电话: 131167875% - O 种答案解析 http://jsyky.taobao.com/

一、解:(1)、

$$\omega = \begin{cases} \frac{1}{EI} (ax^4 + Lx^3 + cx^2), 0 \le x \le L \\ \frac{1}{EI} (dx^3 + cx^2 + ex), L \le x \le 2L \end{cases}$$

$$\theta = \omega' = \begin{cases} \frac{1}{EI} (4ax^3 + 3Lx^2 + 2cx) & 0 \le x \le L \\ \frac{1}{EI} (3dx^2 + 2cx + e) & L \le x \le 2L \end{cases}$$

$$M(x) = -EI\omega'' = \begin{cases} -(12ax^{2} + 6Lx + 2c), 0 \le x \le L \\ -(6Lx + 2c), L \le x \le 2L \end{cases}$$

(2)、
$$F_s(x) = \frac{\partial M(x)}{\partial x} = \begin{cases} -(24ax + 6b), 0 \le x \le L \\ -(6dL + 2c), L \le x \le 2L \end{cases}$$
(3)、C 处存在集中外力偶,则对于
在 AC 段上: $M_1(L) = -(12aL^2 + 6bL + 2c)$

在 AC 段上:
$$M_1(L) = -(12aL^2 + 6bL + 2c)$$

在 BC 段上:
$$M_2(L) = -(601 + 20)$$

因此
$$M_1(L) \neq M_2(L)$$
,即

在 BC 段上:
$$M_2(L) = -(6dL + 2d)$$
因此 $M_1(L) \neq M_2(L)$, 即
$$12aL^2 + 6bL + 2c \neq 0$$
, $2aL + b + d \neq 0$

(4)、A 处存在外集中力,则 AC 段:
$$F_s(D) = -6b \neq 0$$
, 即 b $\neq 0$

(5)、挠度:
$$\omega_1(L) = \omega_2(L)$$
, 即 $aL^4 + bL^3 + cL^2 = dL^3 + cL^2 + eL$,

化简为aL³ +
$$(b - d)L^2 - e = 0$$

转角:
$$\theta_1(L) = \theta_2(L)$$
, 即: $4aL^3 + 3bL^2 + 2cL = 3dL^2 + 2d + e$

二、解: (1)、以 0°方向为 x 轴正方向, 90°方向为 y 轴正方向

$$\sigma_{4s} = \frac{\sigma_0 + \sigma_{90}}{2} + \frac{\sigma_0 - \sigma_{90}}{2} \cos 90 - \tau_{xy} \sin 90$$
及时雨差研表博网。http://www.fc/

$$110 = \frac{180 + 100}{2} + \frac{180 - 100}{2} \times 0 - \tau_{xy}, \ \ \text{θ τ_{xy}} = 30 \text{MPa.}$$

$$\begin{cases} \sigma_{\text{max}} \\ \sigma_{\text{min}} \end{cases} = \frac{\sigma_{x} + \sigma_{y}}{2} \pm \sqrt{\left(\frac{\sigma_{x} - \sigma_{y}}{2}\right)^{2} + \tau^{2}}$$

$$= \frac{180 + 100}{2} \pm \sqrt{\left(\frac{180 - 100}{2}\right)^{2} + 20^{2}}$$

$$= \begin{cases} 190 \text{MPa} \\ 90 \text{MPa} \end{cases}$$

故
$$\sigma_1 = 190 MPa$$
, $\sigma_2 = 90 MPa$, $\sigma_3 = 0$

(2)、最大切应力为:
$$\tau_{\text{max}} = \frac{\sigma_1 - \sigma_3}{2} = 95 MPa$$

$$\varepsilon_0 = \frac{1}{E} \left(\sigma_0 - \nu \sigma_{90} \right) = \frac{1}{200 \times 10^9} \times \left(-180 = 0.3 \times 100 \right) \times 10^6 = 7.5 \times 10^{-4}$$

$$\varepsilon_{90} = \frac{1}{E} \left(\sigma_{90} - \nu \sigma_0 \right) = -\frac{1}{200 \times 10^9} \times (100 - 0.3 \times 180) \times 10^6 = 2.3 \times 10^{-4}$$

$$\sigma_{135} = \frac{\sigma_0 + \sigma_{90}}{2} + \frac{\sigma_0 - \sigma_{90}}{2} \cos 270 - \tau_s \sin 270 = 140 + 30 = 170 MPa$$

$$\varepsilon_{45} = \frac{1}{E} \left(\sigma_{45} - \nu \sigma_{135} \right) = \frac{1}{200 \times 10^9} \times \left(100 - 0.3 \times 170 \right) \times 10^6 = 2.95 \times 10^{-4}$$

(4)、体积改变能密度:

$$V_{\nu} = \frac{1 - 2\nu}{6E} \left(\sigma_1 + \sigma_2 + \sigma_3 \right)^2 = \frac{1 - 2 \times 0.3}{6 \times 200 \times 10^9} \times \left(190 + 90 + 0 \right)^2 \times 10^{12} = 2.61 \times 10^4$$

形状改变能密度:

$$V_{d} = \frac{1+\nu}{6E} \left[(\sigma_{1} - \sigma_{2})^{2} + (\sigma_{1} - \sigma_{3})^{2} + (\sigma_{2} - \sigma_{3})^{2} \right]$$

$$= \frac{-1+0.3}{6\times200\times10^{9}} \times \left[(190-90)^{2} + (190-0)^{2} + (90-0)^{2} \right] \times 10^{12} = 5.87\times10^{4} \text{ J/m}^{2}$$

$$\equiv \mathcal{M}: (1)$$

$$\xrightarrow{A} \xrightarrow{B}$$

$$F_{y} = F \sin \alpha = \frac{1}{2} F$$

$$F_z = F \cos \alpha = \frac{\sqrt{3}}{2} F$$

$$N_y = F_z a = \frac{\sqrt{3}}{2} F_a$$

$$M_z = F_z a = \frac{1}{2} Fa$$

(2),
$$I_{\rm v} = \frac{\pi d^4}{64} - \frac{2b \cdot b^3}{12} = \frac{23b^4}{64}$$

$$I_{n} = \frac{\pi d^{4}}{64} - \frac{b \cdot (2b)^{3}}{120b^{3}}$$

中性轴方程为:

代入数值,
$$-\frac{\sqrt{3} Fa}{\frac{2}{23b^4}}z = 0$$

设 θ 为中性轴与 y 轴的夹角,则 $\tan \theta = \frac{z}{y} = \frac{23}{20\sqrt{3}}$,故 $\theta = \arctan \frac{23}{20\sqrt{3}}$

(3),
$$\sigma_{\text{max}} = \frac{M_y}{I_y} \cdot \frac{d}{2} + \frac{M_z}{I_z} \cdot \frac{d}{2} = \frac{\frac{\sqrt{3}}{2} Fa}{\frac{23}{6} b^4} \cdot \frac{d}{2} + \frac{\frac{1}{2} Fa}{\frac{10}{3} b^4} \cdot \frac{d}{2} = \frac{Fa}{b^3 \pi^{\frac{1}{4}}} \left(\frac{6\sqrt{3}}{23} + \frac{3}{10} \right)$$

(4).
$$\sigma_{II} = \frac{M_{y}}{I_{y}} \cdot \frac{b}{2} + \frac{M_{z}}{I_{z}} \cdot b = \frac{\frac{\sqrt{3}}{2} Fa}{\frac{23}{6} b^{4}} \cdot \frac{b}{2} + \frac{\frac{1}{2} Fa}{\frac{10}{3} b^{4}} \cdot b = \frac{30\sqrt{3} + 69}{460} \frac{Fa}{b^{3}}$$

(5),

$$\sigma_{\max} = \frac{M_{y}}{I_{y}} \cdot \frac{d}{2} + \frac{M_{z}}{I_{z}} \cdot \frac{d}{2} = \frac{Fa\cos\alpha}{\frac{23}{6}b^{3}\pi^{\frac{1}{4}}} \cdot \frac{1}{2} + \frac{Fa\sin\alpha}{\frac{10}{3}b^{3}\pi^{\frac{1}{4}}} \cdot \frac{1}{2} = \frac{Fa}{b^{3}\pi^{\frac{1}{4}}} \left(\frac{12}{23}\cos\alpha + \frac{3}{20}\sin\alpha\right)$$

当 $\sigma_z = \sigma_y$ 时,最大弯曲正应力取得极小值,

故
$$\frac{Fa\cos\alpha}{23} \cdot \frac{1}{6} = \frac{Fa\sin\alpha}{\frac{10}{3} b^3 \pi^{\frac{1}{4}}} \cdot \frac{1}{2}$$
, $\tan\alpha = \frac{20}{23}$, 解得 $\alpha = \arctan\frac{20}{23}$

四、解: (1)、M(x) = -Fx

$$V_{Ab} = \int_0^L \frac{M^2(x)}{2EI} dx = \int_0^L \frac{(Fx)^2}{2EI} dx = \frac{F^2 L^3}{4Eb^4}$$

(2)、截面为矩形,故 $\alpha = \frac{6}{5}$

$$V_{s} = \int_{0}^{L} \alpha \frac{F^{2}(x)}{2GA} dx = \alpha \frac{F^{2}L}{2GA} \frac{2F^{2}L}{8Eb^{2}}$$

(3).
$$\frac{V\varepsilon b}{V\varepsilon S} = \frac{\frac{F^2L^3}{4Eb^2}}{\frac{3F^2L}{8Eb^2}} = \frac{2}{2} \left(\frac{b^3}{L}\right)^2$$

当
$$\frac{b}{L} = \frac{1}{10}$$
时, $\frac{V\varepsilon b}{V\varepsilon S} = \frac{3}{200}$

故
$$V\varepsilon$$
S 所占百分比为 $\frac{3}{200}$ =1.48%

五、请参照孙驯服的课本第二册例 3-17

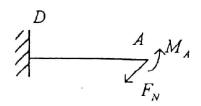
解:正三角形的内力为超静定,利用对称性,截开 A、B 两点,只存在对称的力。

即只可能有轴力和弯矩,由于 AB 段结构和荷载都关于 CD 轴对称,故轴向截面

AB上的轴力和弯矩相等,其轴力可由静力平衡方程求得,即 $\sum F_{i}=0$,

$$2F_N \sin 60^\circ - F = 0$$
, $F_N = \frac{F}{\sqrt{3}}$

故仅有M_A未知,由于A截面的转角为0,(反对称的位移为0)将结构化简为



$$M(x) = -\frac{F}{2}x + M_{\Lambda}$$

故
$$\theta = \int_0^a \frac{M_A - \frac{F}{2}x}{EI} dx = 0$$

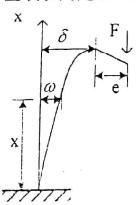
解得 $M_A = \frac{Fa}{4}$

所以 $M_{ij} = M(a) = -\frac{Fa}{4}$

故 D 处的内力为 $M_n =$

$$F = \frac{F}{\sqrt{3}} \cosh 60^\circ = -\frac{\sqrt{3}}{6} F$$
 (法)

六、这道题严重被所谓的网络答案误导,而且在 15 年考研又考出类似的题,在 刘鸿文的材料中绝对找不到,某些商家还申称指定用书只有刘鸿文。其实是孙训 方下册,4-6 的课后题,4 章为《压杆稳定问题的进一步研究》,很多同学看到这 里误以为超纲而没有仔细研读,当年我考试也是被所谓的答案害惨了。



解:
$$M(x) = -F(e + \delta - \omega)$$

$$EI\omega'' = -M(x) = F(e + \delta - \omega)$$

设
$$\frac{F_{cr}}{EI} = k^2$$
,则 $\omega'' + k^2 \omega = k^2 (e + \delta)$

$$\omega = A \operatorname{sinkx} + B \operatorname{coskx} + e + \delta = \delta$$

$$\omega' = A k \cos k x - B k \sin k x$$

当
$$x = 0$$
 时, $\omega = 0$ 即 $B + e + \delta = 0$, $B = -e - \delta$

当
$$\omega'=0$$
, 即 $Ak=0$

当
$$x = L$$
时, $\omega = \delta$,即 $-(\delta + e)\cos kL + e + \delta = \delta$,

$$-(\delta + e) = \frac{e}{\cos kL}$$

$$\delta = \frac{1 - \cos kL}{\cos kL} e$$

故 B 截面的最大应力
$$\sigma = \frac{F}{A} + \frac{M}{W}$$

$$M = F(e + \delta) = \frac{Fe}{\operatorname{coskL}}$$
, $\forall \sigma = \frac{F}{A} + \frac{Fe}{\operatorname{coskL}W}$

临界力表达式
$$\sigma_{st} = \frac{F}{A} + \frac{Fe}{W \cos\left(\sqrt{\frac{F}{EI}L}\right)} \le [\sigma]$$

