

# Aerospace Propulsion

Lecture 10

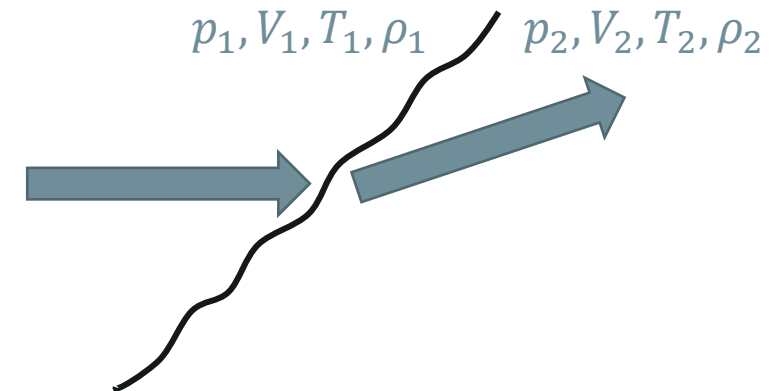
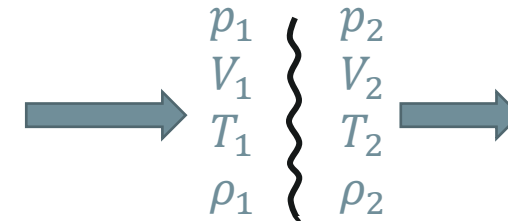
Compressible Flows: Part IV

# Compressible Flows: Part IV

- Isentropic Shocks?
- Expansion Waves
- Advanced Compressible Flows
- Shocks and Expansions + Nozzles

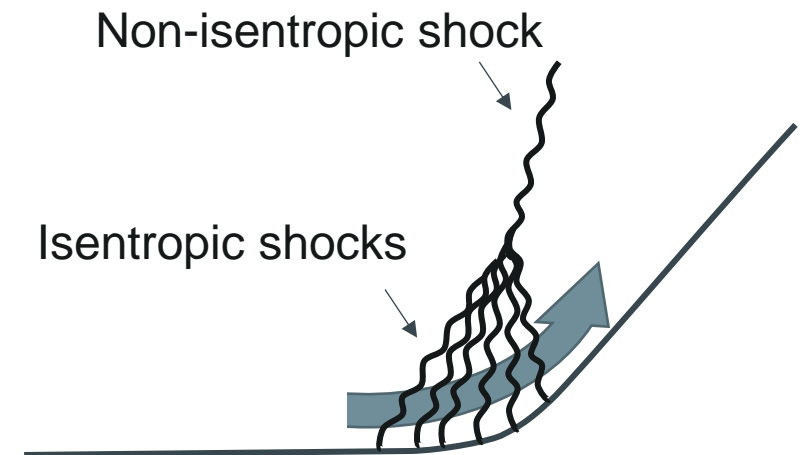
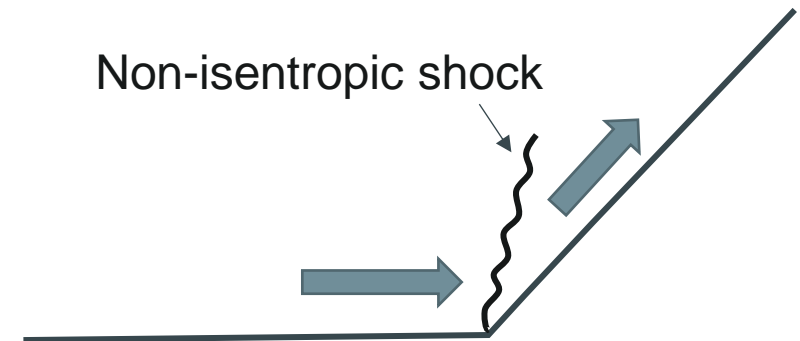
# Isentropic Shocks?

- Previously, we discussed normal and oblique shocks, both of which are **non-isentropic**
- We can (but will not) show that shocks can be isentropic if their angle and therefore effect (e.g., pressure change across shock) is infinitesimal



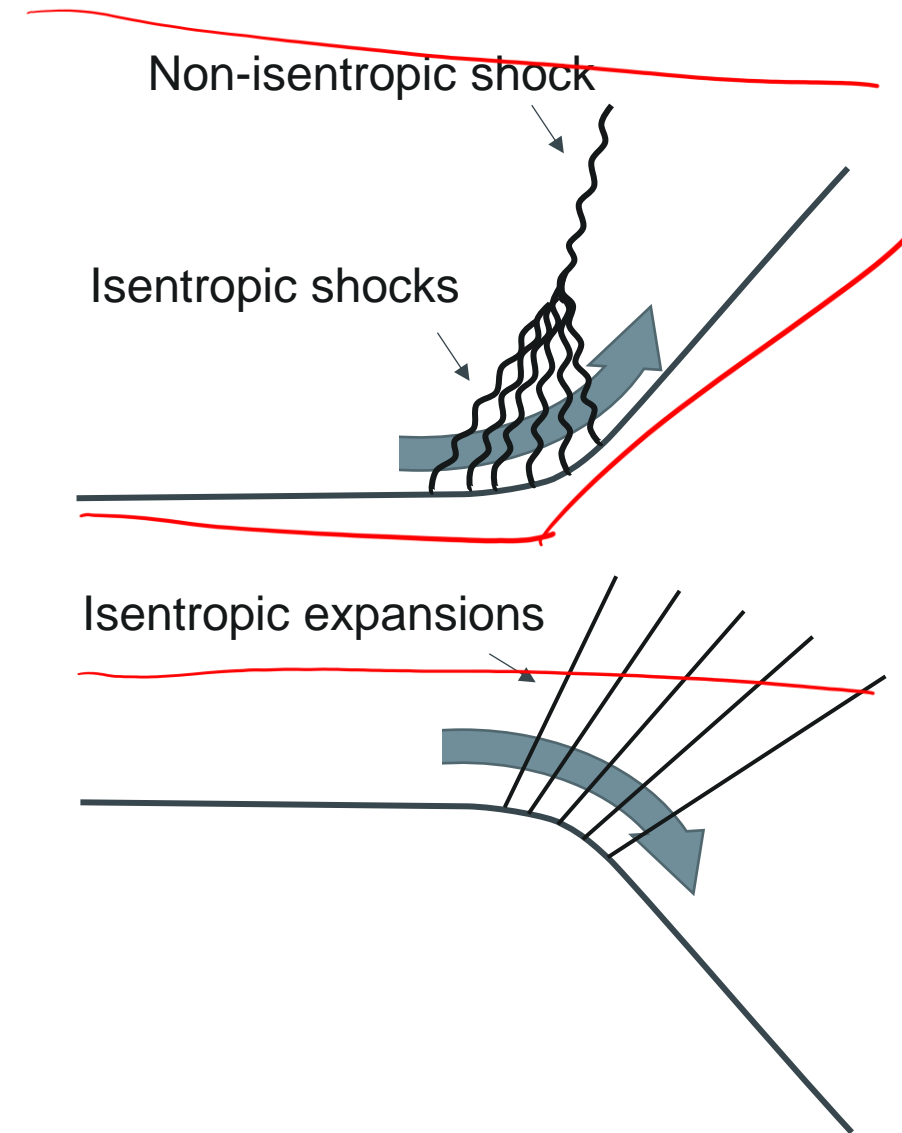
# Isentropic Shocks?

- How do we take an infinitesimal effect and make it significant?
  - Many (approaching infinite) shocks
    - Possible with e.g., smoothly curved wall
- Infinitesimal oblique shocks nearly always coalesce into a single oblique shock
  - Rarely consider such shocks because coalescence is so close to wall
    - Assume obliques are always non-isentropic



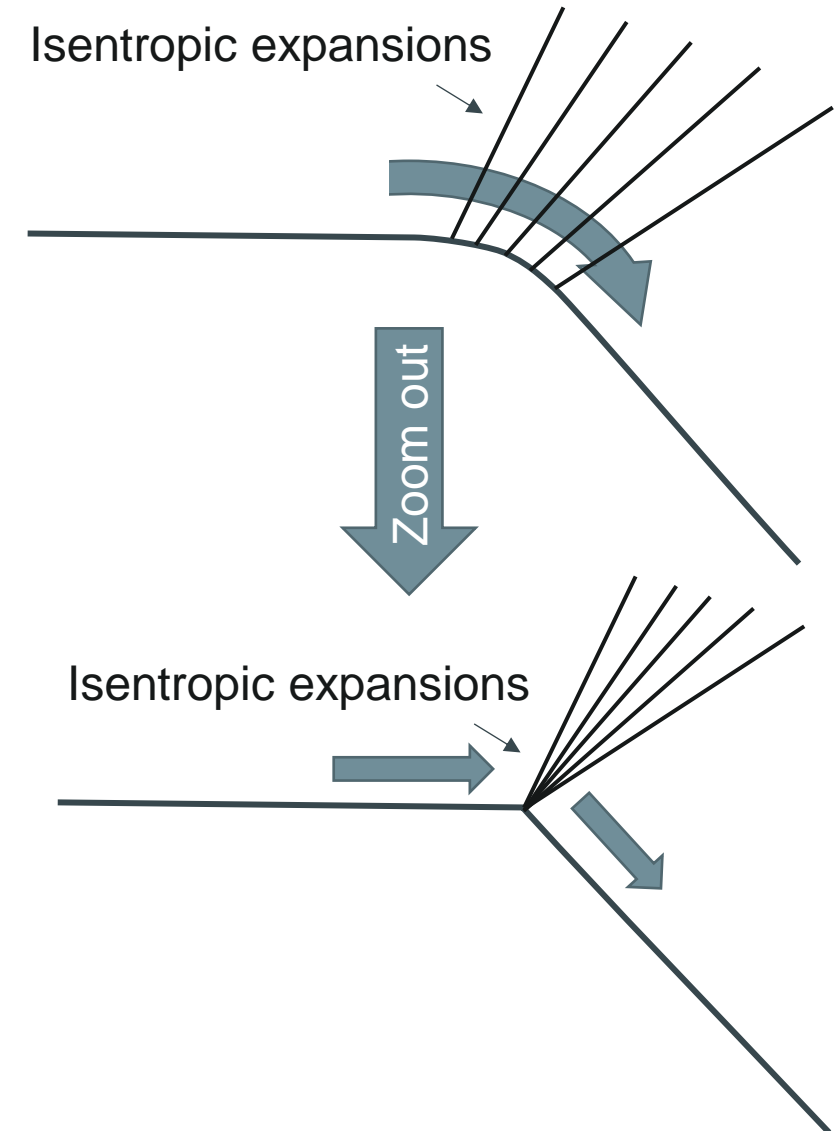
# Expansion Waves

- So far, we've only explored compressions
- What about expansions?
- Just like we had isentropic compression waves (oblique shocks), we can have isentropic expansion waves
- Expansion waves increase Mach number and decrease pressure



# Expansion Waves

- Due to the geometry of expansion waves, they **do not** coalesce
  - All expansion waves are isentropic
- Also called Prandtl-Meyer Flow
- We will not calculate state changes across expansion waves in this course
  - See Farokhi 2.14 if interested
  - Generally, isentropic equations hold

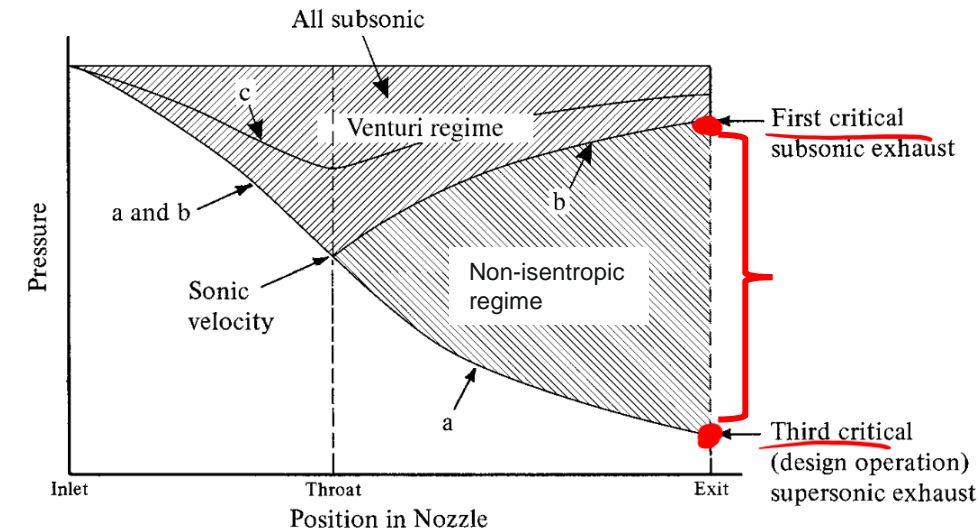


# Advanced Compressible Flows

- Only four lectures on compressible flows – focused on essentials
- Some slightly more advanced concepts if interested:
  - Duct flow with Heat Transfer (e.g., combustor) a.k.a *Rayleigh Flow*
    - See Farokhi 2.15
  - Duct flow with Friction (i.e., boundary layers) a.k.a *Fanno Flow*
    - See Farokhi 2.16
- We will stick to our simple (but reasonably accurate) approximations throughout the remainder of this course

# Shocks and Expansions + Nozzles

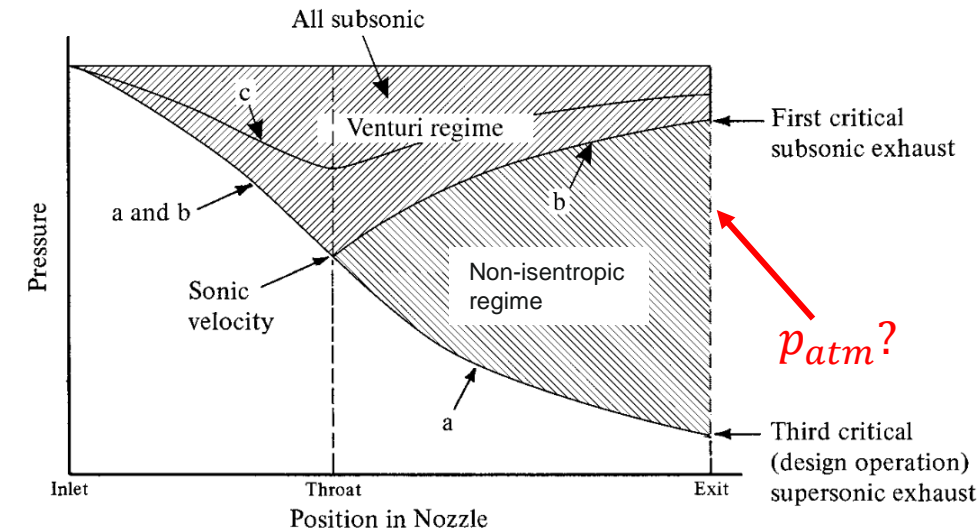
- In previous discussions about nozzles, we only focused on isentropic behavior
- Quick summary:
  - For a given inlet pressure, if the throat reaches sonic conditions ( $M_2 = 1$ ), there are only two possible outlet Mach numbers for an isentropic nozzle
    - Subsonic outlet – first critical (higher pressure)
    - Supersonic outlet – third critical (lower pressure)
- What happens at outlet pressures between the first and third critical?





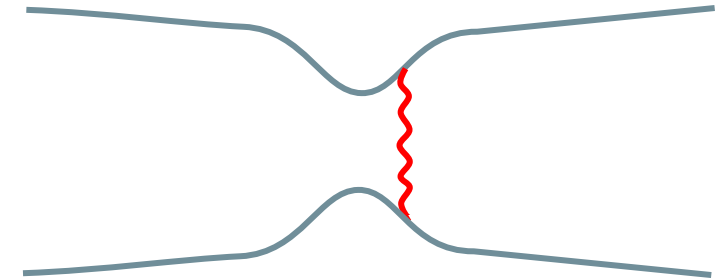
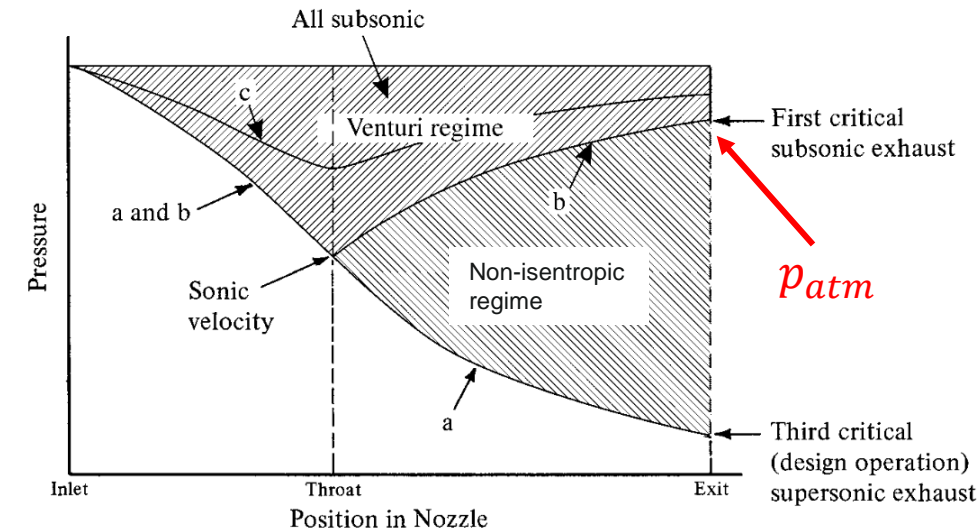
# Shocks and Expansions + Nozzles

- Remember, we need outlet pressure to match outside pressure
- What if outside pressure is  $p_{atm}$  as shown on the right?
  - For the given inlet pressure and area ratio, this is isentropically impossible
  - Luckily, we learned about non-isentropic compressible flows in last lecture



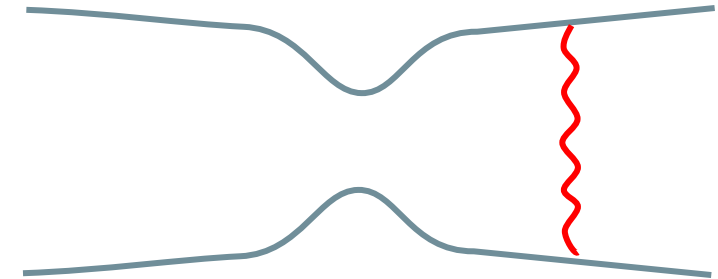
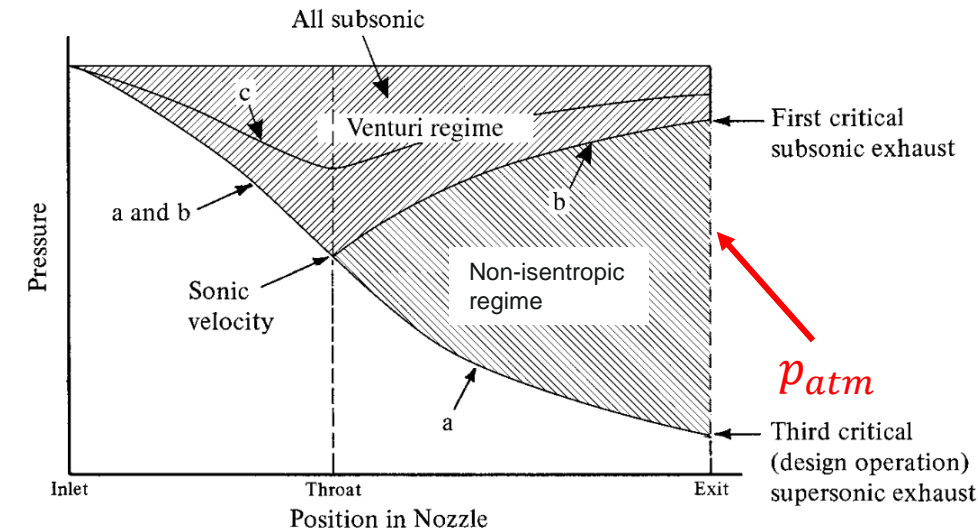
# Shocks and Expansions + Nozzles

- Imagine an outside pressure slightly below the outlet pressure
  - Need a small non-isentropic adjustment
- A normal shock will form slightly downstream of the throat
  - The Mach number before the shock will be slightly larger than 1
  - The Mach number after the shock will be slightly smaller than 1
  - The pressure after the shock will be slightly higher than before the shock



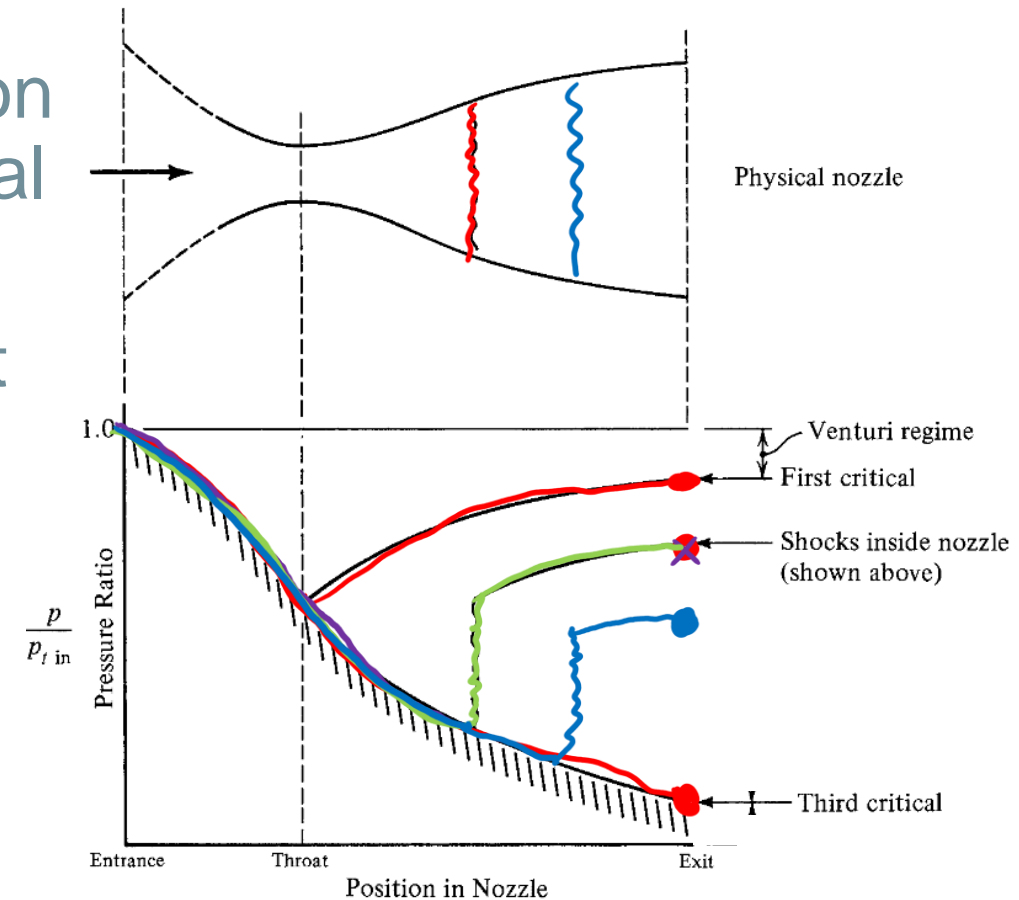
# Shocks and Expansions + Nozzles

- Imagine an outside pressure far below the outlet pressure
  - Need a larger non-isentropic adjustment
- A normal shock will form far downstream of the throat
  - The Mach number before the shock will be larger than 1
  - The Mach number after the shock will be smaller than 1
  - The pressure after the shock will be higher than before the shock



# Shocks and Expansions + Nozzles

- The normal shock occurs at the location that guarantees outlet pressure is equal to outside pressure
- The bigger the difference between first critical and outlet pressure, the further downstream the shock
  - Stronger shock to make up the remaining pressure difference
- After the shockwave, flow is subsonic
  - Subsonic diffuser



# Shocks and Expansions + Nozzles

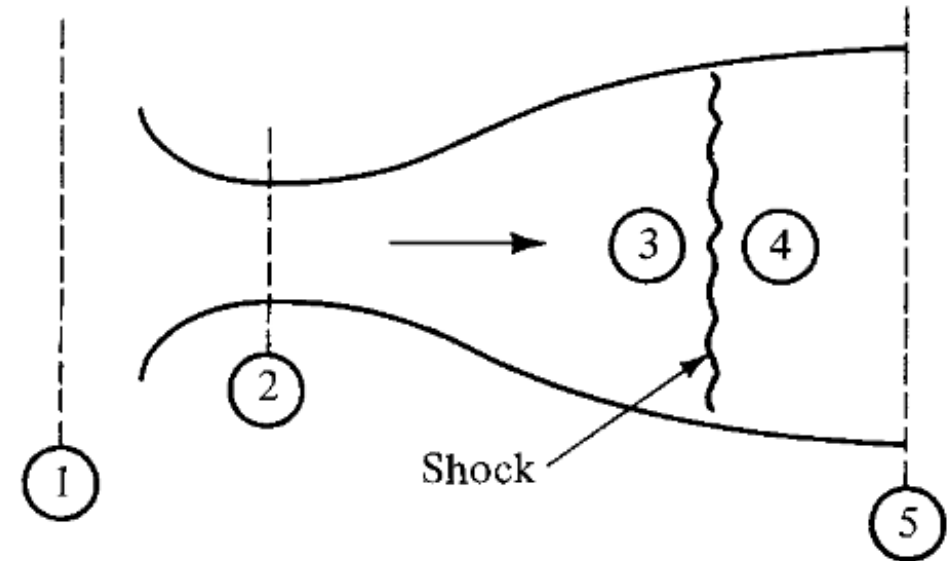
- Nozzle shock analysis

- 1 → 2: Subsonic Nozzle
- 2: Sonic Throat
- 2 → 3: Supersonic Nozzle
- 3 → 4: Normal Shock
- 4 → 5: Subsonic Diffuser
- 5: Outlet Pressure = Outside Pressure

isentropic

non-isentropic

isentropic



# Shocks and Expansions + Nozzles

- Example:
- Find the location of the shock (area ratio at shock)

- $\frac{A_5}{A_2} = 2.5$

- $M_5 = 0.38$

$$\frac{A_5}{A_4} = \frac{M_4}{M_5} \left( \frac{1 + \frac{\gamma-1}{2} M_5^2}{1 + \frac{\gamma-1}{2} M_4^2} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (1)$$

$$\frac{A_3}{A_2} = \frac{M_2}{M_3} \left( \frac{1 + \frac{\gamma-1}{2} M_3^2}{1 + \frac{\gamma-1}{2} M_2^2} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (2)$$

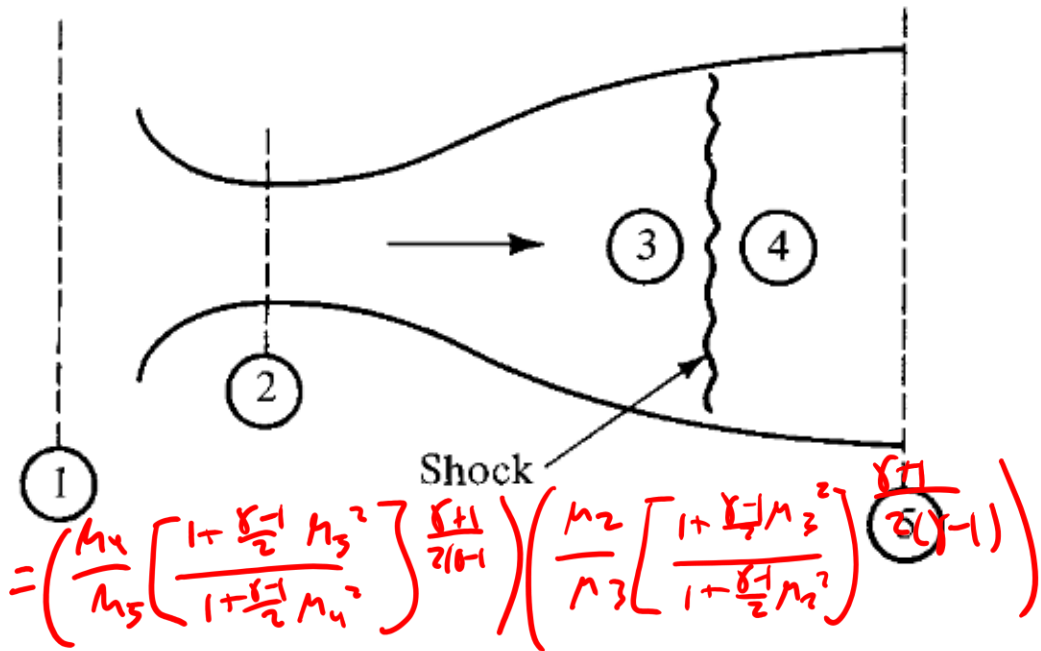
3 Eqs.

Joint know:  $\frac{A_5}{A_4}$ ,  $\frac{A_3}{A_2}$ ,  $M_3$ ,  $M_4$

$$\frac{A_5}{A_2} = \frac{A_5}{A_4} \frac{A_4}{A_2} \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{combine}$$

$$A_3 = A_4$$

$$\frac{A_5}{A_2} = \frac{A_5}{A_4} \frac{A_3}{A_2} \quad (3)$$



$$\frac{A_5}{A_2} = \left( \frac{M_4}{M_5} \left[ \frac{1 + \frac{\gamma-1}{2} M_5^2}{1 + \frac{\gamma-1}{2} M_4^2} \right]^{\frac{\gamma+1}{2(\gamma-1)}} \right) \left( \frac{M_2}{M_3} \left[ \frac{1 + \frac{\gamma-1}{2} M_3^2}{1 + \frac{\gamma-1}{2} M_2^2} \right]^{\frac{\gamma+1}{2(\gamma-1)}} \right)$$

$$M_4^2 = M_3^2 + \frac{2}{\gamma-1}$$

$$\frac{2\gamma}{\gamma-1} M_3^2 - 1$$

2 Eqs.

2 unknowns.

Solve for  $M_3$ ,  $M_4$



# Shocks and Expansions + Nozzles

- How to numerically solve the previous example
  - Use whatever solver you're comfortable with

Wolframalpha.com

solve  $2.5 = \left( \frac{y}{0.38} \right) \left( \frac{(1+0.2 \cdot (0.38)^2)}{(1+0.2 \cdot y^2)} \right)^3 \left( \frac{1}{x} \right) \left( \frac{(1+0.2 \cdot x^2)}{(1+0.2)} \right)^3, y^2 = \frac{\left( x^2 + \frac{2}{.4} \right)}{\left( \frac{2.8}{0.4} \cdot x^2 - 1 \right)}$

$x = -2.19905 - 2.79202i$  and  $y = 0.366778 - 0.0766685i$   
 $x = -2.19905 + 2.79202i$  and  $y = 0.366778 + 0.0766685i$   
 $x = -2.12311$  and  $y = -0.557837$   
 $x = -0.893595 - 4.16855i$  and  $y = -0.326835 + 0.0249879i$   
 $x = -0.893595 + 4.16855i$  and  $y = -0.326835 - 0.0249879i$   
 $x = -0.579062 - 0.337033i$  and  $y = -1.09242 + 0.827722i$   
 $x = -0.579062 + 0.337033i$  and  $y = -1.09242 - 0.827722i$   
 $x = -0.349386 - 0.0962593i$  and  $y = 1.73061 - 2.63062i$   
 $x = -0.349386 + 0.0962593i$  and  $y = 1.73061 + 2.63062i$   
 $x = -0.312505 - 0.0289573i$  and  $y = -0.721048 + 3.76825i$   
 $x = -0.312505 + 0.0289573i$  and  $y = -0.721048 - 3.76825i$   
 $x = -0.761701i$  and  $y = -0.93448i$   
 $x = 0.761701i$  and  $y = 0.93448i$   
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 $x = 2.19905 + 2.79202i$  and  $y = -0.366778 + 0.0766685i$

Find real, non-negative solution →

Excel

Guess		Normal Shock Relation	$A_5/A_2$		Other side of equation
M3	M4	LHS	RHS	DIFF	
2	0.57735027	2.5	2.30095202	0.199048	
2.1	0.56127694	2.5	2.46023172	0.0397683	
2.11	0.55977648	2.5	2.47730087	0.0226991	
2.12	0.55829419	2.5	2.49458273	0.0054173	
2.13	0.55682978	2.5	2.51207867	-0.0120787	
2.14	0.55538294	2.5	2.52979008	-0.0297901	
2.15	0.55395342	2.5	2.54771835	-0.0477184	

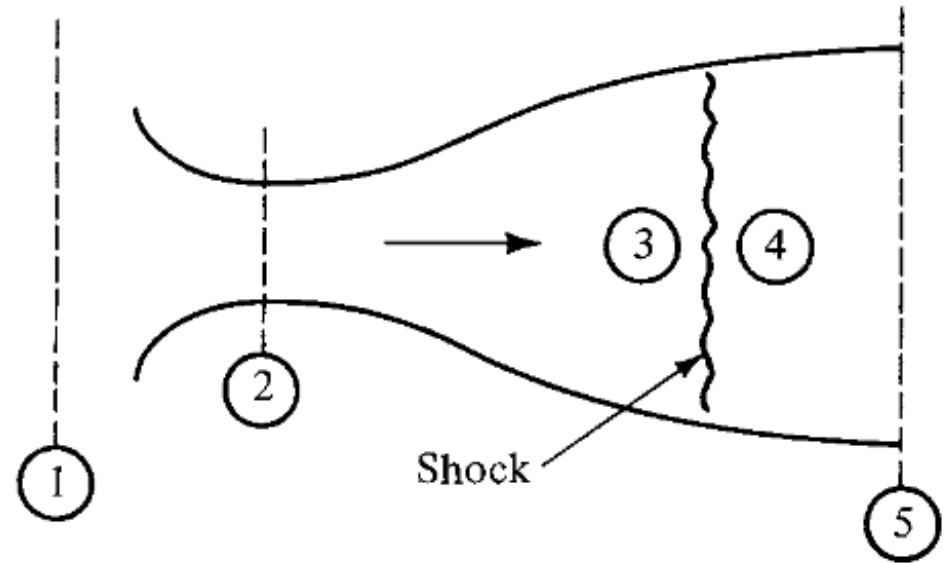
# Shocks and Expansions + Nozzles

- Example:
- Find the location of the shock (area ratio at shock)

- $\frac{A_5}{A_2} = 2.5$
- $M_5 = 0.38$
- $M_3 = 2.12$
- $M_4 = 0.56$

$$\frac{A_3}{A_2} = \frac{A_2}{A_3} \left( \frac{1 + \frac{\gamma-1}{2} M_3^2}{1 + \frac{\gamma-1}{2} M_2^2} \right)^{\frac{\gamma+1}{2(\gamma-1)}}$$

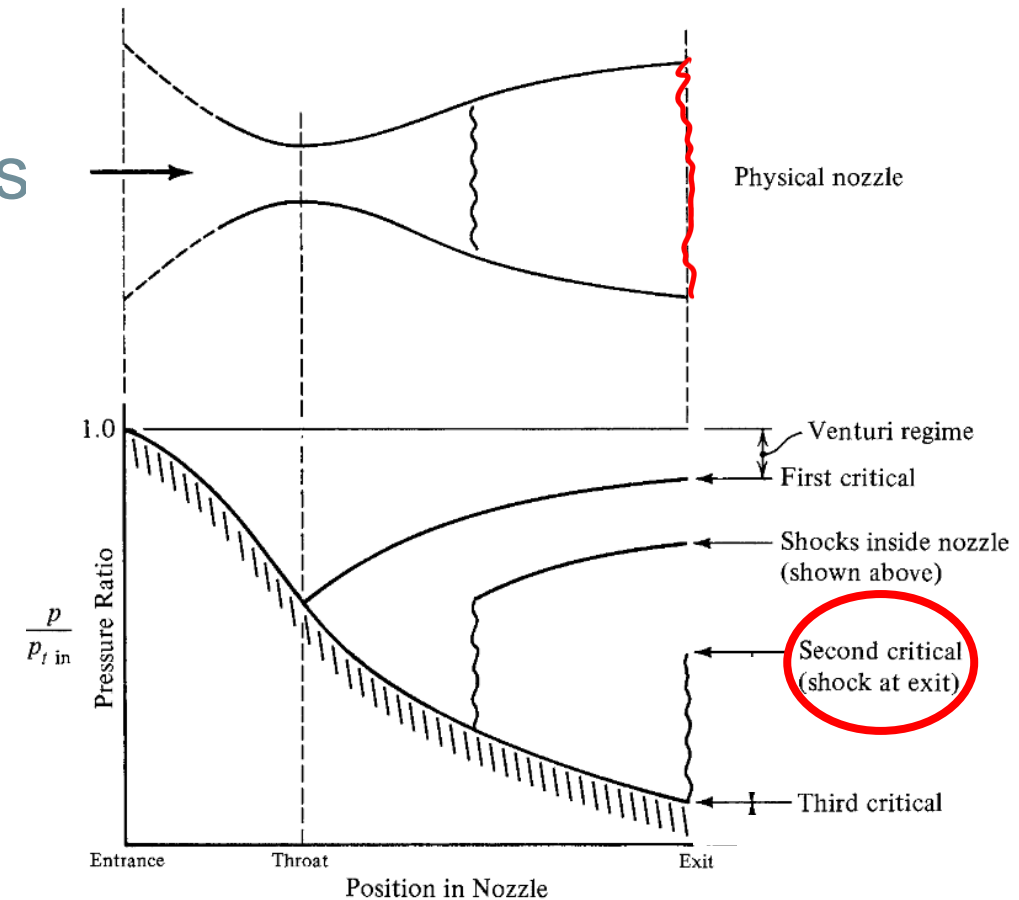
$$\frac{A_3}{A_2} = 1.67$$





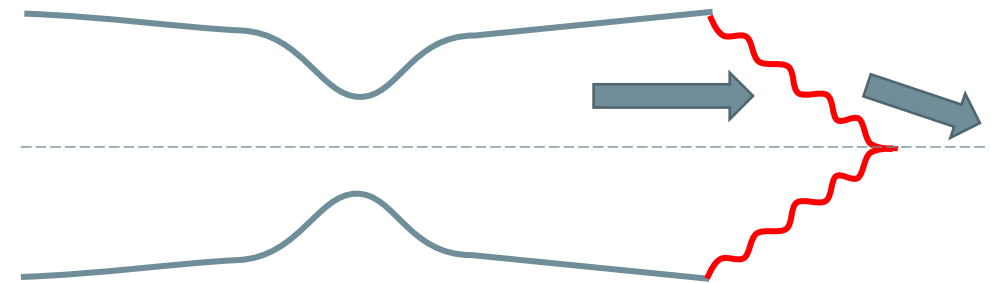
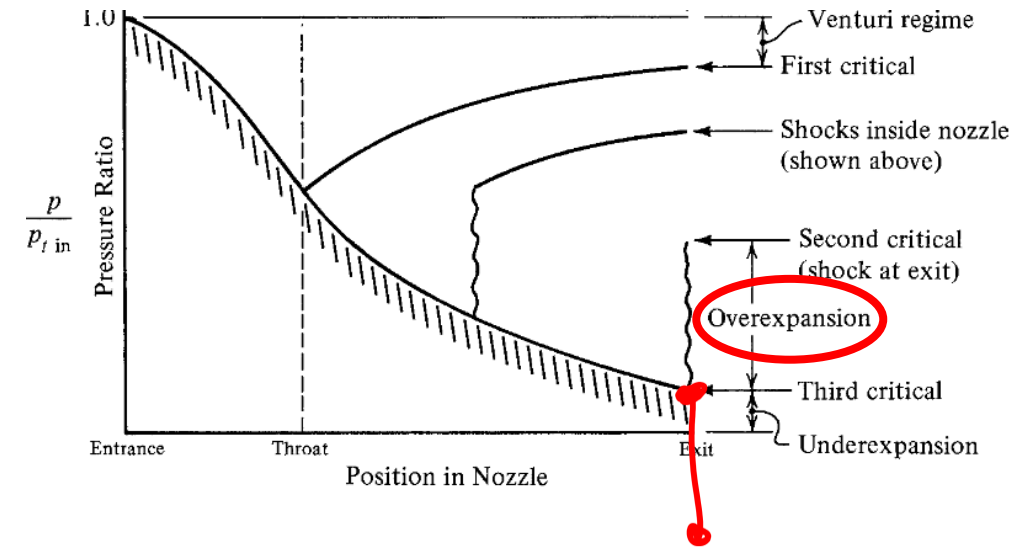
# Shocks and Expansions + Nozzles

- If we keep lowering the outside pressure, eventually the shock reaches the outlet
  - This is the second critical limit
  - Corresponds to the strongest shock possible within the nozzle
- What if we keep lowering the outside pressure...



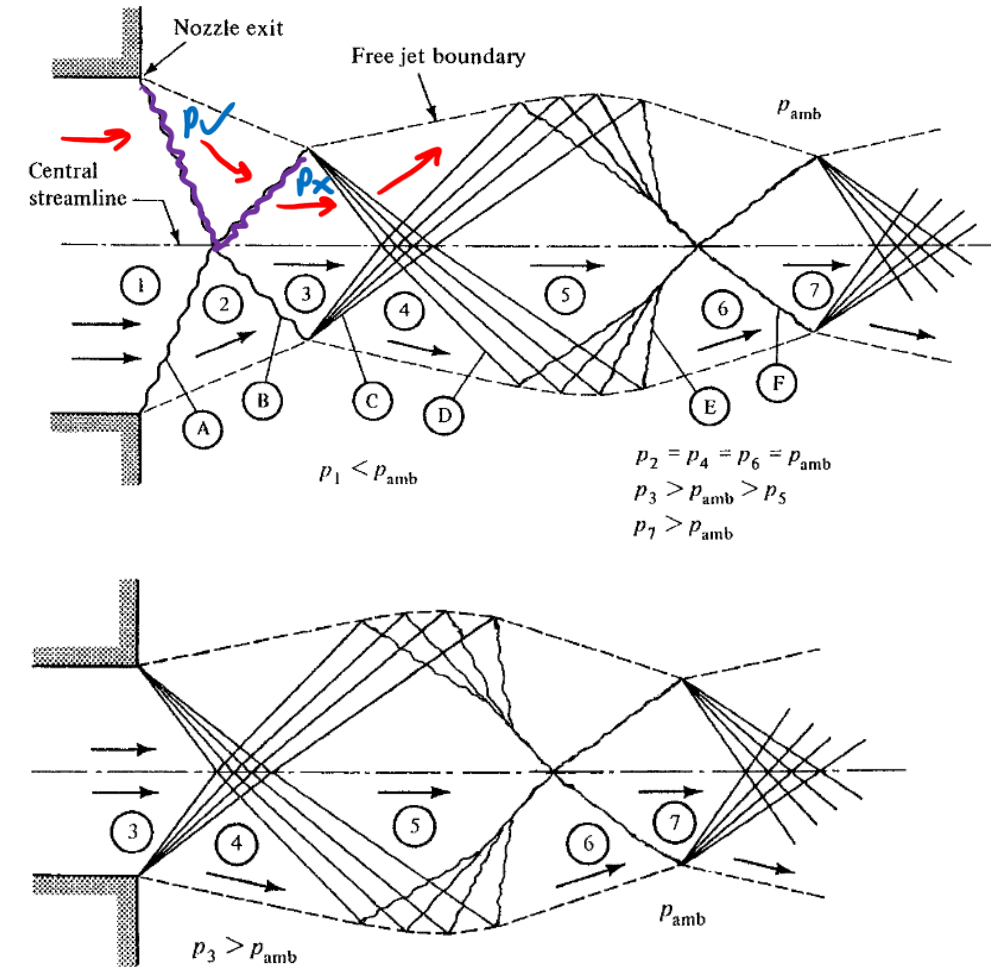
# Shocks and Expansions + Nozzles

- Overexpanded nozzle
  - A normal shock within the nozzle can no longer give us the conditions we require
  - Oblique shocks outside the nozzle form
- Outlet pressure equals outside pressure! (This is good)
- Does the flow direction after the shock makes sense...?



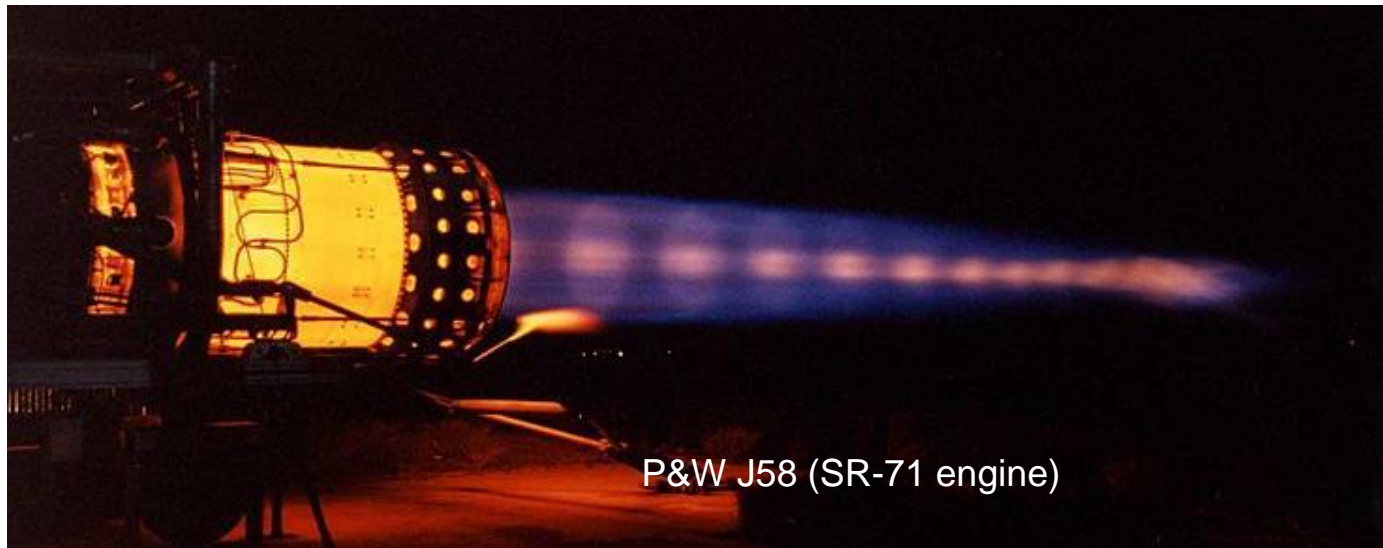
# Shocks and Expansions + Nozzles

- Overexpanded nozzle
  - An overexpanded nozzle leads to a series of shocks and expansions to alternate matching pressures and flow directions
  - Ends due to non-isentropic effects
- Underexpanded nozzle
  - Outside pressure below third critical (see figure on previous slide)
  - Similar to above, starts with an expansion wave before alternating to shocks



# Shocks and Expansions + Nozzles

- Shock/Mach/Thrust Diamonds
  - Common terminology for the visible effect of the pressure waves in over/underexpanded nozzle



*lunar recovery*