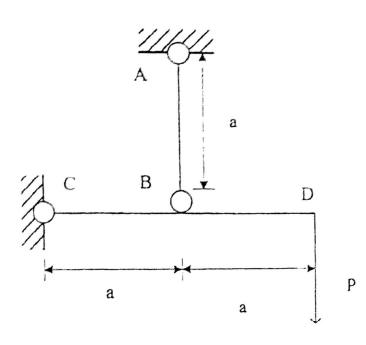
## 二O一六年真题

## 答案解析

一、已知: AB 杆和 CD 杆都是半径为 d 的圆杆, AB 杆的弹性模量为 E, 其中 AB 杆纵向线应变为  $\varepsilon$ , BD 刚性杆(30 分)



求: (1)、P的大小

- (2)、求 D 的竖向位移
- (3)、求 AB 杆所具有的应变能

解: (1)、BD 杆为刚性杆,所以 $EI 
ightarrow \infty$ ,不发生弯曲变形

$$\sum M_{C} = 0, \quad F_{NAB} \cdot a - P \cdot 2a = 0, \quad \text{if } P = \frac{F_{NAB}}{2}$$

$$\varepsilon = \frac{F_{NAB}}{EA} , \quad A = \frac{1}{4} \pi d^2$$

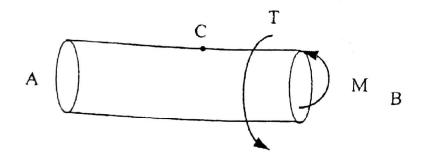
综上, 
$$P = \frac{\pi d^2 E \varepsilon}{8}$$

(2), 
$$\Delta D_y = 2\Delta B_y \approx 2\varepsilon a$$

(3). 
$$v_{\varepsilon} = \frac{1}{2} E \varepsilon^2$$

$$V_{\varepsilon} = \int_{L} \frac{1}{2} E \varepsilon^{2} dV = \frac{1}{2} E \varepsilon^{2} \cdot \frac{1}{4} \pi d^{2} \cdot 2a = \frac{\pi E \varepsilon^{2} d^{2} a}{4}$$

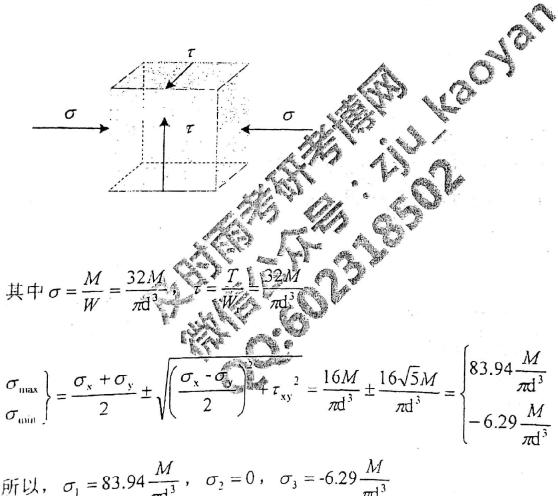
二、在 AB 圆杆上的 B 端受力如图, 己知T=2M, EI,  $\upsilon=0.3$ 



求: (1) C 处的主应力 $\sigma_1$ ,  $\sigma_2$ ,  $\sigma_3$ 

- (2)、C 处的最大切应力
- $(3), \ \varepsilon_1, \ \varepsilon_2, \ \varepsilon_3$
- (4)、C 处的第三主应力 $\sigma_{r_3}$

解:(1)、C点单元体受力情况:



所以,
$$\sigma_1 = 83.94 \frac{M}{\pi d^3}$$
, $\sigma_2 = 0$ , $\sigma_3 = -6.29 \frac{M}{\pi d^3}$ 

(2)、最大切应力
$$\tau = \frac{\sigma_1 - \sigma_3}{2} = 45.12 \frac{M}{\pi d^3}$$

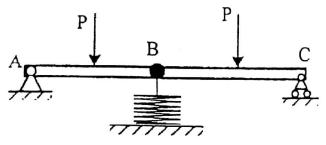
(3), 
$$\varepsilon_1 = \frac{1}{E} \left[ \sigma_1 - \upsilon (\sigma_2 + \sigma_3) \right] = \frac{1}{E} \left[ 83.94 \frac{M}{d^3} - \upsilon \left( 0 - 6.29 \frac{M}{d^3} \right) \right] = 88 \frac{M}{Ed^3}$$

$$\varepsilon_2 = \frac{1}{E} \left[ \sigma_2 - \nu (\sigma_1 + \sigma_3) \right] = \frac{1}{E} \left[ 0 - \nu \left( 83.94 \frac{M}{d^3} - 6.29 \frac{M}{d^3} \right) \right] = -23.30 \frac{M}{Ed^3}$$

$$\varepsilon_3 = \frac{1}{E} \left[ \sigma_3 - \nu (\sigma_1 + \sigma_2) \right] = \frac{1}{E} \left[ -6.29 \frac{M}{d^3} - \nu \left( 83.94 \frac{M}{d^3} + 0 \right) \right] = -31.47 \frac{M}{Ed^3}$$

(4), 
$$\sigma_{r3} = \sqrt{\sigma^2 + 4\tau^2} = \frac{32\sqrt{5}M}{\pi d^3} = 22.78 \frac{M}{d^3}$$

三、简支梁 AC 杆中点 B 有弹簧支撑, 受力情况如图所示.



求:(1)、弹簧的反力(2)、弹簧的刚度 k

易知,  $M_B=0$ , 分析结构的左半部分,  $\sum M_B=0$ ,  $F_A$  2L PL=0

$$F_A = \frac{P}{2}$$

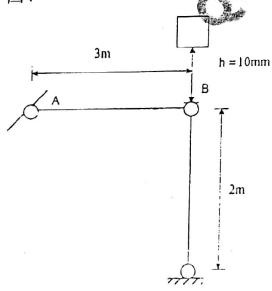
左右对称,所以 $F_B = \frac{P}{2}$ ,

整体而言, $\sum F_{i} = 0$ ,所以弹簧反为F = P

(2) 分析左半部分,
$$\omega_{BL} = \frac{PL^3}{3EL} + \frac{PL^2}{2EI} \times L = \frac{FL^3}{3EI} = \frac{FL^3}{2EI}$$

所以弹簧的刚度 $k = \frac{2}{a_{kk}} = \frac{EI}{L^3}$ 

四、



已知: AB 杆:  $EI = 5 \times 10^5 N \cdot m^2$ ,  $A = 150 cm^2$ ,  $n_{st} = 2.5$ 

AB, BC 杆: E=200GPa, d=38mm, P=300N,  $\sigma_P=200MP$ a

求: (1)、Kd (2)、BC 杆的稳定性

解: (1)、设 BC 杆的内力为 X,

$$\omega_B = \Delta L_{BC}$$
,  $\omega_B = \frac{(P - X)L^3_{AB}}{3EI}$ ,  $\Delta L_{BC} = \frac{XL_{BC}}{EA}$ 

解得 X = 299.85N

$$\Delta_{\rm st} = \omega_B = 2.7 \times 10^{-6}$$

$$K_d = 1 + \sqrt{1 + \frac{2h}{\Delta st}} = 87.1$$

(2)、对于 BC 杆:

$$\lambda_{I'} = \pi \sqrt{\frac{E}{\sigma_{I'}}} = 99.35$$

$$\lambda_{RC} = \frac{\mu L}{i} = \frac{\mu L}{\frac{d}{4}} = \frac{1 \times 2}{0.038} \ge \lambda_p$$
,所以 BC 杆属于大家度됨。

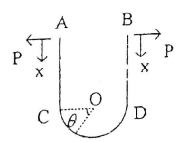
$$F_{\rm cr} = \frac{\pi^2 EI_{BC}}{(\mu L)^2} = \frac{\pi^3 \frac{1}{64} 0.038^4 \times 200 \times 10^9}{4} = 50.5$$

$$\sigma_{\rm cr} = \frac{F_{\rm cr}}{A} = 44.54 MPa$$

$$\sigma_{\text{st. d}} = K_{\text{d}} \frac{X}{A} = \frac{299.85}{\frac{1}{4} \pi 0.038^2} \times 87.1 = 23.03 MPa$$

 $\sigma_{\rm st, d} \leq \sigma_{\rm cr}$ ,故结构稳定

五、



己知:

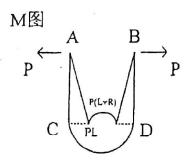
求: (1)、各杆弯矩

(2)、AB之间的位移

解: (1)、AC 段: M(x) = Px,  $0 \le x \le L$ 

$$CD$$
 段:  $M(\theta) = PR \cos + PL$ ,  $0 \le \theta \le \pi$ 

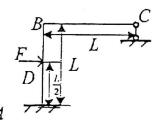
BD 段: 
$$M(x) = Px$$
,  $0 \le x \le L$ 



(2),

$$\Delta_{AB} = 2 \int_0^L \frac{Px^2}{EI} dx + \int_0^{\pi} \frac{PR(R\cos\theta + L)^2}{EI} d\theta = \frac{2PL}{3EI} + \frac{\pi PR^3}{2EI} + \frac{\pi PL^2R}{EI}$$
$$= \frac{P(4L^3 + 6\pi RL^2 + 3\pi R^3)}{6EI}$$

六、

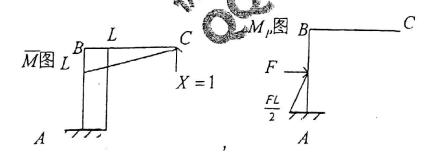


己知结构和受力情况如图频示

求: (1) A、B 处的反对

- (2) 刚性杆的最大弯矩
- (3) D 处的水平位移

解: (1)、用单位力法、解除 C 处多余约束,代之以未知反力 X,令 X=1,做弯矩图和实际受力图:



则 
$$\delta_{11} = \frac{1}{EI} \left( \frac{1}{2} L^2 \times \frac{2}{3} L + L^3 \right) = \frac{4L^3}{3EI}$$

$$\Delta_{1P} = -\frac{1}{EI} \left( \frac{1}{2} \times \frac{1}{2} L \times \frac{1}{2} FL \times L \right) = \frac{FL^3}{8EI}$$

所以, 
$$X = -\frac{\Delta_{1P}}{\delta_{11}} = \frac{3}{32}F$$

所以
$$F_{Cy} = \frac{3}{32}F(\uparrow)$$
,  $F_{Ay} = \frac{3}{32}F(\downarrow)$ ,  $F_{Ax} = F(\leftarrow)$ ,

$$M_{A} = -\frac{1}{2}FL + L \times \frac{3}{32}F = -\frac{13}{32}FL($$
逆时针 $)$ 

(2)、
$$M_{\text{max}} = M_A == \frac{13}{32} FL(逆时针)$$

(3)、CB 段: 
$$M(x) = \frac{3}{32}Fx$$
,  $0 \le x \le L$ 

BD 段: 
$$M(x) = \frac{3}{32} FL$$
,  $0 \le x \le \frac{L}{2}$ 

DA 段: 
$$M(x) = \frac{3}{32}FL + Fx$$
,  $0 \le x \le \frac{L}{2}$ 

所以
$$\Delta_{Dx} = \int_{0}^{L} \frac{F\left(\frac{13}{32}x\right)^{2}}{EI} dx + \int_{0}^{L} \frac{F\left(\frac{13}{32}L\right)^{2}}{EI} dx + \int_{0}^{L} \frac{F\left(\frac{13}{32}L + X\right)^{2}}{EI} dx = \frac{23FL^{3}}{768EI}$$