# Reference-free Structural Health Monitoring for Detecting Delamination in Composite Plates

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## Outline

- 1 Introduction
- 2 Reference-free Delamination Detection Technique
- Numerical Simulation
- Experimental Setup and Test Results
- 5 Summary and Conclusion

# What Makes the Detection of Delamination Challenging?

#### **Technology**

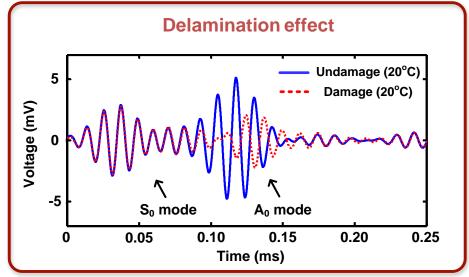
Lamb wave, embedded PZT transducer, pitchcatch sensing

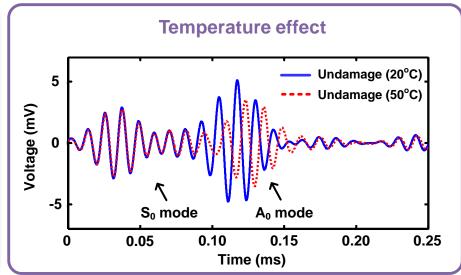
#### Challenges

- Lamb wave mode complexity
- Similarity of delamination and temperature effects on Lamb wave modes
- Autonomous decision making

#### Final target

Real-time autonomous delamination detection





## Research Objective and Uniqueness

### **Objective**

Development of a delamination detection technique in a single wave propagation path without using prior baseline data or a predetermined decision boundary even under changing operational and environmental conditions of a structure

### Uniqueness

Invariant of environmental variation (real-time monitoring)



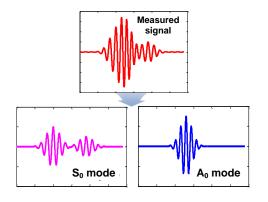
## Autonomous delamination detection



Health?

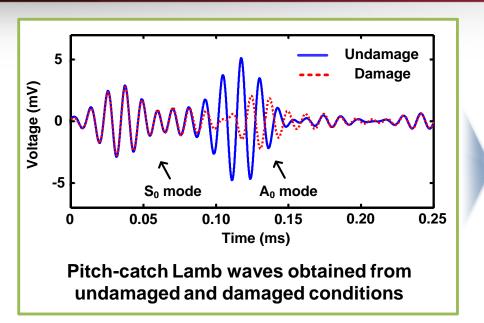
Damage?

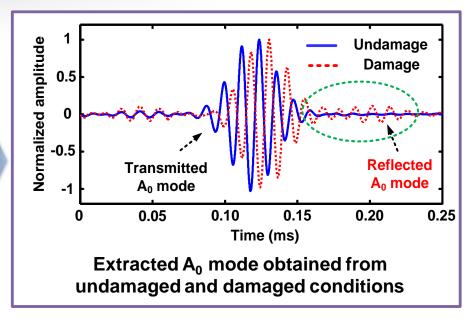
# Mode extration using a dual PZT



# Interaction of Lamb Waves with Delamination

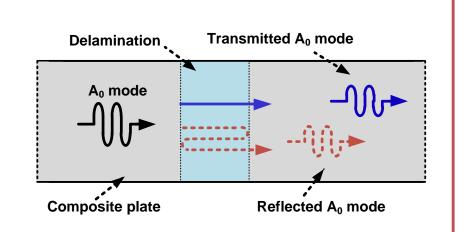
Reference-free delamination detection technique





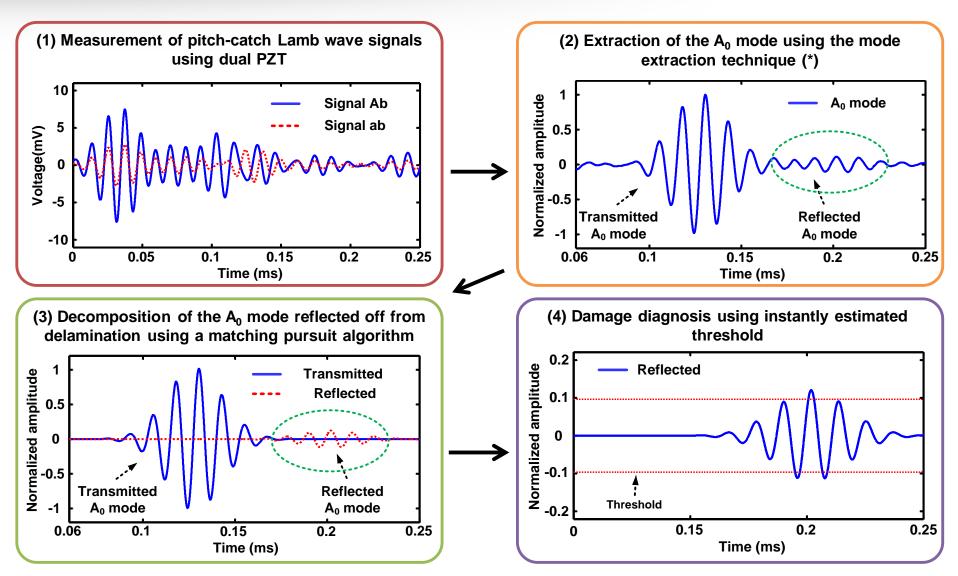
#### Effects of delamination on Lamb waves

- 1. Attenuation and delay of the  $A_0$  mode rather than the  $S_0$  mode
- Hardly distorted waveforms of the A<sub>0</sub> and S<sub>0</sub> modes by delamination
- 3. Little mode conversion
- Creation of the reflected A<sub>0</sub> mode



# Procedure of the Proposed Reference-free Delamination Detection Technique

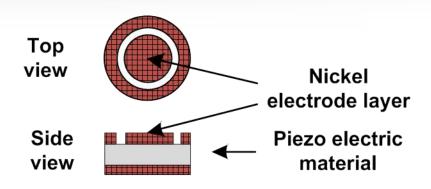
Reference-free delamination detection technique



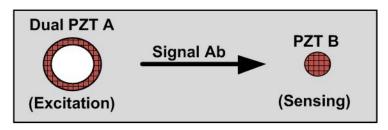
(\*): Chul Min Yeum et al "Lamb wave mode decomposition using concentric ring and circular PZT Transducers," Wave Motions, Vol. 48, pp. 358-370, 2011.

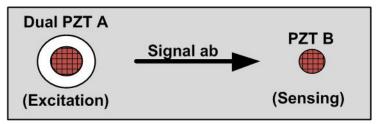
# Introduction of a Dual PZT and Signal Notations

Reference-free delamination detection technique

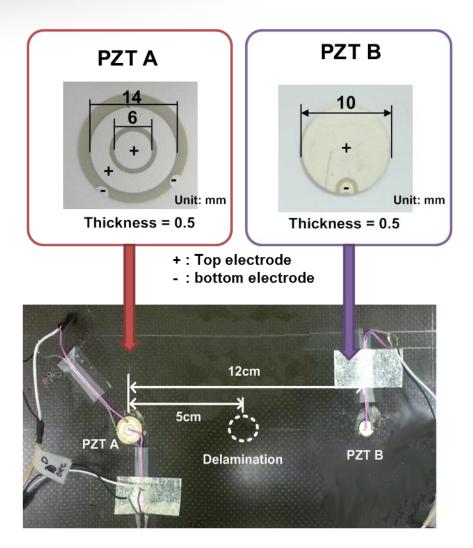


### Schematic drawing of a dual PZT





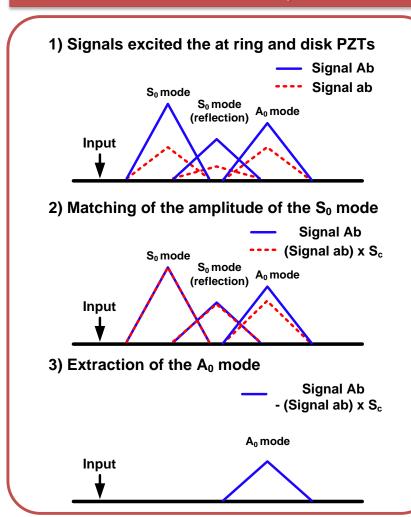
Notations of signals



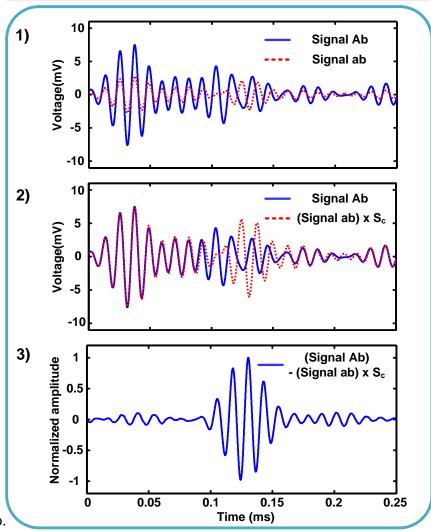
A composite specimen with PZTs and a delamination location

## Extraction of the A<sub>0</sub> mode from Measured Signals

## Schematic drawings of the A<sub>0</sub> mode extraction technique

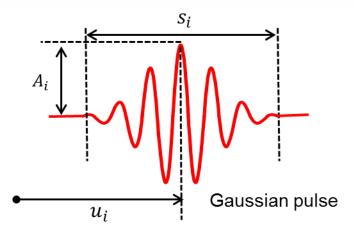


## The proposed technique using signals Ab and ab obtained from the test specimen



 $S_c$  is the amplitude ratio of the  $S_0$  mode in signal Ab to that in signal ab.

**Basis Function**  $g_i = (u_i, s_i, \xi_i, \phi_i)$ 



Let f(t) is the measured signal to be analyzed

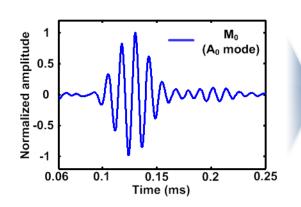
$$f(t) = \sum_{i=0}^{m-1} A_i g_i(t) + R_m f(t)$$

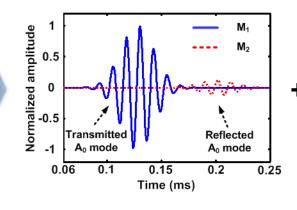
 $R^{i+1}f$ : the residual after i iterations

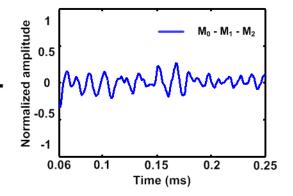
g<sub>i</sub>: the basis Gaussian function

 $A_i$ : the amplitude;  $u_i$ : the arrival time; ;  $\phi_i$ : the phase

 $s_i$ : the pulse duration;  $\xi_i$ : the central frequency







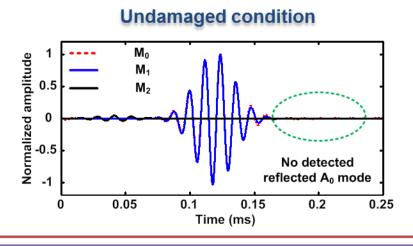
 $M_0$ : Extracted  $A_0$  mode;  $M_1$ :  $1^{st}$  decomposed  $A_0$  mode (transmitted  $A_0$  mode);

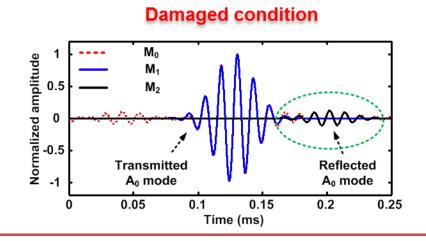
M<sub>2</sub>: 2<sup>nd</sup> decomposed A<sub>0</sub> mode (reflected A<sub>0</sub> mode)

Reference: Hong JC et al, 2005

## **Reference-free Damage Classification**



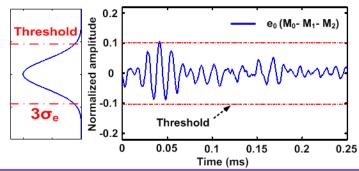




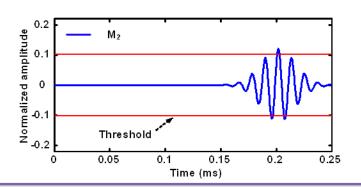
Step 2. Check if  $\mathbf{M}_2$  is the reflected  $\mathbf{A}_0$  mode using a threshold value instantaneously obtained from an error signal

Fit a parametric distribution to the  $e_0$  and compute a threshold value ( $e_0 = M_0 - M_1 - M_2$ ,  $\sigma_e$  is the standard deviation of  $M_0 - M_1 - M_2$ )

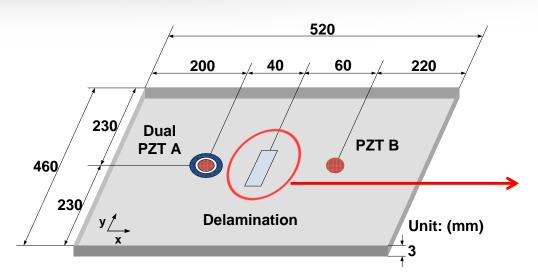
Fitting a distributing using e<sub>0</sub>



If maximum amplitude of  $M_2 > 3 \sigma_e$ , a delamination exists.

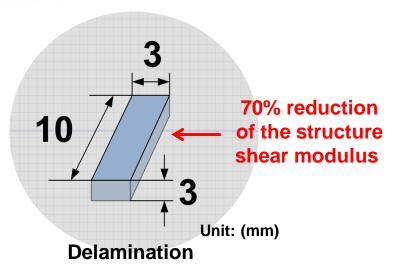


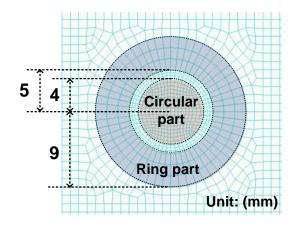
## **Numerical Simulation Setup**



#### Configuration of the simulated plate

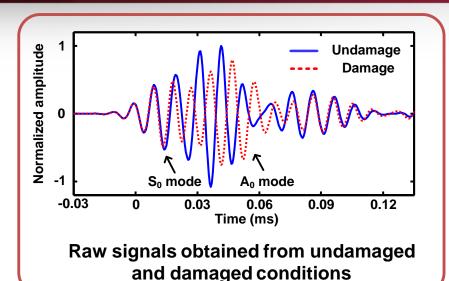
Input	Pin-force, 100 kHz, 7 cycle toneburst
Material (structure)	E = 50G pa, G = 18.7Gpa
Material (delamination)	E = 50G pa, G = 5.61Gpa (↓ 70%)
Sampling rate	2 MHz
Mesh size	1 mm x 1mm x 1mm
Software	MSC/NASTRAN

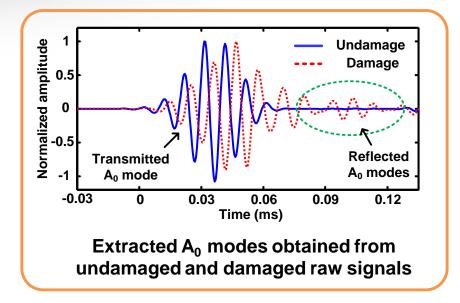


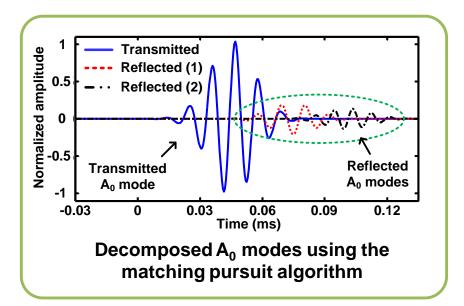


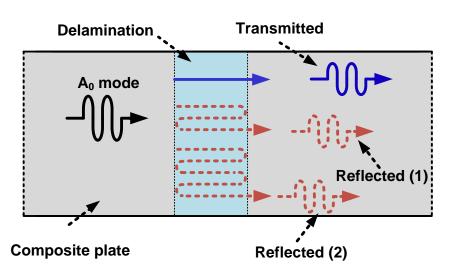
**Dimension of the dual PZT** 

## **Numerical Simulation Results**

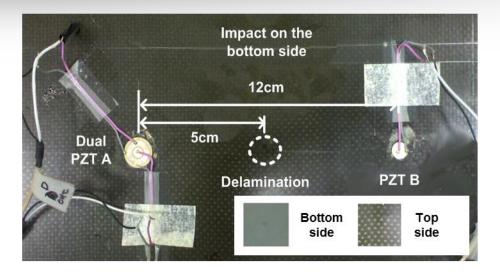




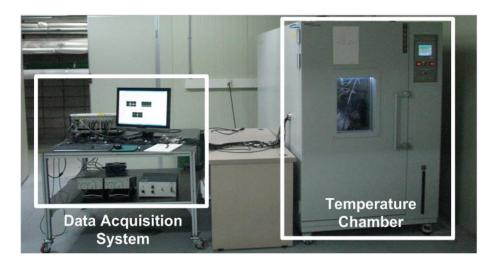




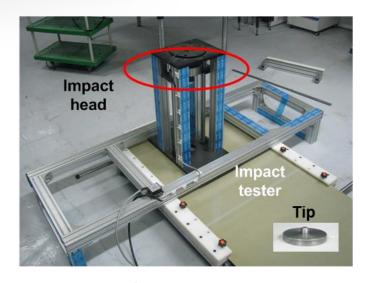
## **Experimental Setup**



Test specimen



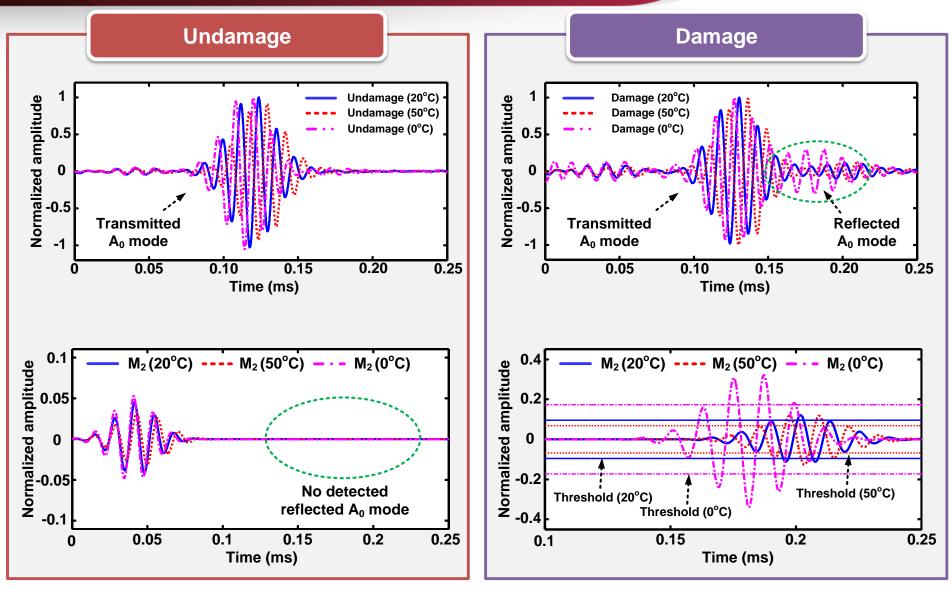
**DAQ system & Temperature chamber** 



**Impact tester** 

- PSI-5A4E PZT
- Input signal: A 80kHz tone-burst signal with ± 10 peak-to-peak voltage
- Sampling rate: 20MS/s
- Data averaging: 30 times
- Testing temperature: -10, 20, 50 °C

## **Reference-free Damage Classification**



For undamaged and damaged conditions, temperature chamber experiments are conducted at '20°C', '50°C' and '0°C'.

## **Summary and Conclusion**

An reference-free delamination detection technique is developed and validated using data
obtained from damage states of a composite plate.
The effectiveness of the proposed technique is demonstrated explicitly under varying temperatures.
A fundamental Lamb wave mode ( $A_0$ mode) was successfully extracted by the proposed mode extraction technique using a dual PZT at any desired frequency without any other special tuning.
Further investigation will be underway to extend the proposed concept to more complex structures and other types of damage.

# **THANK YOU!**

Do You Have Any Questions?

# Back up slides

# Why Do You Use the Mode Extraction Technique?

#### **Double sided PZT installation?**

The PZT cannot be installed on the both side of the aircraft structure.

#### Frequency tuning?

- A tuning curve is the function of the material properties of the structure so it is varied depending on the temperature of the structure.
  - Ex) At normal temperature, a specific mode is dominant but, at a different temperature, this tuned mode may not be dominant.

### **Question and Answer**

Q1: What kinds of composite material are you use for your experiment?

A1: The material properties and prepreg lay-up information of the specimen are unknown to us.

The Boeing company didn't let us know these information.

Q2: Is your technique able to apply complex structures?

A2: Not yet. A critical problem is that complex geometries produce reflected and converted modes, making extraction of delamination reflected A0 mode challenging.

Q3: is the damage delamination or surface breaking? How did you know about that?

A3: We have scanned delamination area in our previous works so we know the proper impact energy to produce impact damage.

Q4: Is it correct the assumption of shear modulus reduction as a delamination model?

A4: In reality, when the composite plate get impact damage, the fibers are broke down and dent is made on the surface. However, we deal with the delamination as a global aspect. The testing frequency of 80khz that doesn't have wave length enough sensitive to detect such small specific damage phenomenon.

### **Question and Answer**

Q5: Is the S0 mode able to be fully cancelled?

A5: Depending on the experimental setup. About the mode decomposition errors, I dealt with one chapter in my paper. Briefly saying that, the size difference of dual PZT make spreading errors because outer ring and disk parts of the dual PZT are differently installed spatially extended on at the structure. However, my conclusion is this error is too small to be consideredt.

Q6: How do you decompose the A0 mode when the first arrival and boundary reflected A0 mode are overlapped?

A6: This is the constraint of the proposed technique. The A0 mode reflected from structural boundary should not be overlapped with the first arrival A0 mode and the A0 mode reflected off from delamination. However this constraint is not a big issue on the composite material because the velocity of the A0 mode in composite material is approximately half of that in metallic material. It is more flexible to install sensors.