MIL-G-5514F 15 JANUARY 1969 Superseding MIL-P-5514E 14 October 1963

MILITARY SPECIFICATION

GLAND DESIGN; PACKINGS, HYDRAULIC, GENERAL REQUIREMENTS FOR

This specification is mandatory for use by all Departments and Agencies of the Department of Defense.

1. SCOPE

- 1.1 Scope. This specification covers basic design criteria recommendations for use and application in packings, gaskets, packing and gasket glands (see 4.2), and related features for use in hydraulic equipment utilized in systems designed in accordance with MIL-H-5440.
- 1.2 <u>Classification</u>.- Hydraulic system packings and gaskets shall be of the following types and classes:

Types Temperature range
Type I -65° to +160° F
Type II -65° to +275° F
Type III -65° to +450° F

Classes
Class 1, 1,500 psi - Where the unit operating pressure at the packing

is a normal 1,500 pounds per square inch (psi).
Class 2, 3,000 psi - Where the unit operating pressure at the packing is a normal 3,000 psi.

2. APPLICABLE DOGUMENTS

2.1 The following documents, of the issue in effect on date of invitation for bids or request for proposal, form a part of this specification to the extent specified herein:

* SPECIFICATIONS

Military

MIL-P-5510 Packing, Preformed Straight Thread Tube
Fitting Boss
MIL-P-5516 Packing Preformed, Petroleum Hydraulic Fluid
Resistant, 160° F

MIL-H-5606

MIL-P-25732

Hydraulic Fluid, Petroleum Base, Aircraft, Missile and Ordnance

Packing, Preformed, Petroleum Hydraulic Fluid Resistant, 275° F

FSC 1650

TANDARDS	
Military :	
MS27595	Retainer, Packing Backup, Continuous Ring, Tetrafluoroethylene
MS28772	Packing, D-Ring, Shock Strut
MS28773	Retainer, Packing Backup, Tetrafluoroethylene, Straight Thread Tube Fitting Boss
MS28774	Retainer, Packing Backup, Single Turn, Tetrafluoroethylene
MS28775	Packing, Preformed, Hydraulic, +275° F (O-Ring)
MS28778	Packing, Preformed, Straight Thread Tube Fitting Boss
MS28782	Retainer, Packing, Back-Up, Teflon
MS28783	Ring, Gasket, Back-up, Teflon
MS33514	Fitting End, Standard Dimensions for Flareless Tube Connection and Gasket Seal
MS33515	Fitting End, Standard Dimensions for Bulkhead Flareless Tube Connections
MS33566	Fittings, Installation of Flareless Tube, Straight- Threaded Connectors
MS33656	Fitting End, Standard Dimensions for Flared Tube Connection and Gasket Seal
MS33649	Bosses, Fluid Connection - Internal Straight Thread
MS33657	Fitting End, Standard Dimensions for Bulkhead Flared Tube Connections
AN6227	Packing, O-Ring Hydraulic
AN6230	Gasket, O-Ring Hydraulic
AND10064	Fittings, Installation of Flared Tube, Straight Threaded Connectors

(Copies of specifications, standards, drawings, and publications required by suppliers in connection with specific procurement functions should be obtained from the procuring activity or as directed by the contracting officer.)

2.2 Other publications. The following document forms a part of this specification to the extent specified herein. Unless otherwise indicated, the issue in effect on date of invitation for bids or request for proposal, shall apply.

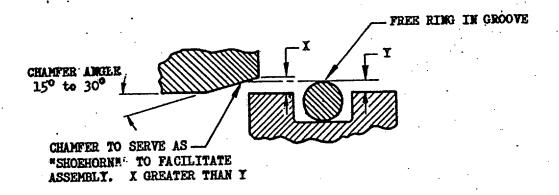
United States of America Standards Institute

USASI B46.1 - 1962 Surface Texture (Surface Roughness, Waviness, and Lay)

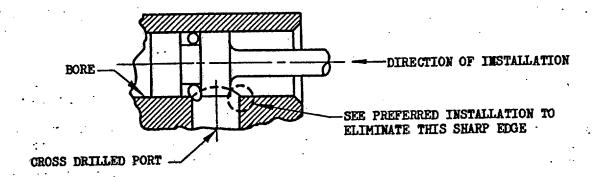
(Application for copies should be addressed to the United States of America Standards Institute, 10 East 40th Street, New York, New York 10017.)

3. REQUIREMENTS

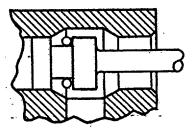
- 3.1 General design requirements for hydraulic units.-
- 3.1.1 Installation of packings.— Mechanisms shall be so designed that no damage to the packings would be incurred on installation by passing the packings over threads or other sharp corners. The diameters or threads over which, or through which, packings confined in glands must be inserted at installation, shall be of such size that there will be a diametrical clearance between the packings and the thread at the most unfavorable extreme tolerances. Chamfered edge annular undercuts shall be used at all cross-holes; in addition, chamfers shall be used at the ends of bores with sloped areas clear of intersecting holes. This is required because where a packing under squeeze (see 4.2) crosses even a round edge cross-hole, it may be partially severed as a result of localized protrusion. Typical methods of undercutting and chamfering, as well as illustration of pinched packings, which are to be avoided, are shown in figure 1.
- 3.1.2 Operation over unrestrained areas. Mechanisms which require that the packing pass over holes, ports, step diameters, etc., which would leave the ID, OD, or sides of the seal (see 4.2) unrestrained during its normal operation, shall be avoided. If, however, it is necessary to deviate from the above, qualification tests satisfactory to the Services must be performed to substantiate the design. In such tests, consideration shall be given to: (a) Use of the appropriate highest swell-approved packings, (b) aging in the appropriate highest swell-approved fluid, (c) adverse maximum packing squeeze if such test conditions are warranted by analysis of the particular design. The Services will designate the applicable high-swell packing and fluid upon request.
- 3.1.2.1 Dynamic seal (see 4.2) travel. A running seal gland shall be so located in a component that the leading edge of the groove or gland, at its position of extreme travel or adjustment, including adverse tolerances, shall remain sufficiently distant from the nearest edge of any chamfer, undercut, or other departure from the bore, or equivalent diameter, that there can be no extrusion, cutting, or other damage to the seal throughout the operating pressure and temperature ranges. In general, the same practice applies to static seals (see 4.2).
- 3.1.3 Gland materials. Materials used in the manufacture of packing glands shall be in accordance with the requirements of the detail specification. All material used in packing glands shall satisfactorily resist corrosion during its normal service life.
- 3.1.4 O-ring packing gland dimensions.— O-ring packing glands, both nominal and otherwise, should be made to the recommended requirements indicated herein. A nominal O-ring installation shall be considered one that uses a cylinder bore or piston rod having the equivalent dimensions (see figure 2) and corresponding to the O-rings as listed in table I herein. Nominal glands shall be used wherever possible.



BEVEL ON PACKING INSTALLATION

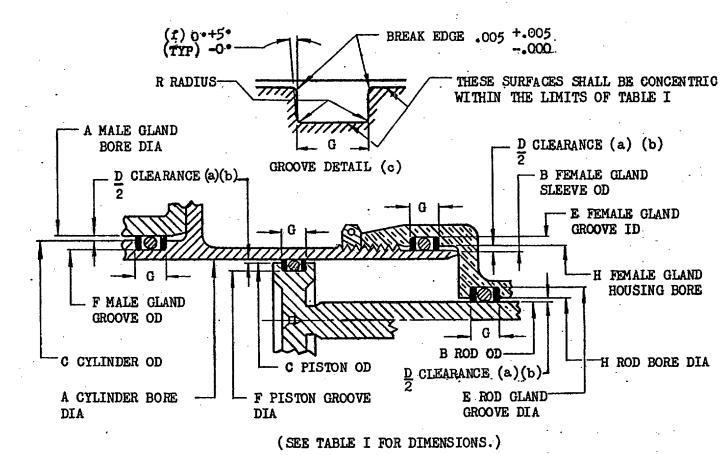


PREFERRED INSTALLATION



UNDERCUT BORE AS INDICATED

FIGURE 1. Methods to avoid sharp installation corners



- (a) DIAMETRICAL CLEARANCE IS THE TOTAL DIFFERENCE BETWEEN THE BORE ID AND THE MEMBER CONTAINED THEREIN.
- (b) SEE 3.5.4 IF USING STATIC O-RING SEALS.
- (c) TOTAL INDICATOR READING, BETWEEN GROOVE AND ADJACENT BEARING SURFACE. SEE GROOVE DETAIL.
- (d) ONE OR TWO NONEXTRUSION RINGS SHALL BE USED IN ACCORDANCE WITH 3.4.3.
- (e) CAUTION SHOULD BE OBSERVED TO INSURE THAT THE RADIUS USED AT THE BOTTOM OF THE GLAND DOES NOT RESULT IN NOTCH SENSITIVITY OF THE GLAND DESIGN OR CREATE AN INSTALLATION PROBLEM.
- (f) FOR THE GROOVE ANGLE, BETTER PERFORMANCE IS OBTAINED AT THE O DEGREE ANGLE.
- (g) EITHER THE GROOVE DIAMETER DIMENSION OR THE OPPOSING SEALING SURFACE DIMENSION MAY BE HELD WITHIN CLOSER LIMITS THAN THOSE SPECIFIED TO GAIN ADDITIONAL MACHINING TOLERANCE ON ITS OPPOSING DIMENSION, PROVIDED THE ACCUMULATED TOLERANCE OF THE TWO DIMENSIONS DOES NOT EXCEED THAT SPECIFIED. EXAMPLE: FOR AN MS28775-221 O-RING

"A" DIAMETER MAY BE HELD TO 1.678/1.679
IN LIEU OF 1.678/1.680 TO GAIN AN "F" DIAMETER
DIMENSION OF 1.435/1.432 IN LIEU OF 1.435/1.433.

TABLE I O-RING CLAND DIMENSIONS SEAL INSTALLATION DIMENSIONS GROOVE WIDTH G HUNTMAN MAXIMUM 3 DIANTRAL DYAMETER ANS 30 DUSH NO. LH6227 DASH NO. CILINDER BORE OR MILE OLAND CYLINDER BORN 1 ORCOVE CORNER RADIUS SECTION OR CTLINDSK (TAXES CLAND SCREWE MAD BOAK OR FRAIK SIAND HOUSING BORK NEED 2775 DLSH SCHOOL STATE A 8 ECCENTRICITY (0) 1045108 1,0000 CHOSS (FEE) ğ BLCKUP BACKUP NO BACKUP "D". PERCENT PERCENT PISTOR OFFING ACTUAL 0-1230 8 Ö EXT. INT .093 .033 .033 .063 .076 .035 .035 .015 .005 001 .ool .00 .005 13. .012 .002 .040 ±.003 .029 ±.004 .050 .051 .126 .048 ,047 .048 .128 .129 ,128 002 .050 ±.003 .04.2 .129 .065 .157 .156 .063 .159 .160 .159 .160 14.d 015 003 .060 ±.003 .056 .188 .187 .190 .191 .076 .076 .190 .191 .094 .104 .078 .079 13.4016 21.9 .207 .217 004 .009 .070 ±.003 .070 .108 .010 .219 .218 .108 .107 .221 .221 .222 005 .101 <u>+</u>.004 .235 .236 .123 .235 .236 .233 .232 .123 .122 .125 900 .017 À .114 <u>+</u>.005 .264 .263 .266 .267 .154 .153 .154 .156 .157 .266 .267 007 .187 .188 .297 .298 .295 .294 .298 .298 .185 .185 .184 008 .176 .217 .216 .217 .219 .220 -327 -326 .329 .330 -329 -330 20A .358 .357 .360 .361 .248 .248 .247 .250 .253 .360 .361 .239 010 .420 .419 .310 .309 .310 .309 .)12 .422 .423 .422 011 .483 .482 .485 .486 .373 -372 .373 .372 .375 .376 .485 .486 .149 .159 .207 .217 012 ,364 ±.005 .005 .070 ±.003 .002 .548 .547 .550 .552 .438 .436 .435 .433 .437 .438 .547 .549 015 005 .094 104 .149 .159 .207 .217 .070 ±.003 .426 ±.005 013 .005 .005 .009 .01/23.3 13.4 .612 .613 .615 .675 .501 .563 .561 .498 .496 .560 .558 .500 .562 .563 .610 .612 .672 .674 .489 014 .673 .672 015 .551 .626 .624 .623 .621 .736 .735 .738 .740 .625 .626 .735 .737 016 .614 .798 .797 .800 .688 .686 .685 .683 .687 .688 .797 .799 .676 017 .863 .865 .748 .746 .861 .860 .751 .750 .751 .860 .862 018 .739 ±.005 FATTO APPLICATIONS ONLY .749 .923 .922 .925 .927 .813 .811 .810 .808 019 .812 .813 .922 .924 801 ±.006 .991 .993 .879 .877 .873 .871 .875 .876 .985 .987 020 .864 1.051 1:050 .937 .938 1.053 1,055 .939 •935 •933 1.047 021 .926 1.114 1.113 1.116 1.118 1.000 1.001 1.110 1.004 1.002 .998 .996 022 1.176 1.175 1.178 1.064 1.060 .062 .063 023 1.051 1.174 1.239 1.238 .241 .243 .129 1.123 .125 1.235 1.237 1.114 1.301 1.300 .303 .305 .191 .189 1.185 1.183 .187 .188 1.297 1.299 025 1.176 1.364 1.363 .366 .368 1.248 1,246 .250 .251 1.360 1.362 **026** 1.239 1.426 1.425 1.428 1.430 .316 .314 11310 1.308 1312 1.313 1,422 1,424 027 1-,301 1.489 1.488 1.491 1.493 •379 •377 .373 .371 1.485 1.487 .375 .376 .149 .159 .207 .015 .005 028 <u>070 ±.003</u> 2.364 ±.006 23. .551 .548 .547 .550 .372 .370 .373 .371 .375 .376 .005 .017 16.0 .141 .151 .183 .193 .009 .015 9.0 .002 .103 ±.003 110 .362 ±.005 .610 .613 .615 .435 .433 .435 .433 .437 .00 .613 .615 n .424 .673 .672 .675 .677 -497 -495 .676 .678 .498 .496 .500 .501 112 .487 .562 .563 .736 .735 .738 .740 .560 .558 .560 .558 .738 .740 113 .549 .800 .802 .622 .623 .621 .625 .626 .798 .797 .801 .803 .612 114 .861 .860 .863 .865 .685 .683 .685 .683 .687 .688 .863 .865 115 £674 .923 .922 .925 .927 .747 .745 .748 .746 .750 .751 .926 .928 116 .245 -015 .005 .009 .989 .980 .991 .993 ,813 ,811 .810 .808 .812 .813 .988 .990 017 16.0 141 151 9.0 ,245 ,255 .015 ,005 .002 .103 ±.003 .799 <u>+</u>.006 117 1.051 1.050 1.053 1.055 .875 .873 .873 .871 .875 .876 1.051 1,053 118 .862 STATIC APPLICATIONS .935 .933 1.114 .116 .938 .936 •937 •938 .113 119 .924 1.176 1.175 1.178 1.180 .998 .998 .996 .176 120 1.000 1997 .178 1.239 .241 ,243 1.063 1.062 1.063 .238 .240 .301 1.060 121 1.049 1.058 .301 1.300 1.303 1.125 1:123 6.设 .005 .005 .009 .017 .002 .103 ±.003 1.112 ±.006

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TARLE I. (Continued) O-RING GLAND IMMENSIONS CROOVE MIDTH C. SPAIL ENSINIZATION MINIMUM MAXIMUM INTERNA! 3 DILLOGIER DIAMETRAL CLEARANCE 8 O SECTION AMÉZZO DASH NO. SLEIVE PISTON OR CILINDER 3 NS28775 DLSK RINGS DISTOR 8 S ORDOVE CORDER CROSS (FE) 1 OR HEAND * 25 TVOCKO OROOVE. BACKUP . NO BLCCOP ROUBING I PERCENT OF ELECT PERCENT OCTA-O "D" MAX. ACTUAL ACTUAL • £ S H ğ EXT. INT, .103 ±.003 1.174 ±.006 .141 .151 .245 .015 .003 1.363 1.365 1.426 1.428 017 .183 1.366 1.368 1.188 1.186 .005 .005 .009 .9.0 16.0 1.364 1.187 1.188 123 1,183 1.237 1.250 1.251 1.426 1.428 1.250 1,248 124 1.299 1.488 1.310 1.312 1.491 1.313 1.489 125 1.313 1.362 1.373 1.375 1.376 1.55Ì 1.553 1.375 1.553 1.555 1.551 .00; 126 1.424 1.437 1.613 1.615 1.616 1.618 1.438 1.435 ,008 1.614 1.613 127 1.487 ±.006 1.500 1.498 1.500 1.502 1.676 1.678 1.680 1.498 1.676 128 1.678 1.549 ±.010 1.562 1.564 .739 .738 1.741 1.563 1.561 1.560 1.738 1.740 005 129 1.625 1.801 1,623 1,621 1.802 1.605 1.627 1.612 130 1.674 1.864 1.863 1.689 1.687 1.685 1.683 1.687 1.863 1.865 1.867 131 1.737 1.748 1.750 1.752 1.752 1.750 1.926 1.927 1.926 1.930 1.932 006 132 1.928 1.992 1.994 1.614 1.612 1.810 1.608 1.813 1.815 1,988 1.990 .007 .989 .988 1.799 133 1.876 1.878 1.862 1.677 1.875 2.051 2.053 2.052 2.051 2.055 1.873 1.871 134 2.115 2.114 2.118 2.120 1.940 1.938 1.936 1.934 1.939 2.114 2.116 1.925 135 2.177 2.176 2.180 2.182 2,002 2,000 1,998 1,996 2.001 2.003 2.176 2.178 1.987 136 2.065 2.063 2.061 2.059 2.064 2.066 .239 2.050 2.240 2.239 2.243 2.245 137 2.126 2.128 2,301 2,303 2.112 2.127 2.125 2.123 2.121 2.302 2.301 2.305 2.307 138 2.368 2.370 2.186 2.184 2.189 2.191 .364 .366 2.175 2.190 2.188 2,365 2,364 139 2.126 2.128 2.251 2.253 2,248 2,246 2.237 2.427 2.426 2.430 2.252 2.250 2.489 2.491 2.315 2.313 2.311 2.309 2,314 2,316 007 2.490 2.488 2.493 2.495 2.300 2.376 2.378 .551 .553 2.362 2.555 2.557 2.377 2.375 2.373 2.371 2.552 2.550 2.440 2.438 2.436 2.434 2.439 2.441 .614 .616 2.618 2,620 2,615 2,613 2.425 . 501 . 503 2_187 2.680 2.682 2.502 2.500 2.498 2.496 2.677 .678 2.675 . 564 . 566 2.550 2.740 2.738 2.743 2.745 2.565 2.563 2.561 2.559 .739 .741 2.627 2.625 2.623 2.621 2.626 2.628 .BO1 2.612 ±.010 2.805 2.807 2,802 2,800 2.675 ±.015 2.865 2.863 2.868 2.870 2,690 2.688 2.686 2.684 2.689 2.691 .864 .866 2.752 2.750 2.748 2.746 2.751 2.753 .926 .928 2.9<u>27</u> 2.925 2,930 2,932 148 .005 .017 16.0 .141 .151 .183 .193 .215 .990 .888 2.993 2.995 2,815 2,813 2.811 2.609 2.814 2.816 .989 .991 .007 .009 2.800 ±.015 103 ±.003 .002 .750 .751 :734 ±.006 .991 .993 .003 .139 ±.004 .991 .993 .748 .746 .989 .988 <u>015</u> 0215 15 :233 005 :31 :025 .796 .053 .810 808. .810 .808 .812 .813 .051 1.053 1.055 .050 .859 .116 .875 .876 1.114 1.116 .873 .873 ,871 .118 .921 .935 .933 .178 .180 .937 .938 18 1.175 .984 1.241 1.243 .998 .996 .000 :241 1.239 .998 .996 1.001 .243 1.046 1.060 1.058 1.060 1.058 .303 .305 .301 1.303 1.305 1,062 1,063 20 1.109 .364 1.366 1.368 1.123 .125 ,366 ,368 .121 1.171 1.187 1.188 .428 1.428 1.430 .185 .183 .425 .183 1.250 1.251 .491 .493 1.489 1.488 1.491 .248 .246 1.248 1.234 .310 .308 1.310 1.308 .312 .313 .553 .555 1.296 .551 .550 1.553 219 1.359 1.373 1.371 .375 .376 .616 .618 1.614 1.613 1.616 1.373 1.371 1.421 1.676 1<u>.675</u> 1.678 1.692 1.435 1.433 1.435 1.433 1.437 .678 .139 ±.004 1.484.±.006 ,005 .005 .COQ\$ 8.5 150 268 .235 .215 .025 .003 1:498 1.739 1.741 1:498 1:58 :743

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		22	244	4.489	4.493	4.250	4.247	4.250	4.490	.000	11			11								4.234
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ŀ	30	L	327	2.115	2,118	1.746	1.748	1.750	2:120 2,122		8	4	+ -	$\dagger \dagger$	+	$\dagger \dagger$	-	 	╁┤╌		+ - -	1.725
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ł	32	-	329	2.365	2.368 2.370 2.493	1.996 1.994 2.121	1.998 1.996 2.123	2.001	2.370 2.372 2.495	1.00	11	$\ \ $	\parallel									1.975
ł	33	-	330	2.490	2.495	2.119	2.121	2,128	2.497	- ·		$\ \cdot\ $										2,225
ı	34	L	331	2.615 2.613 2.740	2.620	2.246	2.248 2.246 2.373	2.251 2.253 2.376	2.622	J 1								.				
J	35 36	-	332	2.738	2,745	2,369	2.371	2.378	2.747	J I].].		$\ .$		$\ $			↓				2.950
		-)))	2.865 2.863 2.990	2,870	2.494	2.496	2.503	2.872	41		$\ \ $				$\ \ $.		1		2.475 2.600 ±.010
- 1	37	\vdash	324	2,988	2.995 3.118	2.619	2.621	2.628	2.997 3.120	41		$\left\ \cdot \right\ $		$\ \ $		11						2.725 ±.015
- 1	38 39	+	335 336	3.240	3.120	2,744	2.746	2,753 2,876 2,878	3.122	-			. 1			$\ \ $				$ \cdot $	1. 1:	2.850
	40	╁	937	3.238	3.245	2.869	2.871	3.000	3.247	\mathbb{H}		.01	78. 78.					-				2.975
	41	t	338	B.363	3.493	3.121	3.122	3.125	3.371	71			11	$\ \ $								3.100
- 1	42	t	339	3.615 3.613	3.618 3.620	3.246 3.244	3.120 3.247 3.245	3.250 3.252	3.619 3.621	71		$\ $.	3.225
	43	T	340	3.740	3.743	3.371	3.372		3.744	71			\parallel	$\ \cdot\ $								3.350
	44	Γ	941	3.863	3.868	3.496	3.497	3.500	3.869	٦'		, ' , 'o. 'k	17 B.	ا 1.0	9 13.	5 .29	12.33 14. E	.424	103		.210 ±.005	3.475 ±.015
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		Γ					1	T		T	Τ	1	7	T	T	T		1	1	T		T

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	۱			XTERNAL L. O.		8	HERNAL		4	3	- Rui	T T	1		1,	Je	<u>a</u> _	100	\ <u>a</u>	8			78		2
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F			3.990	3.993	3.621	3.622 3.620	3.625 3.627	3.994 3.996	.007	.001	.01	1 8.1	202	9 13	.5 .2	劉	:数		121. 131.	.035 .030	.002		210 ±.	005	3.600 ±.015
4.5	-	34.2	3.988	3.995 4.118	3.619	3.747	3.750 3.752	4.119 4.121	1	1	1	1	1			Ï	T	'	۲					. [3.725
166	Н	343_	4.240 4.238	4.120	3.744 3.871 3.869	3.745 3.872 3.870	3.875	4.244 4.246			П												.		3.850
147	Н	345	4.365	4.368	3.996	3.997	4.000	4.369	.007		П					$\ $							ŀ		3.975
48		346	4.489	4.493	4.121	4.122	4.125	4.494	.008		11					П						۱	.		5.100
Γ		•	4.614	4.618	4.246	4.247	4.250 4.252	4.619	11	$\ \ $						$\ $			1				ļ		4.225
50	\vdash	247	4.739	4.743	4.371	4.372	4.375	4.744	11		П			1		H					1	1	ł		4.350
1	Г	340	4.737	4.868	4.496	4.494	4.500	4.869 4.871	008	007	.01	7 8.	1 .0:	9 12	.5	201 291	.334	Ŀ	134 134		.00	<u>. </u> .	210 ±	005	4.475
52	二	349	4.970	4.974	4.497	4.497	4.501	1.971	.009	÷00	9 -02	7 10	2 .0	25 1.		375 385		-	579 589	-		1	275.‡,	006_	1.175
138	Τ	426	5.095 5.093		4.622	4.622	4.626	5.099 5.102	1. 1	11	Н			Н	Π		1		1				1		4.600
51	1	427	5.220 5.218	5.224 5.227	4.747	4.747	4.751	5.224 5.227							Ш			1				۱			4.725
24	T	428	5.345 5.343			4.872	4.876	5.349 5.352	11				11		$\ \ $	١				11		1			4.850
55	十	1	5.470		4.997	4.997	5.001	5.474	11		I				П		1	İ	1			1			4.975 ±.015
56 57	t	430	5.595	5.599	5.122	5.122 5.119	5.126 5.128	5.599	11		1	11	11		Ш					11					5.100 ±.023
58	T	431	5.720 5.718		5.247	5.247	5.251 5.253	5.72L 5.727	11		ļ				$\ $			1	1	1		1	•		5.225
	十	432	5.845 5.843	5.849	5.372	5.372	5.376 5.378	5.849 5.852	11				11		$\ $				1						5.350
· 80	╁	433	5.970	5.974	5.497	5.497		5.974	11	1.	۱]].		Ш	١			.	1.				أمعت أ	5.475
61		434	6.09	6.099	5.622		5.626	6.102] [Ш	$\ \ $		١						1			5,600
62	1	435	6.22	6,22	5.747	5.747	5.751	6.224	71			Ш	П	П	\prod	١	\ [l	5.725
63	Т	A36	6.34	6.349		5.672	5.876	6.349] [1		П	41	\cdot					1			Ì	5.850
64		437	6.46	6.47E	5.99	5.997	5.501	6.474				$\ \ $		H	$\parallel \parallel$										5.975
6:	Т	438	6.72	0 6.72 8 6.72	6.247	6,247	6.251]]		109	Ш				۱		ŀ							6.225
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6	1	440	7.22					7.221]			$\ \cdot \ $	П	$\ \ $	$\parallel \parallel$			١	1		-			1	6.725
6	T	441	7.47	0 7.47	4 6.99	6.99	7.001	7.474	71			$\ $	Ш	\mathbb{H}				1						1	6.975 ±.023
6	Т	442	7.72	0 7.72	4 7.24	7 7.24	7 7.251	7.724	7			\prod	П		Ш				1		1			·	7.225 ±.030
7	╗	443	7.97	0 7.97	4 7-49		7. 7.501	7.974				$\ \cdot \ $	11						Ì						7.475
į,	Т	444	£.22	0 8.22		7 7.74	7 -75	8,224]_	.	$ \cdot $	-	11	- -	4								<u>.</u>		7.725
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,	7	446	8.97	0 8.97	4 8.49	7 8.49			:	10		225	0.2			Н									8:475
	П	447	9.47	0 9.47	4 8.99	7 8.99	7 9.00	9.474		11		027	9.9			$\ \ $								1	8.975
- [5	44	9.9	70 9.9		7 9.49	7 9.50	1 9.974					11							1				1	9.475
Γ	6	44	10.4	70 10.4° 67 10.4°	4 9.9	7 9.99		01 10.47 04 10.47		\prod	$\ \ $									1			1		9.975
- [7	45	18.9	70 10.97 67 10.9				01 10.97 C4 10.97				$\ \ $				$\ \ $								f	10.475
- 1	18	45	11.4	70 11.4°	74 10.5	97 10.9	97 LL.0	01 11.47 04 11.47	/4	$\ \ $						Ш									10.975
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	30	45	12.4	70 12.4 67 12.4	74 11.4	97 11.9	97 12.0	01 12.4° 04 12.4°	74		$\ \ $														11.975
1	,,	45	12,9	70 12.9	74 12.1 78 12.1	97 12.1	.97 12.5 .94 12.5	01 12.9 04 12.9	74.			'												1	12.475
Ī	32	45	13.4	70 13.4 67 13.4	74 12. 78 12.	997 12. 994 12.	997 13.0 994 13.0	01 13.4° 04 13.4°	74	$\ $						П							Ì	1	12.975
	33	45	6 13.9	70 13.9 67 13.9	78 13.	94 13.4	194 12.5	01 13.9 04 13.9	78										1						13.475
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	87	44		970 L5.9 967 L5.9	7/4 15. 7/8 15.	497 15. 494 15.	497 15. 494 15.	501 15.9 504 15.9	78	on.	010	.027	9.9	D4,25	15.	زار	?5 .4 85 .4	75 85	•579 •589		035 220	(e)	.27	±.006	15.475 ±.030

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TABLE I (Continued)

NOTE: Caution should be used in applying the -OO1 through -OO5 sizes. While being installed in an external groove, they might be stretched beyond the elastic limit, with probable failures or incipient failures resulting. Moreover, there is no standard backup ring for -OO1 through -OO3; therefore, for pressures in excess of 1500 PSI the diametral clearance (extrusion gap) must be reduced.

It is recommended that wherever possible, 0-mings with a larger cross sectional diameter ("W" dimension) be used in preference to -020 through -028 and -131 through -149, so as to provide a more adequate seal. Therefore, these sizes are not preferred.

- 3.1.4.1 Nominal sized installations.— Dimensions, tolerances, and allowable eccentricities for piston rods, cylinder bores, and rod and head gland groove diameters, lengths and shapes, and allowable diametrical clearances for nominal O-ring installations shall be carefully selected and closely controlled in order to provide for required service life, prevention of extrusion, minimum leakage, and freedom from binding throughout the required range of operating temperatures and pressures. For glands to seal up to and including 2,500 psi pressure, the data given in table I of this specification, under the columntitled "No backup rings," are suitable for type I systems. For glands to seal up to and including 3,000 psi pressure, the data given in table I of this specification under the columns titled "One backup ring" and "Two backup rings" are suitable for type I and type II systems.
- 3.1.4.2 Other than nominal sized installations.- Glands of sizes other than nominal will be referred to as nonstandard herein. The use of nonstandard gland cylinder bores, piston rods, etc., shall be held to a minimum consistent with the design performance and weight considerations of the component. When a nonstandard bore or rod is used, the closest standard packing dash number shall be selected as determined from the nominal packing size as listed in table I. The selection of packing size in a nonstandard gland shall be based primarily on the consideration of performance. The nonstandard groove diameter and dimensions pertaining thereto should be calculated in the same manner as for standard nominal glands by the formulas of table I. However, where O-rings are stretched, consideration should be given to low-temperature leakage, since the stretch and shrinkage combine in reducing the O-ring's cross-sectional area. In addition, when using nonstandard gland dimensions, great care in the selection of a nonextrusion device must be taken. For example, MS28782 rings cannot be used indiscriminately on nonstandard gland dimensions.
- 3.1.5 Qualification of special packing glands.— When packing gland designs differ from the recommended design practices as given in this section, or design conditions in the component dictate, the particular gland shall be qualified by tests suitable to the prozuring activity. The Services will base their requirements for such tests on past Service experience and laboratory tests, and may require the use of particular makes of approved packings, gaskets, and fluids in the qualification tests.
- 3.1.5.1 Service experience has shown that low squeeze 0-ring installations designed to provide reduced 0-ring friction are unsatisfactory, although the low squeeze installation may have passed qualification tests. For this reason, a design 0-ring squeeze that is less than the minimum value specified in table I shall be tested to adverse tolerances. This shall be accomplished by the use of MIL-H-5606 low swell fluid specified by the Services and machining the 0-ring gland to provide the low limit of design 0-ring squeeze.

3.2 Standard packings .-

- 3.2.1 Type I systems. All packings used in hydraulic equipment for type I systems, designed in accordance with this specification, shall be standard-approved packings conforming to MIL-P-5516, AN6227, AN6230, and MS28772.
- 3.2.2 Type II systems. All O-ring packings used in hydraulic equipment for type II systems, designed in accordance with this specification, shall be standard-approved packings conforming to MIL-P-25732 and MS28775.
- 3.2.3 Type III systems. Since there are no standard packings presently available for use in type III hydraulic system equipment, any packing installation selected for this temperature range shall be qualified in the component and subsequently approved by the procuring activity based on the component qualification test.
- 3.2.4 <u>Use of O-ring packings.</u>— O-ring packings are intended for use as static or running seals in hydraulic system components. If used as running seals without nonextrusion devices, the O-ring seals shall be used only at operating pressures not greater than 1,500 psi in types I, II, and III systems, unless the extrusion gap is maintained small enough to prevent extrusion of the O-ring for the life of the component at the highest pressure. Usage with nonextrusion devices is specified in 3.4. O-ring packings may be used for static seals. Design and installation details for such use are specified in 3.5.
- 3.2.4.2 <u>Use of D-ring packings.</u>— D-ring packings are intended for use as rod seals only in landing gear shock struts. The D-ring packing is designed primarily for use in lieuof the O-ring packings in landing gear installations where spiral failure of the O-ring packing is a problem. It may be used without backup or with one or two backup rings (see 4.2), depending on the pressure, deflection, and other requirements of the specific utilization. For the diametrical dimensions of the installation of D-rings, the dimensions established in table I for O-rings are recommended. For groove width (dimensions "G"), the dimensions of table II are recommended. The MS28772 D-rings in their full range of sizes are equivalent in ID and OD dimensions to the MS28775 O-rings in sizes -335 through -460.
- * 3.2.5 <u>Surface finishes of glands.</u>— The following surface finishes shall be used in units containing 0-ring packings, unless performance or qualification tests indicate that other surface finishes are satisfactory. These finishes are indicated as surface roughness as defined in USASI B46.1 1962.

	Surface roughness
Part of Unit	height rating
Cylinder bor or piston rod (diameter over which packing must slide)	16 (max.)
O-ring groove diameter:	00 ()
Dynamic seals	32 (max.)
Static seals	63 (max.)
O-ring groove sides when no backup ring is used:	
Dynamic seals	32 (max.)
Static seals	63 (max.)
O-ring groove sides when backup rings are used	63 (max.)

The groove surfaces must be free from all machining irregularities exceeding the above values, scratches, etc. Groove edges shall be smooth and true and free of nicks, scratches, burrs, etc.

TABLE II. D-ring gland width dimensions

	Groo	Groove width "G" $\underline{1}/$							
Dash No.	No back-	One back-	Two back-						
	up ring	up ring	up rings						
-335 to -349	0.424	·0.507	0.597						
	.434	.517	.607						
-425 to -460	.579	.729	.854						
	.589	.739	.864						

1/ See (d) of figure 2.

3.2.6 O-ring groove shape. - Rectangular type groove shapes, following the general design criteria of table I, are preferred. The grooves may have up to 5 degrees slope on the sides to facilitate machining; the radius in the bottom corners of the groove must be a compromise between strength requirements, type of nonextrusion device, and adequate groove volume. When TFE (see 4.2) rings are used, the radius must be a minimum consistent with installation and performmance requirements. The width of the groove shall be consistent with the performance requirements of the gland and the type of nonextrusion device used. Consideration should be given to cross-sectional squeeze and volumetric swell of the O-ring owing to oil immersion and temperature. The recommended groove width dimensions are shown in table I. Narrower grooves make it more difficult to remove the O-ring for inspection and replacement and increase the possibility of nicking and scratching the edge of the groove during removal of the O-ring. The outer corner of the groove must be smooth with the corner broken slightly to prevent sharpness. Too large a corner radius will contribute toward local failure. This effect will be greater with increased operating pressures and temperatures.

3.2.7 Number of 0-rings per gland.— The use of two or more 0-rings in the same groove or in adjacent grooves can produce pressure traps between the adjacent 0-rings and a subsequent rise in temperature takes place causing thermal expansion of the fluid or lubricant. Such conditions have caused jamming of units in service. If the use of two or more 0-rings are required for some design reason, adequate provision, such as venting of the space between the 0-rings, must be made to prevent pressure trap.

3.2.8 Breathing .- The piston head gland of actuating cylinders and similar components in which the gland is confined by a lightweight cylindrical member, which breathes diametrically as pressure is applied, may have a total diametrical working clearance greater than that shown by the clearance columns of table I in type I systems. Experience with actuators up to 5-1/2 inch bore diameter has indicated that the diametrical breathing, owing to pressure application only, should not exceed approximately 0.0020 inch per inch of bore diameter at the midpoint of the cylinder barrel with the piston bottomed at one end of the cylinder. The breathing should actually be less than 0.0020 inch per inch of bore diameter in the transverse plane immediately adjacent to the normal actuating cylinder piston head seal, owing to decreasing cylinder material flexure at this point. Breathing will usually be less in smalldiameter low-pressure cylinders owing to manufacturing considerations. In large diameter cylinders, or units which have large values of diametrical breathing, tests will have to be made the satisfaction of the procuring activity to insure adequate life of the seal and gland.

3:3 Nonstandard hydraulic packings.-

3.3.1 Use of nonstandard hydraulic packings.-

- 3.3.1.1 Type I and type II systems.— When a satisfactory installation using standard packings is not possible owing to performance requirements, nonstandard packings such as TFE cap rings may be used, subject to approval by the procuring activity, and provided the unit satisfactorily completes qualification tests.
- 3.3.2 Design considerations.— On nonstandard packing and packing gland designs, consideration shall be given to the design application and the following point shall be noted: Surface finish, extreme temperature, sealing, low-pressure and high-pressure leakage, air inclusion as a result of servo operation without fluid pressure, etc.

3.4 Nonextrusion devices .-

3.4.1 Application of nonextrusion devices (backup rings).-

- 3.4.1.1 Type I and type II systems.— Where required, to permit a component to conform to performance or qualification tests, nonextrusion devices within the packing gland may be used. At lower pressures, nonextrusion devices will prolong the normal wearing life of the O-ring and, at higher pressures, nonextrusion devices permit greater diametrical clearances between mating parts. Unless otherwise approved by the procuring activity, the applicable standard packings and backup devices shall be used.
- 3.4.1.2 Type III systems. Packings and backup rings for use in type III systems shall be designed in such manner as to fulfill the performance and qualification test requirements of the individual hydraulic component.

- 3.4.2 Glands for packings and gaskets with nonextruion devices.— Glands for combination of packings with backup rings and for gaskets with backup rings shall be designed to the same considerations as for nominal rectangular grooves, but with the following additional considerations. The width of the groove is of great importance, since a groove which is too wide may permit the backup rings to roll and thus become ineffective as a nonextrusion device. Angles in excess of 5 degrees on the side of the groove may produce the same result. A groove which is too narrow may cause high friction and extreme difficulty on installation. The data shown in table I have been found to be acceptable and desirable. Glands for TFE nonextrusion devices must have corner radii consistent with the performance and cross-sectional requirements of the TFE backup rings; otherwise difficult installation and operation problems may result.
- 3.4.3 <u>Installation of nonextrusion rings.</u>— The use of two backup rings in each gland, one on either side of the O-ring seal, even though the pressure application is from one side only, is desired in all cases to facilitate standardization of groove dimensions and service procedures. Where it is self-evident, however, that pressure can be applied from one direction only, and space limitations to provide for two rings create a hardship, a single backup ring may be used; this ring to be placed on the side of the O-ring away from the pressure. When the pressure differential across a packing is unidirectional, only one backup ring need be installed. This backup ring shall be on the low-pressure side. The groove width dimensions shown in table I for one backup ring may be used, as applicable.
- * 3.4.3.1 Continuous turn TFE backup rings.— A continuous TFE ring may be used for new designs. Installation of the small sizes of this ring into the gland will probably require use of split— or multiple—piece adapters. Continuous turn backup rings shall be in accordance with the uncut sizes of MS28774. For Air Force use, continuous turn backup rings shall be in accordance with MS27595, or the uncut sizes of MS28774.
- 3.4.3.2 Spiral TFE backup rings.— Great care must be exercised in the installation of spiral TFE backup rings. If the groove radii are large for structural reasons, the spirals may be sheared upon installation. Therefore, it is important that when installing spiral TFE backup rings that the mating part be rotated in the proper direction, so that the spiral will tend to wrap itself deeper into the groove and will not be sheared off when the parts are assembled. Spiral TFE backup rings shall be in accordance with MS28782 and MS28783.
- 3.4.3.3 <u>Single-turn TFE backup rings</u>.— This ring may be used for new designs. It is the simplest to install and does not require any special installation procedures. Single turn backup rings shall be in accordance with MS28774.

3.5 Static seals.-

3.5.1 Type I and type II systems. All nonmoving packings (static seals) used for sealing of fluid pressures shall be standard-approved static seals. These static seals shall not be compressed into threads or against other irregular or rough surfaces which would cut or otherwise damage them. Recommended static seal glands are shown in table I. The groove fillet radius and the fatigue requirements should receive very careful consideration.

- 3.5.2 Type III systems. Static seals and backup rings for use in type III systems shall be designed in such manner as to fulfill the performance and qualification test requirements of the individual hydraulic component.
- 3.5.3 O-ring gasket seals. O-ring gaskets conforming to part nos. AN6230-1 through -25 and MS28775 -013 through -028, -117 through -149, and -223 through -247 are intended only for use as static (nonmoving) seals and shall not be used as dynamic (moving) seals. All the detail requirements specified for O-ring packings will apply to the use of O-ring static seals conforming to part nos. AN6230-1 through -25, and MS28775-223 through -247, except as noted in the following paragraphs.

3.5.4 Pressure limitations and use of O-ring static seals.-

- 3.5.4.1 Type I systems. Static seals conforming to AN6230 may be used at pressures up to and including 1,500 psi, provided the clearances, eccentricities, and other requirements of table I are not exceeded. Above 1,500 psi pressure, the AN6230 O-ring static seals and the sizes of AN6227 O-ring packings used as static seals, shall be used with the applicable backup rings in accordance with table I. If the diametrical clearance can be held to a maximum of 0.0025 inch under the worst condition of tolerances, eccentricities, breathing, etc., the backup rings need not be used. The use of AN6227 packings as static seals in lieu of AN6230 static seals is preferred in all sizes.
- 3.5.4.2 Type II systems. Static seals conforming to MS28775 should be used at pressures up to 3,000 psi with backup rings in accordance with table I and requirements herein on nonextrusion devices, unless it can be proven by qualification tests that glands will perform satisfactorily without nonextrusion backup rings. Leather backup rings shall not be used in type II systems.

3.5.5 Use of straight thread tube fitting boss gasket .-

- * 3.5.5.1 Type I systems. The gasket for type I systems is a 90 Shore Durometer O-ring gasket, defined by MS28778 and MIL-P-5510. This gasket is not suitable for interchangeable usage with MIL-P-5516 and MIL-P-25732 seals owing primarily to lack of flexibility at cold temperatures and lack of resilience. For this reason, the MS28778 gasket shall be used only in connection with straight thread tube fitting glands, such as in the boss conforming to MS33649, with end fittings in accordance with MS33656 and MS33657 assembled in accordance with AND10064; and MS33514 and MS33515 assembled in accordance with MS33566. This usage includes such other parts as end caps on check valves wherein the dimensions of the gland duplicate the tube fitting and boss drawings enumerated above. In certain fitting installations, as shown on AND20064, the MS28773 nonextrusion rings must be used with the MS28778 gasket.
- * 3.5.5.2 Type II systems. The requirements of type II systems are identical to type I systems.

3.5.5.3 Type III systems. Gaskets suitable for the temperature ranges of this system which satisfactorily pass the qualification test requirements of the fitting installation shall be used.

3.5.6 Static face seals.-

- 3.5.6.1 Type I systems.— The use of static face seals should be avoided wherever a breathing problem exists and a submerged radial squeeze seal design is feasible. Where static face seals are desired, gaskets conforming to AN6227 or AN6230, may be used. In such installations the depth of the groove shall be in accordance with table I.
- 3.5.6.1.1 Design details.— Metallic surfaces contacting the O-ring face seals shall have a surface finish no rougher than 32 microinches, in accordance with USASI B46.1 1962. The cap or coverplate must be as rigid as necessary to prevent excessive breathing which would introduce an extrusion gap at the joint. The important feature in face seal design is to provide squeeze on the groove section and prevent any possible radial movement of the O-ring uder pressure application. Provisions shall be made to insure that the O-ring cannot be displaced from its groove under any flow or pressure condition.
- 3.5.6.2 Type II and type III systems. Static face seals, suitable for the temperature ranges of these systems, shall satisfactorily pass the qualification test requirements of the installation to be used. Usage of MS28775 seals is recommended for type II systems.

3.6 Design data on use of dynamic and static seals.-

- 3.6.1 Design data. The design data contained in this section are intended to supply the designer with the basic fundamental reasons behind the requirements of this specification and the results which may be expected when there is deviation from those requirements. Typical installation of static seals is shown in figure 3.
- 3.6.2 O-ring squeeze. Referring to table I, the O-ring squeeze is represented by the difference between the free O-ring cross-section diameter and dimensions $\frac{A-F}{2}$ or $\frac{E-B}{2}$ (as applicable).
- 3.6.2.1 Type I systems.— In order to produce an acceptable product that will perform satisfactorily throughout its normal life, it is recommended that O-ring packing squeeze and dimensions listed in table I be used. The minimum squeeze and dimensions shown in table I are so established that with all tolerances, clearances, eccentricities, side loads, and linear contraction of the packing compound taken into consideration, there will still be a positive interference remaining on the O-ring section throughout the temperature range of this type system.

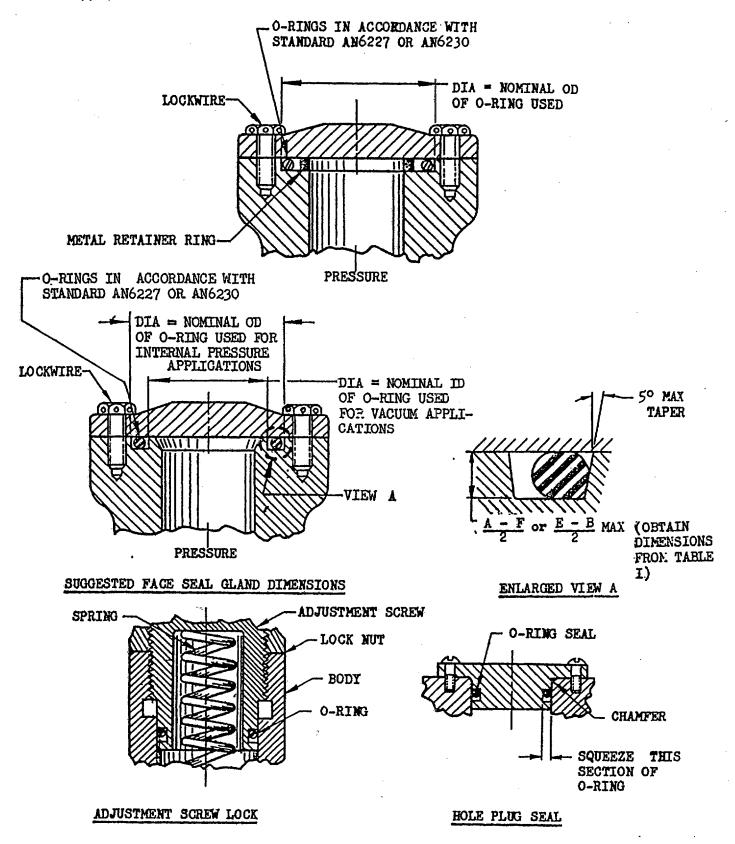


FIGURE 3. Typical installation of static seals

- 3.6.2.2 Type II systems. For these systems, it is recommended that the O-ring packing squeeze dimensions listed in table I be used. However, since insufficient test information is available as of the date of this revision, other squeeze dimensions may be desirable for particular applications.
- 3.6.2.3 Change of squeeze considerations.— The following items were considered in setting up the dimensions shown in table I for type I systems and must be given due consideration when deviations from these dimensions are made. For type II systems, these considerations may not be directly applicable.
- 3.6.2.3.1 Decrease squeeze.- Decreasing the squeeze will slightly reduce friction and breakout under low hydraulic pressure (under 500 psi) operating conditions. When reduced squeeze is used, a better surface finish is usually required for low-pressure sealing. The saving in friction will be neutralized at high pressures owing to compression of the 0-ring into the end of the groove. Figure 4 illustrates this condition as well as positions of packing in their grooves under various degrees of pressure. Breakout friction of 0-ring type packing will be higher than running friction, being dependent on factors of surface finish, time, pressure, squeeze, etc. Particular care must be taken to insure that low-pressure and low-temperature leakage is not encountered.
- 3.6.2.3.2 <u>Increase squeeze.</u>— Greater O-ring squeeze than specified in table I may result in greater assembly problems, requiring larger or flatter angle levels, or both, at shoulders, etc., (see figure 1). Increasing the squeeze will also tend to increase the scrubbing and rolling of the O-ring during operation which may in turn result in shorter packing life. The friction at low-operating pressure will be increased. The greater squeeze may, however, result in lowering the critical cold temperature of the unit from the standpoint of low-temperature leakage. When squeeze is increased beyond that shown in table I and backup rings are required, those listed in table I cannot be used owing to interference.
- 3.6.3 <u>Diametrical clearance.</u>— The greatest factor in reducing the life of O-ring packings is the extrusion of the O-ring into the clearance gap. The clearance consequently should be held as small as practicable with special attention given to factors such as thermal expansions, pressure expansions, side load, eccentricities, type of motion, and other basic considerations of surface finish, lubrication, and accuracy which affect O-ring life. Backup rings or nonextrusion devices permit the use of slightly larger gaps. Diametrical clearance is the total difference between the diameter of the bore and the diameter of the member contained therein.
- 3.6.4 General limitations of O-rings.— O-ring packings and gaskets have some general limitations which should be kept in mind when designing hydraulic units. Some of these limitations are as follows.

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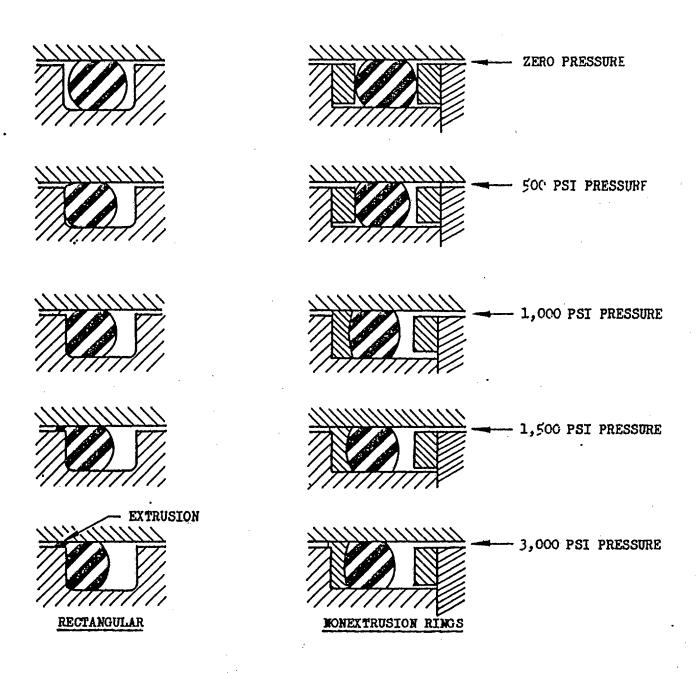


FIGURE 4. Relative positions of O-ring packings in different grooves at increasing pressures

- 3.6.4.1 Friction.- In some units, such as surface control boost cylinders, the breakout friction of O-rings can cause undesirable drag, which if not taken into consideration in the original design, may produce designs which are not suitable for the purpose intended. Breakout friction is caused by the extrusion of the packing material into the surface irregularities of the mating surfaces or adhesion, or both, of these materials (see 3.6.2). Breakout friction of O-rings is higher than running friction. All standard packings have some minimum friction value which cannot be materially reduced by practical methods of design. When friction problems are encountered, a special gland installation should be considered preferable to special packings (see 3.6).
- 3.6.4.2 Oscillation. O-ring packings, when used to seal rapidly oscillating mechanisms, have not always proven successful in past installations. Special studies must be made in designs of this type to provide for proper life and performance.
- 3.6.4.3 Rotary seals.— Standard packings are not specifically designed as rotary seals. However, where infrequent rotary motion or low peripheral velocity is required, they may be used, provided consistent surface finishes over the entire gland are used and eccentricities are accurately controlled. In addition, the use of low-friction nonextrusion devices have been found to be helpful in prolonging life and improving performance.
- 3.6.4.4 <u>Precaution.-</u> Glands in which the O-ring is seriously deformed or distorted by crushing or other loads (stretching and twisting) can induce permanent set and disintegration in the O-ring. Increased temperatures or strains, or both, induced in a seal will cause rapid deterioration of the seal owing to the strain aging and permanent set properties of seal compounds.

4. NOTES

- 4.1 Intended use. The procedures covered by this specification are intended to establish gland design and installation methods of packings and gaskets for use in hydraulic equipment design in accordance with MIL-H-5440.
 - 4.2 Definitions.- General terms used herein are defined as follows:
 - (a) Squeeze: The dimension by which a packing is distorted from its molded shape when installed in a packing gland.
 - (b) Seal: A device to retain fluid within a hydraulic component.

 The seal may consist of two or more components, such as a packing in a gland, and a packing and backup ring in a gland, etc.
 - (c) Packing: The component of a seal which serves as a sealing medium by nature of its plastic or elastic properties, or its ability to deform into the shape of the gland.
 - (d) Gland: The component of the seal which forms the cavity or inclusion which surrounds and supports the packing and controls the squeeze.

- (e) Gasket: A type of seal which if formed by crushing the packing material into the gland such that the cavity formed by the gland is normally filled with the packing material.
- (f) Dynamic seal: A type of seal where there is relative motion between some part of the gland and the packing, such as a piston or shaft seal.
- (g) Static seal: A type of seal where there is no relative motion between the packing and any part of the gland, although limited freedom may be provided to permit the packing to change its shape within the gland when under pressure.
- (h) Backup ring: A device used to prevent pressure and friction from extruding the O-ring packing through the clearance gap of a seal,
- (i) TFE: A tetrafluoroethylene resin.
- * 4.3 Marginal indicia.— The margins of this specification are marked to indicate where changes, deletions, or additions to the previous issue have been made. This is done as a convience only and the Government assumes no liability whatsoever for inaccuracies in these notations. Figures are not so marked. Bidders and contractors are cautioned to evaluate the requirements of this document based on the entire content as written, irrespective of the marginal notations and relationship to the last previous issue.

Custodians:

Army - AV

Navy - AS

Air Force - 11

* Reviewer activities:

Army - AV, MI, MR, WC

Navy - AS, SH

Air Force - 11, 71, 82

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