Aerospace Propulsion

Lecture 4

Combustion: Part II



Combustion: Part II

- Rich Combustion
- Chemical Equilibrium
- Chemical Reactions
- Rate Coefficients
- Equilibrium Constants



Rich Combustion

- Recall from last lecture:
 - Lean combustion (ϕ < 1)
 - More air than needed to oxidize all fuel molecules
 - Fuel + Air $\rightarrow CO_2 + H_2O + N_2 + O_2$
 - Stoichiometric combustion ($\phi = 1$)
 - Exactly the right amount of air to oxidize all fuel molecules
 - Fuel + Air $\rightarrow CO_2 + H_2O + N_2$
 - Rich combustion ($\phi > 1$)
 - Not enough air to oxidize all fuel molecules
 - Can't just assume fuel remains unchanged like O_2 , so what does it form?
 - Fuel + Air $\rightarrow CO_2 + H_2O + N_2 + ?$

Based on the methods we've been using, how many products can the rich system have without being over/under-determined?



Rich Combustion (Approach #1)

• Step 1:

Can you derive this stoichiometric reaction at $\phi = 1$?

• The general stoichiometric equation ($\phi = 1$) can be written as:

$$C_x H_y O_z + \left(x + \frac{y}{4} - \frac{z}{2}\right) (O_2 + 3.76N_2) \rightarrow xCO_2 + \frac{y}{2}H_2O + 3.76\left(x + \frac{y}{4} - \frac{z}{2}\right)N_2$$

- Then we can say, $\left(\frac{F}{A}\right)_{stoich} = 1/\left(x + \frac{y}{4} \frac{z}{2}\right)$
- Assume that just above $\phi = 1$, we begin to form CO, then generally:

$$C_x H_y O_z + a(O_2 + 3.76N_2) \rightarrow bCO_2 + cCO + \frac{y}{2}H_2O + 3.76aN_2$$

- CO requires less O than CO_2 so with higher ϕ , get less CO_2 and more CO

• Range where above products are valid:
$$1 \le \phi \le \frac{\left(x + \frac{y}{4} - \frac{z}{2}\right)}{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}$$

Figure Scarlo \Rightarrow to wre Co_{7}

Assure $b \Rightarrow 0$
 $C = X = C$
 $0 \le z + 2a = C + \frac{z}{2} = 7$
 $a = \frac{x}{2} + \frac{y}{4} - \frac{z}{2}$
 $A = \frac{x}{2} + \frac{y}{4} - \frac{z}{2}$

Valid.
$$1 \le \varphi \le \frac{x}{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}$$

$$= \frac{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}$$

$$= \frac{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}$$

Rich Combustion (Approach #1)

- Step 2:
 - Next, assume we start forming H_2 , then generally: $C_x H_y O_z + a(O_2 + 3.76N_2) \rightarrow xCO + bH_2O + cH_2 + 3.76aN_2$
 - H_2 requires less 0 than H_20 so with higher ϕ , get less H_20 and more H_2
 - Range where above products are valid: $\frac{\left(x+\frac{y}{4}-\frac{z}{2}\right)}{\left(\frac{x}{2}+\frac{y}{2}-\frac{z}{2}\right)} \leq \phi \leq \frac{\left(x+\frac{y}{4}-\frac{z}{2}\right)}{\left(\frac{x}{2}-\frac{z}{2}\right)}$
- Step 3:
 - Even less oxygen available, start forming solid carbon instead of CO...

• This is not how it happens, but is a decent approximation

Extra
$$(x)$$
: (x) $(x$

Rich Combustion (Approach #1)

- Summary
 - For fuel $C_x H_v O_z$ reacting with air

とう。 CHY vith air ×=1 Products to consider: メニケーマーク

 CO_2, H_2O, N_2, O_2

$$CO_2$$
, CO , H_2O , N_2

For ϕ between

 CO, H_2O, H_2, N_2

For ϕ between -

 $C(s), H_2O, H_2, N_2$

— For ϕ between

 ϕ lean

 ϕ rich

$$\phi=1$$
Coz,Ho, Nz

$$\phi = \frac{\left(x + \frac{y}{4} - \frac{z}{2}\right)}{\left(\frac{x}{2} + \frac{y}{4} - \frac{z}{2}\right)}$$

$$\phi = \frac{\left(x + \frac{y}{4} - \frac{z}{2}\right)}{\left(\frac{x}{2} - \frac{z}{2}\right)}$$



• Global Reactions
•
$$CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O$$

- Global reactions do not actually occur
- Chemistry proceeds through a series of "elementary reactions"
 - Elementary reactions describe physical collisions between actual molecules
 - Elementary reactions can go forward or backwards
- For example, Methane combustion relies on these reactions:

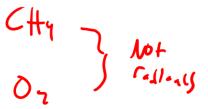
$$CH_4 \leftrightarrow CH_3 + H \qquad CH_4 + H \leftrightarrow CH_3 + H_2$$

$$H + O_2 \leftrightarrow OH + O \qquad H_2 + OH \leftrightarrow H_2O + H \qquad H_2 + O \leftrightarrow OH + H$$

$$CH_3 + O \leftrightarrow CH_2O + H \qquad CH_2O + H \leftrightarrow HCO + H_2 \qquad HCO \leftrightarrow CO + H$$

$$CO + OH \leftrightarrow CO_2 + H$$





- Radicals and Chain Reactions
 - Combustion chemistry driven by production of radicals (molecules with unpaired valence electrons)
 - Examples: *OH*, *H*, *O*, *CH*₃
 - Radicals generally present in very small concentrations
 - However, they are extremely reactive
 - Explosive mixtures (i.e., ignition) require radical production to be faster than consumption
 - Chain Branching

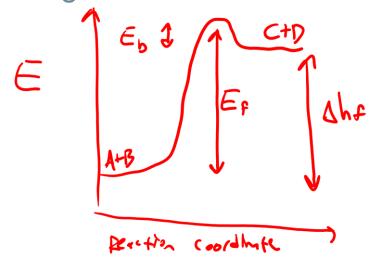


- Chain Branching
 - Series of reactions that ultimately increases total number of radicals
 - Combustion chemistry shares a common chain branching mechanism
 - $H + O_2 \leftrightarrow O + OH$
 - $H_2 + O \leftrightarrow OH + H$
 - $H_2 + OH \leftrightarrow H_2O + H$
 - $H_2 + OH \leftrightarrow H_2O + H$
 - Net: $3H_2 + O_2 \rightarrow 2H_2O + 2H$



- Chain Initiation
 - Initial formation of radicals from stable species
 - Example: $CH_4 \leftrightarrow CH_3 + H$
- Chain Termination
 - Consumption of radicals to form stable species
 - Example: $H + OH + M \leftrightarrow H_2O + M$

- How quickly do reactions occurs?
 - Consider a general bimolecular reaction: $A + B \leftrightarrow C + D$



• # reactions per time = (# collisions per time) × (probability that collision partners have sufficient energy)

- How quickly do reactions occurs?
 - Number of collisions per time: $A(T)C_AC_B$
 - Comes from kinetic theory
 - Probability of collision having sufficient energy: $\exp\left(-\frac{E}{\bar{R}T}\right)$
 - Comes from statistical mechanics

• Reaction Rate (Arrhenius Form),
$$[w] = \text{mol/(m}^3\text{s})$$

$$w = A(T) \exp\left(-\frac{E}{\bar{R}T}\right) C_A C_B = KC_A C_B$$

k(T): Reaction Rate Coefficient

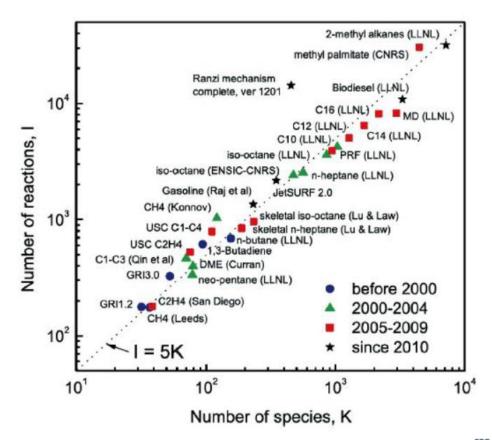


- Reaction Rates
 - For a general elementary reaction
 - $aA + bB + \dots \leftrightarrow zZ + yY + \dots$
 - Forward reaction rate: $w_f = A_f(T) \exp\left(-\frac{E_f}{\bar{R}T}\right) C_A^a C_B^b$...
 - Backward reaction rate: $w_b = A_b(T) \exp\left(-\frac{E_b}{\bar{R}T}\right) C_Z^z C_Y^y \dots$
 - Species Production Rates

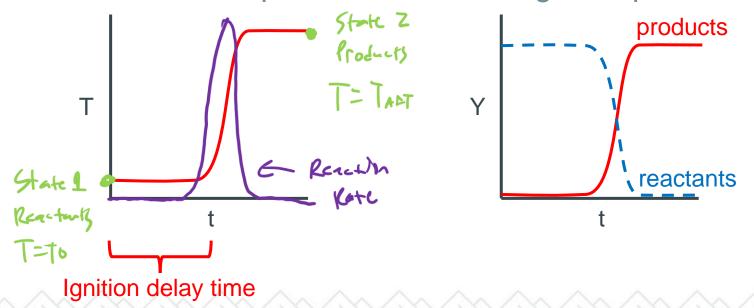
$$\bullet \ \frac{dC_A}{dt} = -a(w_f - w_b)$$

$$\bullet \ \frac{dC_Z}{dt} = z(w_f - w_b)$$

- Total species production rate is the sum of production rates from many individual elementary reactions
 - Methane combustion is usually described with 10's of species and 100's of reactions
 - Larger hydrocarbons (e.g., transport fuels) require 1000's of species and 100,000's of reactions



- Ignition delay time
 - Consider an adiabatic box homogeneously filled with reactants
 - Given enough time, reactants will become products
 - Slow at low temperatures, fast at high temperatures



Equilibrium Constants

- Chemical Equilibrium
 - At the molecular scale, molecules are constantly colliding and reacting
 - At the macro scale, nothing happens at equilibrium
 - Concentration of each species is not changing

$$\frac{dC_A}{dt} = -k_f C_A C_B + k_b C_C C_D = 0$$

 However, note that it is the *sum* of forward and backward that is zero, not that either forward or backward is zero

Equilibrium Constants

Reaction rates and equilibrium constants

A+Beach)

Formed: KECACB

Bakuard: KhCcCo

At equilibrium

KECACB = KOCCCB

• For a general **elementary** reaction:

•
$$aA + bB + \dots \leftrightarrow zZ + yY + \dots$$

•
$$K_C(T) \equiv \frac{c_Z^z c_Y^y \dots}{c_A^a c_B^b \dots} = K_p(T) \left(\frac{p_{ref}}{\bar{R}T}\right)^{z+y+\dots-a-b-\dots} = \frac{k_f}{k_b}$$

Definition

Elementary reaction only

Rich Combustion (Approach #2)

- How can we include all the products we've considered so far at once without creating an under-determined system?
 - *CO*, *CO*₂, *H*₂, *H*₂*O*
 - Preferably something valid at all ϕ
- Consider chemical equilibrium
 - Adds additional equations to balance our mathematical system
 - For example, water-gas shift reaction: $CO + H_2O \leftrightarrow CO_2 + H_2$

Chemical Equilibrium

- In short, chemical equilibrium represents the "steady state" for a chemical system where the ratio of molecules doesn't change
- For a general reaction:
 - $aA + bB + ... \leftrightarrow zZ + yY + ... (a, b, z, y, are moles of molecule A, B, Z, Y)$
 - There exists an equilibrium constant which is the ratio of the rate of forward reaction to the rate of backwards reaction at equilibrium.

•
$$K_p(T) \equiv \frac{\left(\frac{p_Z}{p_{ref}}\right)^z \left(\frac{p_Y}{p_{ref}}\right)^y \dots}{\left(\frac{p_A}{p_{ref}}\right)^a \left(\frac{p_B}{p_{ref}}\right)^b \dots} = \exp\left(-\frac{\Delta \overline{h}}{\overline{R}T}\right) \exp\left(\frac{\Delta \overline{s}^0}{\overline{R}}\right)$$

Additional equation Computed from state relating moles of products

Rich Combustion (Approach #2)

• Let's look at a rich methane example, what are the products? $CH_4 + (O_2 + 3.76N_2) \rightarrow aCO_2 + bH_2 + cCO + dH_2O + 3.76N_2$ $CO + H_2O \leftrightarrow CO_2 + H_2$ (Water-gas shift reaction)

• 1 =
$$a + c$$

• 2 = $b + d$
• 2 = $2a + c + d$
• $\frac{ab}{dc} = \exp\left(-\frac{\Delta \bar{h}}{\bar{R}T}\right) \exp\left(\frac{\Delta \bar{s}^{0}}{\bar{R}}\right) \frac{\Delta \bar{h}(T) = \bar{h}_{CO_{2}}(T) + \bar{h}_{H_{2}}(T) - \bar{h}_{CO}(T) - \bar{h}_{H_{2}O}(T)}{\Delta \bar{s}^{0}(T) = \bar{s}^{0}_{CO_{2}}(T) + \bar{s}^{0}_{H_{2}}(T) - \bar{s}^{0}_{CO}(T) - \bar{s}^{0}_{H_{2}O}(T)}$

• Eq. 4 needs T of products (T_{AFT} , must be computed)

CHy + (Oz+3.96Nz) + & COz+ LHz + CCO+ JHz + 7.46Mz

C: 1 = A+C

H: 4 = 2b + 2d

O: 2 = 2x + c + d

Y was,

O: 7 = 7x + c + d

Corsider vas - 9x) shift

Co + HzO & Coz + Hz

Assure products & Equilibrium

$$Kp = \frac{\binom{1}{1}}{\binom{1}{1}} + \binom{p_y}{p_{rec}} + \binom{p_y}{p_{rec}} = \exp\left(-\frac{\Delta h}{RT}\right) ext \left(\frac{\Delta s^*}{R}\right)$$

= $\frac{\binom{p_{coz}}{r_{coz}}}{\binom{p_{coz}}{r_{coz}}} + \binom{p_{g_{coz}}}{\binom{p_{g_{coz}}}{r_{coz}}} = \frac{\binom{x_{coz}}{r_{g_{coz}}}}{\binom{x_{coz}}{r_{coz}}} + \binom{x_{coz}}{r_{coz}}$

\[
\begin{align*}
\left(\frac{p_{coz}}{p_{rec}}\right) & \frac{p_{coz}}{p_{rec}} & \frac{p_{co

Xcoz XHZ
$$= \frac{a}{a+b+c+J+3.96} \left(\frac{b}{a+b+c+J+3.96}\right)^{\frac{1}{16}} \frac{AGNOVOSES}{AGNOVOSES}$$

$$= \frac{ab}{cJ} = ext\left(\frac{-Jh}{ZT}\right) ext\left(\frac{J}{R}\right)$$

$$= \frac{a}{a+b+c+J+3.96} \left(\frac{J}{a+b+c+J+3.96}\right)$$

$$= \frac{J}{cJ} = ext\left(\frac{-Jh}{ZT}\right) ext\left(\frac{J}{R}\right)$$

$$= \frac{J}{cJ} = ext\left(\frac{J}{ZT}\right) ext\left(\frac{J}{R}\right)$$

$$= \frac{J}{cJ} = \frac{J}{cJ} = \frac{J}{cJ} ext\left(\frac{J}{ZT}\right)$$

$$= \frac{J}{cJ} = \frac{J}{cJ} = \frac{J}{cJ} ext\left(\frac{J}{ZT}\right)$$

$$= \frac{J}{cJ} = \frac{J}{c$$

Rich Combustion (Approach #3)

- In approach #2, we were able to consider an additional product species by adding an additional equilibrium reaction
- In approach #3, we consider every (reasonably) possible chemical species by adding many equilibrium reactions
 - E.g., $H_2 + \frac{1}{2}O_2 \leftrightarrow H_2O$ $H_2 + O_2 \leftrightarrow 2OH$ $N_2 + O_2 \leftrightarrow NO$
 - Need $N_S 4$ reactions along with C, H, O, N element balance
 - How do additional species affect the AFT vs. complete combustion?
- This is extraordinarily tedious by hand
- Rely on computational codes to do it for us
 - See pset #2 for more details

