

# Aerospace Propulsion

Lecture 19  
Rocket Propulsion II

# Rocket Propulsion: Part II

- Definitions
- Rocket Thrust
- Basic Rocket Analysis

# Definitions

- Major differences between air-breathing and rocket engines
  - Rockets keep all propellants on board
  - Rockets directly overcome gravity with thrust (low/no lift forces)
    - Every little bit of propellant is important
- Rocket capabilities are often measured in terms of how much total energy can be extracted from propellants

# Definitions

- Total impulse

- $I_t = \int_0^t F dt$

- Thrust force  $F$

- May vary in time

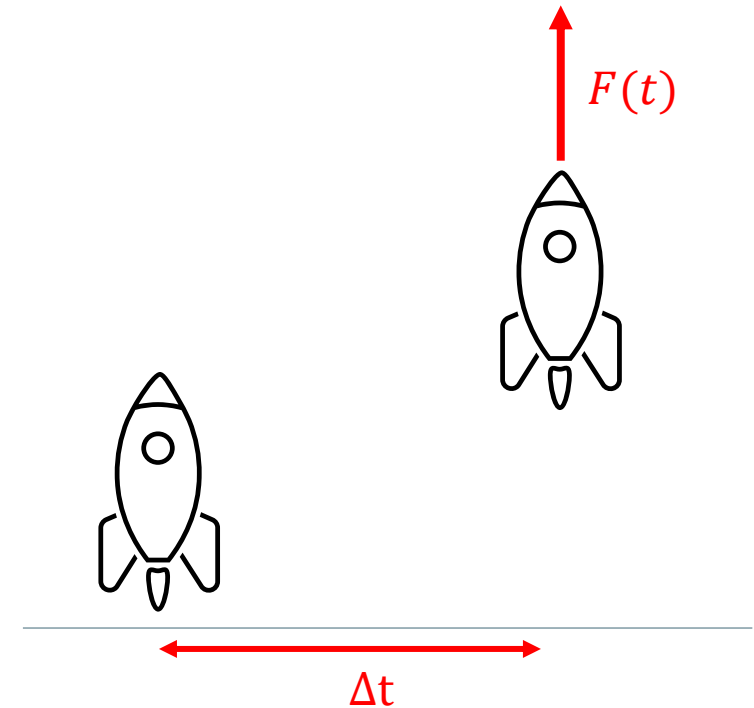
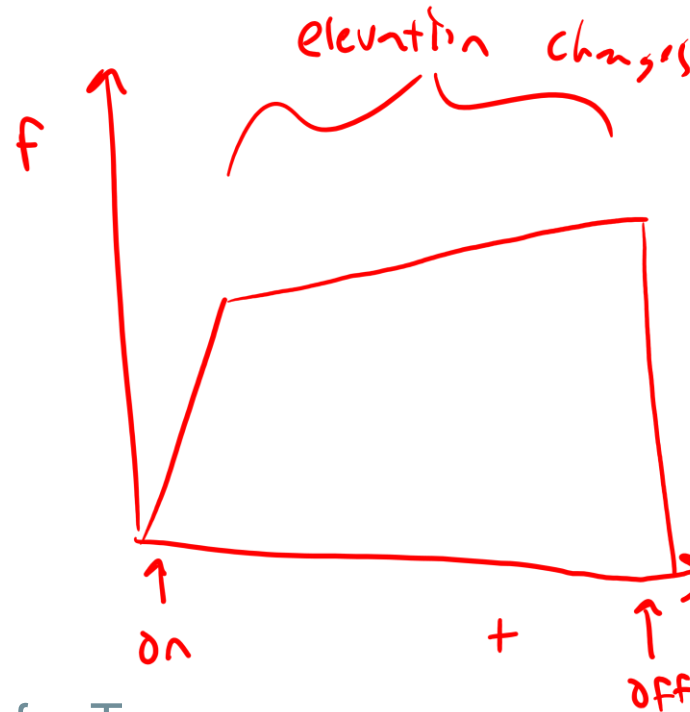
- $T$  typically reserved for Torque

- Time  $t$

- For constant thrust with instant on/off

- $I_t = F\Delta t$

- Proportional to total energy released by the propellant



# Definitions

$$\bar{I}_s = \frac{\int_0^t F dt}{g_0 \int_0^t \dot{m} dt}$$

Assume  
Constant  
thrust  
 $\frac{1}{2}$

$$\rightarrow \bar{I}_s = \frac{F \Delta t}{g_0 \cdot m_p} = \frac{I_t}{g_0 m_p}$$

define  
 $\int_0^t \dot{m} dt = m_p$

## • Specific impulse

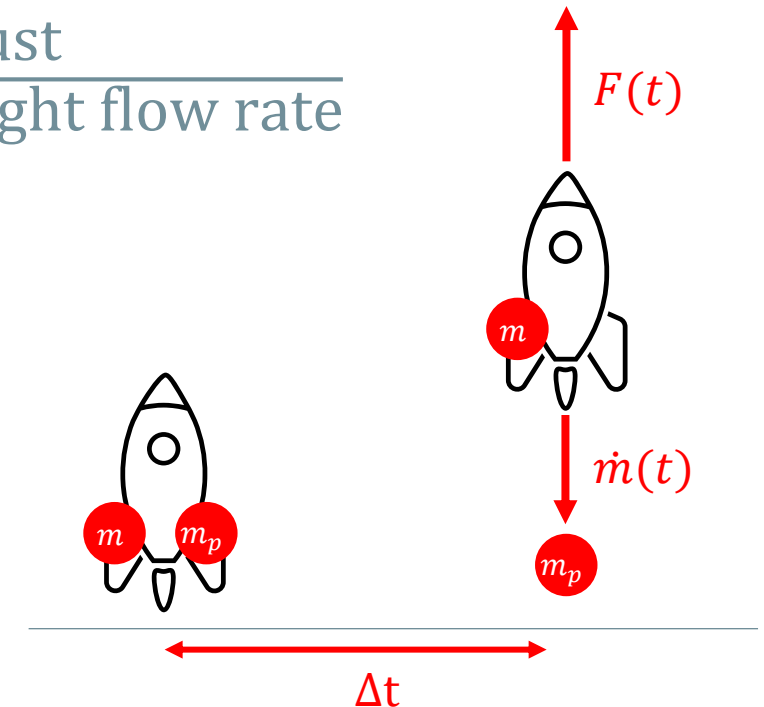
$$I_s = \frac{\int_0^t F dt}{g_0 \int_0^t \dot{m} dt} = \frac{\text{Total impulse}}{\text{Propellant weight}} = \frac{\text{Thrust}}{\text{Propellant weight flow rate}}$$

- Nominal earth gravity  $g_0$ 
  - $g_0 = 9.8066 \text{ m/s}^2$
- Propellant mass flow rate  $\dot{m}$

## • Average value (useful over small $\Delta t$ )

- $I_s = \frac{I_t}{m_p g_0}$ 
  - Mass exhausted  $m_p$

## • Important/common way to describe rockets



# Definitions

Low TSFC = good  
High  $I_s$  = good

- Quick note – have we seen  $I_s$  before?

- $$I_s = \frac{\int_0^t F dt}{g_0 \int_0^t \dot{m} dt} \approx \frac{F}{\dot{m} g_0} \propto \frac{F}{\dot{m}}$$

$$I_s = \frac{\int_0^t F dt}{g_0 \int_0^t \dot{m} dt}$$

Assume,  
 $F, \dot{m}$

- $$TSFC = \frac{\dot{m}}{F} \text{ (air breathing propulsion)}$$

$$I_s = \frac{F \Delta t}{g_0 \dot{m} \Delta t}$$

~~$$I_s \propto \frac{1}{TSFC}$$~~

$$= \frac{F}{\dot{m} g_0}$$

constant

- Different fields use different quantities
  - TSFC is historically not used in the field of rockets

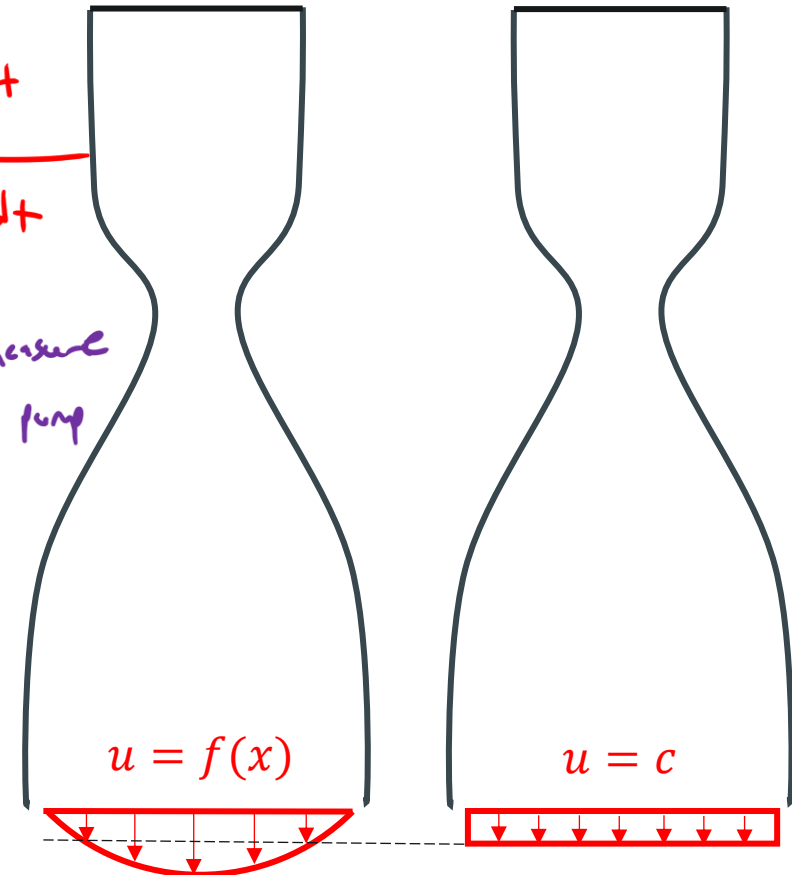
force sensor →  
Solid:  $I_s = \frac{F \Delta t}{g_0 m_p}$  ← clock  
← scale

# Definitions

- Effective Exhaust Velocity
  - $c = I_s g_0 = F / \dot{m} (= V_e)$
  - Mean velocity leaving rocket nozzle
  - Note that this is basically a constant multiplied by specific impulse
    - Varies between source,  $I_s$  more common
- Measuring  $I_s$  and  $c$  for ground tests
  - Solid motor
    - Tough to measure flow rate, use  $m_p$
  - Liquid Engine
    - Can measure flow rate (pumps), use  $\dot{m}$

Liquid:  $I_s = \int_0^t F dt$

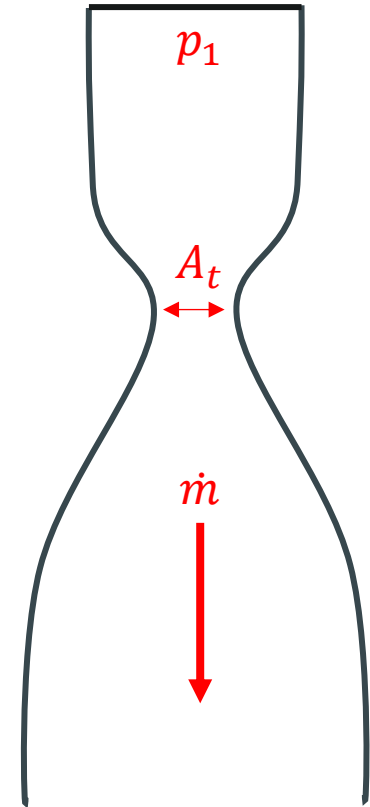
$g_0 \int_0^t \dot{m} dt$   
↑  
can measure through pump



# Definitions

- Characteristic Velocity

- $c^* = \frac{p_1 A_t}{\dot{m}}$
- Both  $I_s$  and  $c$  are measured based on properties that come *after* the nozzle
  - Both quantities are measures of overall rocket efficiency
- The characteristic velocity is a measure of the rocket's efficiency excluding the nozzle
  - Related to efficiency of combustion process
- Note that the characteristic velocity is not related to any physical velocity, but has dimensions of velocity





# Definitions

- Mass Ratio

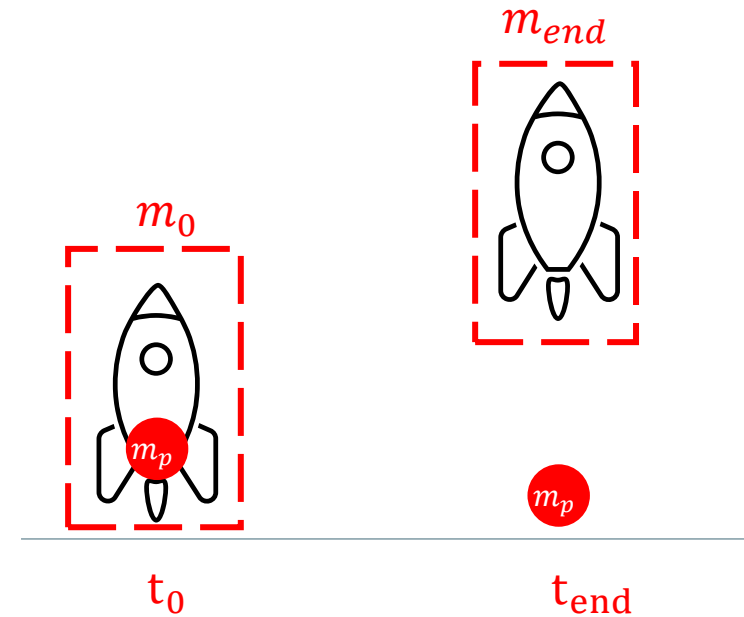
- $MR = \frac{m_{end}}{m_0}$

- Final vehicle mass  $m_{end}$ 
    - Often  $m_f$  is used, this is not fuel mass

- Initial vehicle mass  $m_0$

- Represents how much of the rocket is not propellant

- $m_0 = m_{end} + m_p$ 
    - Assuming all mass lost was propellant



The diagram shows the equation  $MR =$  followed by a rocket icon, a diagonal line, and another rocket icon with a red circle labeled  $m_p$  below it. This represents the ratio of the final mass to the initial mass.

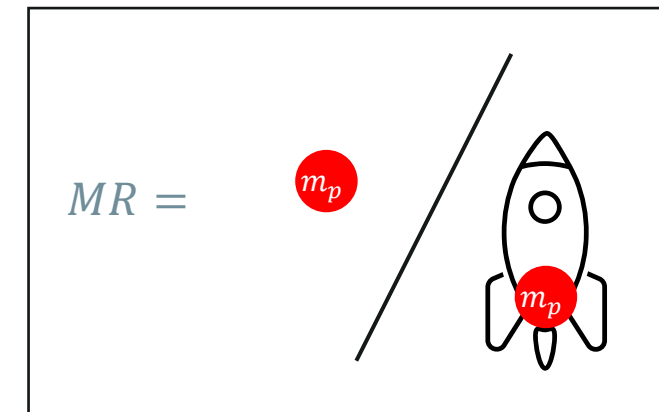
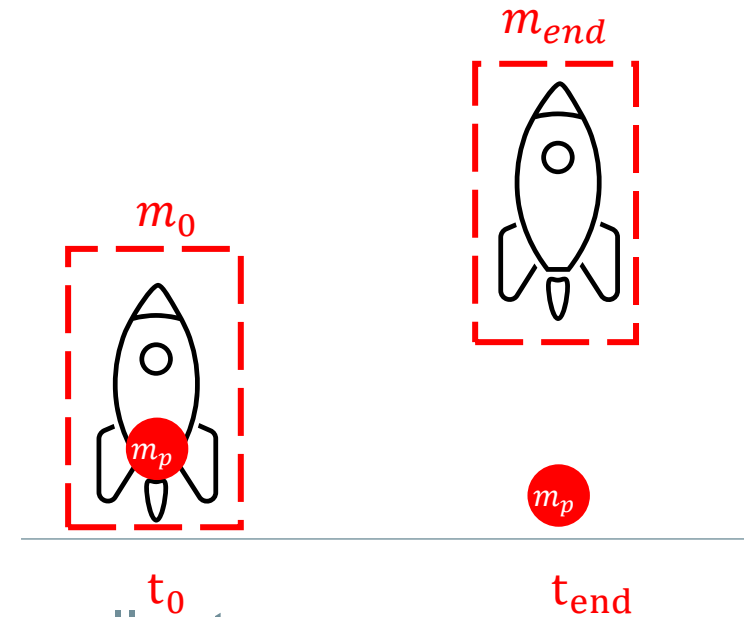
# Definitions

- Propellant Mass Fraction

- $\zeta = \frac{m_p}{m_0} = \frac{m_0 - m_{end}}{m_0}$

- Represents how much of the rocket is propellant

$$\zeta = \frac{m_0 - m_{end}}{m_0} = 1 - \frac{m_{end}}{m_0} = 1 - MR$$



# Definitions

- Impulse to Weight Ratio  $\frac{I_t}{w_0}$

- Total impulse divided by total sea-level weight  $w_0$
- Assuming constant thrust and instant on/off

- $\frac{I_t}{w_0} = \frac{I_t}{(m_{end} + m_p)g_0} = \frac{I_s}{m_{end}/m_p + 1}$

$$\frac{I_t}{w_0} = \frac{I_t}{m_{total} g_0} = \frac{I_t}{(m_{end} + m_p) g_0} = \frac{I_s m_p g_0}{(m_{end} + m_p) g_0}$$

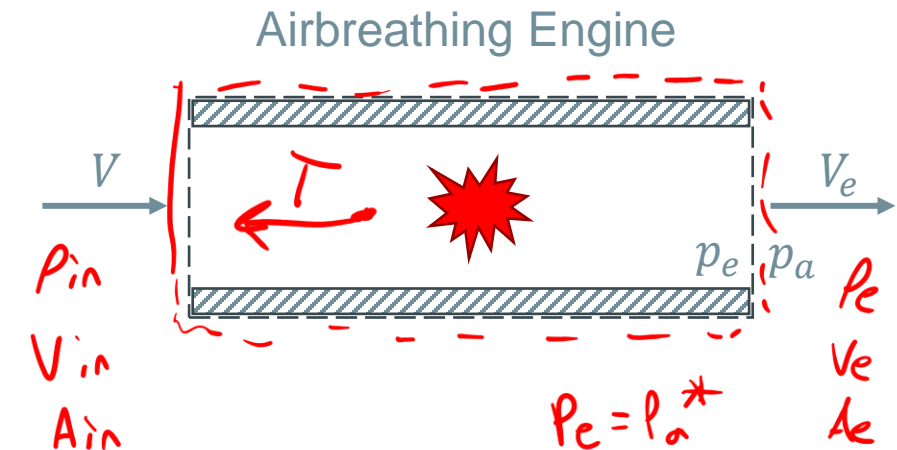
- Thrust to Weight Ratio  $\frac{F}{w_0}$

- Acceleration that an engine can apply to itself (in  $g_0$ 's)

$$= \frac{I_s}{\left(\frac{m_{end}}{m_p}\right) + 1}$$

# Rocket Thrust

- For airbreathing propulsion, we derived
  - $T = \dot{m}(V_e - V)$
- Airbreathing propulsion assumed:
  - Flow entering and exiting
  - Outlet pressure = ambient pressure
    - Not necessarily true for supersonic exhaust
    - Neglected over/under-expanded outlets
- These assumptions do not hold for rockets!



$$\iint \rho \vec{V} (\vec{V} \cdot \hat{n}) dA = \sum F$$

$$P_e V_e^2 A_e - P_{in} V_{in}^2 A_{in} = T$$

$$T = \dot{m} (V_e - V_{in})$$

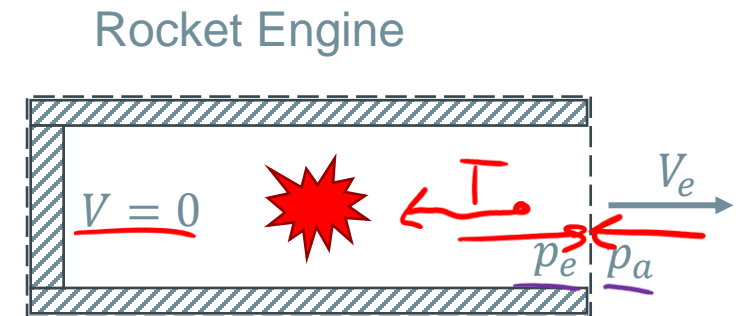
↑ velocity of aircraft

# Rocket Thrust

- For rocket propulsion:

- Inlet velocity  $V = 0$
- $p_e \neq p_a$ 
  - Extreme case of vacuum ( $p_a = 0$ )
  - \*Actually, they are equal at one specific elevation
  - Variable area rocket nozzles are rare
    - Most rockets are expendable
    - Multiple stages each designed for different  $p_a$

- $F = \dot{m}V_e + (p_e - p_a)A_e$



$$\iint \rho \vec{V} (\vec{V} \cdot \hat{n}) dA = \sum \vec{F}$$

$$\rho_e V_e^2 A_e = T + p_a A_e - p_e A_e$$

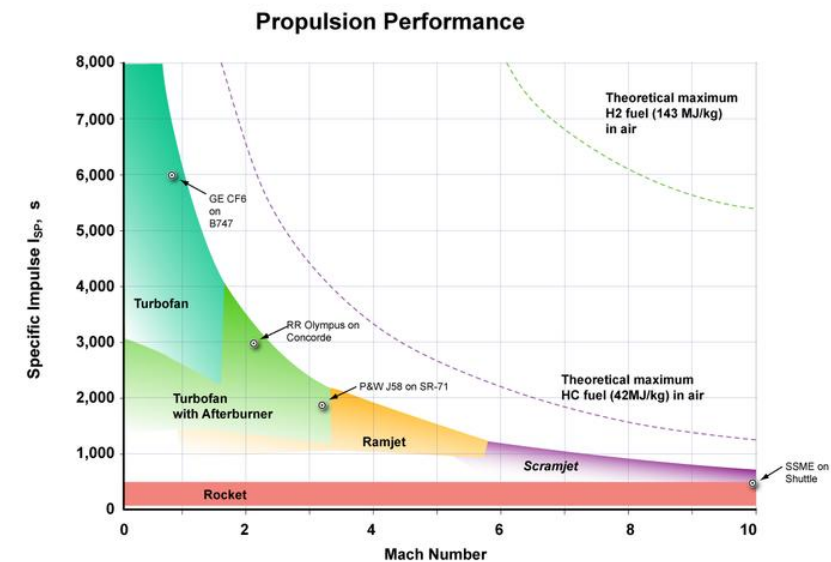
$$T = \dot{m} V_e + (p_e - p_a) A_e$$

# Rocket Thrust

- $F = \dot{m}V_e + (p_e - p_a)A_e$
- Rocket thrust consists of two terms
  - First term – Momentum thrust
    - Differs from airbreathing propulsion because  $V = 0$
  - Second term – Pressure thrust
    - Can give negative thrust
    - Negative thrust avoided by making sure  $p_e > p_a$
  - Generally, momentum thrust is larger than pressure thrust
- Note that in a vacuum,  $p_a = 0$ 
  - $F = \dot{m}V_e + p_e A_e$  (max thrust)

# Rocket Thrust

- $F = \dot{m}V_e + (p_e - p_a)A_e$
- A few notes about rocket thrust
  - Unlike airbreathing engines, rocket engine thrust is independent of the flight speed of the rocket
  - Both airbreathing and rocket engine thrust is affected by elevation
    - Pressure (and temperature) decreases with elevation
    - Airbreathing engines encounter inlet air with varying properties
      - Thrust decreases with elevation
    - Rocket engines have a varying pressure thrust
      - Thrust increases with elevation
      - Note that specific impulse also increases with elevation



# Rocket Thrust

## • Power

### • Exhaust Power

- $P_e = \frac{1}{2} \dot{m} V_e^2 = \frac{1}{2} \dot{m} g_0 I_s^2 = \frac{1}{2} F V_e$
- Power from exhaust gases

### • Chemical Power

- $P_c = \dot{m}(LHV)$
- Same as airbreathing propulsion

### • Vehicle Power

- $P_v = FV$
- Power transmitted to vehicle flying at speed  $V$

Assume

$$P_c = P_a$$

$$P_e = \frac{1}{2} \dot{m} V_e^2$$

$$= \frac{1}{2} \dot{m} V_e V_e$$

$$= \frac{1}{2} F V_e$$

$$\downarrow$$

$$\frac{1}{2} (\dot{m} g_0 I_s) V_e$$

$$\downarrow$$

$$\frac{1}{2} (\dot{m} g_0 I_s) I_s g_0$$

$$P_e = \frac{1}{2} \dot{m} g_0 I_s^2 g_0$$

$$= \frac{1}{2} \dot{m} g_0 I_s^2$$

$$I_s = \frac{F}{\dot{m} g_0}$$

$$\Rightarrow F = \dot{m} g_0 I_s$$

when  $P_c = P_a$

$$I_s = \frac{V_e}{g_0}$$

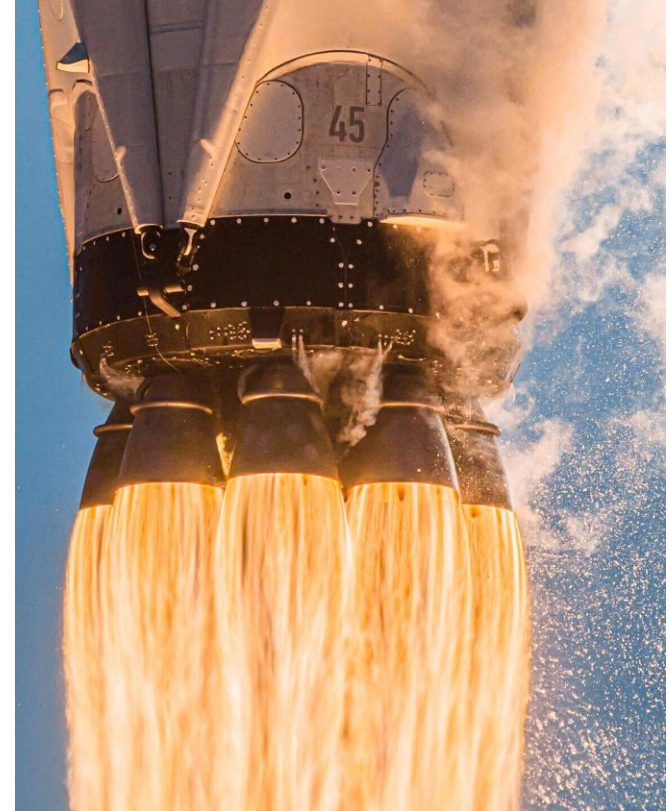
$\Downarrow$

$$V_e = I_s g_0$$



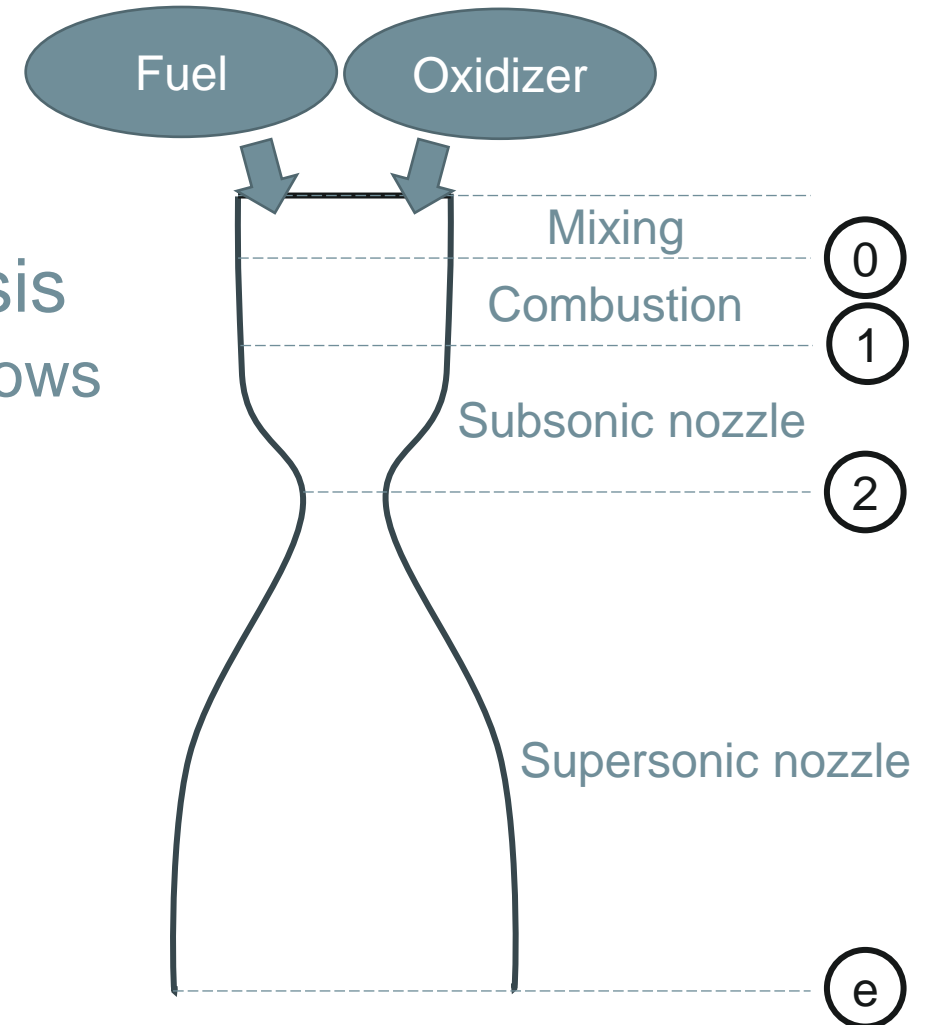
# Rocket Thrust

- Multiple propulsion systems
  - Consider multiple simultaneous sources of thrust
    - E.g., Falcon 9 simultaneously uses 9 first stage engines
    - We are not considering staging here
  - $F_{tot} = \sum F_i$ 
    - Total thrust equal to sum of individual thrusts
  - $\dot{m}_{tot} = \sum \dot{m}_i$ 
    - Total mass flow rate equal to sum of individual flow rates
  - $(I_s)_{tot} = \frac{F_{tot}}{g_0 \dot{m}_{tot}}$ 
    - Total specific impulse calculated with above two parameters



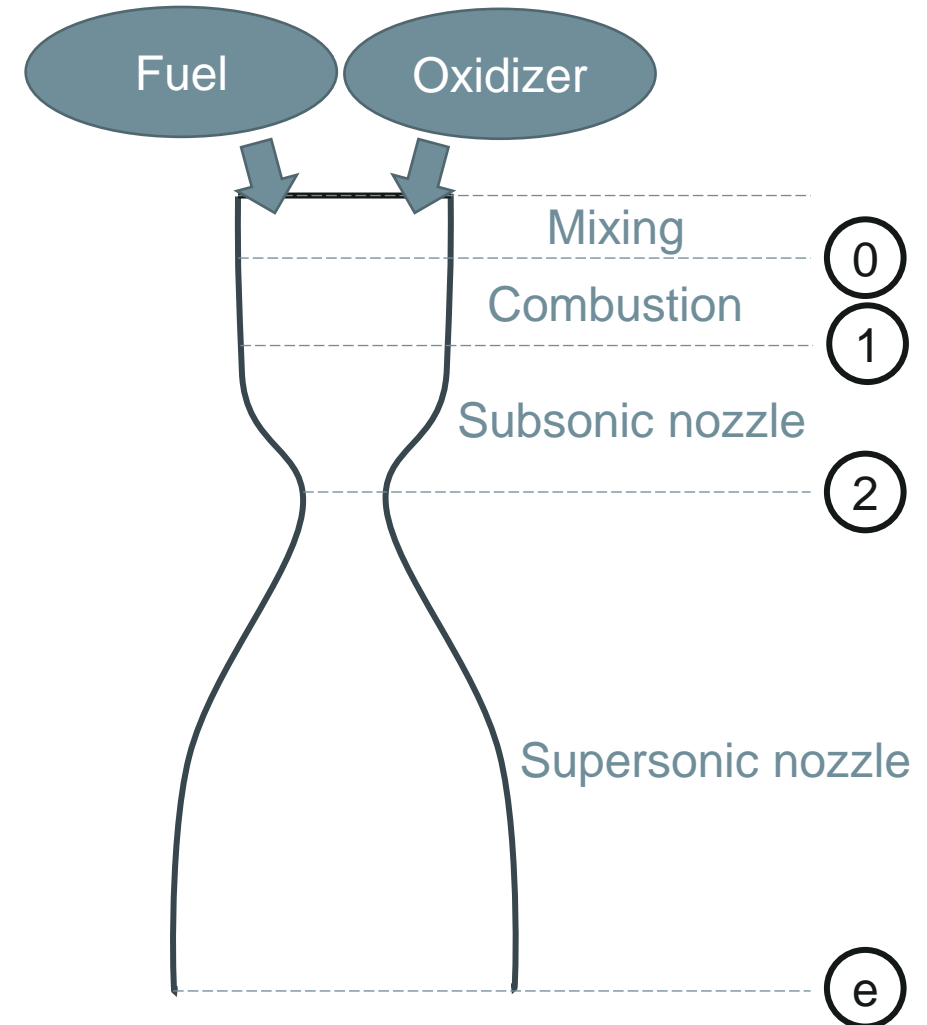
# Basic Rocket Analysis

- Major assumptions of the basic analysis
  - Quasi-1D approach from compressible flows
  - Flow throughout the engine is isentropic
  - Propellants are perfectly mixed
- This is even simpler than a ramjet
  - No inlet, propellants already mixed
  - Combustor
  - Isentropic Nozzle



# Basic Rocket Analysis

- Start at state 0
  - Assume small initial velocity
  - $T_{t0} = T_0$
  - $p_{t0} = p_0$
- State 0 to state 1 (combustion)
  - $T_{t1} = T_{t0} + \frac{\phi \left( \frac{F}{A} \right)_{st} LHV}{c_p} = T_{t0} + \frac{\left( \frac{F}{A} \right) LHV}{c_p}$
  - $p_{t1} = p_{t0}$



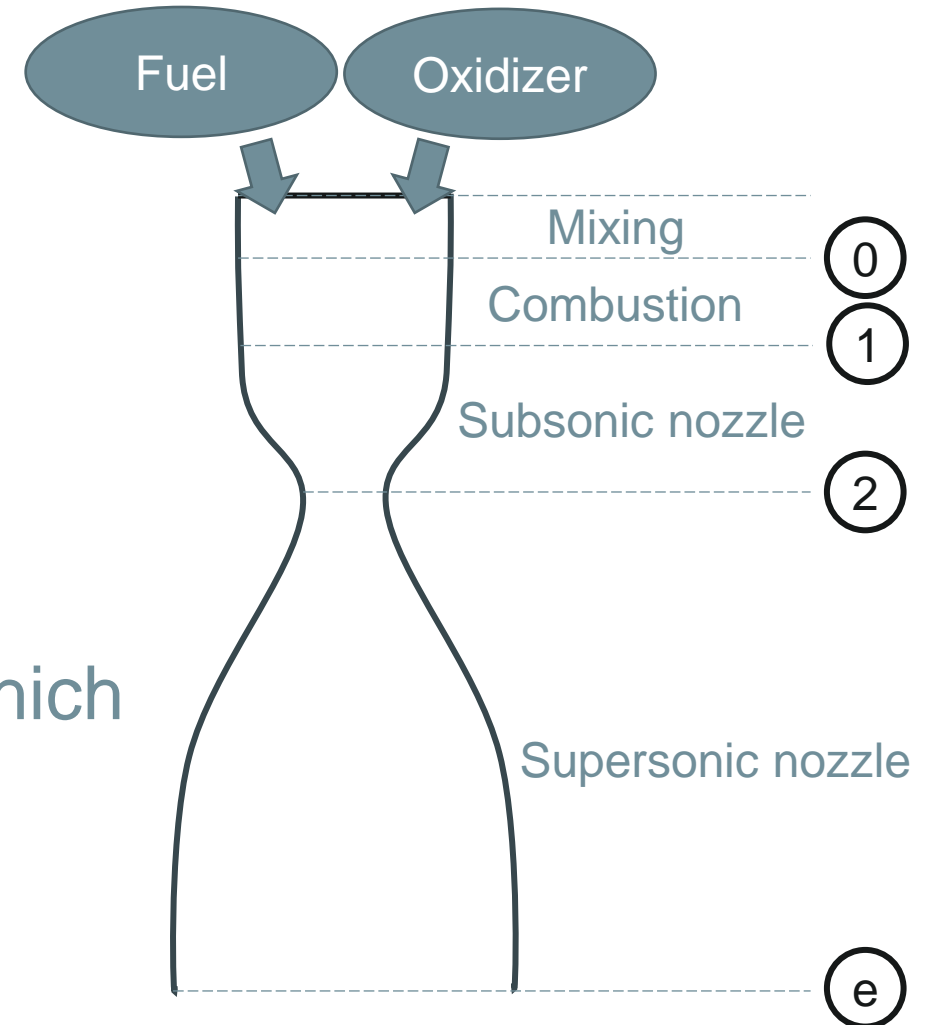
# Basic Rocket Analysis

- State 1 to exhaust (isentropic nozzle)

$$V_e = \sqrt{2 \frac{\gamma}{\gamma-1} R T_{t1} \left[ 1 - \left( \frac{p_a}{p_{t1}} \right)^{\frac{\gamma-1}{\gamma}} \right]}$$

- This is valid for isentropic flow only, which assumes that  $p_e = p_a$

- Thrust (assuming  $p_e = p_a$ )
  - $F = \dot{m} V_e$

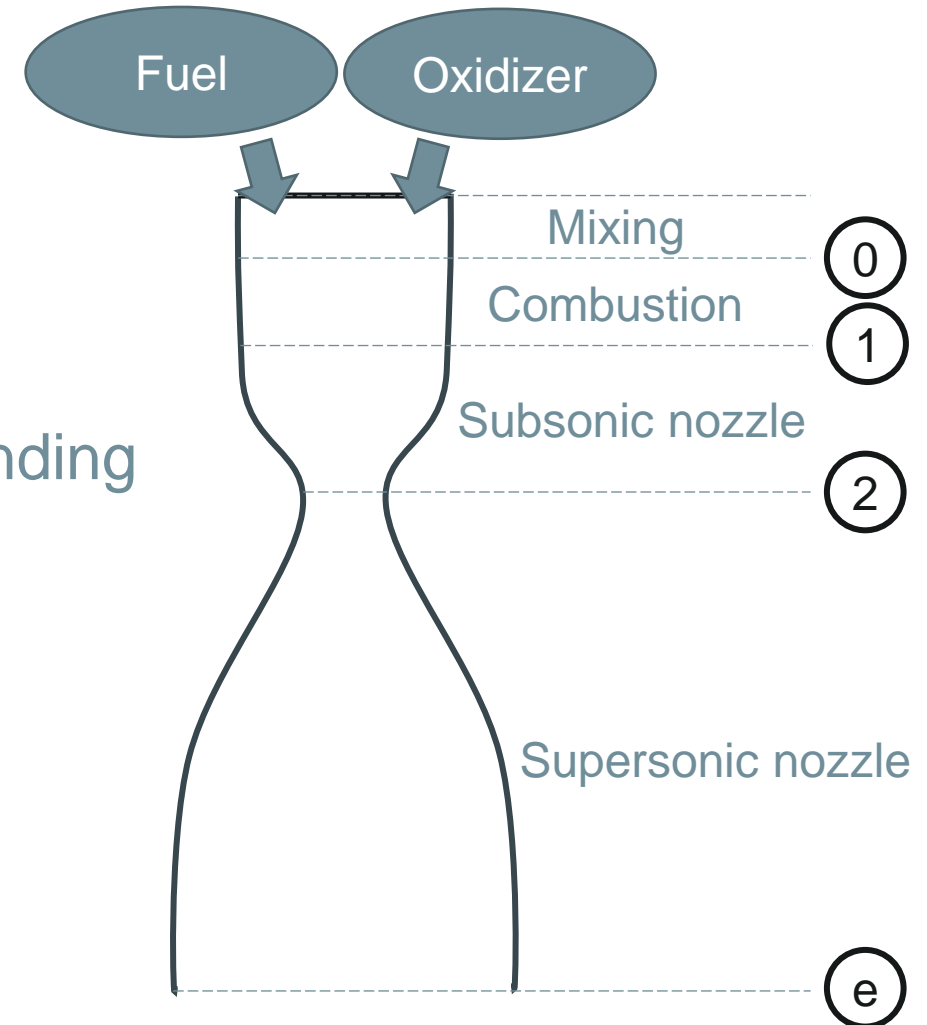


# Basic Rocket Analysis

- What are we expelling?
  - It's no longer mostly air
  - Rocket exhaust varies significantly depending on which propellants are used
- Lower molecular mass increases  $V_e$

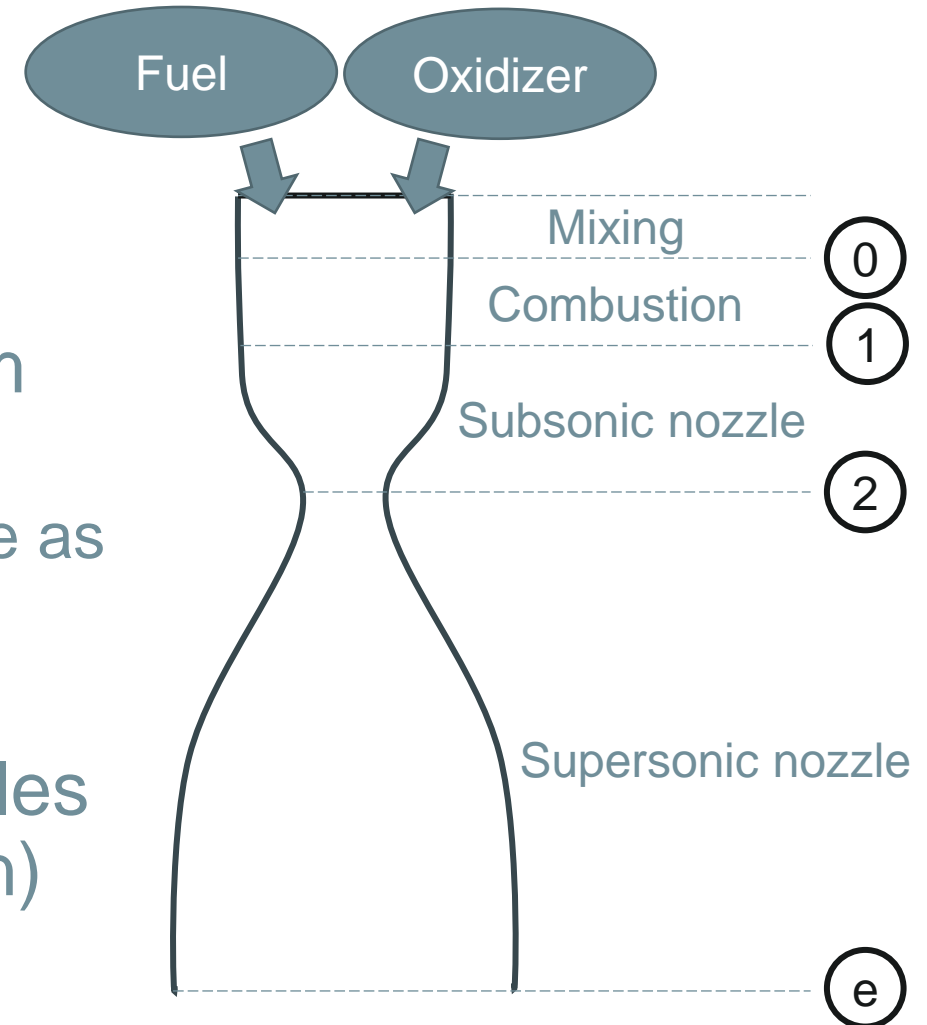
$$V_e = \sqrt{2 \frac{\gamma}{\gamma-1} R T_{t1} \left[ 1 - \left( \frac{p_a}{p_{t1}} \right)^{\frac{\gamma-1}{\gamma}} \right]}$$

$$V_e = \sqrt{2 \frac{\gamma}{\gamma-1} \left( \frac{\bar{R}}{\bar{m}} \right) T_{t1} \left[ 1 - \left( \frac{p_a}{p_{t1}} \right)^{\frac{\gamma-1}{\gamma}} \right]}$$



# Basic Rocket Analysis

- Note that since this is an isentropic nozzle, all our previous equations from compressible flows are also valid
  - Account for combustion before the nozzle as an increased temperature
- Our equations for non-isentropic nozzles are also valid (considering combustion)
  - Normal shock within nozzle
  - Over/under-expanded nozzles



# Basic Rocket Analysis

- Relevant equations refresher

## Isentropic Flows (Static)

$$\frac{T_2}{T_1} = \frac{1 + \frac{\gamma-1}{2} M_1^2}{1 + \frac{\gamma-1}{2} M_2^2}$$

$$\frac{p_2}{p_1} = \left( \frac{1 + \frac{\gamma-1}{2} M_1^2}{1 + \frac{\gamma-1}{2} M_2^2} \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{\rho_2}{\rho_1} = \left( \frac{1 + \frac{\gamma-1}{2} M_1^2}{1 + \frac{\gamma-1}{2} M_2^2} \right)^{\frac{1}{\gamma-1}}$$

$$\frac{A_2}{A_1} = \frac{M_1}{M_2} \left( \frac{1 + \frac{\gamma-1}{2} M_2^2}{1 + \frac{\gamma-1}{2} M_1^2} \right)^{\frac{\gamma+1}{2(\gamma-1)}}$$

## Isentropic Flows (Stagnation)

$$T_{t1} = T_{t2}$$

$$p_{t1} = p_{t2}$$

## Normal Shocks (Stagnation)

$$T_{t1} = T_{t2}$$

$$\frac{p_{t2}}{p_{t1}} = \left[ \frac{\frac{\gamma+1}{2} M_1^2}{1 + \frac{\gamma-1}{2} M_1^2} \right]^{\frac{\gamma}{\gamma-1}} \left[ \frac{1}{\frac{2\gamma}{\gamma+1} M_1^2 - \frac{\gamma-1}{\gamma+1}} \right]^{\frac{1}{\gamma-1}}$$

## Normal Shocks (Static)

$$M_2^2 = \frac{M_1^2 + \frac{2}{\gamma-1}}{\frac{2\gamma}{\gamma-1} M_1^2 - 1}$$

$$\frac{T_2}{T_1} = \frac{\left( 1 + \frac{\gamma-1}{2} M_1^2 \right) \left( \frac{2\gamma}{\gamma-1} M_1^2 - 1 \right)}{\left[ \frac{(\gamma+1)^2}{2(\gamma-1)} \right] M_1^2}$$

$$\frac{p_2}{p_1} = \frac{2\gamma M_1^2}{\gamma+1} - \frac{\gamma-1}{\gamma+1}$$

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma+1) M_1^2}{(\gamma-1) M_1^2 + 2}$$