm (limit st^2)

If selection of acceleration range: should be able to handle the acceleration the robot is moving with (force associated with acceleration)

Scale: 1 : $\pm 2g$ = dot experiencing 2 times the force of gravity.

scale 3 ± 8 g : " " 8 4 " 6 " 2 " 1 " 1 "

greatest integer function

ACR ✓

* Post data calculations: (after reading raw data):

→ raw data is simply the off of 16bit ADCs of the corresponding sensors.

→ for accelerometers: sensitivity is defined in LSB/g:

$\pm 2g$	16384	LJB/g
$\pm 4g$	8192	LJB/g
$\pm 8g$	4096	LJB/g
$\pm 16g$	2048	LJB/g

So, real data in g is: raw-data | (LSB1g);

Ex: for $\pm 1\sigma$: raw data | 2048; \Rightarrow g's
 $\text{raw data} = 12,000$;

$$\text{value in g} = 12,000 / 2048 = 5.85 \text{ g}$$

Note: Trade-off between sensitivity and range; optimum use is to select lowest possible scales for each sensor

for gyro: value in degrees per second = raw-data / (188/dps)

± 250 dps	131
± 500 dps	65.5
± 1000 dps	32.8
± 2000 dps	16.4

Example: Select scale 4: ± 2000 dps: suppose raw data is 32,000

$$\text{value in dps} = 32,000 / 16.4 \\ = 1951.21 \text{ dps}$$

* Degrees per second to degrees

$$\text{dps } f(t) = \frac{d\theta}{ds} = \text{output of sensor data in dps}$$

$$\text{Integrating: } \int f(t) \times ds = \int d\theta$$

$$\Rightarrow \theta = \int f(t) \times ds$$

= integration of sensor data with net time

Code: $\text{degrees} = \text{value in dps} \times \text{time of refresh}$

* for better results: $\frac{1}{\text{Time of refresh}} \geq 250 \text{ Hz}$

$$\text{Time of refresh} \geq \frac{1}{250}$$

$$\text{Time of refresh} \geq \frac{1}{250}, 4 \times 10^{-3} \text{ seconds} = 4000 \mu\text{s} = 4 \text{ ms}$$

$$\text{from above example: degrees} = 1951.21 / 250 \\ = 7.80^\circ$$

$$\text{on degrees} = 1951.21 \times 4 \times 10^{-3} \\ = 8.88^\circ$$

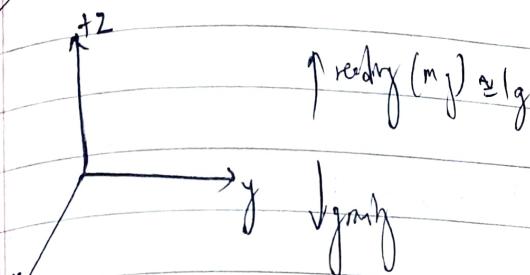
for integration:

~~$$\text{new_degree} = \text{previous degree} + 4 \times 10^{-3} + \text{new previous degree};$$~~
~~$$\text{previous_degree} = \text{degree};$$~~

$$\text{new_degree} = \text{new_degree} + \text{previous degree} \times 4 \times 10^{-3};$$

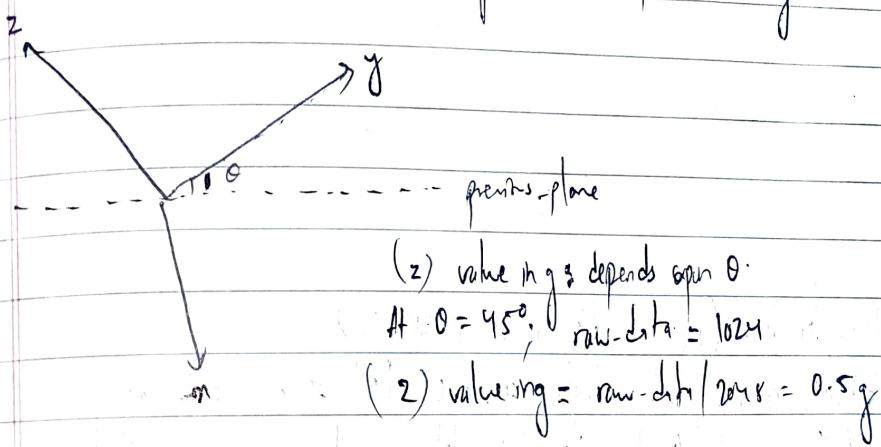
- gyro accumulates error with time (integral error)
- needs to be solved before use (solved by using reference of acc(moto))
- (roll, pitch, yaw) some calculations

* Accelerometer calculations:



As in our previous example: $hw \pm 16g$: raw_data = 2048

$$(2) \text{ value in } g = \text{raw_data} / 2048 = 1g$$



(2) value in g depends upon θ .

$$\text{At } \theta = 45^\circ, \text{ raw_data} = 1024$$

$$(2) \text{ value in } g = \text{raw_data} / 2048 = 0.5g$$

Using pythagoras theorem; $h^2 = p^2 + b^2$

$$\text{Here, } h^2 = (1024)^2$$



$$z^2 = x^2 + y^2$$

$$\text{Also, } \tan \theta = \frac{y}{x} = \frac{y}{z} \Rightarrow \tan 45^\circ = \frac{y}{z} \Rightarrow x = y$$

$$\therefore h^2 = x^2 + z^2$$

$$1024^2 = 2x^2$$

$$\therefore \theta = \tan^{-1} \frac{y}{x} = \sin^{-1} \frac{y}{\sqrt{x^2 + z^2}} = \cos^{-1} \frac{z}{\sqrt{x^2 + z^2}}$$

$$y = 724.07 = z$$

* (for a moving body; the acceleration should be normalized; ??)

$$\text{total_acceleration}(\alpha) = \sqrt{x^2 + y^2 + z^2} \quad \text{where } \alpha = \text{value at } n\text{-axis in g}$$

$$y = " " \quad y-a_{axis} " " g$$

$$z = " " \quad z-a_{axis} " " g$$

$$\text{for pitch: } \sin^{-1}\left(\frac{y}{g}\right) \quad (\text{in radians})$$

$$\text{for roll: } \sin^{-1}\left(\frac{z}{g}\right) \quad (\text{in radians})$$

(use complementary filter to compensate gyro drift:)

~~AK8963 magnetometer~~

⇒ calibration for first raw data (raw, pitch, calculate roll & angle & compensate drift)

AK8963 Magnetometer: (separate die made MPU9250)

- 3-axis electronic compass with high sensitive hall sensor technology
- Built-in ADC ⇒ 14/16 bit selectable data output for each axis
- Sensitivity: 0.6 μT / LSB (14 bit)
0.15 μT / LSB (16 bit)
- DRDY access for measurement ready
- Magnet sensor overflow monitor function
- Built-in oscillator for internal clock source
- Self test function with built-in internal magnet source
- Measurement range ± 4900 μT

- * Operation Modes \Rightarrow (7) modes \rightarrow Power-down Mode (0000)
 - \rightarrow Single Measurement Mode (0001)
 - \rightarrow Continuous Measurement Mode 1 (0010)
 - \rightarrow Continuous Measurement Mode 2 (0011) (0110)
 - \rightarrow External trigger measurement mode (0100)
 - \rightarrow Self-test Mode (1000)
 - \rightarrow Fuse ROM access mode (1111)
- CNTLL register [3:0] bits configures the modes.
- * Single Measurement Mode: \rightarrow measured for 1 times and data 0 output
 \rightarrow goes to power down mode automatically after measurement ended
- * Continuous Measurement Mode 1: \rightarrow sensor is measured in 8Hz periodically
 \rightarrow doesn't go back to power down mode automatically
- * Continuous Measurement Mode 2: \rightarrow sensor is measured periodically in 10Hz
- * External trigger Mode: \rightarrow sensor is measured for one time by ext trigger
 \rightarrow waits for next trigger to read the sensor
- * Fuse ROM access Mode: \rightarrow factory calibrated values are stored here in fuse
 - \rightarrow ROM of the device
 - \rightarrow to access the fuse ROM, this mode is used
 - \rightarrow needs manual transition to power down mode
- * After mode selection, wait 10ms for sensor to stabilize

(*) AK8963 has the limitation for measurement range that the sum of absolute values of each axis should be smaller than 4912 uT
 i.e. $|X| + |Y| + |Z| \leq 4912 \text{ uT}$

when magnetic field exceeds this, the data is not correct. (overflow)
 during overflow HOFL of 1, returns to 0 when next measurement starts

= Output of Magnetometer is the output of ADC of Magnetometer
for 14-bit selection; (scale of 0.6 uT/LSB)

Max. value: 1FFE (Hex) 8190 (Decimal) 4912 uT

Min. value: 80002 (Hex) -8190 (Decimal) -4912 uT

Unit: 0001 1 . 0.6 uT

for 16-bit selection

Sensor raw-data

Calculated mag. field (uT)

	Hex	Decimal	
Max	7FF8	32760	4912
Min	8008	-32760	-4912
Unit:	0001	1	0.15 uT

(CNLL register Bit[4] has selection bit for 14 or 16 bit op.

Bit[4] = 1 = 16 bit op.

⇒ 0 = 14 bit op

* Calibration of Magnetometer:

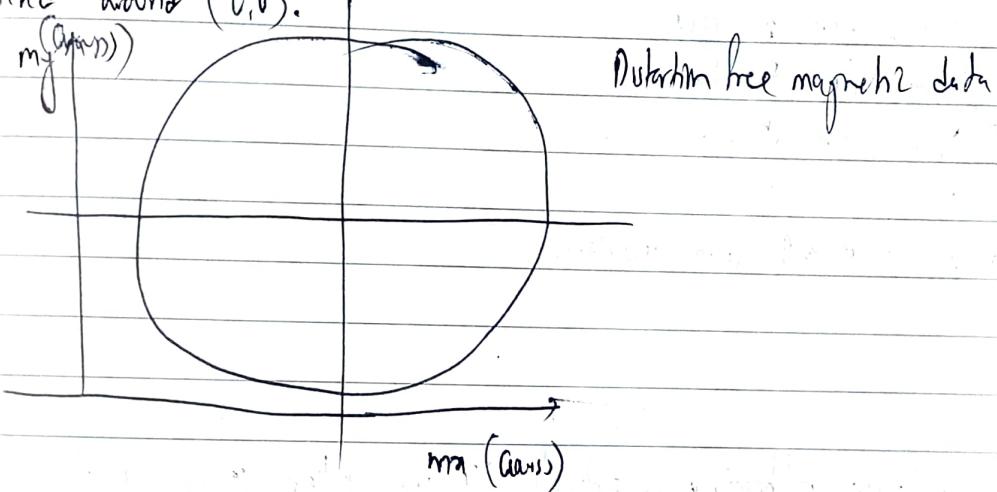
- ① → Offset calibration of raw-data
 - ② → Environmental Calibration (soft iron & hard iron)
 - ③ → Magnetic declination off at that place
 - ④ → bank angle and elevation calibration
 - ⑤ → Offset calibration: → read data from FUSE ROMs
 - perform sensitivity adjustment
- Registers → 10H (AJAX) → mag. sensor X-axis sensitivity adjustment
 11H (AJAY) → " " Y-axis " "
 12H (AJAZ) → " " Z-axis "

$$\text{Adjusted-value} = H_{\text{raw-data}} \times \left(\frac{(A_{SA} - 128) \times 0.5}{128} + 1 \right)$$

- (e) Environmental club calibration → for soft iron and hard iron in the affinity
- 8 shape movement for 3D calibration
 - simple rotation about yaw for 2D calibration

reference: <https://www.nxp.com/cn/application-note/AN9246.pdf>

- If no disturbing fields are present (absence of soft & hard iron), a rotating magnetometer through a minimum of 360° and plotting the result data as x and y vs. π axis will result in a circle centered around $(0,0)$.



- But presence of hard/soft iron produces perturbation of the circle as a simple offset from $(0,0)$ in case of hard iron and deform the circle in case of soft iron.

Note: Soft iron: distorts the shape of the circle

Hard iron: shifts the circle beyond origin $(0,0)$.

This calibration is for only at that specific time and surrounding. The values will change for change in surrounding metallic substances.

- * Hard-iron distortion: → produced by materials that exhibit a constant additive field to the earth's magnetic field, thereby generating a constant additive value to the o/p of each of the magnetometer axes.
 - compensated by determining the x and y offsets and then applying these constants directly to the raw data
 - sensor should be rotated minimum of 360°

$$\alpha = \frac{(x_{\max} - x_{\min})}{2}, \quad \beta = \frac{(y_{\max} + y_{\min})}{2}$$

α = X-axis offset

β = Y-axis offset

x_{\max} = max. x value

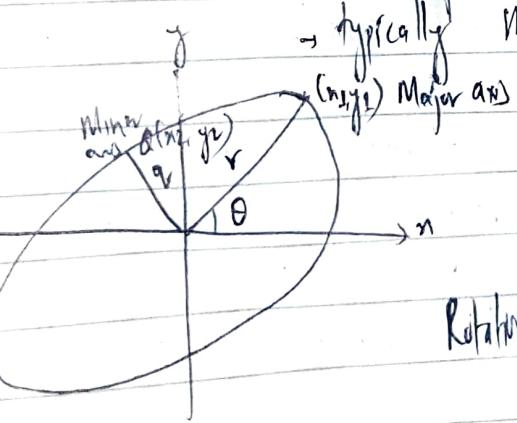
x_{\min} = min. x value

y_{\max} = max. y value

y_{\min} = min. y value

- subtract α & β from raw data

- * soft-iron calibration: → materials like iron, nickel causes soft iron distortion
 - needs more complicated procedure to calibrate and computation is a bit resource heavy
 - typically the distortion creates an ellipsoid



$$\text{Here, } r = \sqrt{n^2 + y_1^2}$$

$$\theta = \sin^{-1} \left(\frac{y_1}{r} \right)$$

$$\text{Rotation matrix (R)} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}$$

$$V_n = R V_g$$

$$V_y = R V_g$$

After rotation, the major axis of the ellipse will be aligned with the reference frame x-axis and the minor axis will align with the y-axis.

To transform this rotated ellipse into a proper circle, the scale factor σ is determined using the eq: $\sigma = \frac{g}{r} = \frac{\text{minor axis}}{\text{major axis}}$

Then each magnetometer z-axis value is divided by σ to obtain the desired circle.

Once the scaling is completed, a final rotation must be made to rotate the data back to their original position, thus compensating for soft-mom distortion.

$$\text{Here, } R^{-1} = \begin{bmatrix} \cos(-\theta) & \sin(-\theta) \\ -\sin(-\theta) & \cos(-\theta) \end{bmatrix} = \begin{bmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{bmatrix}$$

$$V_1 = R V_g$$

$$V_2 = R^{-1} V_y$$

Algorithm of for soft mom calibration (wMR-around)

$$\alpha' = \frac{\gamma_{\max} - \gamma_{\min}}{2}, \quad \beta' = \frac{y_{\max} - y_{\min}}{2}, \quad \gamma = \frac{z_{\max} - z_{\min}}{2}$$

$$\text{Average} = \frac{\alpha' + \beta'}{2} \quad \text{or} \quad \text{Average} = \frac{\alpha' + \beta' + \gamma}{3}$$

$$\text{offset}\alpha = \text{average} \mid \alpha'$$

$$\text{offset}\beta = \text{average} \mid \beta'$$

(2) Magnetic declination:

Latitude: $27^{\circ} 40' 9.4''$ N

Longitude: $85^{\circ} 13' 52.3''$ E

Magnetic Declination: $+0^{\circ} 35'$

Magnetic Inclination: $43^{\circ} 34'$

Magnetic field strength: 46523.5 nT

Without tilt compensation

$$(1) \text{ Heading} = \tan^{-1} \left(\frac{y}{x} \right) \quad (\text{in radians}) \quad \left(* \frac{180}{\pi} \right) \text{ to degrees}$$

Tilt compensation:

$$(2) y = g \times \cos(\text{roll}) - z \times \sin(\text{roll})$$

$$z = x \times \cos(\text{pitch}) + y \times \sin(\text{roll}) \times \sin(\text{pitch}) + z \times \cos(\text{roll}) \times \sin(\text{pitch})$$

$$\text{Heading} = \tan^{-1} \left(\frac{-y}{x} \right) \quad (\text{in radians})$$