

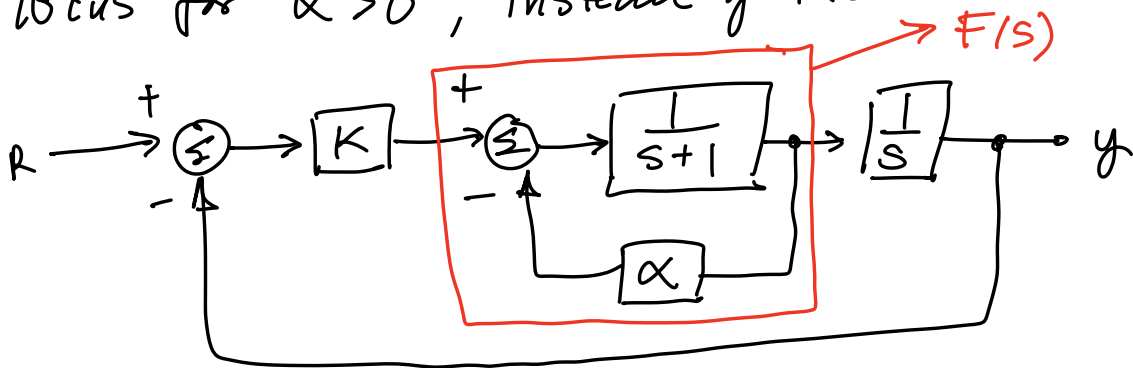
## Design by root locus :

what we will focus on:

- A) loci versus other parameters
- B) Improving Steady-state and transients
  - Lead/Lag controllers
- C) PID controllers

### A) Root locus for other parameters

Consider this system - we want to draw root locus for  $\alpha > 0$ , instead of  $K$ .



Approach: we need to put the equation for the roots of closed-loop system into this form:  $1 + \alpha \hat{G}(s) = 0$

Find the closed-loop T.F.

$$\frac{Y(s)}{R(s)} = \frac{K F(s) \left(\frac{1}{s}\right)}{1 + K F(s) \left(\frac{1}{s}\right)}$$

$$\text{Poles are: } 1 + K F(s) \left(\frac{1}{s}\right) = 0 = 1 + \alpha \hat{G}(s)$$

expand:

$$\Rightarrow 1 + K \left[ \frac{\frac{1}{s+1}}{1 + \alpha \left(\frac{1}{s+1}\right)} \right] \left[ \frac{1}{s} \right] = 1 + \frac{K}{s(s+1+\alpha)}$$

$$\Rightarrow s(s+1+\alpha) + K = s^2 + s + \alpha s + K$$

$$\text{Rearrange into } 1 + \alpha \hat{G}(s) = 0$$

$$\Rightarrow s^2 + s + \alpha s + K = s^2 + s + K + \alpha s$$

Divide by  $s^2 + s + K$  gives:

$$\frac{s^2 + s + K + \alpha s}{s^2 + s + K} = 0$$

$$\Rightarrow 1 + \alpha \left[ \frac{s}{s^2 + s + K} \right] = 0 \quad \rightarrow \hat{G}(s)$$

Therefore, to draw root locus for  $\alpha$ ,  
we treat  $\hat{G}(s) = \frac{s}{s^2 + s + K}$  as the  
"open-loop" system.

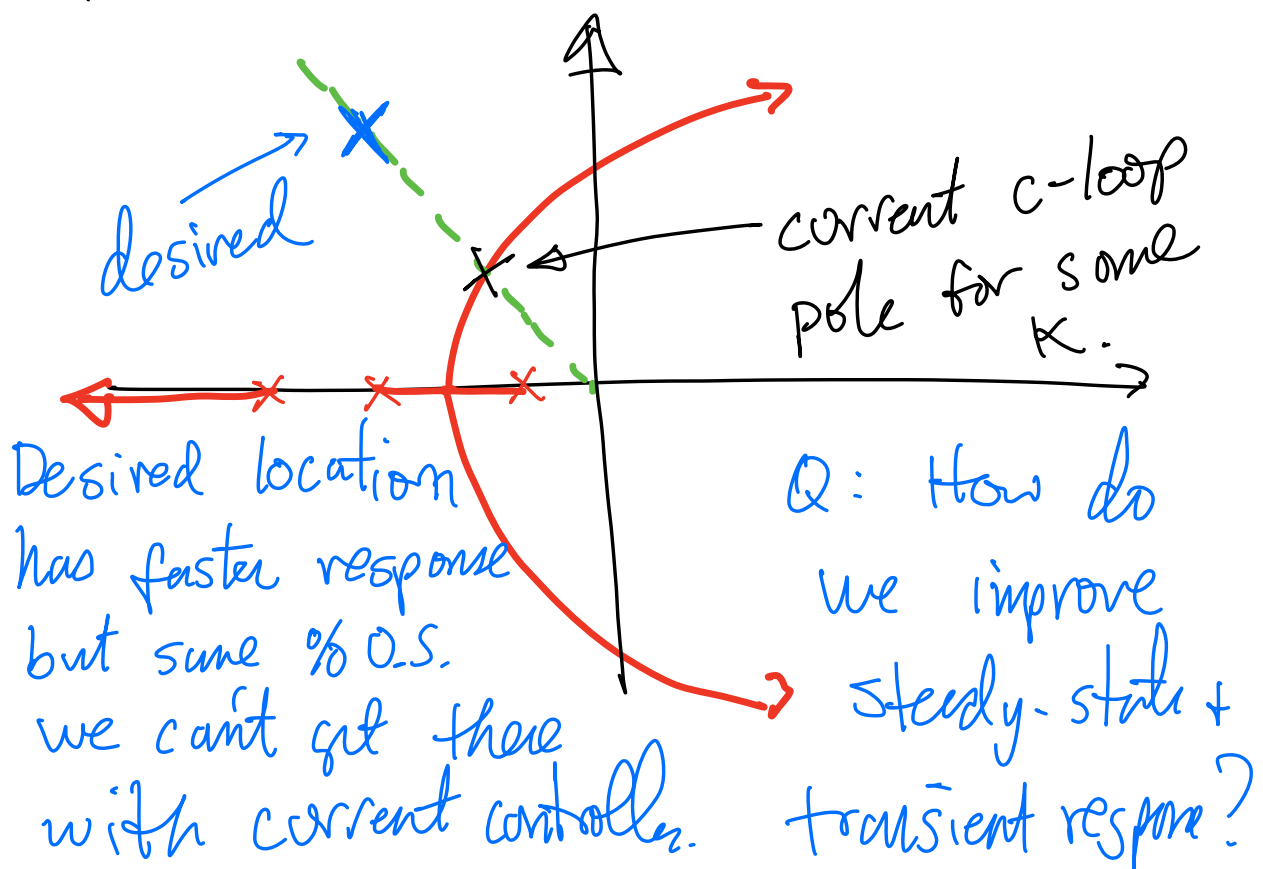
$$\hat{G}(s) = \frac{s}{s^2 + s + K} \Rightarrow \begin{array}{l} s=0 \text{ open-loop zero} \\ s^2 + s + K = 0 \text{ open-loop poles} \end{array}$$

we need to select nominal  
 $K$  value.

From here, we apply the steps described  
to draw root locus, but now it's  
for  $\alpha > 0$ .

B) Improving steady-state + transient response.

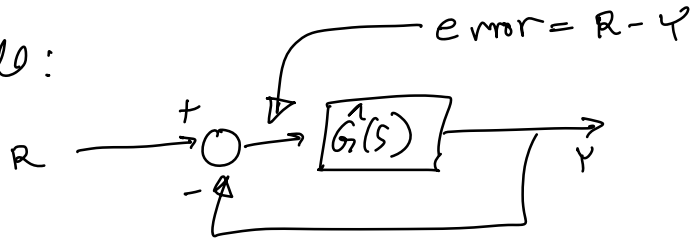
Suppose our closed-loop system has a root locus for some parameter  $K$  that looks like:



## Lag Compensators

lag controller is used to reduce steady-state error.

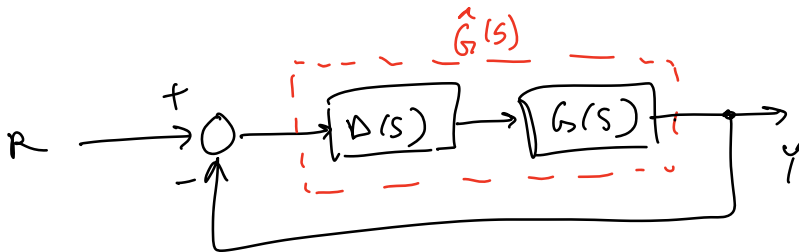
Recall:



s.s. error

step:	$e_{ss} = \frac{1}{1 + K_p}$	$K_p = \lim_{s \rightarrow 0} \hat{G}(s)$	position constant
ramp:	$e_{ss} = \frac{1}{K_v}$	$K_v = \lim_{s \rightarrow 0} s \hat{G}(s)$	
parabolic:	$e_{ss} = \frac{1}{K_a}$	$K_a = \lim_{s \rightarrow 0} s^2 \hat{G}(s)$	

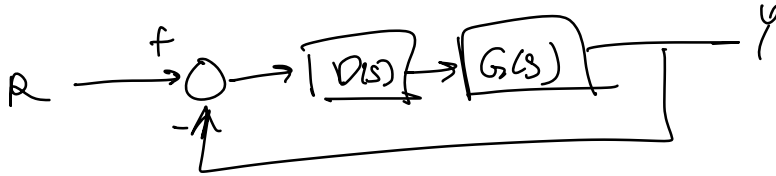
To achieve small s.s. error, we like the constants  $K_p, K_v, K_a$  to be as large as possible.



$$D(s) = \frac{s+z}{s+p} \quad z > p \quad \Rightarrow \quad \frac{z}{p} \gg 1$$

Pick  $\frac{z}{p} \approx 3$  to 10  $\rightarrow$  Design guidelines

---



$$G(s) = \frac{1}{s(s+1)} \quad \text{and} \quad D(s) = \frac{s+0.1}{s+0.01}$$

s.s. error

w/o lag control: Assume we have a ramp input.

$$e_{ss} = \frac{1}{K_v} \quad K_v = \lim_{s \rightarrow 0} sG(s) = \lim_{s \rightarrow 0} \frac{1}{s+1} = 1$$

$$\Rightarrow e_{ss} = \frac{1}{1} = \boxed{1}$$

w/ Lag:

$$e_{ss} = \frac{1}{K_v} \quad K_v = \lim_{s \rightarrow 0} s\hat{G}(s) = \lim_{s \rightarrow 0} s \left( \frac{s+1}{s+0.1} \right) \left( \frac{1}{s(s+1)} \right) = 10$$

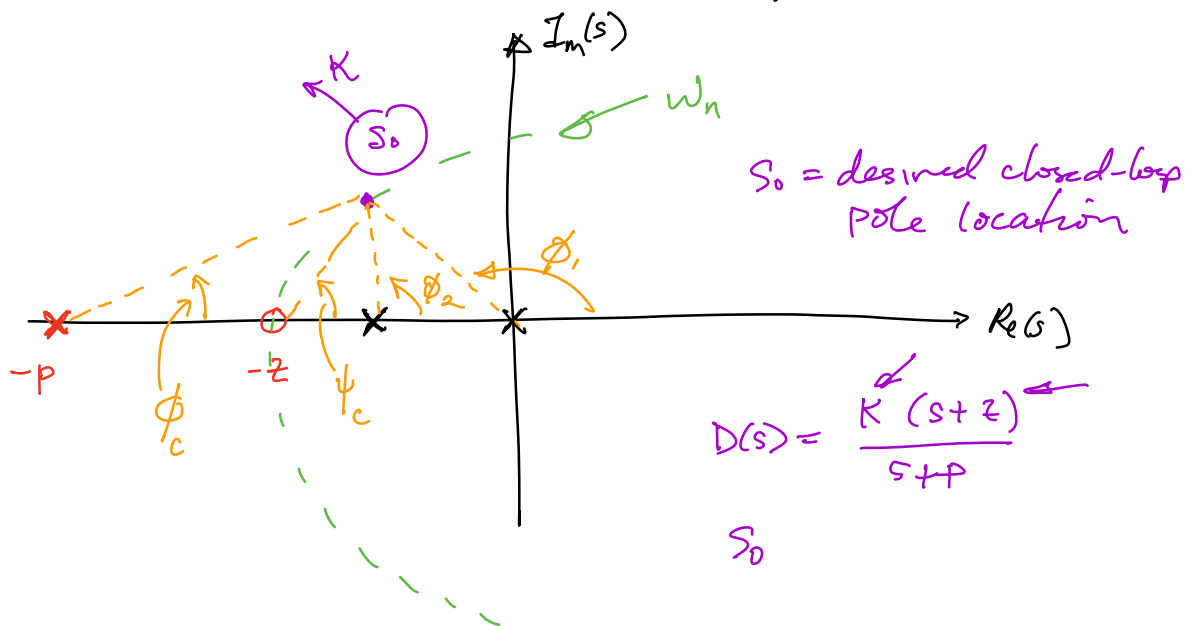
$$e_{ss} = \frac{1}{10} = 0.1$$

## Lead Controller Design Guidelines :

$$D(s) = K \frac{s+z}{s+p}$$

$$\text{lead: } z < p$$

- \* Place zero in the neighborhood of the desired closed-loop  $\omega_n$ , as determined by rise-time or settling time requirements.
- \* Place the pole at least 3 to 20 times the value of the zero.
- \* Lead controller must meet the angle condition:



$$\angle D(s)G(s) = 180^\circ + 360^\circ l \quad l = 0, \pm 1, \pm 2, \dots$$

$$\sum \psi_i - \sum \phi_i = 180 + 360^\circ l$$

$$\psi_c - [\phi_1 + \phi_2 + \phi_c] = -180^\circ + 360^\circ l$$

$$\psi_c - \phi_c - (\phi_1 + \phi_2) = 180^\circ + 360^\circ l$$

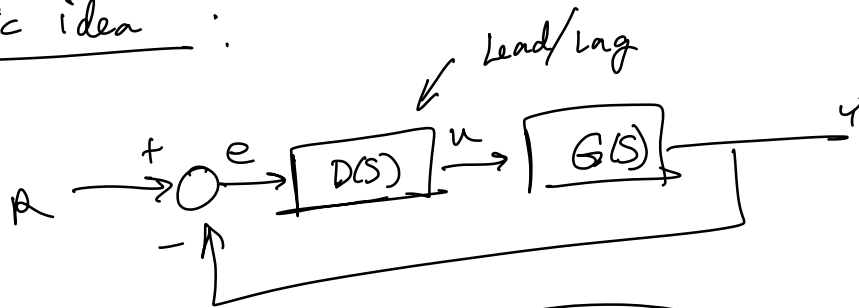
lead controller

\* Can choose  $\psi_c$  based on  $\omega_n$  and  $t_s$  conditions,  
then find  $\phi_c$  for location of pole of  
lead controller.

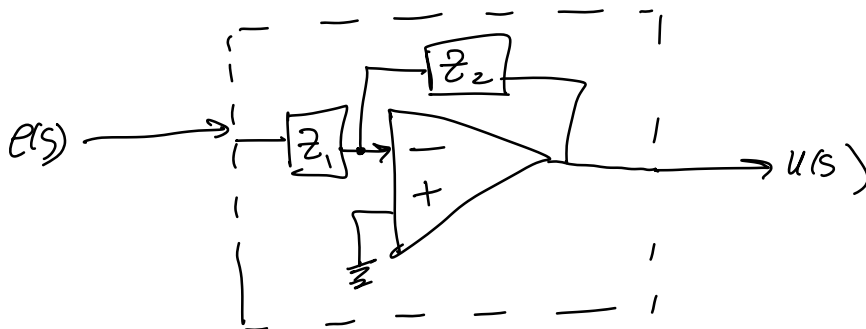
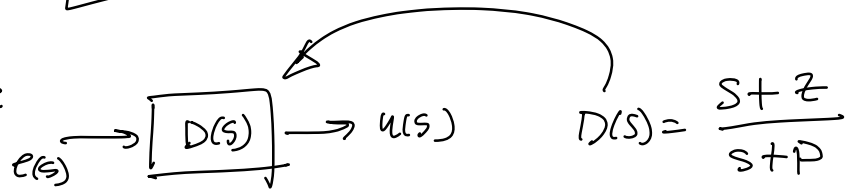


# Implementing Lead/Lag Controllers (Analog circuit)

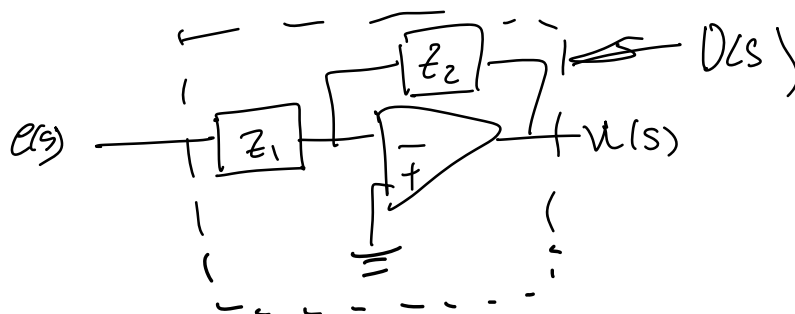
Basic idea :

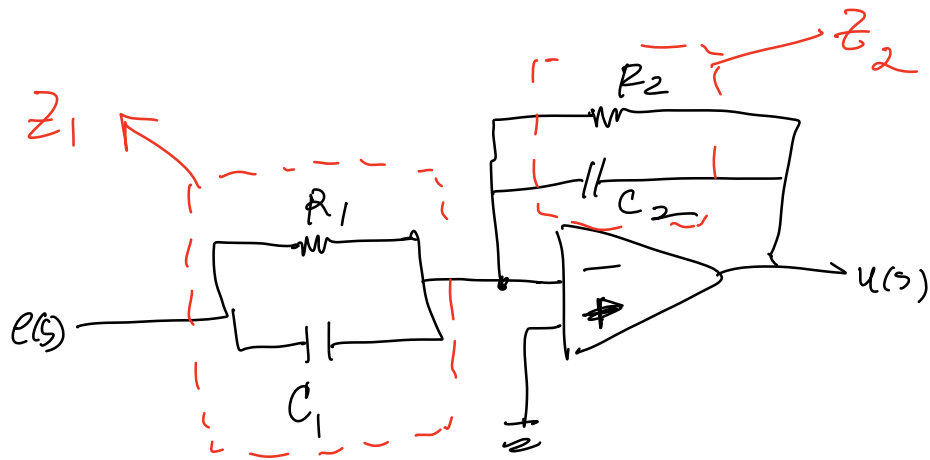


Isolate:



$$\frac{u(s)}{e(s)} = -\frac{z_2}{z_1} = \frac{s+z}{s+p} = D(s)$$





$$\frac{u(s)}{e(s)} = - \frac{Z_2}{Z_1}$$

$$Z_1 = \left[ \frac{1}{Z_{R_1}} + \frac{1}{Z_{C_1}} \right]^{-1} = \left[ \frac{1}{R_1} + \frac{1}{1/sC_1} \right]^{-1}$$

$$Z_2 = \left[ \frac{1}{Z_{R_2}} + \frac{1}{Z_{C_2}} \right]^{-1} = \left[ \frac{1}{R_2} + \frac{1}{1/sC_2} \right]^{-1}$$

$$\Rightarrow Z_1 = \left[ \frac{1}{R_1} + sC_1 \right]^{-1} = \frac{R_1}{C_1 R_1 s + 1}$$

$$Z_2 = \left[ \frac{1}{R_2} + sC_2 \right]^{-1} = \frac{R_2}{C_2 R_2 s + 1}$$

$$\frac{u(s)}{e(s)} = - \frac{Z_2}{Z_1} = - \frac{R_2 (C_1 R_1 s + 1)}{(C_2 R_2 s + 1) (R_1)}$$

$$\frac{u(s)}{e(s)} = - \frac{R_2}{R_1} \left[ \frac{C_1 R_1 (s + 1/C_1 R_1)}{C_2 R_2 (s + 1/C_2 R_2)} \right]$$

$$\frac{u(s)}{e(s)} = - \frac{C_1}{C_2} \left[ \frac{s + 1/C_1 R_1}{s + 1/C_2 R_2} \right]$$

$$\frac{u(s)}{e(s)} = D(s) = K \frac{s + z}{s + p}$$

$$z = 1/C_1 R_1 \quad p = 1/C_2 R_2$$

$$K = -C_1/C_2$$