

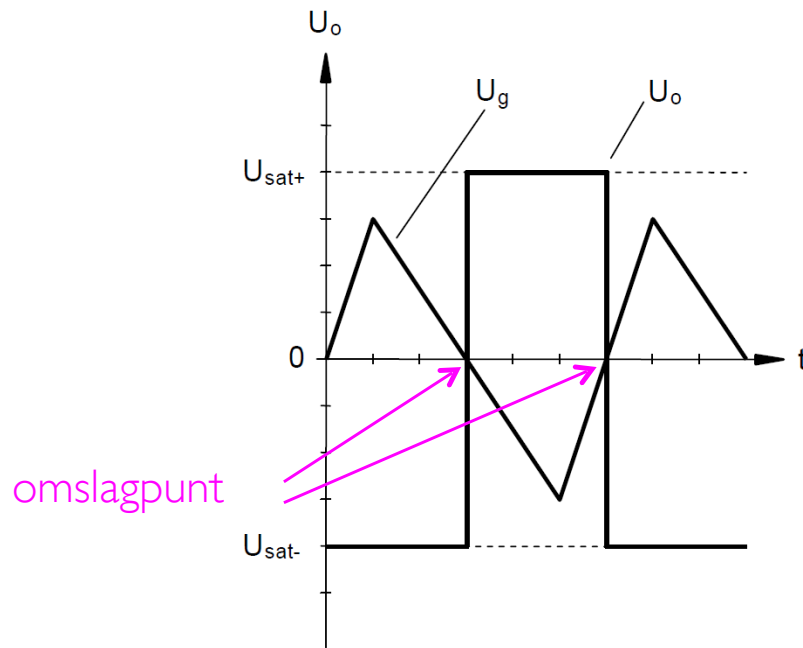
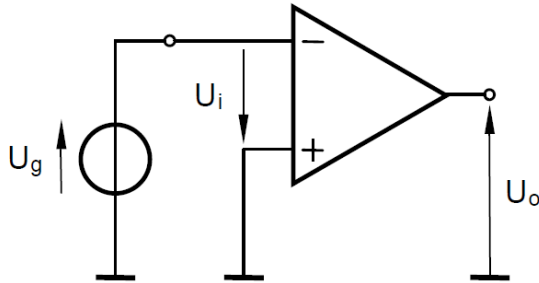
## Elektronische signalen 2

# Spanningscomparatoren

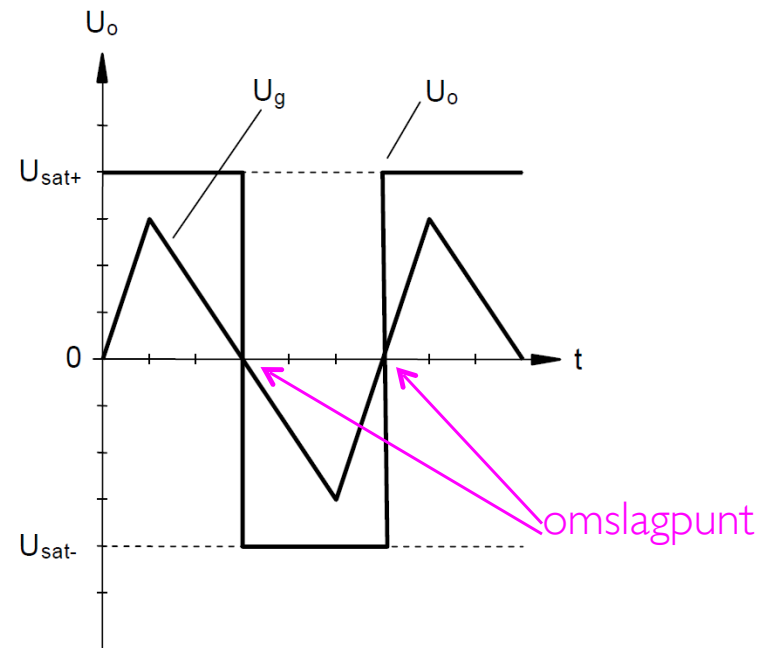
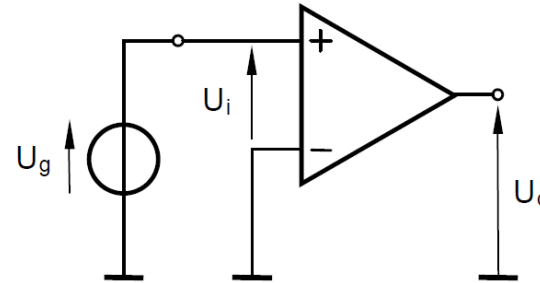
P. Debbaut

# Nuldoorgangsdetector

Inverterende-nuldoorgangsdetector

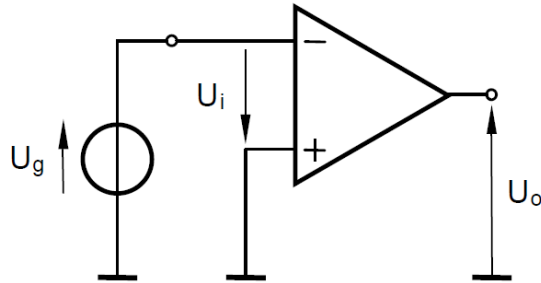


Niet-inverterende-nuldoorgangsdetector

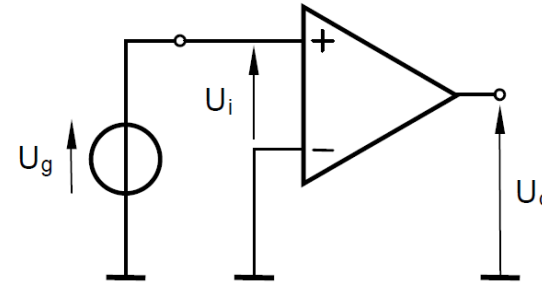


# Nuldoorgangsdetector

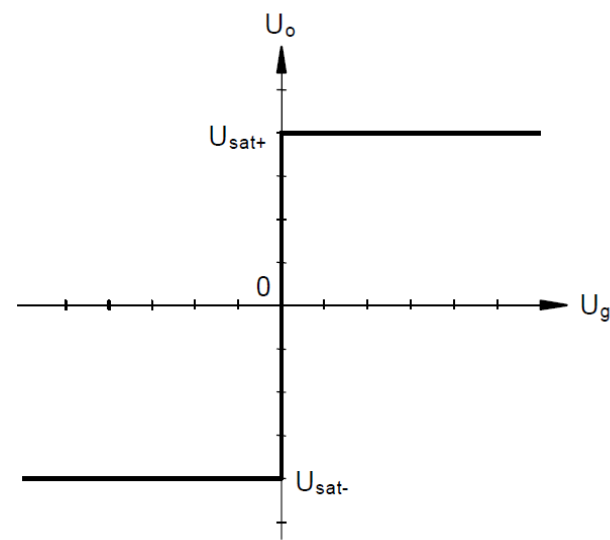
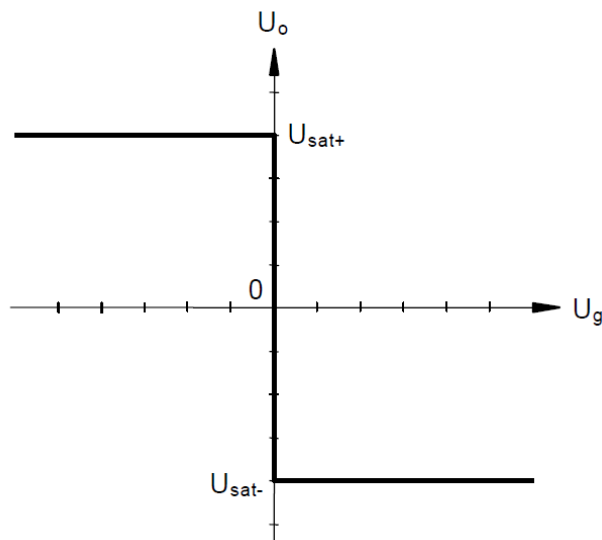
Inverterende-nuldoorgangsdetector



Niet-inverterende-nuldoorgangsdetector

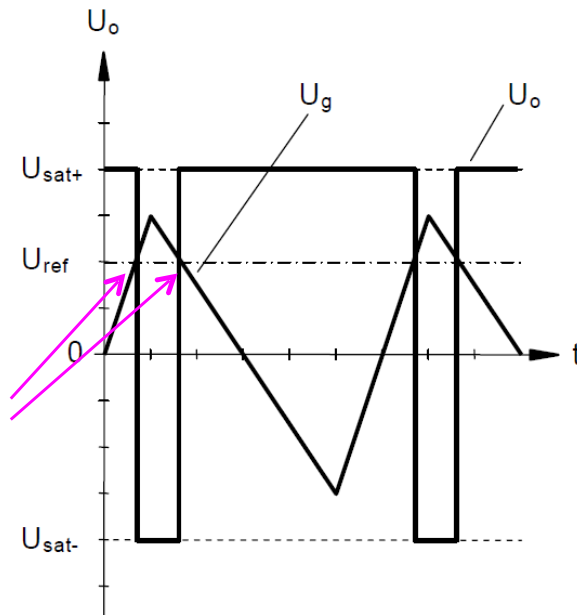
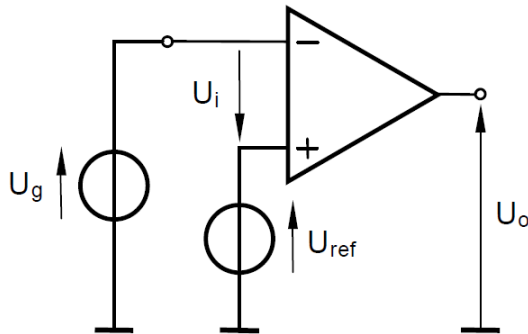


Transferkarakteristieken



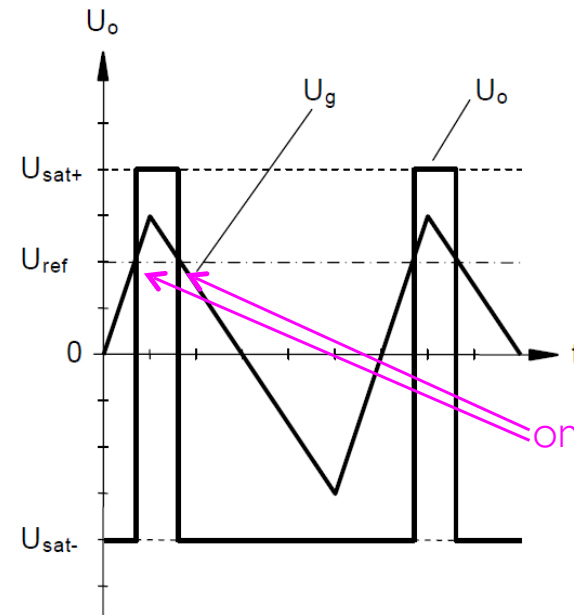
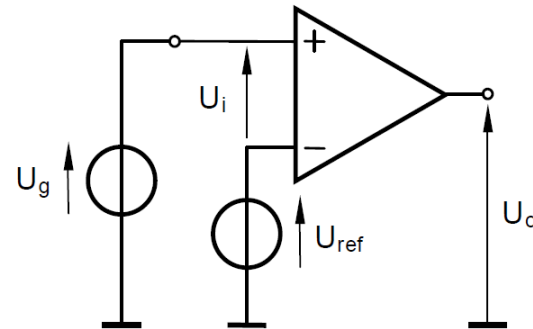
# Niveaudetector

## Inverterende-niveaudetector



omslagpunt

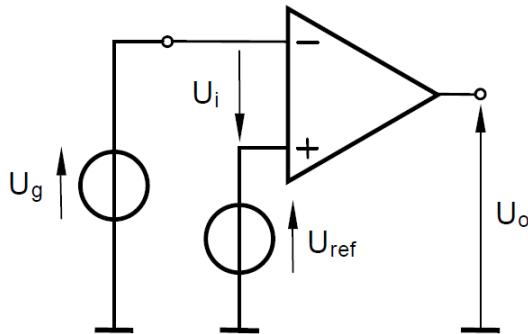
## Niet-inverterende-niveaudetector



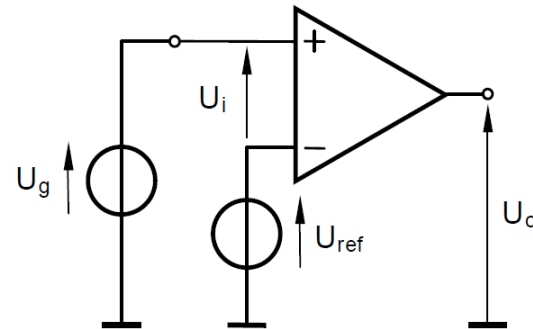
omslagpunt

# Niveaudetector

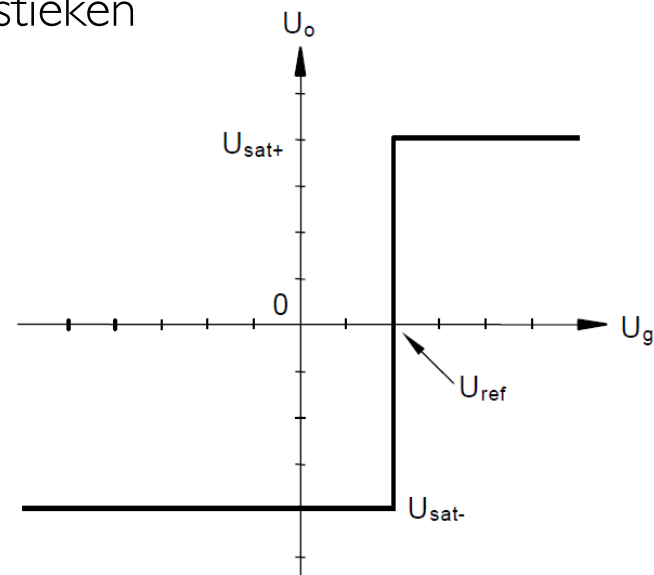
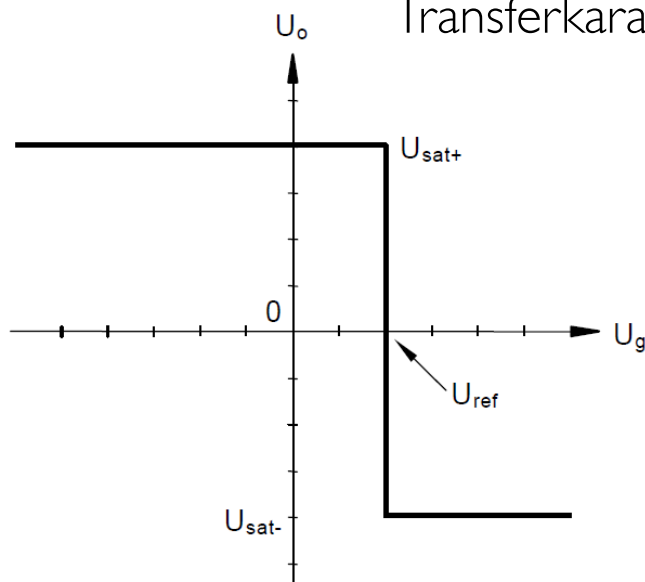
Inverterende-niveaudetector



Niet-inverterende-niveaudetector

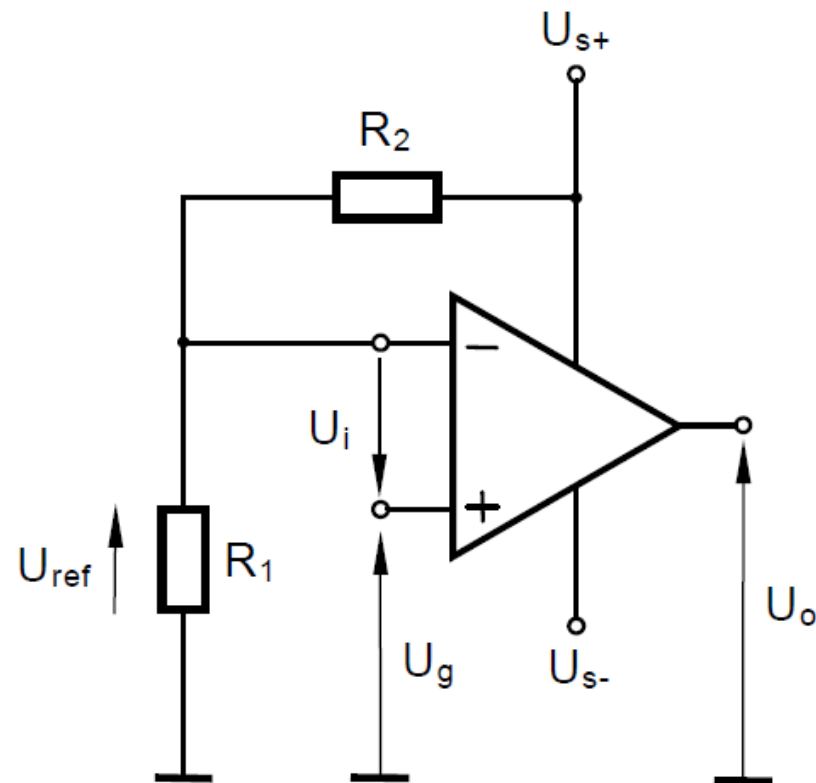


Transferkarakteristieken

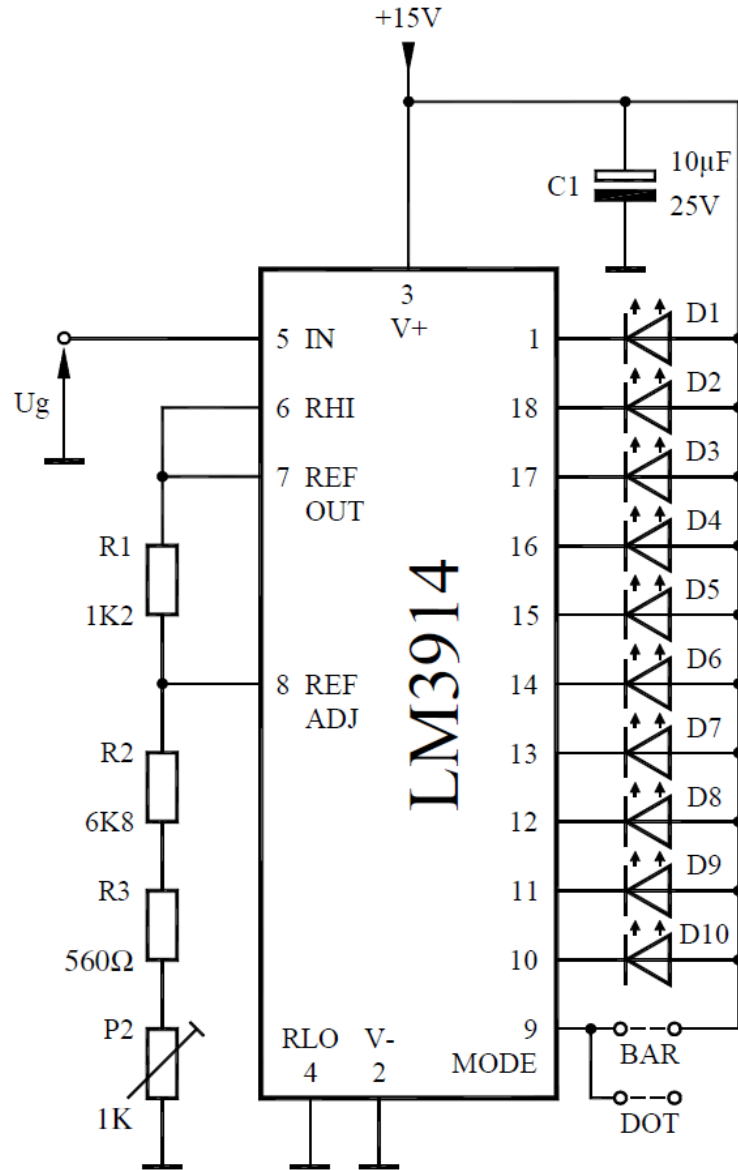


# Niveaudetector

Voorbeeld: niet-inverterende niveaudetector met spanningsdeler als  $U_{\text{ref}}$



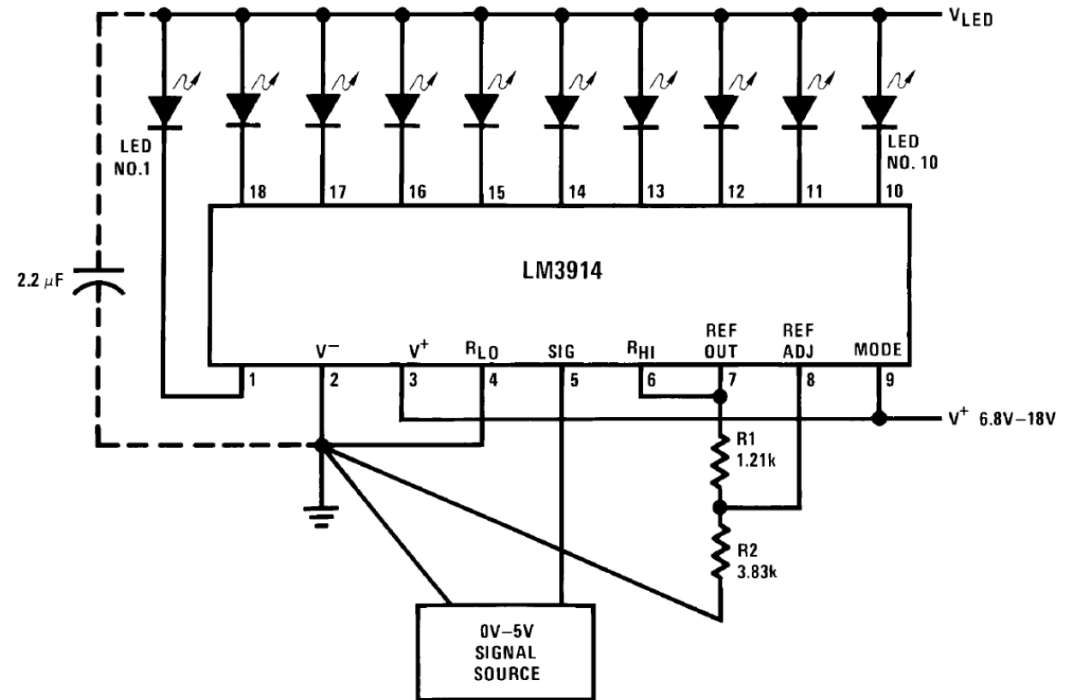
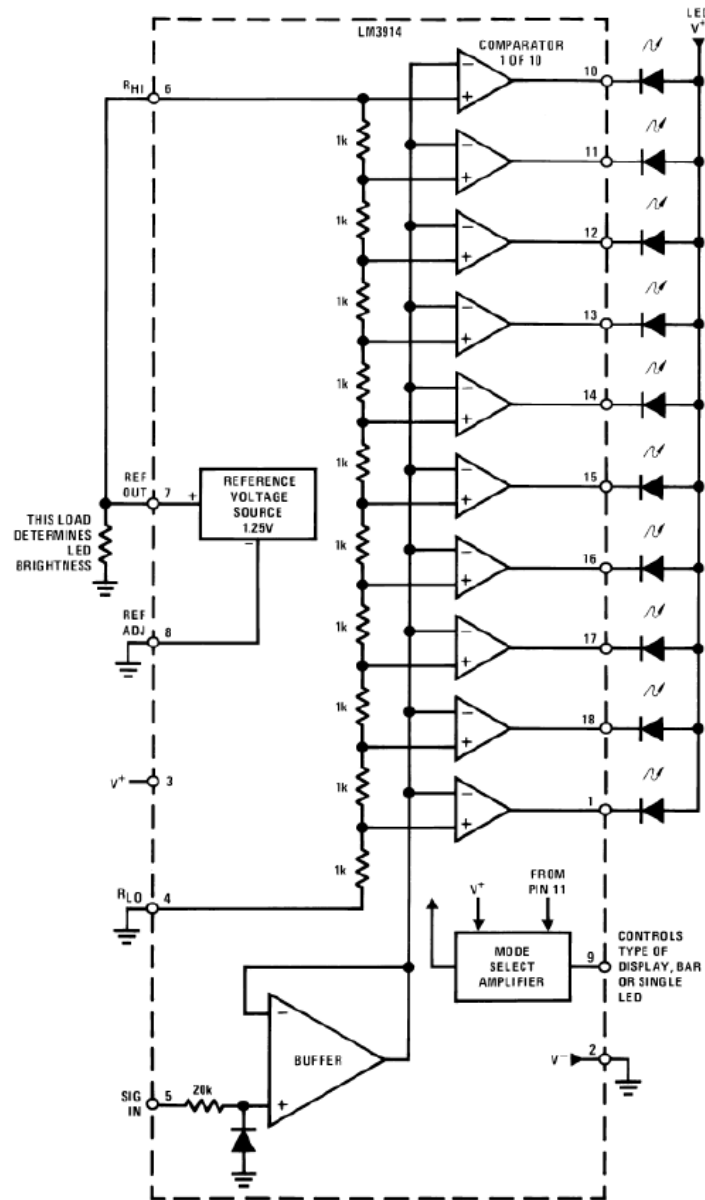
# Dot/Bar Graph Display



Toepassing:

ontwerpen van een  
lineaire voltmeter van  
0V...10V met LM3914

# Dot/Bar Graph Display



Stroom door de LED's

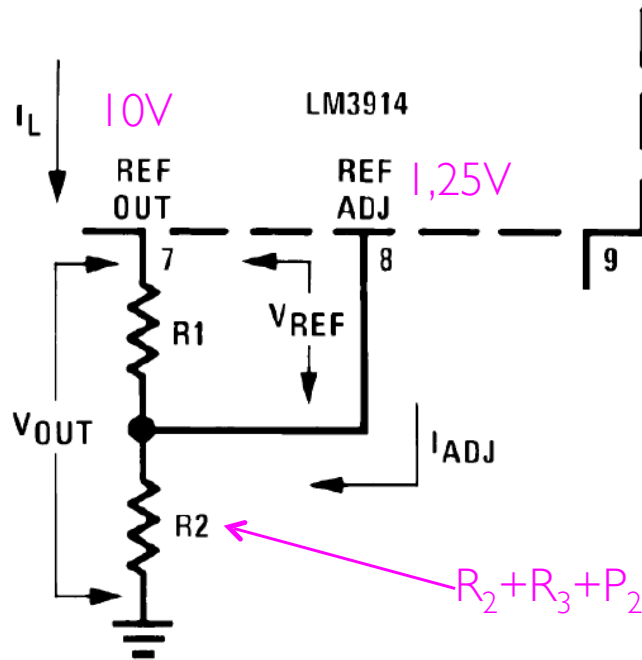
$$I_{LED} = \frac{12,5}{R_1}$$

Bij  $R_1 = 1,2k\Omega \rightarrow \approx 10mA$



# Dot/Bar Graph Display

$$V_{OUT} = V_{REF} \left( 1 + \frac{R_2}{R_1} \right) + I_{ADJ} R_2$$



≈ middenstand  
potmeter 1K

Bepalen  $R_2$

$$R_2 = \frac{V_{OUT} - V_{REF}}{\frac{V_{REF}}{R_1} + I_{ADJ}}$$

$I_{ADJ} = 75\mu A$  en  $U_{REF} = 1,25V$

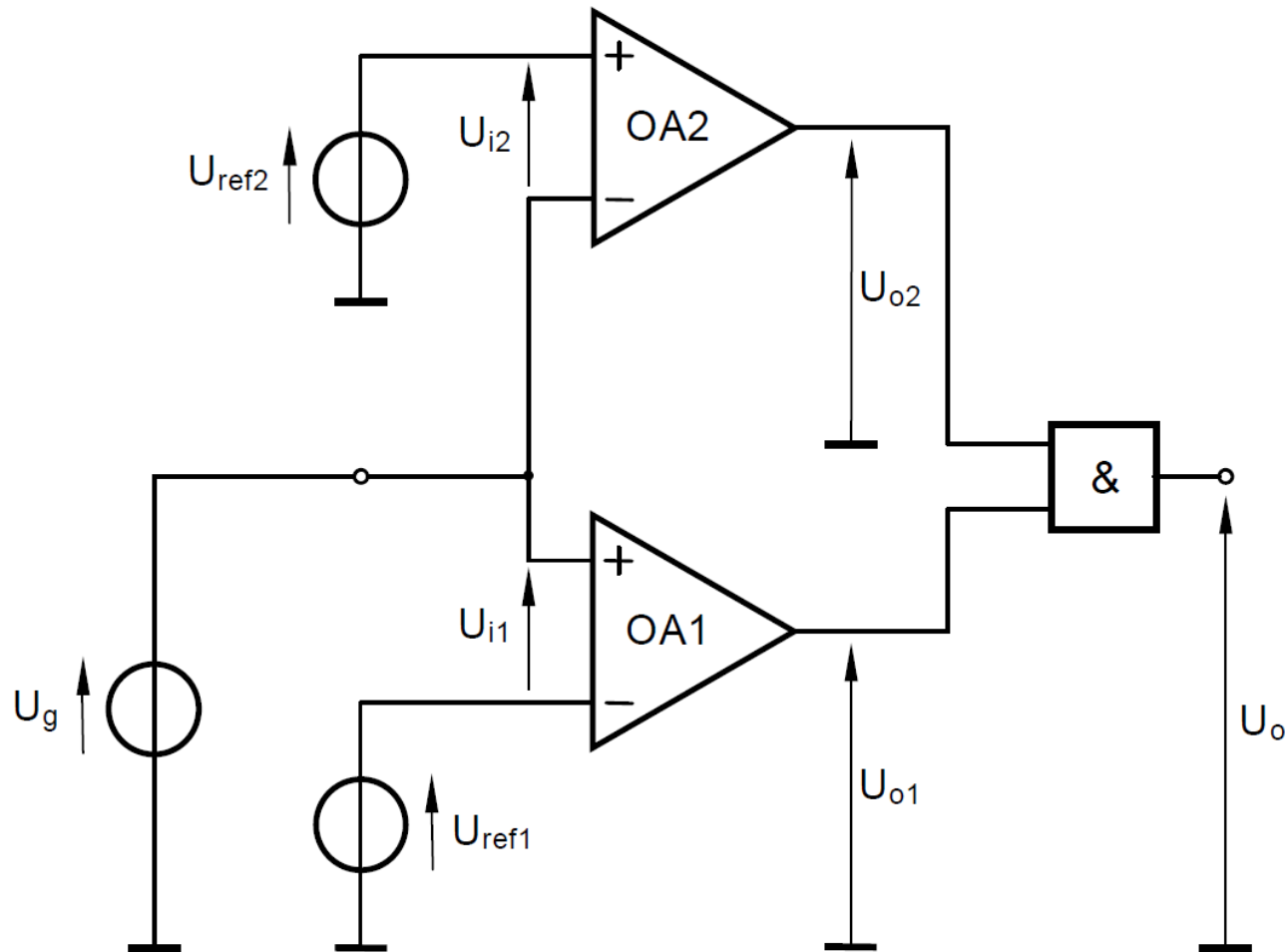
$$R_2 = \frac{10 - 1,25}{\frac{1,25}{1,2 \cdot 10^3} + 75 \cdot 10^{-6}} = 7836\Omega$$

$$P2 = R_2 - R2 - R3$$

$$= 7836\Omega - 6800\Omega - 560\Omega$$

$$= 475,82\Omega$$

# Venstercomparator



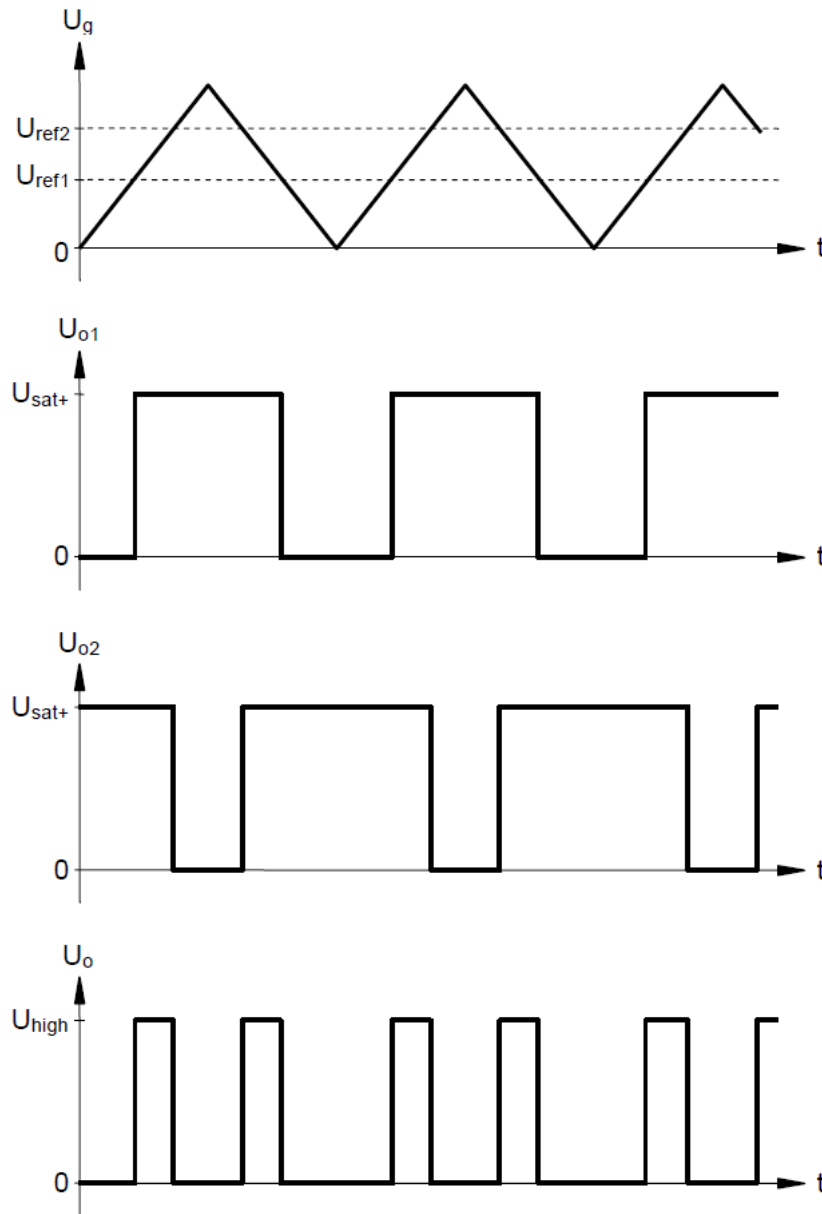
Voorwaarde:

$$U_{ref2} > U_{ref1}$$

Uitgang hoog:

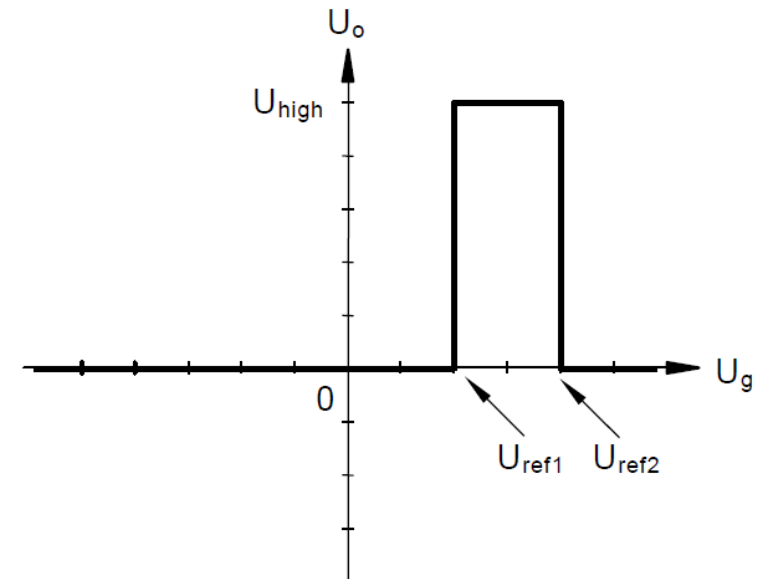
$$U_g < U_{ref2} \text{ en } U_g > U_{ref1}$$

# Venstercomparator-signalen

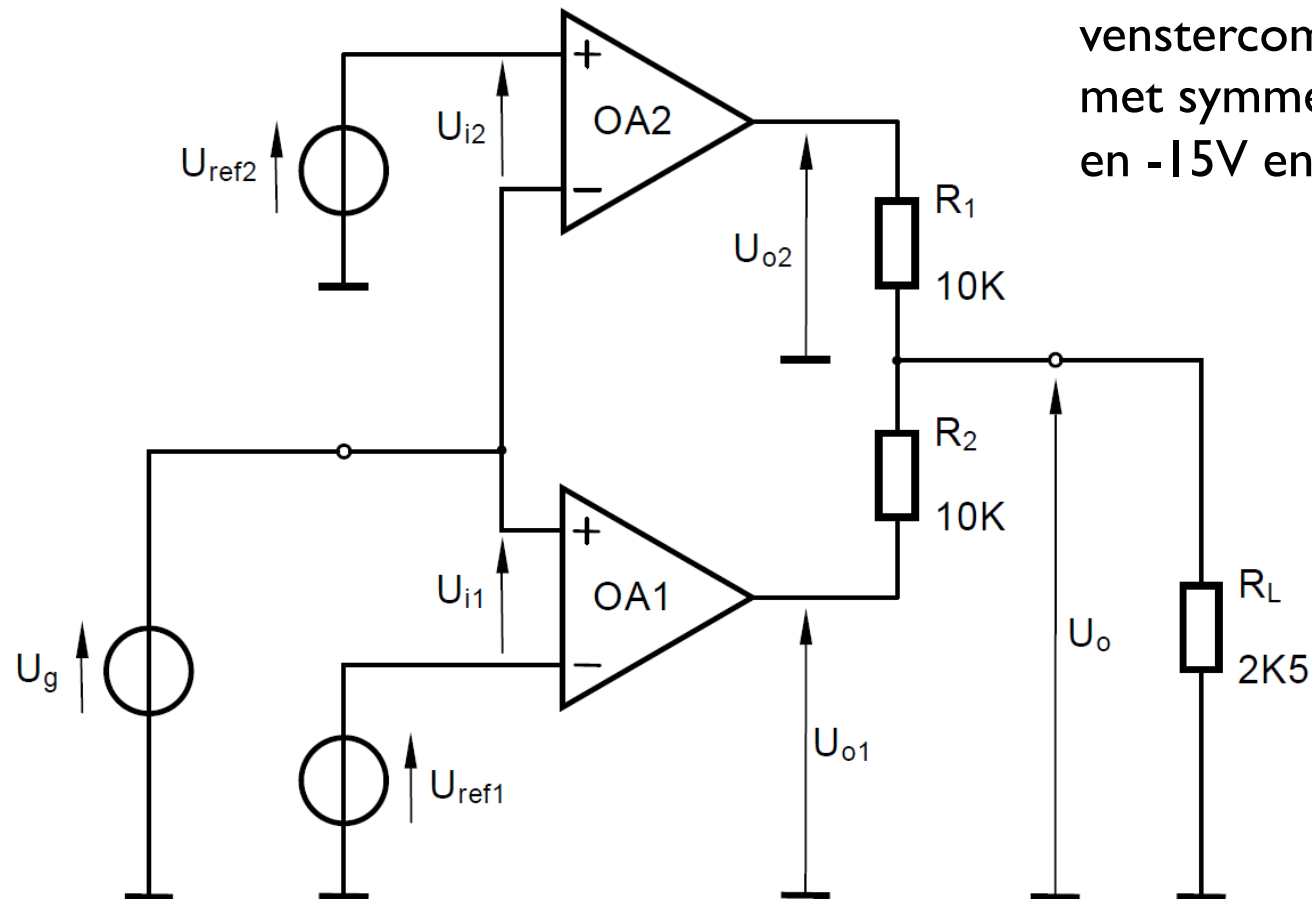


Opamps asymmetrisch gevoed ( $U_{s+}$  15V en  $U_{s-}$  0V)

Transferkarakteristiek



# Venstercomparator

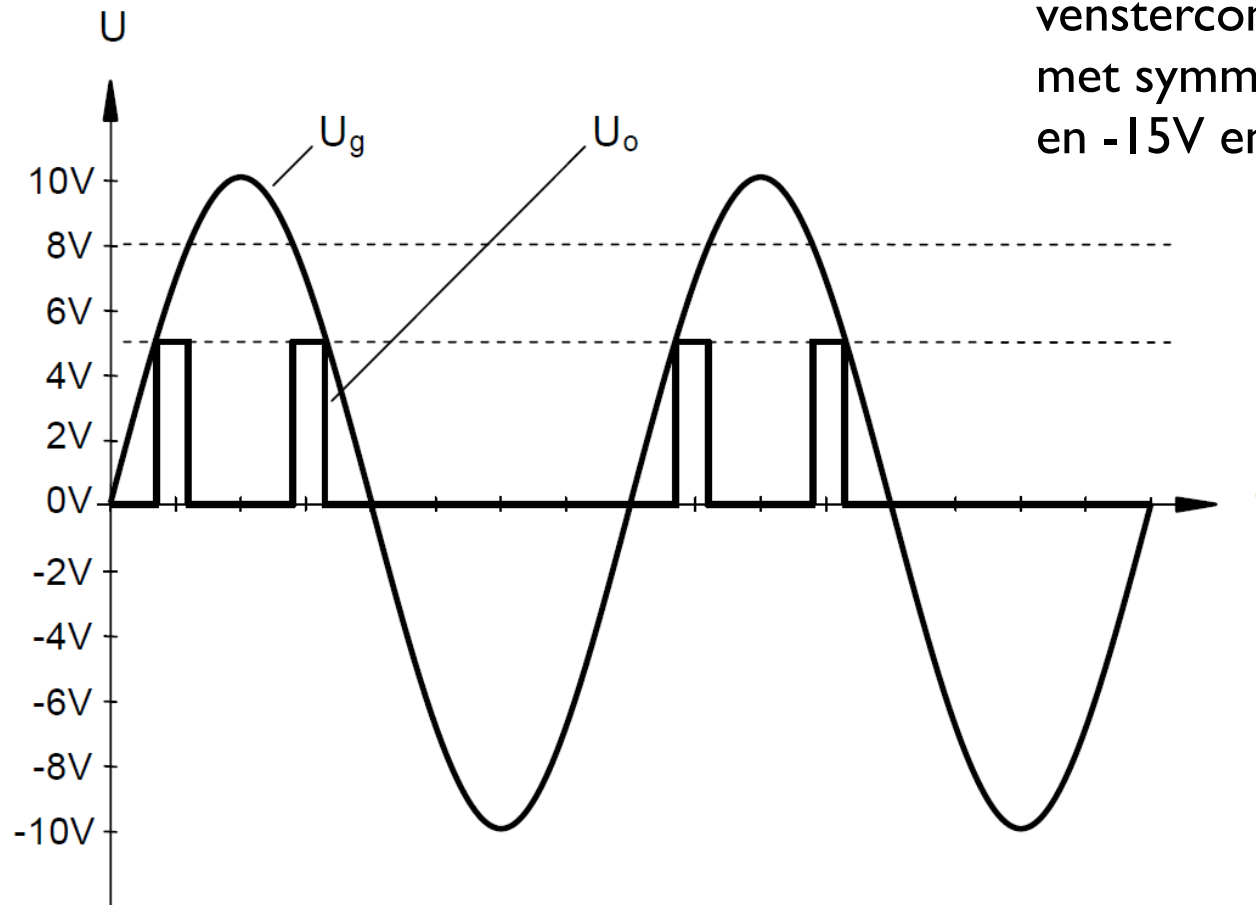


Voorbeeld:  
venstercomparator zonder AND-poort  
met symmetrische voeding van +15V  
en -15V en ideale opamp

$U_{ref1} = 5V$   
 $U_{ref2} = 8V$   
 $U_g$ : sinus van  $20V_{tt}$

# Venstercomparator

Voorbeeld:  
venstercomparator zonder AND-poort  
met symmetrische voeding van +15V  
en -15V en ideale opamp

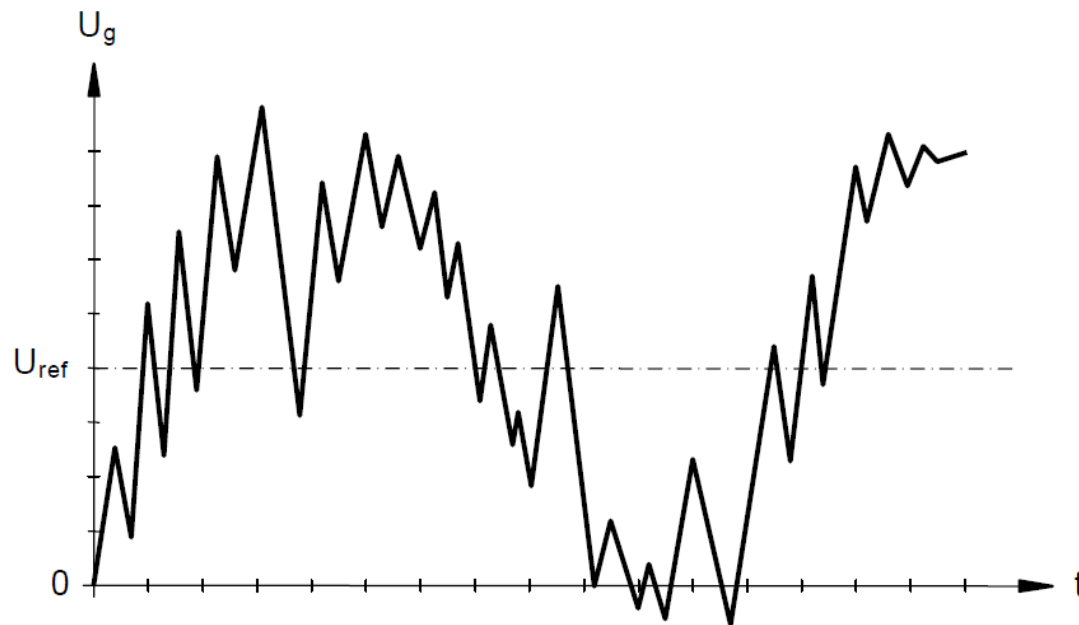


$$U_{\text{ref1}} = 5\text{V}$$

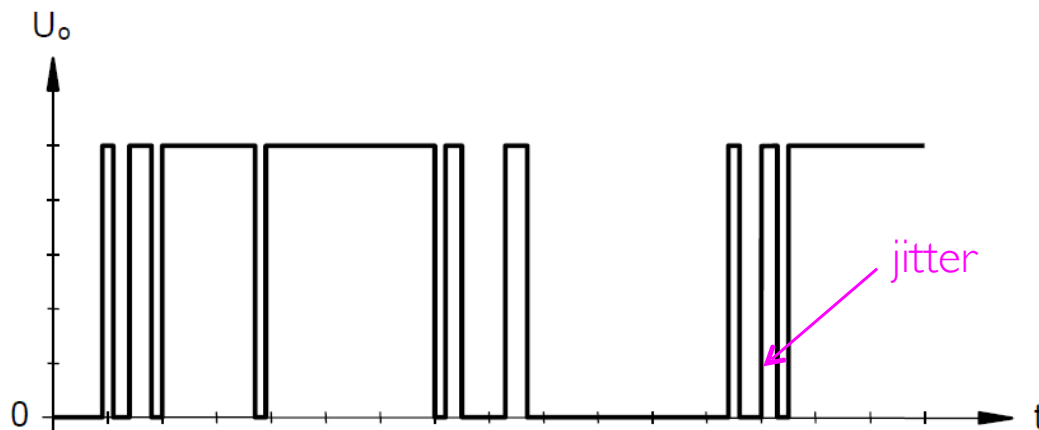
$$U_{\text{ref2}} = 8\text{V}$$

$$U_g: \text{sinus van } 20V_{\text{tt}}$$

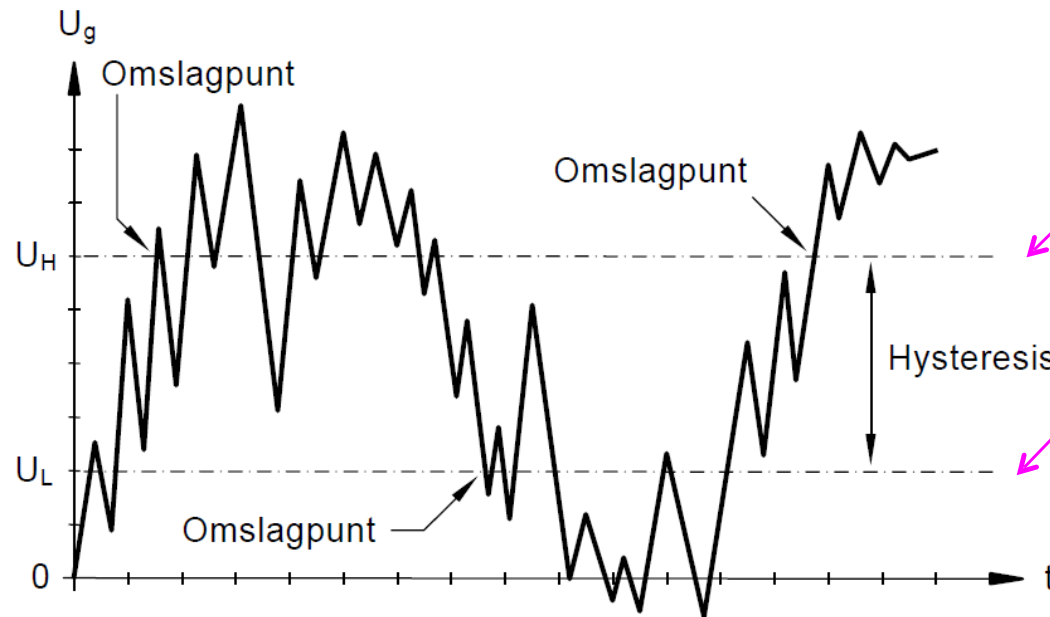
# Schmitt-trigger



Foutieve pulsreconstructie bij gewone comparatoren met signaalstoringen



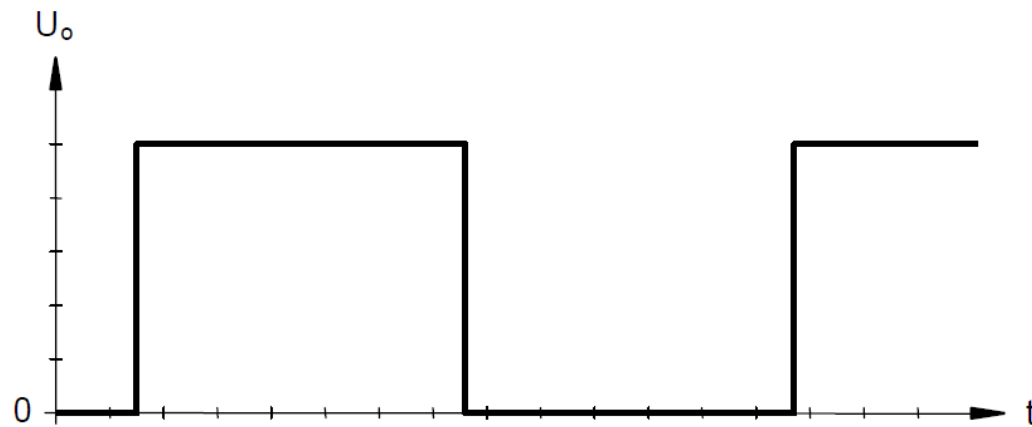
# Comparator met hysteresis



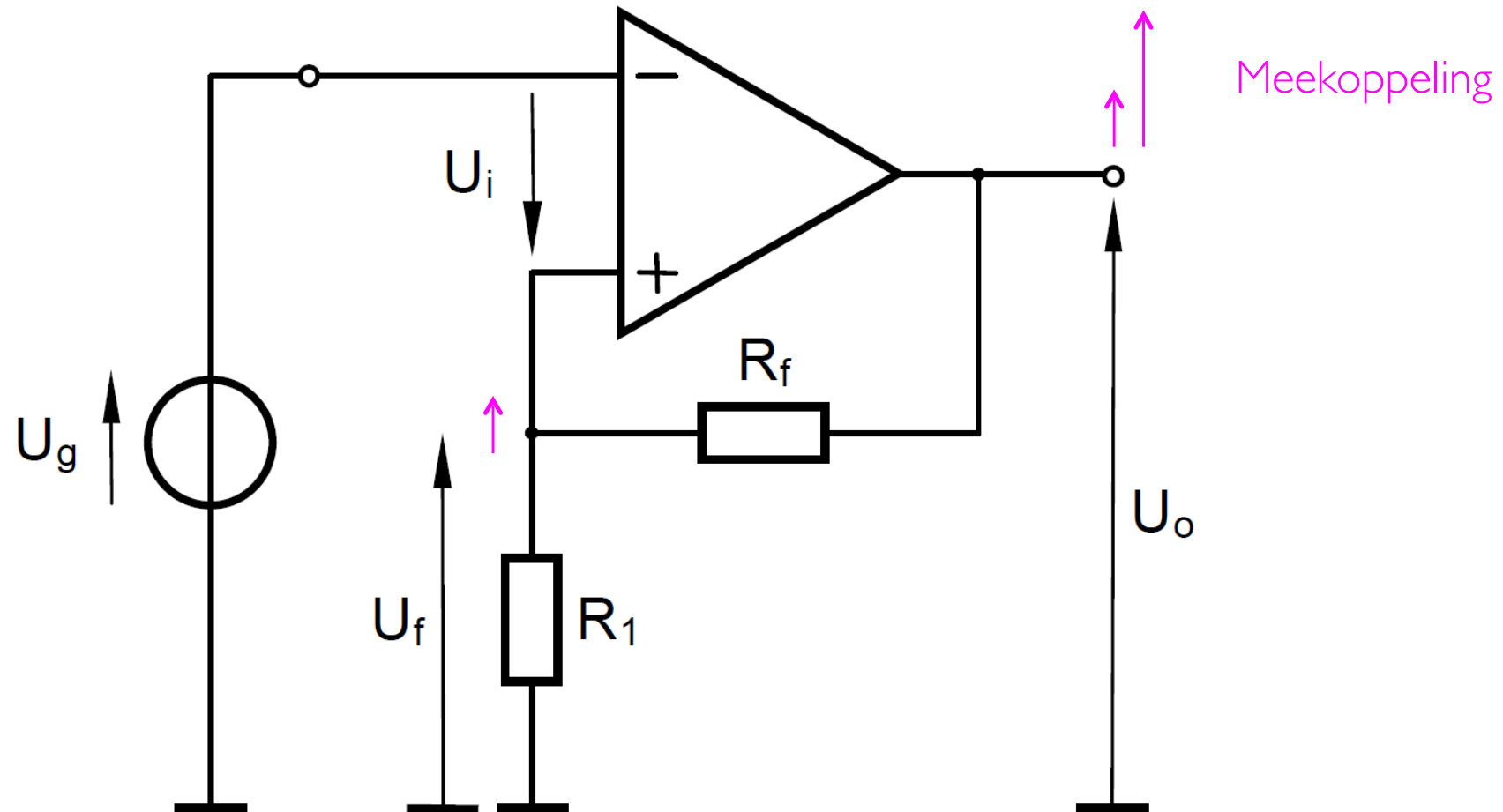
Hoog omklapniveau

Laag omklapniveau

Correcte pulsreconstructie bij een comparator met hysteresis = Schmitt-trigger met signaalstoringen

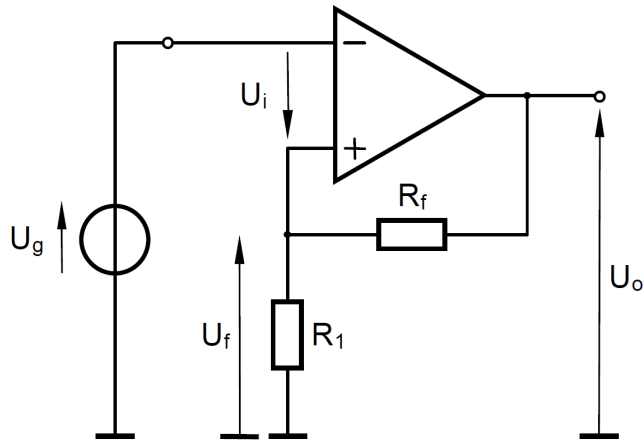


# Inverterende Schmitt-trigger





# Inverterende Schmitt-trigger



Wanneer de uitgangsspanning  $U_o$  op  $U_{sat+}$  staat

$$U_{(+)} = U_{sat+} \frac{R_1}{R_1 + R_f}$$

$$U_L = U_{sat+} \frac{R_1}{R_1 + R_f}$$

Zolang  $U_g < U_L$  blijft  $U_o = U_{sat+}$

Wordt nu echter  $U_g > U_L$  dan klapt de uitgang zeer snel om van  $U_{sat+}$  naar  $U_{sat-}$ .

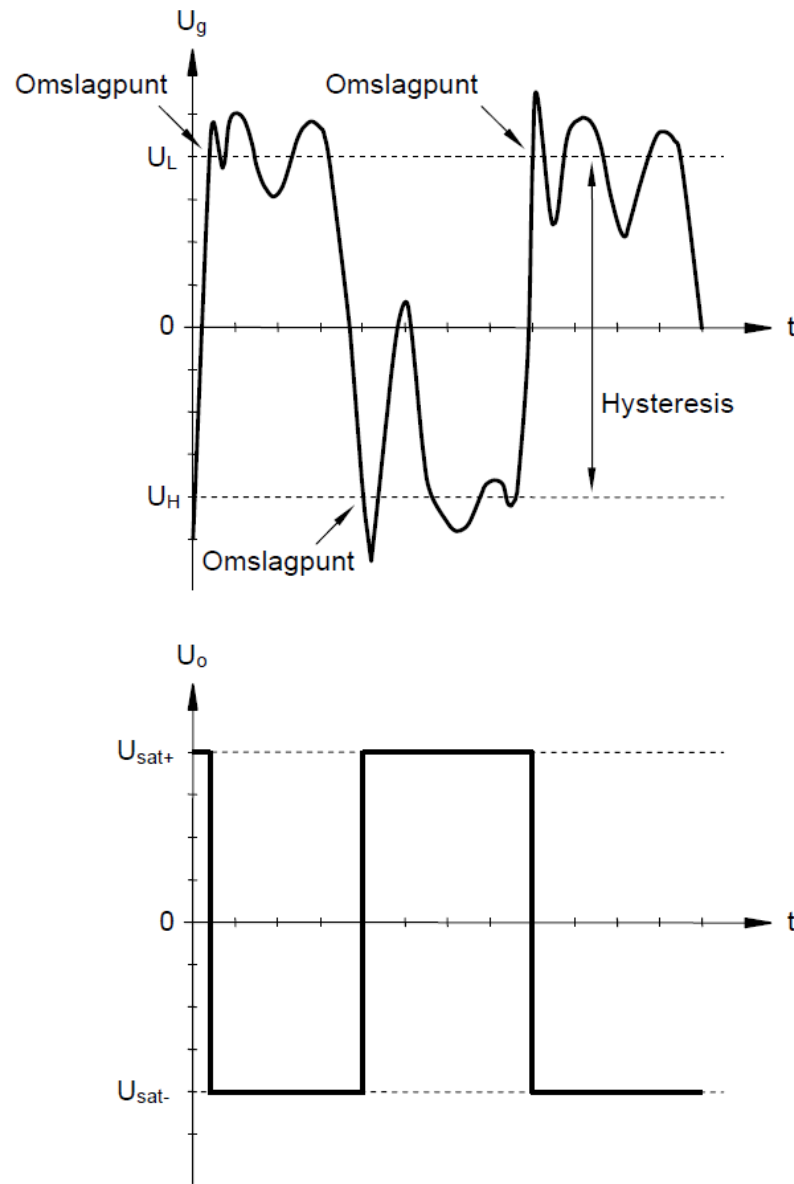
De nieuwe spanning ( $U_f$ ) op de (+) klem wordt

$$U_{(+)} = U_{sat-} \frac{R_1}{R_1 + R_f}$$

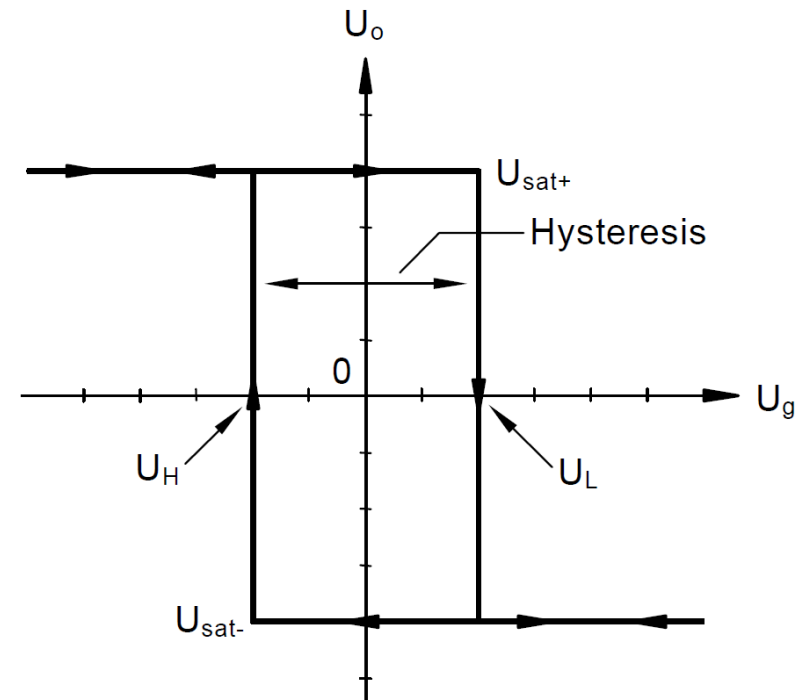
De ingangsspanning moet nu dalen tot onder dit niveau om de uitgang opnieuw te laten omschakelen van  $U_{sat-}$  naar  $U_{sat+}$ .

$$U_H = U_{sat-} \frac{R_1}{R_1 + R_f}$$

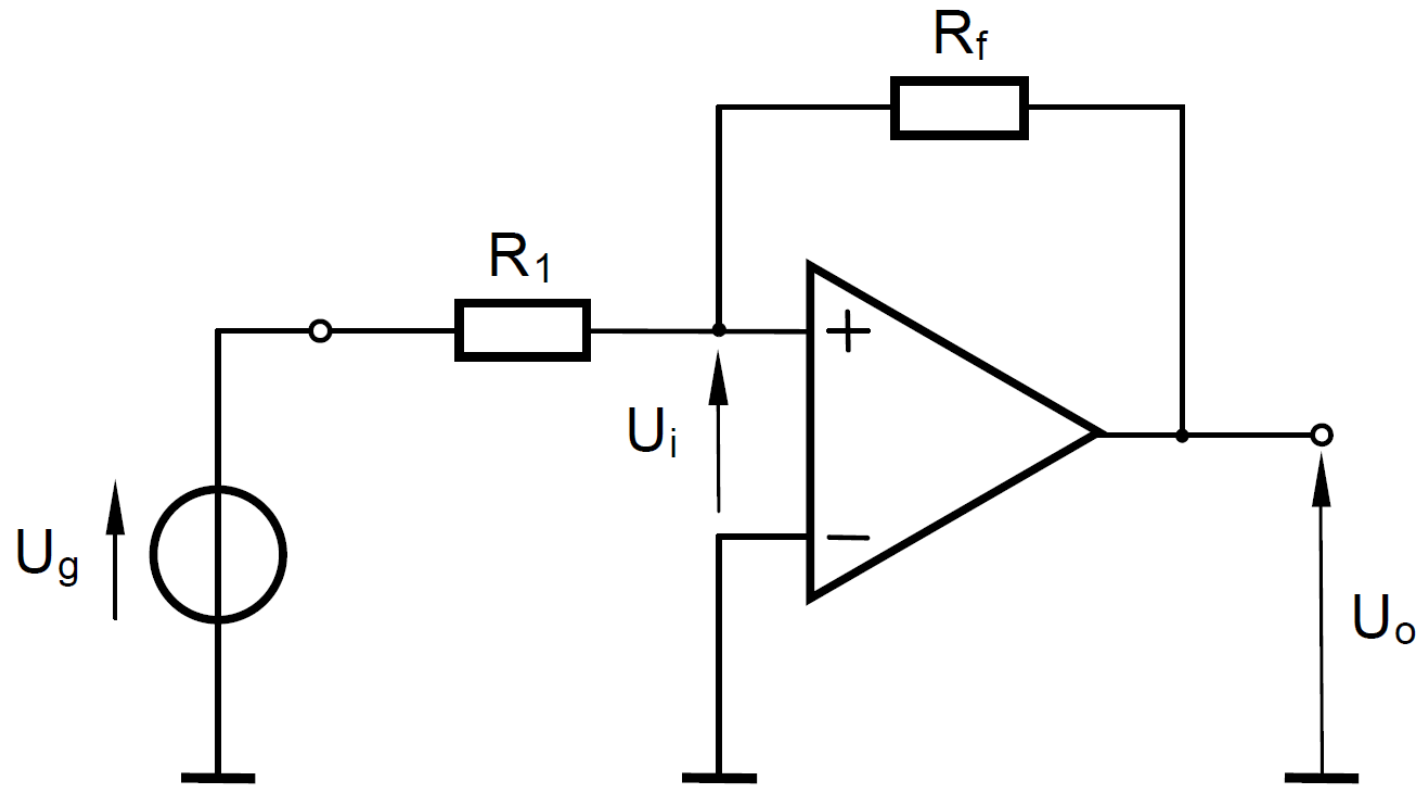
# Inverterende Schmitt-trigger



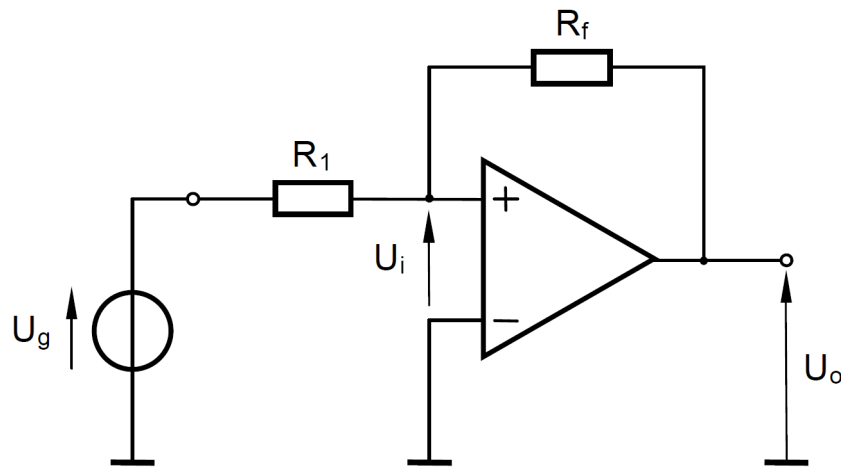
Transferkarakteristiek



# Niet-inverterende Schmitt-trigger



# Niet-inverterende Schmitt-trigger



Wanneer de uitgangsspanning  $U_o$  op  $U_{sat+}$  staat

Op het omschakelpunt ( $U_{(+)}=0V$ ) staat  $U_{sat+}$  over  $R_f$

$$I_{R_f} = \frac{U_{sat+}}{R_f}$$

$$U_L = -I_{R_f} \cdot R_1$$

$$U_L = -U_{sat+} \frac{R_1}{R_f}$$

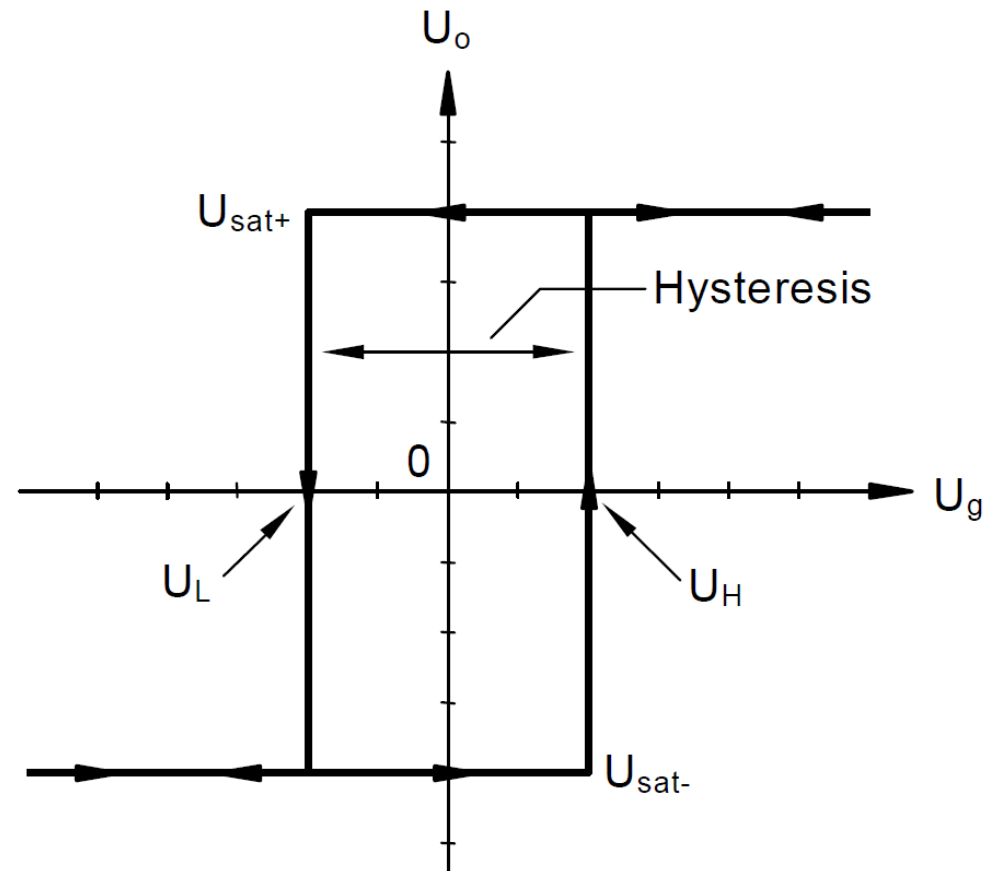
Wordt  $U_g < U_L$  dan klapt de uitgang zeer snel om van  $U_{sat+}$  naar  $U_{sat-}$

Op analoge wijze vinden we  $U_H$

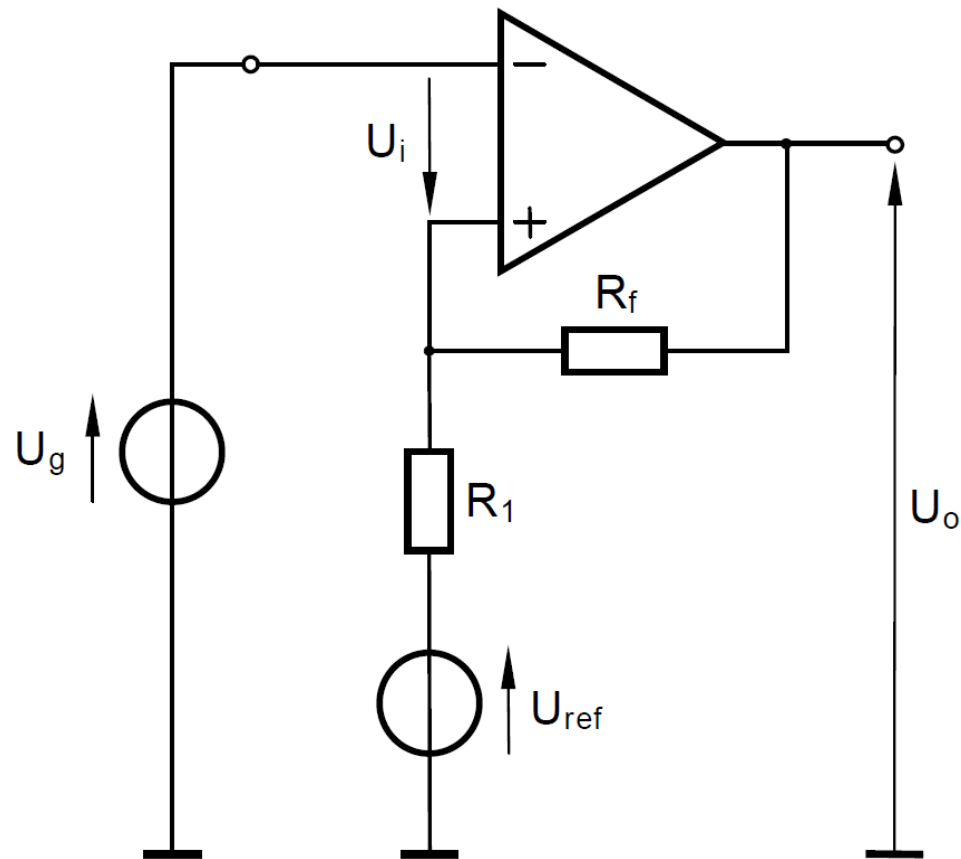
$$U_H = -U_{sat-} \frac{R_1}{R_f}$$

# Niet-inverterende Schmitt-trigger

Transferkarakteristiek



# Inverterende ST met referentiespanning

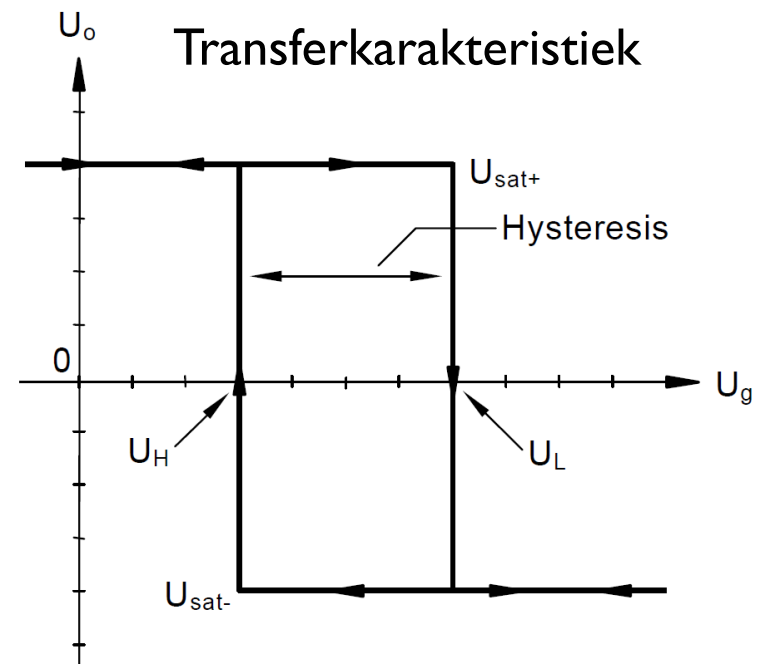


Schakelpunten

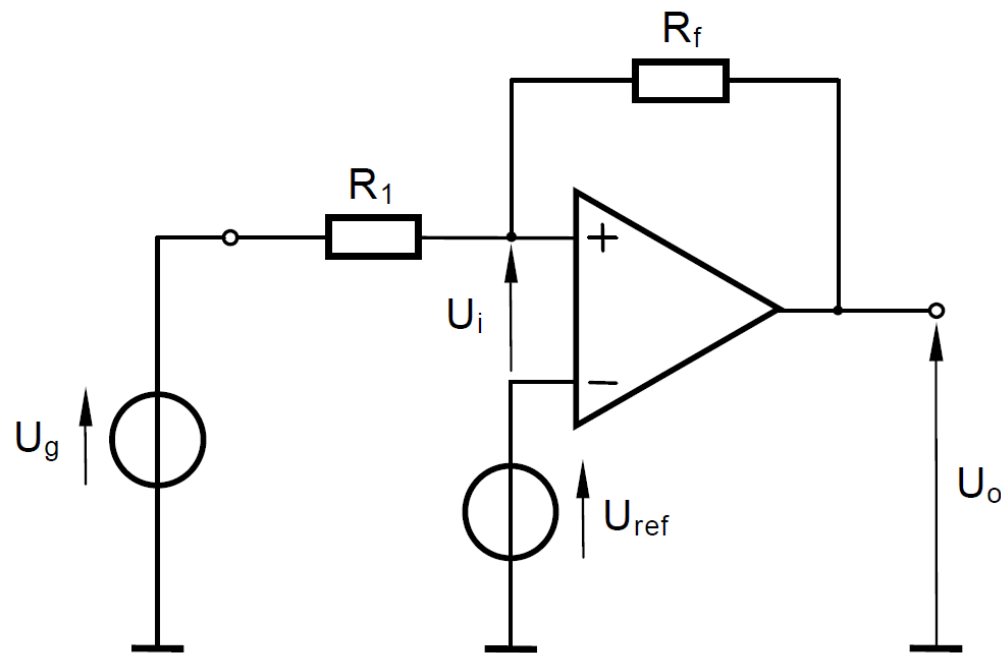
$$U_L = \frac{U_{ref} \cdot R_f + U_{sat+} \cdot R_2}{R_2 + R_f}$$

$$U_H = \frac{U_{ref} \cdot R_f + U_{sat-} \cdot R_2}{R_2 + R_f}$$

Transferkarakteristiek



# Niet-inverterende ST met referentiespanning

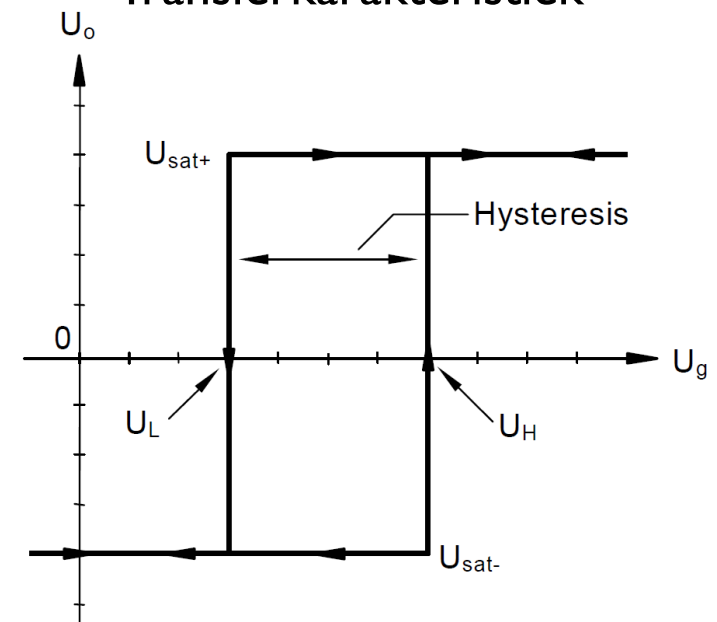


## Schakelpunten

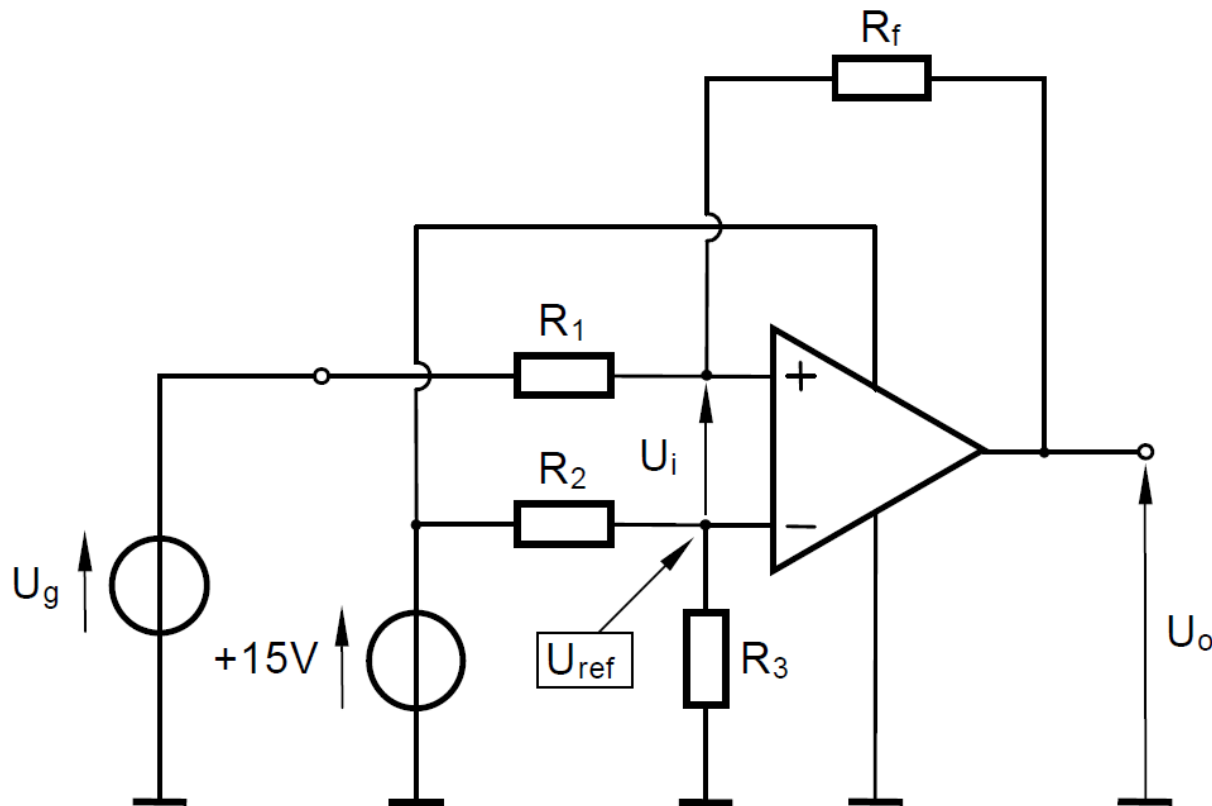
$$U_H = U_{ref} + \frac{R_1}{R_f} (U_{ref} - U_{sat-})$$

$$U_L = U_{ref} + \frac{R_1}{R_f} (U_{ref} - U_{sat+})$$

## Transferkarakteristiek



# Oefening



## Componenten

$R_1$ :  $20k\Omega$

$R_2$ :  $100k\Omega$

$R_3$ :  $200k\Omega$

$R_f$ :  $100k\Omega$

Niet-inverterende ST met referentiespanning



# Oefening

Bepaling  $U_{ref}$

$$U_{ref} = 15V \frac{R_3}{R_2 + R_f}$$

$$U_{ref} = 15V \frac{200k\Omega}{100k\Omega + 200k\Omega} = 10V$$

# Oefening

Berekening van de schakelpunten

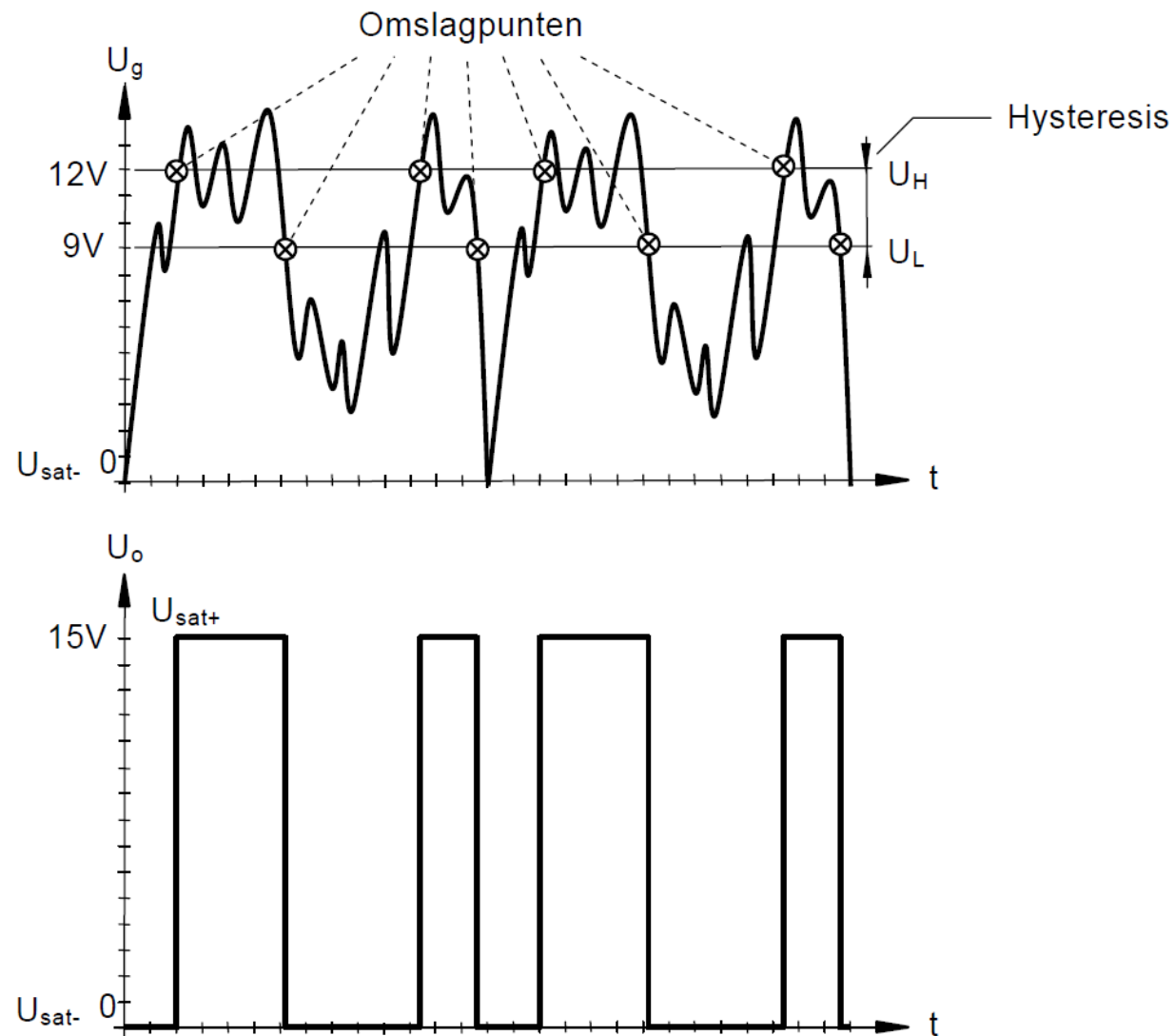
$$U_H = U_{ref} + \frac{R_1}{R_f} (U_{ref} - U_{sat-})$$

$$U_H = 10V + \frac{20k\Omega}{100k\Omega} (10V - 0V) = 12V$$

$$U_L = U_{ref} + \frac{R_1}{R_f} (U_{ref} - U_{sat+})$$

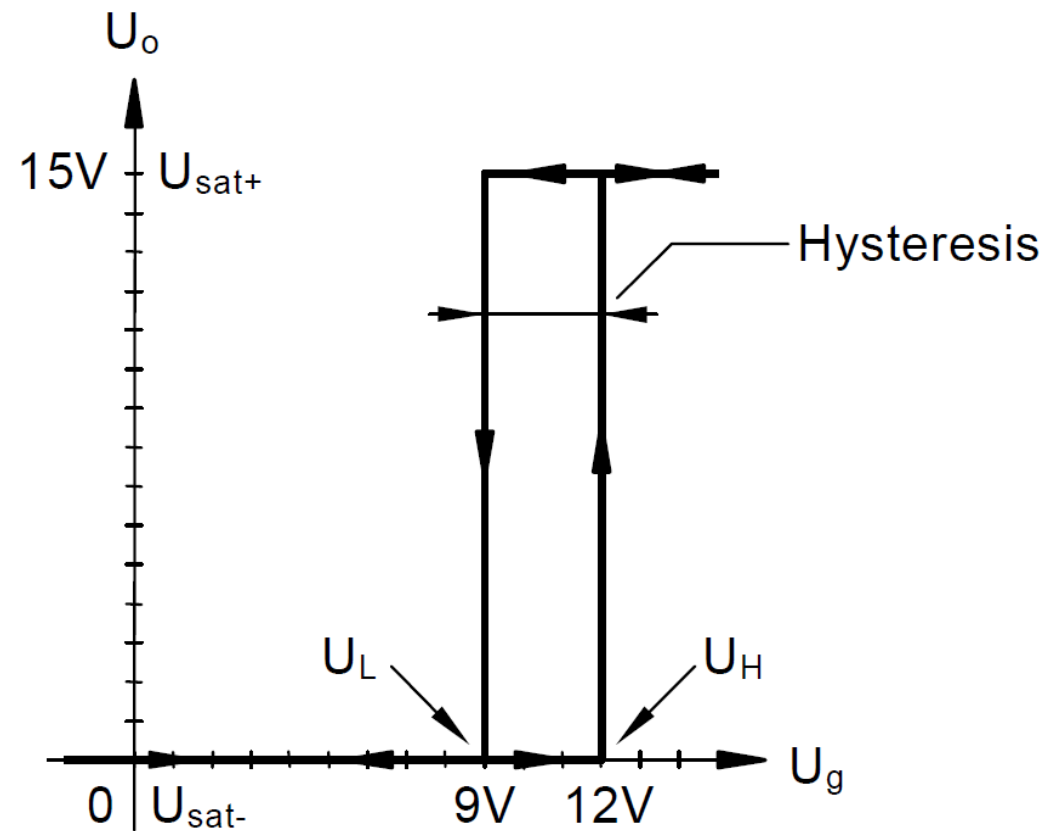
$$U_L = 10V + \frac{20k\Omega}{100k\Omega} (10V - 15V) = 9V$$

# Oefening

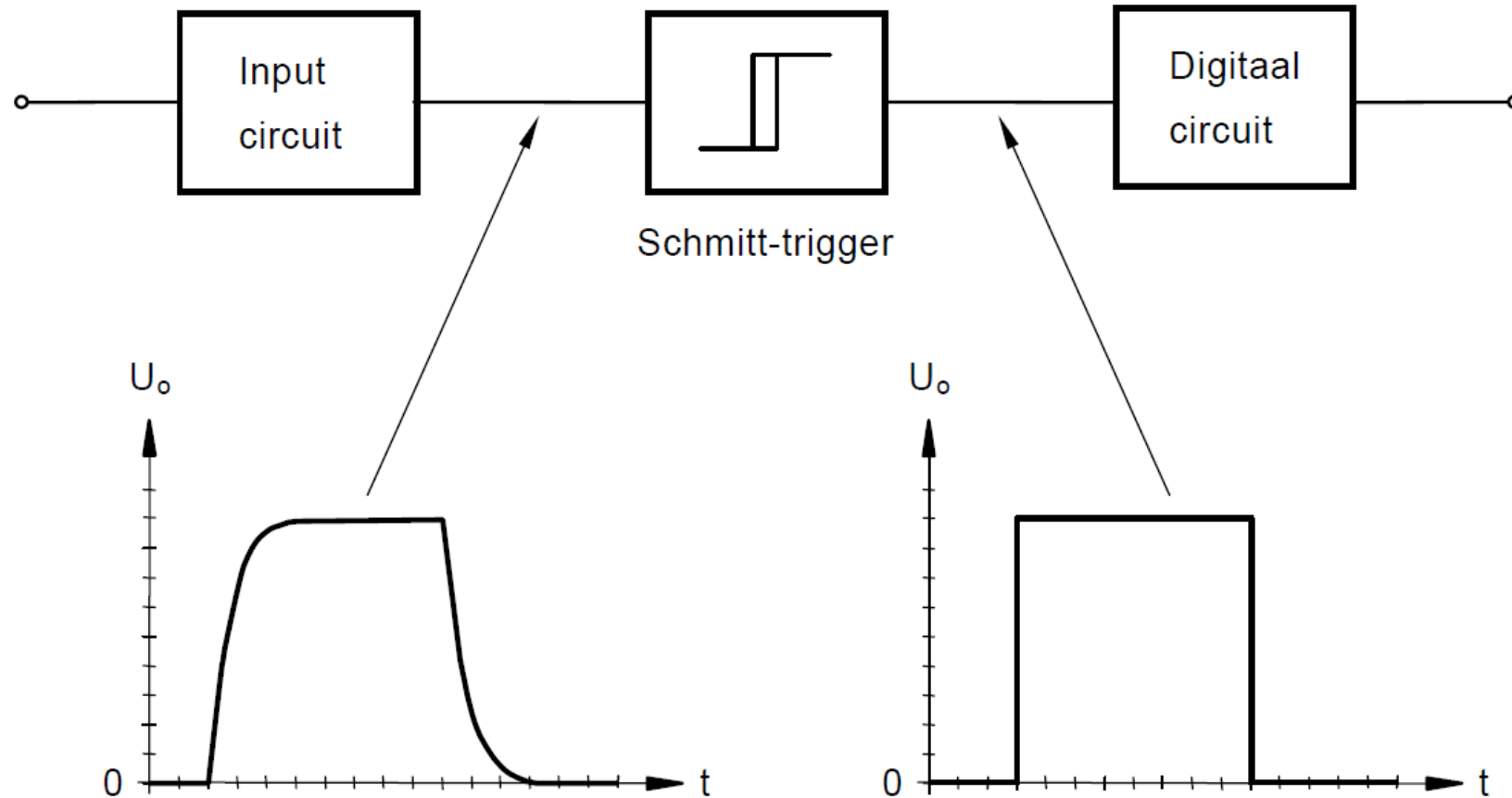


# Oefening

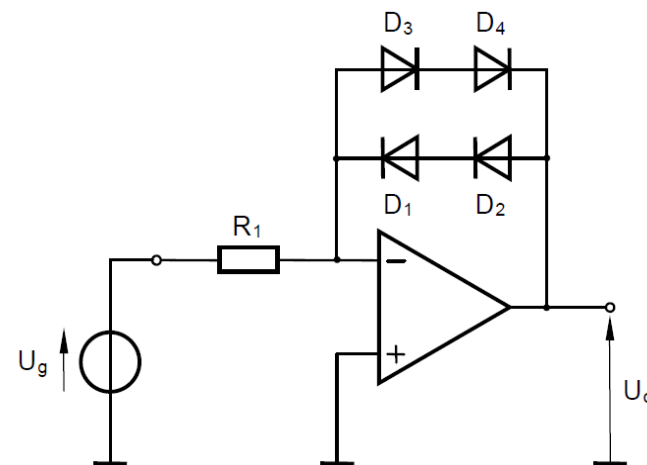
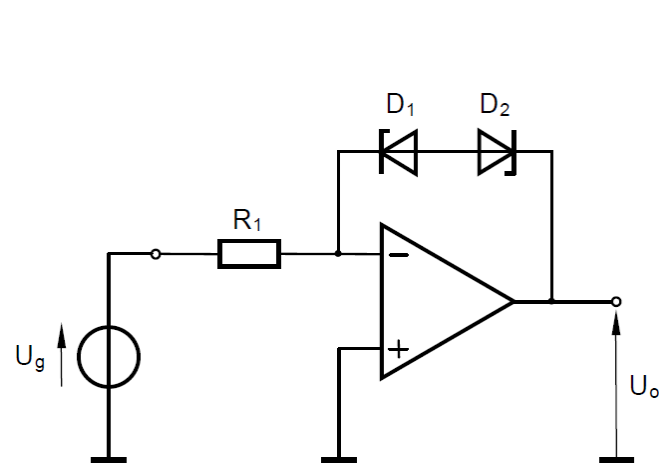
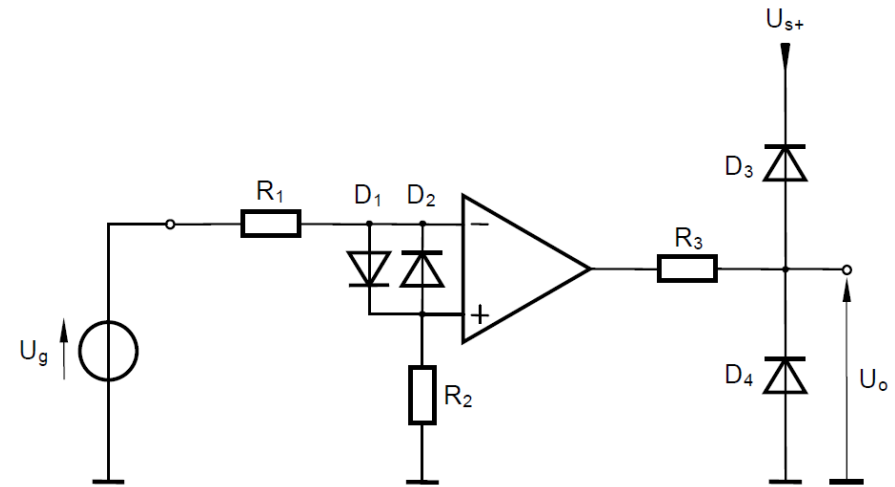
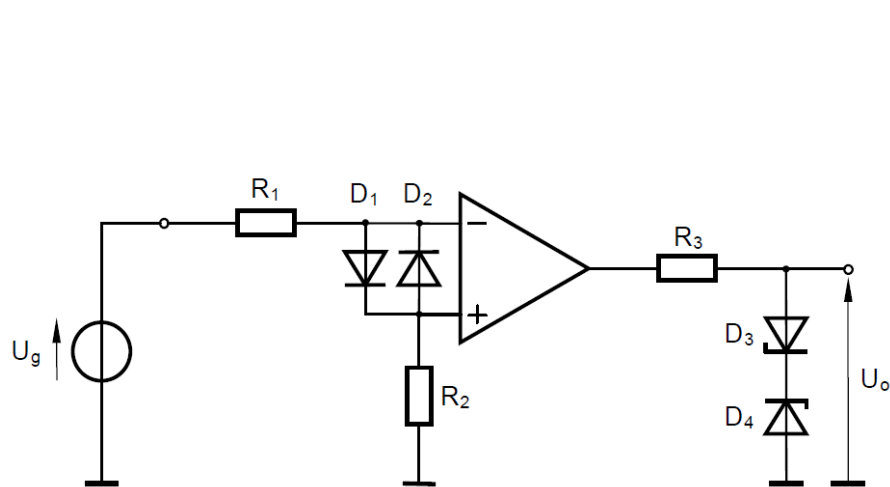
## Transferkarakteristiek



# Schmitt-trigger als pulsvormer



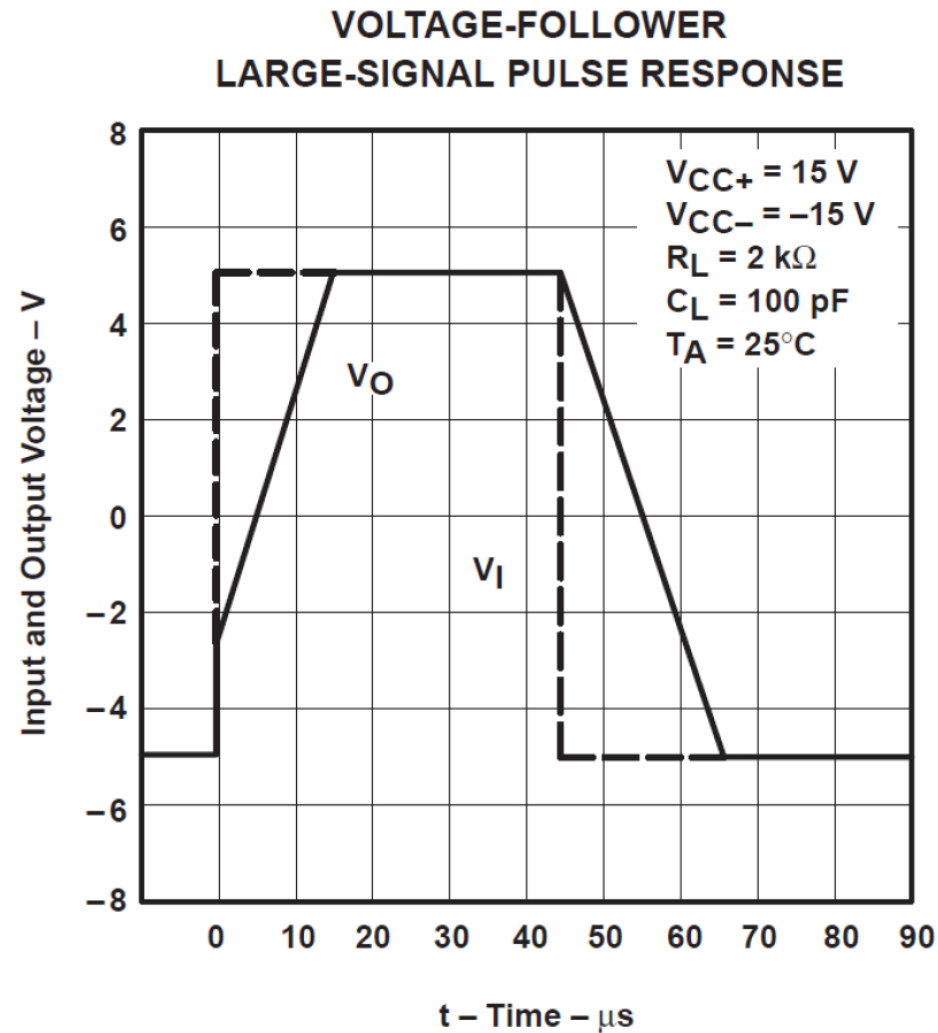
# Beveiliging en begrenzing



# Eigenschaften comparatoren

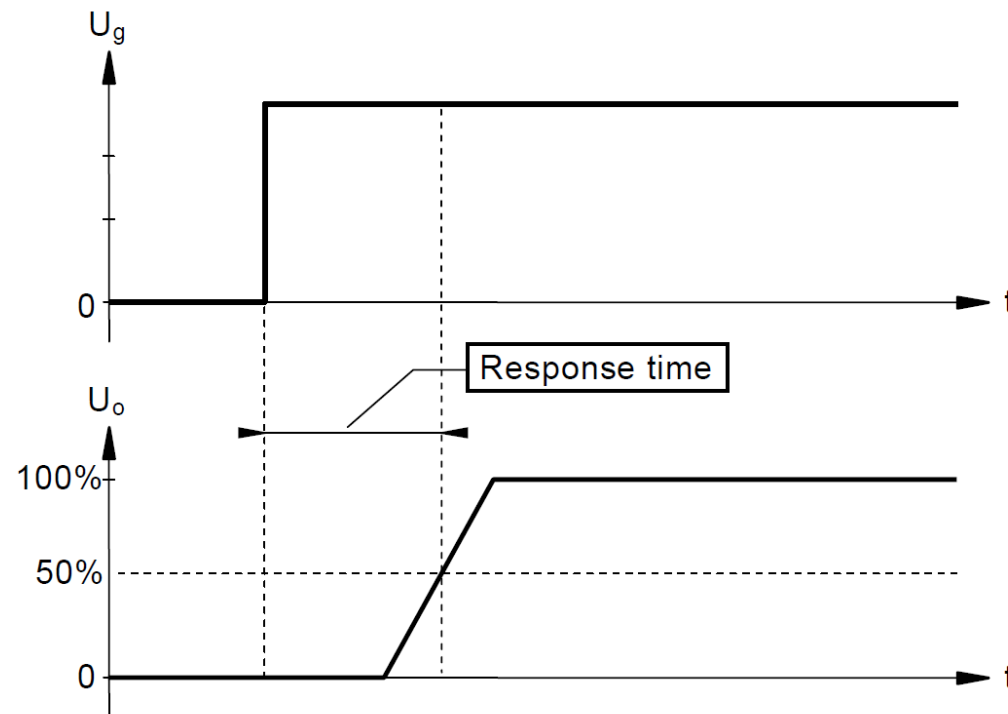
Slew rate

$$SR = \left( \frac{\Delta U_o}{\Delta t} \right)_{max}$$



# Eigenschappen comparatoren

Response time



Ingangs offset-spanning

Input Bias Current