

Steady-state Error

Goal: Study Steady-state error for various inputs

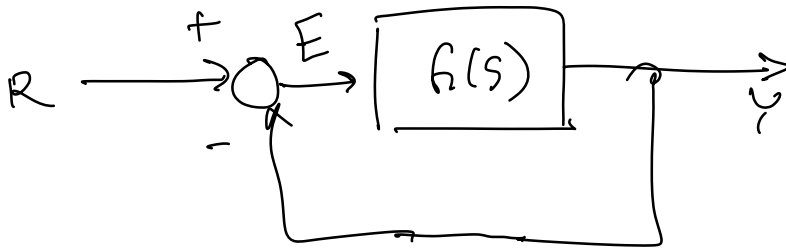
A. What is error:

error = desired behavior - Actual behavior

$$e(t) = y_d(t) - y(t)$$

B. Use the final value theorem

Consider the following (Note - unity feedback!)



$$E(s) = R(s) - Y(s) \text{ and } \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)} = T(s)$$

$$\Rightarrow Y(s) = T(s)R(s)$$

From error: $E(s) = R(s) - Y(s)$

$$E(s) = R(s) - T(s) R(s)$$

$$\Rightarrow E(s) = R(s) [1 - T(s)] = R(s) \left[1 - \frac{G(s)}{1+G(s)} \right]$$

$$\Rightarrow E(s) = \left[\frac{1+G(s) - G(s)}{1+G(s)} \right] R(s)$$

$$E(s) = \underbrace{\left[\frac{1}{1+G(s)} \right]}_{\text{for unity F.B. system}} R(s) = \underbrace{[1 - T(s)]}_{\text{for all c.l. systems}} R(s)$$

Find s_i error using F. v. T.:

\Rightarrow Assume that poles of $SE(s)$ are in OLHP. \Rightarrow poles of loop system are in OLHP.

If the closed-loop system has unity feedback, then:

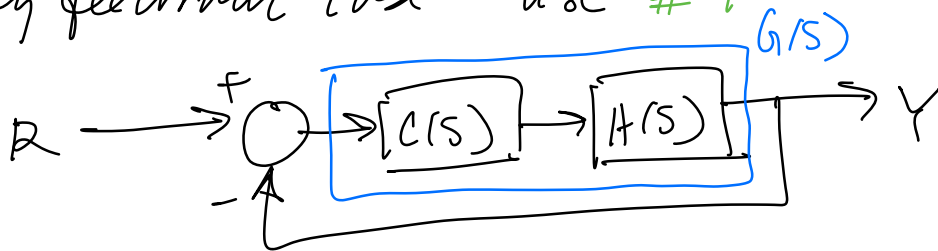
$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \left[\frac{1}{1+G(s)} \right] R(s) \quad \#1$$

Otherwise, we can use this expression

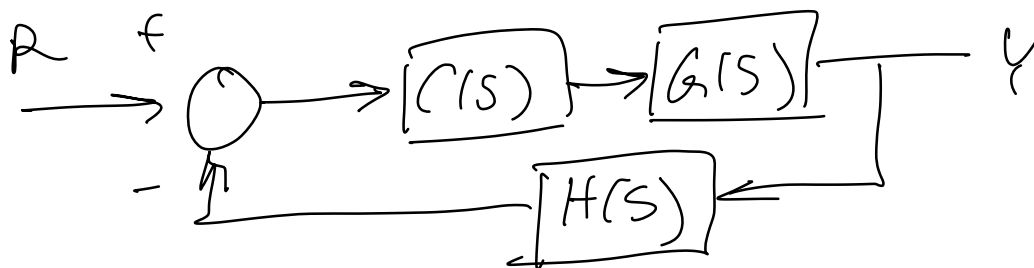
$$e_{ss} = \lim_{s \rightarrow 0} s(1 - T(s))R(s) \quad \#2$$

Note these 2 expressions and when to use them!

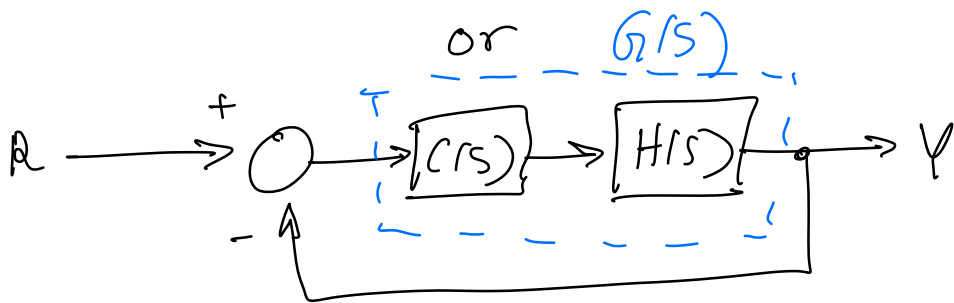
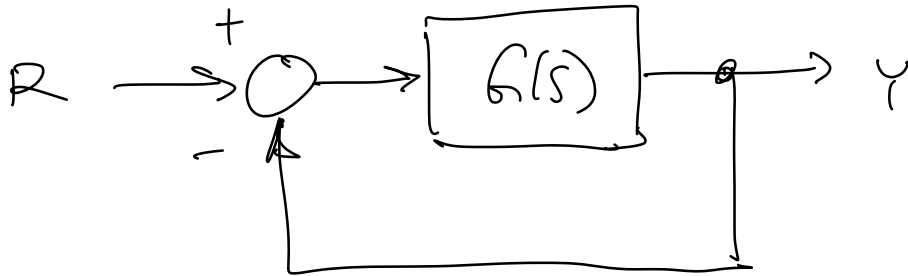
Unity feedback case - use #1



For non-unity or unity feedback - use #2



For unity feedback systems

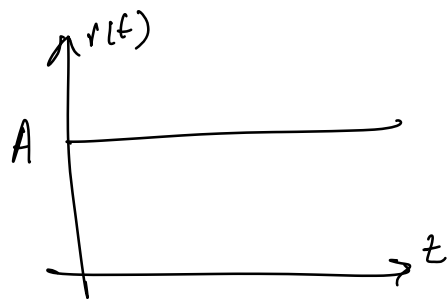


$$e_{ss} = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + G(s)} = 0$$

We want: $e_{ss} = 0$ or $e_{ss} = \text{constant}$.

we do not want $e_{ss} = \infty$

Suppose
input is
a step



$$r(t) = \begin{cases} A & t \geq 0 \\ 0 & t < 0 \end{cases}$$

$$R(s) = \frac{A}{s}$$

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + G(s)} = \lim_{s \rightarrow 0} \frac{s \left(\frac{A}{s} \right)}{1 + G(s)}$$

$$= \lim_{s \rightarrow 0} \frac{A}{1 + G(s)} = \frac{A}{1 + \lim_{s \rightarrow 0} G(s)}$$

$$e_{ss} = \frac{A}{1 + \lim_{s \rightarrow 0} G(s)} = \frac{A}{1 + K_p}$$

$$\text{where } K_p = \lim_{s \rightarrow 0} G(s)$$

↑
s.s. error expression for unity feedback system when reference is a step of mag. A.

we call $K_p = \lim_{s \rightarrow 0} G(s) = \text{DC gain of } G(s)$

or K_p is called the position constant.

How do we get $e_{ss} = 0$?

$$e_{ss} = \frac{1}{1 + K_p} = 0 \Rightarrow \underline{\underline{K_p = \infty}}$$

OK, then

$$K_p = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \left(\frac{(s+z_1)(s+z_2)\dots}{s^n (s+p_1)(s+p_2)\dots} \right)$$

$$\text{for } n \geq 1 \Rightarrow K_p \rightarrow \infty$$

we need at least 1 pole
at origin!

we call n the system type

$n=0$ type zero system

$$e_{ss} = \text{constant}$$

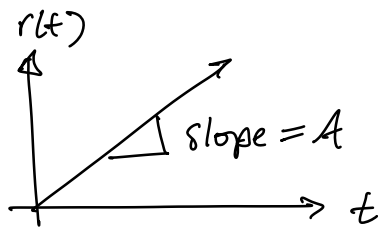
$n=1$ type 1 system

$$e_{ss} = 0$$

$n=2$ type 2 system

$$e_{ss} = 0$$

For ramp input:



constant velocity signal

$$R(s) = \frac{A}{s^2}$$

S.S. error:

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + G(s)} = \lim_{s \rightarrow 0} \frac{s (A/s^2)}{1 + G(s)}$$

$$e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s + s G(s)} = \frac{A}{0 + \underbrace{\lim_{s \rightarrow 0} s G(s)}_{K_v}}$$

or we have:

$$e_{ss} = \frac{A}{K_v} \quad \text{where} \quad K_v = \lim_{s \rightarrow 0} s G(s)$$

we call K_v the velocity constant.

To get $e_{ss} = 0$ for a ramp input,

we need $K_v \rightarrow \infty$

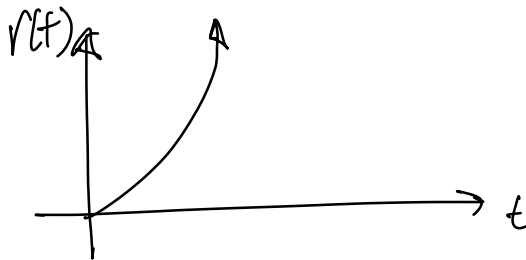
So,

$$K_v = \lim_{s \rightarrow 0} s G(s) = \lim_{s \rightarrow 0} s \left[\frac{(s+z_1)(s+z_2)\dots}{s^n(s+p_1)(s+p_2)\dots} \right]$$

\Rightarrow we need $n \geq 2$ (type 2) to

$$\text{get } K_v = \infty \Rightarrow \underline{\underline{e_{ss} = 0}}$$

For parabolic input :



constant acceleration

$$R(s) = \frac{A}{s^3}$$

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + G(s)} = \lim_{s \rightarrow 0} \frac{s (A/s^3)}{1 + G(s)}$$

$$= \lim_{s \rightarrow 0} \left[\frac{A}{s^2 + s^2 G(s)} \right] = \frac{A}{\lim_{s \rightarrow 0} s^2 G(s)}$$

$$e_{ss} = \frac{A}{K_a} \quad \text{where} \quad K_a = \lim_{s \rightarrow 0} s^2 G(s)$$

we call K_a the acceleration constant

What system type do we need to get $e_{ss} = 0$ for a parabolic input?

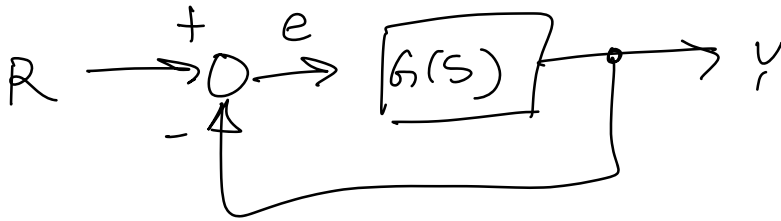
$$K_a = \lim_{s \rightarrow 0} s^2 G(s) = \lim_{s \rightarrow 0} s^2 \left[\frac{(s+z_1)(s+z_2)\dots}{s^n(s+p_1)(s+p_2)\dots} \right]$$

need $K_a = \infty$ to get $e_{ss} = 0$

so, we need $n \geq 3$ (type 3)!

Summary

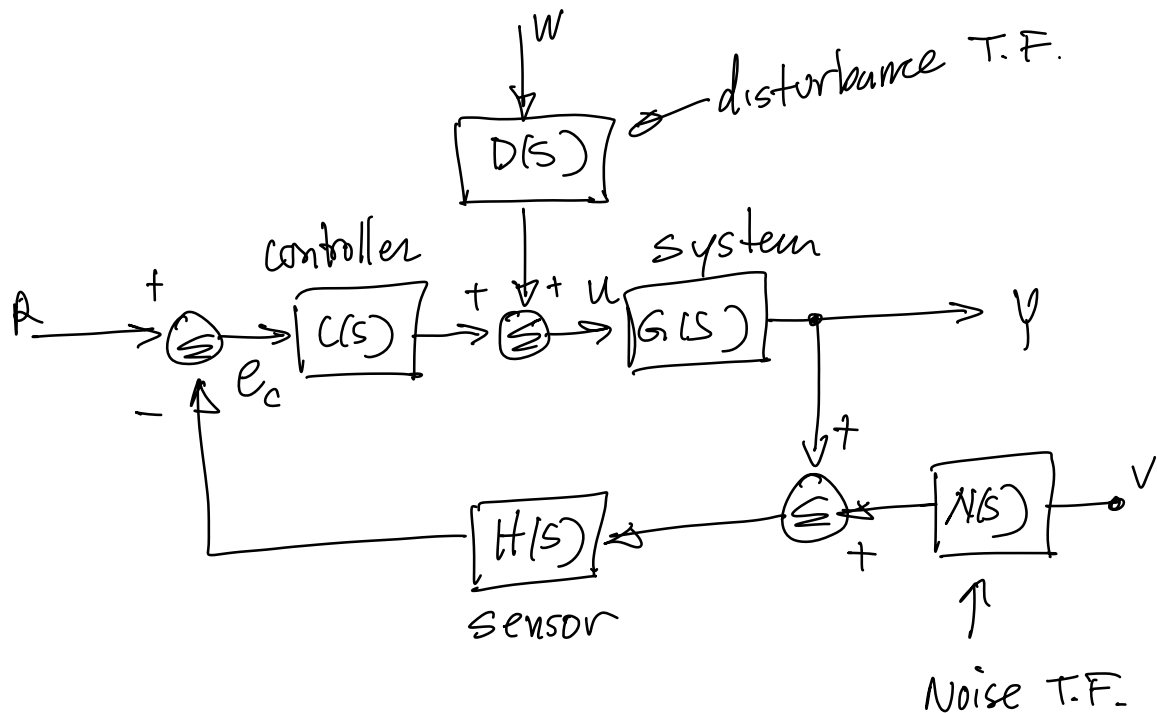
For unity feedback system:



$$e_{ss} = \lim_{s \rightarrow 0} \frac{R(s)}{1+G(s)} \quad \text{where } G(s) \text{ is the "system"}$$

system type	step input	ramp input	parabolic input
0 ($n=0$)	$\frac{A}{1+K_p}$	∞	∞
I ($n=1$)	0	$\frac{A}{K_v}$	∞
II ($n=2$)	0	0	$\frac{A}{K_a}$
III ($n=3$)	0	0	0

Error due to disturbance and sensor noise



Where:

W = disturbance

V = noise

$D(s)$ and $N(s)$ are T.F. that modify W and V before they affect the closed-loop system

Let's find the error due to r , w , and v :

$$e = r - y \quad (\text{tracking error})$$

$$\text{where } y = y_r + y_w + y_v$$

From the block diagram:

$$\frac{Y_r(s)}{R(s)} = \frac{C(s)G(s)}{1 + C(s)G(s)H(s)} = T_R(s)$$

$$\frac{Y_w(s)}{W(s)} = \frac{D(s)G(s)}{1 + C(s)G(s)H(s)} = T_W(s)$$

$$\frac{Y_v(s)}{V(s)} = \frac{N(s)H(s)C(s)G(s)}{1 + C(s)G(s)H(s)} = T_V(s)$$

Therefore:

$$Y(s) = Y_r(s) + Y_w(s) + Y_v(s)$$

$$Y(s) = \frac{C(s)G(s)}{1 + C(s)G(s)H(s)} R(s) +$$

$$\frac{D(s)G(s)}{1 + C(s)G(s)H(s)} W(s) +$$

$$\frac{N(s)H(s)C(s)G(s)}{1 + C(s)G(s)H(s)} V(s)$$

So,

$$E(s) = R(s) - Y(s)$$

$$E(s) = R(s) - T_R(s) R(s) - T_w(s) W(s) - T_v(s) V(s)$$

$$E(s) = \underline{\underline{[1 - T_R(s)]R(s) - T_w(s)W(s) - T_v(s)V(s)}}$$

To find e_{ss} :

$$e_{ss} = \lim_{s \rightarrow 0} s E(s)$$

$$e_{ss} = \lim_{s \rightarrow 0} \left\{ s \left[1 - T_R(s) \right] R(s) - T_w(s)W(s) - T_v(s)V(s) \right\}$$

So, we need to look at limits to determine final error!

Note, they all have same closed-loop poles!!