
Fluid Mechanics (ME EN 5700/6700)

Final exam, Fall 2013

(Open Book, Open Notes, Closed neighbor)

0. [1 pt] What is your name?

1. [14 pt] Short answer questions.

a. Write the following vector quantity in index notation: $(\vec{\nabla} \times \vec{a}) \cdot (\vec{c} \times \vec{b})$

b. Consider a boundary layer developing over a flat plate starting from the plate's leading edge. At what point does this boundary layer become fully developed?

c. Under what conditions can a two-dimensional turbulent flow exist?

d. In the following equations a is a constant, u and v are random variables (e.g., velocity components), $u' = u - \langle u \rangle$ and $v' = v - \langle v \rangle$ are the deviations of u and v from their mean values, and the angle brackets $\langle \rangle$ denote an appropriate averaging operator. Reducing the following averaging operations to their simplest form.

1. $\langle \langle a(u + v) \rangle \rangle$

2. $\langle a(\langle u \rangle^2 + \langle u' \rangle^2) \rangle$

3. $\langle (\langle u \rangle + u')(\langle v \rangle + v') \rangle$

e. In words describe the following:

1. Favorable pressure gradient –

2. Adverse pressure gradient –

2. [8 pt] Vorticity transport.

- a. Consider the vorticity transport equation shown below.

$$\underbrace{\frac{\partial \vec{\omega}}{\partial t}}_I + \underbrace{(\vec{u} \cdot \vec{\nabla}) \vec{\omega}}_{II} = \underbrace{(\vec{\omega} \cdot \vec{\nabla}) \vec{u}}_{III} + \underbrace{\frac{\vec{\nabla} \rho \times \vec{\nabla} P}{\rho^2}}_{IV} + \underbrace{\nu \vec{\nabla}^2 \vec{\omega}_V}_{V}$$

1. Give the name and a short description of the physical meaning of each term I–V.

I –

II –

III –

IV –

V –

2. Which term in the vorticity transport equation is linked to the turbulent energy "cascade" process?

- b. Define (in words) what a vortex line is.

- c. What is the solenoidal condition for vorticity?

3. [6 pt] Navier-Stokes equations.

- a. List all the assumptions required to derive the following form of the Navier-Stokes equations

$$\rho \frac{Du_i}{Dt} = \rho g_i - \frac{\partial P}{\partial x_i} + \mu \frac{\partial}{\partial x_j} \left[\frac{\partial u_i}{\partial x_j} + \frac{1}{3} \frac{\partial u_m}{\partial x_m} \right] + F_i$$

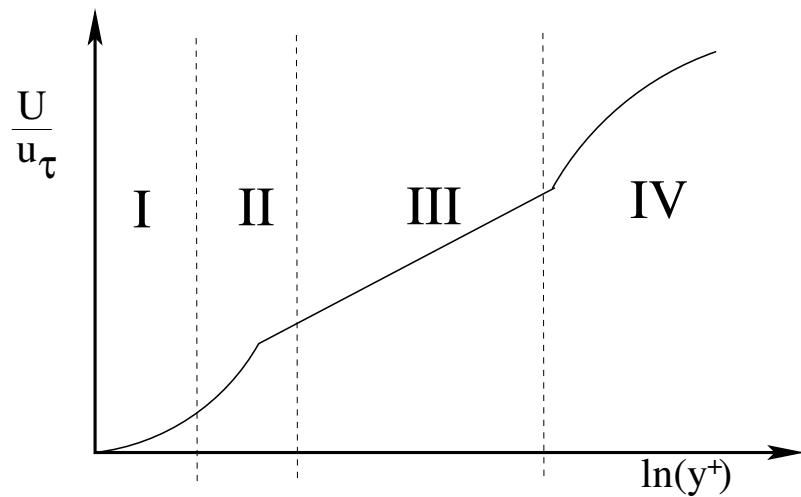
- a. Write the equation from part [a.] with the additional assumption that the flow is incompressible.

4.[10 pt] Turbulent boundary layers.

a. What is the “law of the wall” for a turbulent boundary layer over a smooth flat plate?

b. What is the “log law” for a turbulent boundary layer over a smooth flat plate?

c. The following graph illustrates the typical velocity profile over a smooth flat plate



Label regions I–IV:

I –

II –

III –

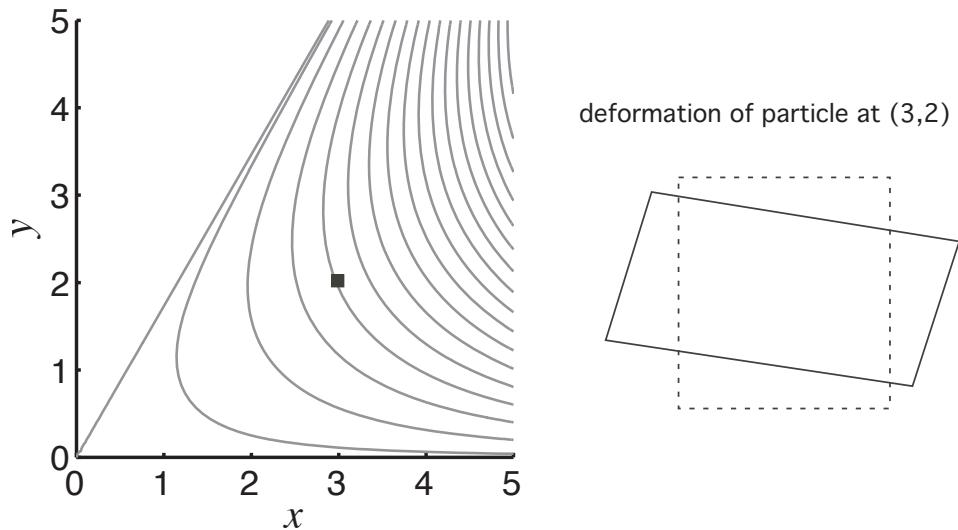
IV –

d. Which layers belong to:

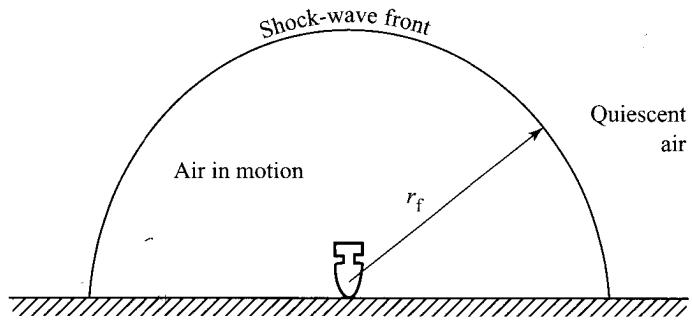
1 – The inner region:

2 – The outer region:

5. [12 pt] Consider incompressible flow in a corner, the streamlines of which are drawn in the left figure below. The corresponding streamfunction is $\psi = x^2 y - y^3/3$. The fluid particle located at $x=3, y=2$ deforms as shown in the right figure. Based on this write the corresponding strain-rate tensor and vorticity at this instant in space-time.



6.[14 pt] In 1940, G. I. Taylor developed a simple yet accurate model for the shock wave propagation from a nuclear blast. The figure shows a basic schematic of the problem.



Taylor assumed that the only variables that were important to model the shock wave radius r_f where:

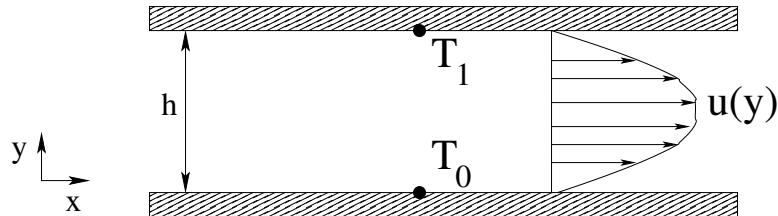
- the total explosion energy energy of the blast E in Joules [$\text{Kg m}^2\text{s}^{-2}$]
- the initial density of the ambient air ρ_0
- the time from the moment of explosion t
- and the ratio of specific heats γ

Using dimensional analysis and these variables, develop a functional relationship for r_f

7. [18 pt] The stream wise velocity profile for fully-developed, steady-state, incompressible flow between two infinite parallel plates driven by a constant stream wise pressure gradient dP/dx is given by:

$$u = \frac{1}{2\mu} \frac{dP}{dx} (y^2 - hy) \text{ where } h \text{ is the distance between the plates}$$

Consider the case where the top and bottom plates are heated to constant temperatures T_0 and T_1 as shown in the figure.



- a. Write down and then simplify (don't solve) the conservation of energy equation for this problem [clearly state all assumptions].

- b. Using the velocity profile given above, solve for the temperature distribution in the channel.

- c. Non dimensionalize your answer to part [b.] using the temperature difference $\Delta T = T_1 - T_0$ and then sketch what the non dimensional profile should look like and how it will change with $\chi = \frac{h^4}{144k\Delta T} \left(\frac{dP}{dx}\right)^2$ for $T_1 > T_0$.

8. [18 pt] Laminar boundary layers:

- a. Write the von Karman integral equation for a boundary layer over a solid wall with no suction/blowing.
- b. Under what assumptions is the above equation valid?
- c. Define mathematically (and in words) the displacement thickness.
- d. Define mathematically (and in words) the momentum thickness.
- e. Simplify the von Karman integral for flow over a flat plate (don't solve just simplify).
- f. Assume a laminar boundary layer stream wise velocity profile given by:

$$\frac{u}{U_\infty} = \left(\frac{y}{\delta} \right) = \eta \text{ where } \eta = y/\delta.$$

Using this and your reduced form of the von Karman integerl from part [e.], solve for $\delta(x)$ [Hint: change the integration limits in the momentum thickness definition from $0 \rightarrow \delta$ to $0 \rightarrow 1$].

f. How does this compare to the $\delta(x)$ you would obtain using the Blasius profile?