Blackbody Radiation

Thermal Fluids and Energy Systems Lab

(ME EN 4650)

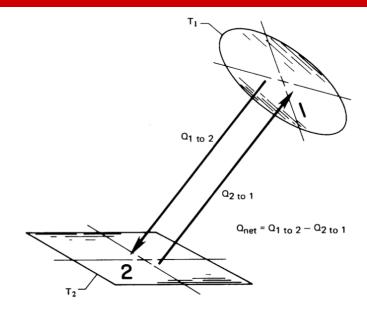
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Department of Mechanical Engineering

University of Utah

Based on Prof. M's slides

Net Radiation Exchange



The net radiation exchange from a hotter to cooler surface depends on:

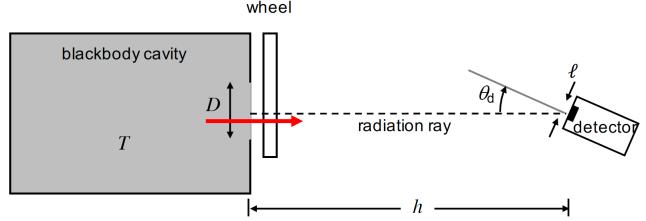
- 1. The temperatures of surface 1 and 2: T₁ and T₂
- 2. The areas of surface 1 and 2: A_1 and A_2
- 3. The shape, orientation, and spacing of surfaces 1 and 2
- 4. The radiative properties of the surface (e.g., ϵ , α , ρ)
- 5. Additional surfaces in the environment that may reflect radiation from surface 1 to surface 2 and vice versa
- 6. The medium between surfaces 1 and 2 (e.g., if it absorbs or emits radiation)

Heat Transfer by Thermal Radiation

What we want to know (simplify the problem):

$$q_{\rm rad} = f(T, h, D)$$

Use our data to validate the theory

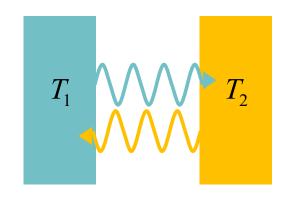


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- What we can measure:
 - $-q_{\rm rad}$ (pyroelectric radiometer)

Thermal Radiation & Electromagnetic Waves

Thermal radiation: Heat transfer via electromagnetic waves

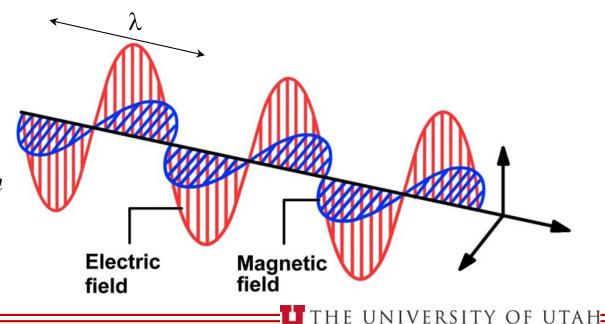


- Heat transfer by radiation <u>requires no matter</u>
- Matter at a finite temperature will emit thermal radiation

 the mechanism of emission is related to energy
 released as a result of oscillations or transitions of the
 electrons the oscillations are sustained by the internal
 energy of the matter

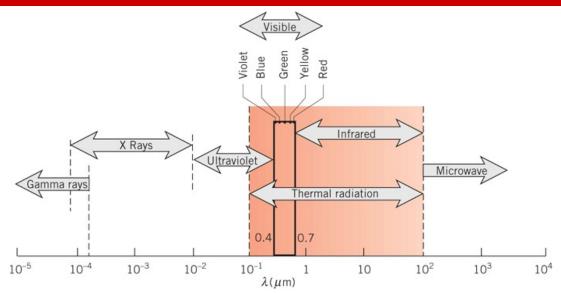
$$\lambda = \frac{c}{v} = \frac{c_0 / n}{v}$$
 frequency

- c is speed of light in a
 medium of refractive index n
- c_0 is speed of light in vacuum (2.998 × 10⁸ m/s)



Electromagnetic Waves

<u>Thermal radiation</u>:
Part of the UV + Visible + IR



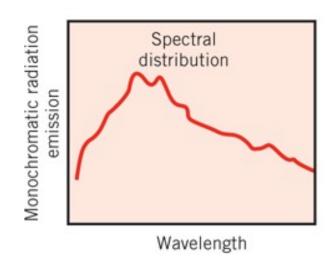
Complexity of radiation: up to 7 independent variables

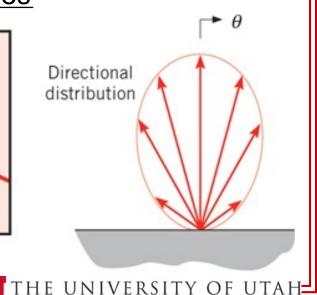
• Space: *x*, *y*, *z*

• Time: *t*

Direction: θ, φ

Wavelength: λ

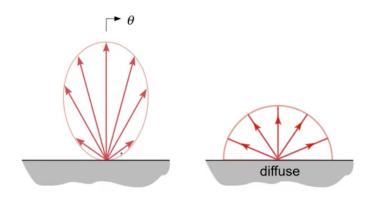




Blackbody Radiation

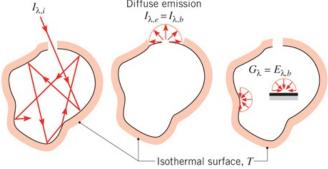
Blackbody (standard against which radiative properties of real surfaces may be compared):

- (1) A blackbody absorbs all incident radiation, regardless of wavelength and direction
- (2) For a prescribed temperature and wavelength, no surface can emit more energy than a blackbody
- (3) Radiation emitted by a blackbody is a function of wavelength and temperature, but it is independent of direction: the blackbody is a diffuse emitter.



Blackbody Radiation – Planck Distribution

A blackbody can be approximated by a cavity with inner surface at a uniform temperature



Blackbody spectral intensity:

$$I_{\lambda,b}(\lambda,T) = \frac{2hc_0^2}{\lambda^5[\exp(hc_0/\lambda k_B T) - 1]} \left[\frac{W}{\mu m \cdot m^2 \cdot sr} \right]$$

- $h = 6.626 \times 10^{-34} \text{ J} \cdot \text{s}$ is the Planck constant
- $k_B = 1.381 \times 10^{-23}$ J/K is the Boltzmann constant
- *T* is the absolute temperature of the blackbody [K]



Planck Distribution

Blackbody spectral emissive power:

$$E_{\lambda,b}(\lambda,T) = \pi I_{\lambda,b}(\lambda,T)$$

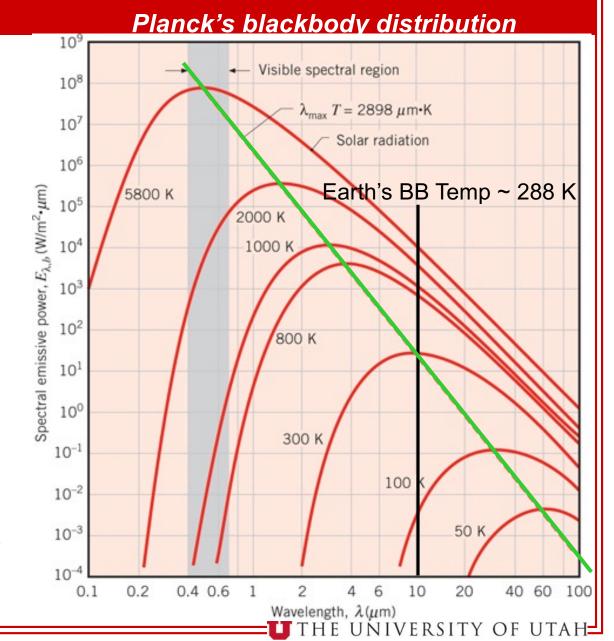
$$\left[\frac{W}{\mu m \cdot m^2}\right]$$
 Diffuse emitter

Wien's displacement law:

$$\lambda_{\max} T = \text{Constant}$$

$$\lambda_{\text{max}}T = 2898 \ \mu m \cdot K$$

Wavelength leading to the maximum emissive power for a given temperature



Directional distribution of thermal radiation is described via solid angles

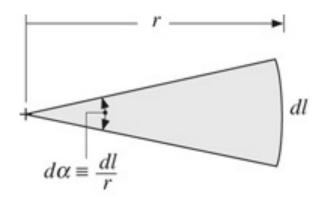
Solid angles are 2D angular spaces:

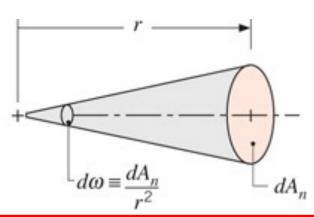
• 1D angular space: $d\alpha = \frac{dl}{r}$ radians [rad]

dl: infinitesimal length on a circle

• 2D angular space: $d\omega = \frac{dA_n}{r^2}$ steradians [sr]

 dA_n : infinitesimal area on a **sphere**





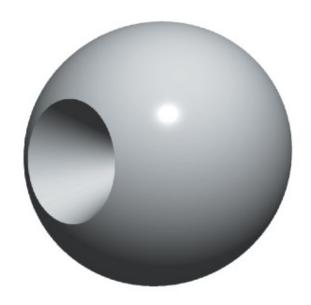


Figure 3.2 — A 1-steradian solid angle removed from a sphere.

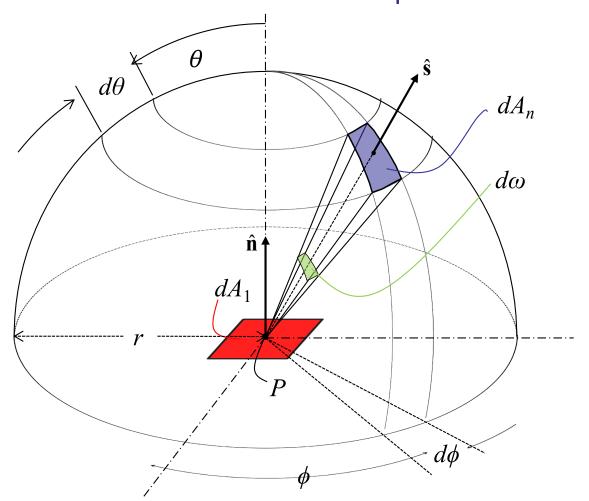


Adapted by James J. Gross from The Light Measuremen Handbook.

Figure 3.3 — For a solid angle that measures 1 steradian, $A = r^2$.

$$d\omega = \frac{dA_n}{r^2}$$

Let's consider an emitting point P on a surface. Point P can radiate into all directions contained within a hemisphere of radius r.



 dA_n : infinitesimal area on the hemisphere of radius r

 θ : polar angle

 ϕ : azimuthal angle

 $d\omega$: infinitesimal solid angle

We say, "The area dA_n , through which the radiation passes, **subtends** a differential solid angle $d\omega$ when viewed from a point on dA_1 "

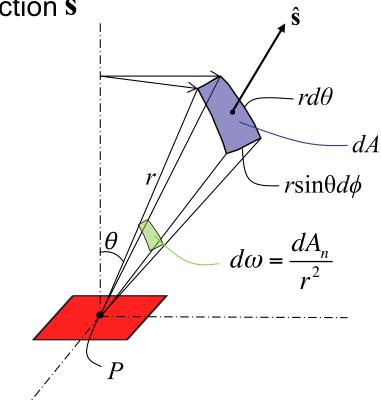
Let's take a closer look at a particular direction $\hat{\mathbf{s}}$

• The infinitesimal area dA_n is given by:

$$dA_n = r^2 \sin\theta d\theta d\phi$$

The infinitesimal solid angle is given by:

$$d\omega = \frac{dA_n}{r^2} = \frac{r^2 \sin\theta d\theta d\phi}{r^2}$$



$$\therefore d\omega = \sin\theta d\theta d\phi$$

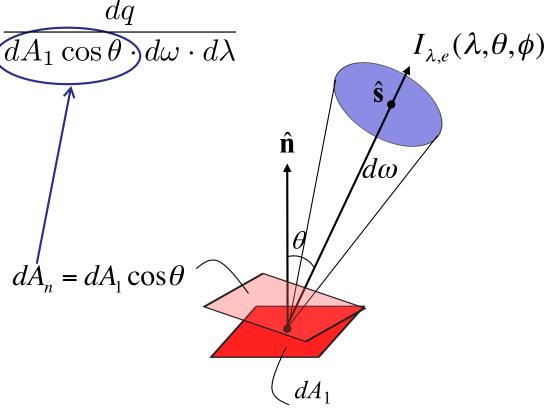
Solid angle in spherical coordinates

Radiation Intensity, I

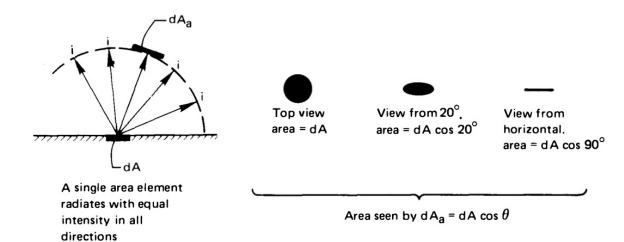
Rate at which radiant energy is <u>emitted</u> at the wavelength λ in the direction (θ,ϕ) , per unit wavelength, per unit solid angle and per unit area normal to the direction (θ,ϕ)

$$I_{\lambda,e}(\lambda,\theta,\phi) = \frac{dq}{dA_n \cdot d\omega \cdot d\lambda} = \underbrace{\frac{dq}{dA_1 \cos \theta} d\omega \cdot d\lambda}_{\text{m}^2 \cdot sr \cdot \mu m}$$

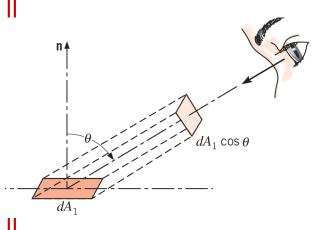
Lambert's Cosine Law

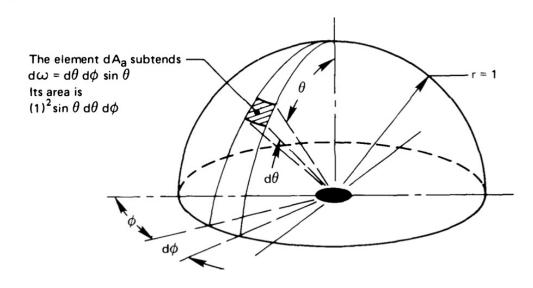


Lamberts Cosine Law



Lambert's Cosine Law





Radiation Exchange Between 2 Black **Bodies**

Radiation transfer from source to the detector is given by:

(1)
$$dq = I_b dA_{\mathbf{s}_n} d\omega$$
 $I_b = \int I_{b,\lambda} d\lambda$

Total Intensity for a BB, since it's a diffuse emitter

(2)
$$I_b = \frac{E_b}{\pi} = \frac{\sigma T^4}{\pi}$$

(3) $d\omega = \frac{dA_{\mathrm{d}_n}}{h^2}$
(4) $dA_{\mathrm{d}_n} = dA_{\mathrm{d}} \cos \theta_{\mathrm{d}}$

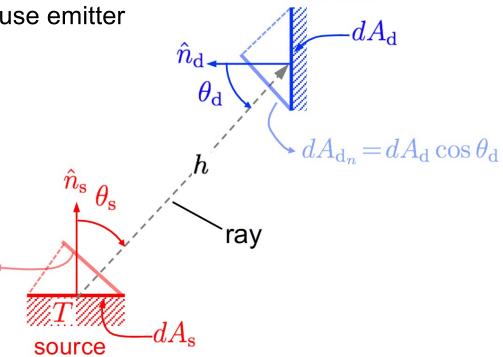
(3)
$$d\omega = \frac{dA_{\mathrm{d}_n}}{h^2}$$

$$(4)dA_{\mathbf{d}_n} = dA_{\mathbf{d}} \cos \theta_{\mathbf{d}}$$

$$(5)dA_{s_n} = dA_s \cos \theta_s \, dA_{s_n} = dA_s \cos \theta_s \leftarrow$$

Plug 2-5 into (1)

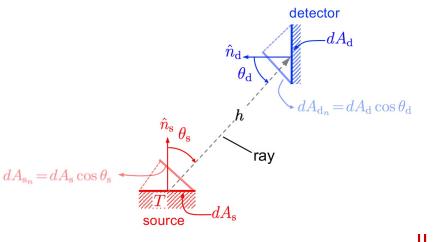
$$dq = \frac{\sigma T^4}{\pi h^2} \cos \theta_{\rm s} \cos \theta_{\rm d} dA_{\rm d} dA_{\rm s}$$



detector

Radiation Exchange Between 2 Black Bodies

$$dq = \frac{\sigma T^4}{\pi h^2} \cos \theta_{\rm s} \cos \theta_{\rm d} dA_{\rm d} dA_{\rm s}$$



Integrate over the Areas

$$q = \sigma T^4 \underbrace{\int_{A_s} \int_{A_d} \frac{\cos \theta_s \cos \theta_d}{\pi h^2} dA_d dA_s}_{=A_s F_{s \to d}}$$

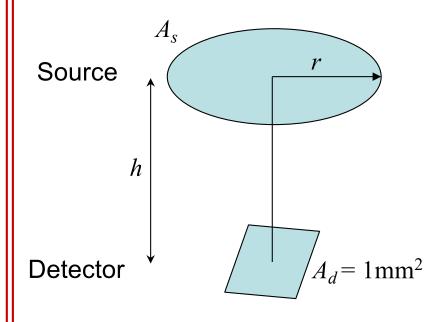
Recall, view factor definition

$$\Rightarrow F_{ij} = \frac{q_{i \to j}}{q_i}$$

$$F_{ij} = \frac{1}{A_i} \int_{A_i} \int_{A_i} \frac{\cos \theta_i \cos \theta_j}{\pi R^2} dA_i dA_j$$

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View Factors



View Factor (from literature):

$$r = D/2$$

$$F_{\rm d\to s} = \frac{1}{1 + \left(\frac{h}{r}\right)^2}$$

Using reciprocity:

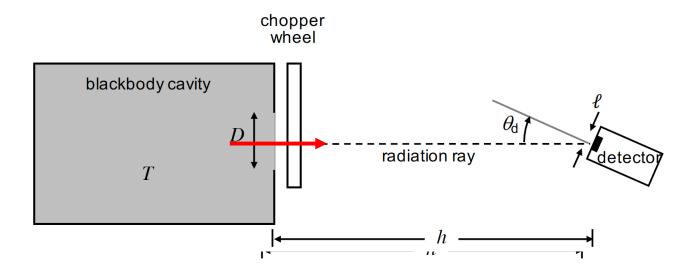
$$A_{\rm s} F_{\rm s \to d} = A_{\rm d} F_{\rm d \to s}$$

Heat transfer rate:

$$q_{\text{theory}} = \frac{\sigma T^4 A_d r^2}{(r^2 + h^2)}$$

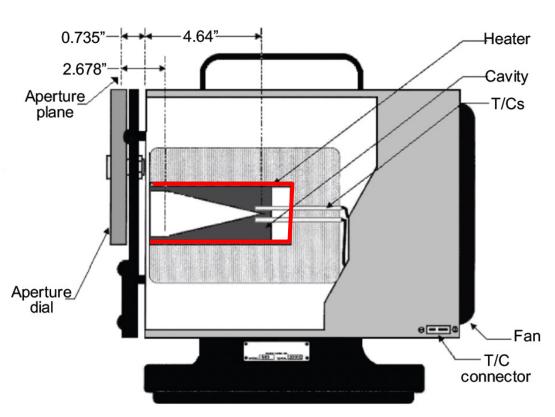
$$q_{\rm theory} = \frac{\sigma \, T^4 \, A_d \, D^2}{(D^2 + 4 \, h^2)}$$

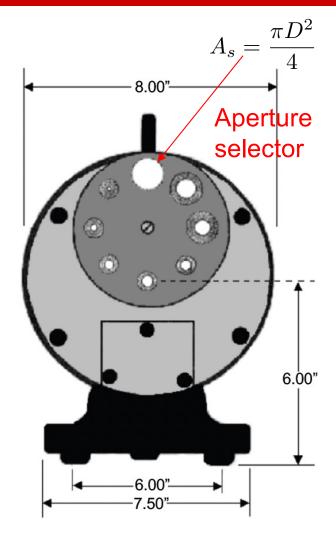
Experimental Setup



Ray - the straight line along which the electromagnetic wave travels between two points

Blackbody Cavity





Experimental Setup

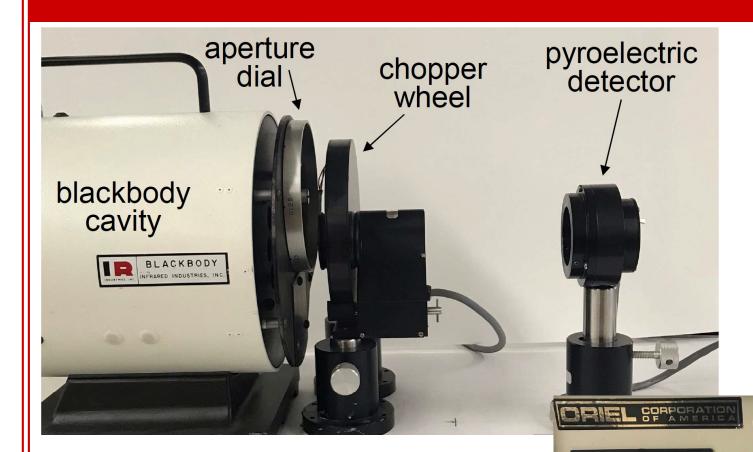
Multiplier

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Ambient Suppress

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Response



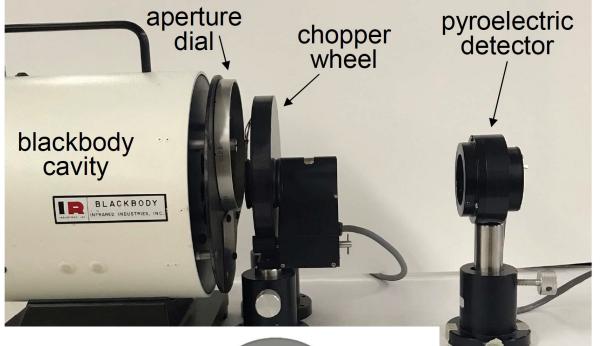
Measures very small heat transfer rates: 10^{-2} to 10^{-6} W

Instrument box

007

Experimental Setup – Pyroelectric detector

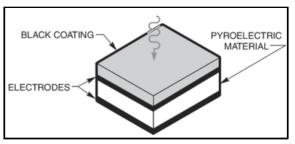
Pyroelectric detector – voltage generated due to a change in temperature

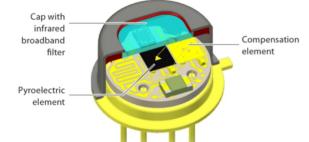


 λ in the range 2-14 μ m

detector

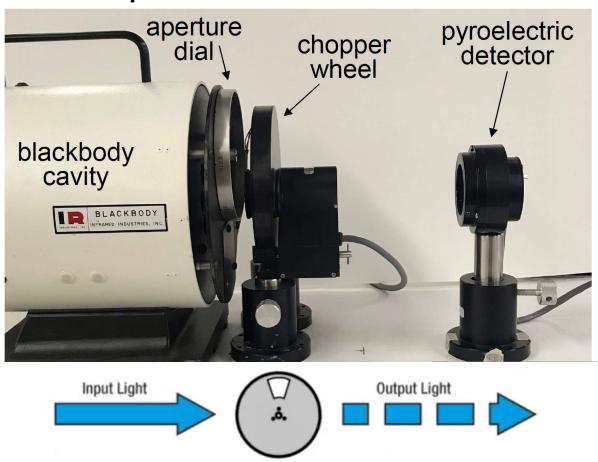




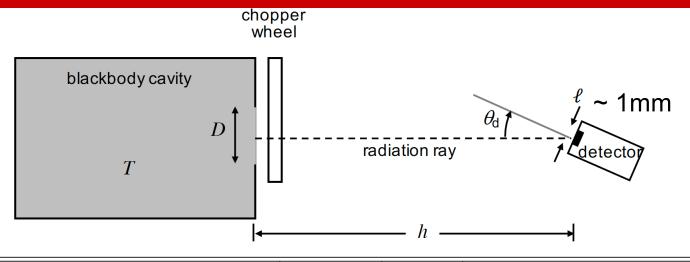


Experimental Setup – Pyroelectric detector

Pyroelectric detector – voltage generated due to a change in temperature



Measurements



Quantity	Symbol	Units	Instrument
Temperature of blackbody	T	°C	thermocouple
Separation distance	h	in	linear ruler
Angle of detector head	$\theta_{ m d}$	deg	rotation table
Aperture diameter of source	D	in	markings on dial
Heat transfer rate	q	W	pyroelectric radiometer

$$q_{\rm rad} = f(T, h, D)$$

Vary *h* hold *T* and *D* constant Vary *T* hold *h* and *D* constant Vary *D* hold *T* and *H* constant

 $\theta_d = 0^{\circ}$ for all experiments

Data Collection Sheet

TFES Lab (ME EN 4650)

Blackbody Radiation Experiment: Raw Data Sheet

T_{atm}:_____(°C)
P_{atm}: (mbat/hPa)

Experiment 1: Variable h

T (oC)	D (in)	h (in)	q (μW)
	0.6	8	
	0.6	9	
	0.6	10	
	0.6	11	
	0.6	12	

Experiment 2: Variable T

T (oC)	D (in)	h (in)	q (μW)
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	
	0.6	9	

Experiment 3: Variable D

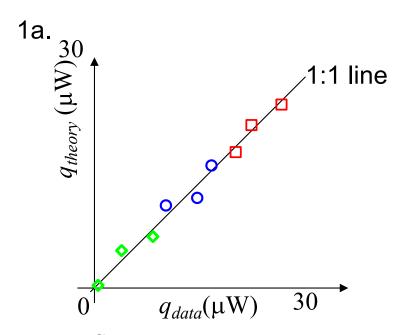
T (oC)	D (in)	h (in)	q (μW)
	0.1	9	
	0.2	9	
	0.4	9	
	0.6	9	

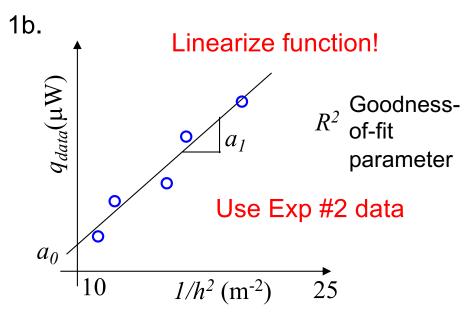
Set T ~ 460 C vary h

Set T ~ 700 C Record q every 20C Set T ~ 700 C Vary aperture ,D

Submission Requirements

$$q = f(T, h, D)$$



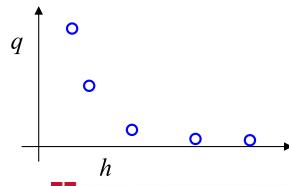


$$R^2 = 1 - \frac{S_R}{S_T} \quad \text{Correlation coef/coef of determination}$$

$$S_R = \sum_{i=1}^{N} (y_i - a_0 - a_1 x_i)^2$$

$$S_T = \sum_{i=1}^{N} (y_i - \overline{y})^2$$

$$S_T = \sum_{i=1}^{N} (y_i - \overline{y})^2$$



Pseudocode for Linearizing and Computing Linear Regression

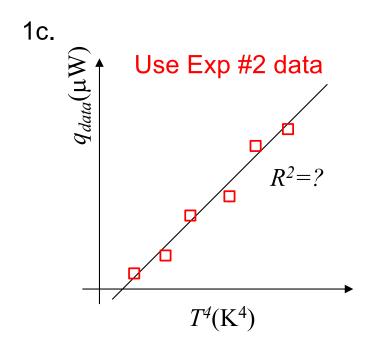
```
h2 = 1./(h.^2); %Linearize h
p = polyfit(h2,qdata,1) %Least squares regression
a1 = p(1) %slope
a0 = p(2) %intercept
SR = sum((qdata - a0 - a1*h2).^2) %compute sum of the squares of the residual
ST = sum((qdata - mean(qdata)).^2) %compute
Rsquared = 1 - SR/ST %compute coefficient of determination
```

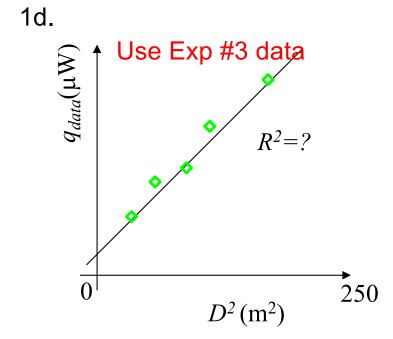
$$R^{2} = 1 - \frac{S_{R}}{S_{T}}$$

$$S_{R} = \sum_{i=1}^{N} (y_{i} - a_{0} - a_{1} x_{i})^{2}$$

$$S_{T} = \sum_{i=1}^{N} (y_{i} - \overline{y})^{2}$$

Submission Requirements





Solid Angle of Moon Subtended from Earth

