

**220311/205001 – Computational engineering**

**Assignment 3 : Numerical resolution of the Navier  
Stokes equations in laminar flows**

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## 1 INTRODUCTION

To solve the Navier Stokes equation we need to use the fractional step method in that case we will describe how to do it taking the differentially heated cavity example.

## 2 DIFFERENTIALLY HEATED CAVITY

I choose to describe the differentially heated cavity because it has also thermal calculations which is a more global approach.

### 2.1 Fractional step method (FSM)

The fractional step method is a method to solve the incompressible Navier Stokes equation.

To solve Navier Stokes equation we need to solve 5 main steps : (for each time step)

1.  $R_T(T^n)$  and  $R(v^n)$
2.  $T^{n+1} = T^n + \frac{\Delta t}{\rho c_p} \left[ \frac{3}{2} R_T(T^n) - \frac{1}{2} R_T(T^{n-1}) \right]$  and  $v^p = v^n + \frac{\Delta t}{\rho} \left[ \frac{3}{2} R(v^n) - \frac{1}{2} R(v^{n-1}) \right]$
3.  $\Delta p^{n+1} = \frac{\rho}{\Delta t} \nabla \cdot v^p$
4.  $v^{n+1} = v^p - \frac{\Delta t}{\rho} \nabla p^{n+1}$
5. New  $\Delta t = \min(\Delta t_c, \Delta t_d, \Delta t_t)$ , where  $\Delta t_t = 0.20 \frac{\Delta x^2}{\lambda / \rho c_p}$

We can see that we need every step to do the next one.

So we will explain the steps in this order.

### 2.2 $R(T^n)$ and $R(v^n)$

$$R(u)\Omega_{xP} = - [\dot{m}_e u_e - \dot{m}_w u_w + \dot{m}_n u_n - \dot{m}_s u_s] + \left[ \mu_e \frac{u_E - u_P}{d_{EP}} A_e - \mu_w \frac{u_P - u_W}{d_{WP}} A_w + \mu_n \frac{u_N - u_P}{d_{NP}} A_n - \mu_s \frac{u_P - u_S}{d_{SP}} A_s \right]$$

where  $\dot{m}_e = (\rho u)_e A_e$ ,  $\dot{m}_w = (\rho u)_w A_w$ ,  $\dot{m}_n = (\rho v)_n A_n$ ,  $\dot{m}_s = (\rho v)_s A_s$  ( here  $\dot{m}$  is positive in the positive coordinate direction).

$R_T(T) = -\rho c_p \mathbf{v} \cdot \nabla T + \nabla \cdot (\lambda \nabla T)$ . then we would need to discretize this function in the same way to calculate RT.

In order to calculate  $R(vn)$ , we have to estimate the velocity for all facets of the control volume ( $ue, us, us, uw$ ). For that, we need to use the scheme of approximation for the convective terms (CDS, UDS, QUICK...). About the terms  $(\rho u)_e, (\rho u)_w, (\rho u)_n, (\rho u)_s$ , it depends on the type of mesh.

Once all facets velocity for each control volume are determined, we obtain the following matrix system:

$$[R(vn)] = [A][u].$$

### 2.3 $T^{n+1}$ and $v^p$

$$v^P = v^n + \frac{\Delta t}{\rho} \left[ \frac{3}{2} R(v^n) - \frac{1}{2} R(v^{n-1}) \right]$$

Computing every values of  $v$  in the mesh with the Adams bendshforth scheme. If we can compute  $RT(Vn)$  we can do the calculation for  $R(Vn-1)$ .

$$T^{n+1} = T^n + \frac{\Delta t}{\rho c_p} \left[ \frac{3}{2} R_T(T^n) - \frac{1}{2} R_T(T^{n-1}) \right]$$

Computing the temperature repartition for the new time step . If we can compute  $RT(Tn)$  we can do the calculation for  $RT(Tn-1)$ .

### 2.4 $\Delta P^{n+1}$

Then we need to take into account the pressure term.

To determine  $\Delta P^{n+1}$  :

$$\begin{aligned} a_P p_P^{n+1} &= a_E p_E^{n+1} + a_W p_W^{n+1} + a_N p_N^{n+1} + a_S p_S^{n+1} + b_P \\ a_P &= a_E + a_W + a_N + a_S \\ a_E &= \frac{A_e}{d_{EP}} & a_N &= \frac{A_n}{d_{NP}} \\ a_W &= \frac{A_w}{d_{WP}} & a_S &= \frac{A_s}{d_{SP}} \\ b_P &= -\frac{1}{\Delta t} [(\rho u^P)_e A_e - (\rho u^P)_w A_w + (\rho v^P)_n A_n - (\rho v^P)_s A_s] \end{aligned}$$

The equation comes from the discretization of the pressure equation.

The matrix system will be :  $A \cdot P^{n+1} = B$  solved by  $P^{n+1} = A^{-1}B$ .

## 2.5 $v^{n+1}$

$$v^{n+1} = v^P - \frac{\Delta t}{\rho} \nabla p^{n+1}$$

if  $v^{n+1}_P$  is known, we can set  $v^P = v^{n+1}_P$ . Thus,

$$\frac{\partial p}{\partial n} = 0$$

So we take into account the pressure term at the time step  $n+1$  to have the correct velocity at the time step  $n+1$ . So we solve : (Where  $v_n$  is equal to  $v_p$ )

The matrix system is  $v^{n+1} = v^n - C \cdot P^{n+1}$

## 2.6 $\Delta t$

We need to calculate the time step of the convective terms, diffusive terms and the thermal terms according to the CFL conditions.

Then we need to choose the minimum time step to be conservative on the over terms.

Then we iterate on the time step to obtain the new values of the physical properties.

We need information to do those operations:

- the initial velocity ( $t=0$ )
- Fluid properties
- Boundary conditions
- Mesh properties
- The scheme used (CDS, UDS, PLDS...)

Once we have these data, we can use the FSM like described previously until the final time ( $t_{steady}$ ).

## 3 CONCLUSION

The fractional step method can be divided into 5 steps and by doing so we can see the concept more clearly the key point is to calculate the pressure terms to finally calculate the velocity with those pressure terms.