

## **Lecture 9:** Stochastic / Predictive Self-Tuning Regulators.

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- Minimum Variance Control.
- Moving Average Controller.

## The stochastic model

Assume the plant is represented by the special ARMAX model

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

where  $\{e(t)\}$  is white noise,

$$A(q) = q^n + a_1 q^{n-1} + \dots + a_n, \quad \deg\{A\} = n$$

$$B(q) = b_1 q^{n-d_0} + \dots + b_n, \quad \deg\{B\} = n - d_0$$

$$C(q) = q^n + c_1 q^{n-1} + \dots + c_n, \quad \deg\{C\} = n$$

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Equivalently,

$$\begin{aligned} y(t) = & -a_1 y(t-1) - \dots - a_n y(t-n) \\ & + b_{d_0} u(t-d_0) + \dots + b_n u(t-n) \\ & + e(t) + c_1 e(t-1) + \dots + c_n e(t-n) \end{aligned}$$

## Remarks on modeling noise.

Assuming that  $C$  is stable is not restrictive:

Typically, such a model is obtained experimentally from spectrum characteristics. It does not change if the unstable roots are substituted by stable, which are symmetrical to them with respect to the unite circle.

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$$y(t + 1) + a y(t) = b u(t) + c e(t)$$

It can be rewritten as

$$(q + a) y(t) = b u(t) + q e_{new}(t)$$

introducing  $e_{new}(t) = c e(t - 1)$ .

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It can be rewritten as

$$y(t+1) + a y(t) = b u(t) + e_{new}(t+1)$$

with  $e_{new}(t) = c e(t-1)$  being white noise with  $\text{var}\{e_{new}(t)\} = c^2 \text{var}\{e(t)\}$ .

## Minimum-variance control: Example

Consider the model

$$y(t) = -a y(t-1) + b u(t-1) + c e(t-1) + e(t)$$

where  $|c| < 1$  and  $\{e(t)\}$  is a sequence of random variables with  $E\{e(t)\} = 0$  and  $\text{var}\{e(t)\} = \sigma^2$ .

*Our goal is to regulate  $y(t)$  to 0 as close as possible.*

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In the absence of noise:

$$y(t) = -a y(t-1) + b u(t-1)$$

the best strategy (dead beat design) is

$$u(t) = \frac{a}{b} y(t) \quad \implies \quad y(t+1) = 0$$

What should we do when noise is present?

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In the absence of noise or when  $c = 0$ :

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the best strategy (dead beat design) is

$$u(t) = \frac{a}{b} y(t) \quad \implies \quad y(t+1) = e(t+1)$$

What should we do when noise dynamics are present?

## Minimum-variance control: Example (cont'd)

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We have the process

$$y(t + 1) + a y(t) = b u(t) + e(t + 1) + c e(t)$$

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$$y(t+1) + a y(t) = b u(t) + e(t+1) + c e(t)$$

Let us try to compute  $e(t)$  symbolically

$$(q + a) y(t) = b u(t) + (q + c) e(t)$$



## Minimum-variance control: Example (cont'd)

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$$e(t) = \frac{q+a}{q+c} y(t) - \frac{b}{q+c} u(t)$$

Substituting back into the model

$$y(t+1) = -a y(t) + b u(t) + e(t+1) + c \left( \frac{q+a}{q+c} y(t) - \frac{b}{q+c} u(t) \right)$$

## Minimum-variance control: Example (cont'd)

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Let us try to compute  $e(t)$  symbolically

$$e(t) = \frac{q+a}{q+c} y(t) - \frac{b}{q+c} u(t)$$

Substituting back into the model

$$y(t+1) = \underbrace{\frac{(c-a)q}{q+c} y(t) + \frac{bq}{q+c} u(t)}_{\text{known and independent from } e(t+1)!} + e(t+1)$$

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Clearly,  $\text{var}\{y(t+1)\} \geq \text{var}\{e(t+1)\} = \sigma^2.$

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The minimal variance is achieved with:  $u(t) = -\frac{c-a}{b} y(t).$

## Minimum-variance control: General case

Assume the plant is represented by the special ARMAX model

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Additional assumptions:

- The polynomials  $A$  and  $B$  are monic (right rescaling).

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- $\deg\{A\} - \deg\{B\} = d_0 \geq 1$  – known relative degree.

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- The polynomial  $C$  is stable (always can be done).

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Additional assumptions:

- The polynomials  $A$  and  $B$  are monic (right rescaling).
- $\deg\{A\} = \deg\{C\} = n \geq 1$  (always can be done).
- $\deg\{A\} - \deg\{B\} = d_0 \geq 1$  – known relative degree.
- The polynomial  $C$  is stable (always can be done).
- The polynomial  $B$  is stable – a serious restriction.

## Minimum-variance control: General case (cont'd)

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## Minimum-variance control: General case (cont'd)

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We have the process

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

Let us solve it for  $y(t)$

$$y(t) = \frac{B(q)}{A(q)} u(t) + \frac{C(q)}{A(q)} e(t)$$

## Minimum-variance control: General case (cont'd)

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We have the process

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

Shifting by the relative degree

$$y(t + d_0) = \frac{B(q)}{A(q)} u(t + d_0) + \frac{C(q)}{A(q)} e(t + d_0)$$

## Minimum-variance control: General case (cont'd)

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We have the process

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

Shifting by the relative degree and rewriting

$$y(t + d_0) = \frac{B(q)}{A(q)} u(t + d_0) + \frac{C(q) q^{d_0-1}}{A(q)} e(t + 1)$$

## Minimum-variance control: General case (cont'd)

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Shifting by the relative degree and rewriting

$$y(t + d_0) = \frac{B(q)}{A(q)} u(t + d_0) + \frac{C(q) q^{d_0-1}}{A(q)} e(t + 1)$$

Using polynomial long division

$$\boxed{\frac{C(q) q^{d_0-1}}{A(q)} = F(q) + \frac{G(q)}{A(q)}}$$

where  $\frac{G(q)}{A(q)}$  is strictly proper and

$$\deg\{F\} = \deg\{C(q) q^{d_0-1}\} - \deg\{A\} = d_0 - 1.$$



## Minimum-variance control: General case (cont'd)

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We have rewritten the process as

$$y(t + d_0) = \frac{B(q)}{A(q)} u(t + d_0) + \left( F(q) + \frac{G(q)}{A(q)} \right) e(t + 1)$$

## Minimum-variance control: General case (cont'd)

Finally the process can be represented by

$$y(t + d_0) = \underbrace{\frac{q^{d_0} B(q)}{A(q)}}_{\text{proper fraction}} u(t) + \underbrace{\frac{q G(q)}{A(q)}}_{\text{proper fraction}} e(t) + F(q) e(t + 1)$$

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Solving the model for  $e(t)$ , we have

$$e(t) = \frac{A(q)}{C(q)} y(t) - \frac{B(q)}{C(q)} u(t)$$

## Minimum-variance control: General case (cont'd)

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Solving the model for  $e(t)$ , we have

$$e(t) = \frac{A(q)}{C(q)} y(t) - \frac{B(q)}{C(q)} u(t)$$

After substituting it back

$$y(t + d_0) = \frac{q^{d_0} B}{A} u(t) + \frac{q G}{A} \left( \frac{A}{C} y(t) - \frac{B}{C} u(t) \right) + F e(t + 1)$$

## Minimum-variance control: General case (cont'd)

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Solving the model for  $e(t)$ , we have

$$e(t) = \frac{A(q)}{C(q)} y(t) - \frac{B(q)}{C(q)} u(t)$$

After substituting it back and collecting terms

$$y(t + d_0) = \frac{q G}{C} y(t) + \frac{q B}{A C} \left( q^{d_0} C - G \right) u(t) + F e(t + 1)$$

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$$y(t + d_0) = \frac{q G}{C} y(t) + \frac{q B}{C} \frac{(q^{d_0} C - G)}{A} u(t) + F e(t + 1)$$

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Solving the model for  $e(t)$ , we have

$$e(t) = \frac{A(q)}{C(q)} y(t) - \frac{B(q)}{C(q)} u(t)$$

Substituting  $F(q)$  from  $\frac{C(q) q^{d_0-1}}{A(q)} = F(q) + \frac{G(q)}{A(q)}$

$$y(t + d_0) = \frac{q G(q)}{C(q)} y(t) + \frac{q B(q) F(q)}{C(q)} u(t) + F(q) e(t + 1)$$

## Minimum-variance control: General case (cont'd)

We have rewritten the process as

$$y(t + d_0) = \underbrace{\frac{q G(q)}{C(q)} y(t) + \frac{q B(q) F(q)}{C(q)} u(t)}_{\text{known and independent from } F(q) e(t + 1)} + F(q) e(t + 1)$$



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Clearly,  $\text{var}\{y(t + d_0)\} \geq \text{var}\{F(q) e(t + 1)\}$

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$$\text{var}\{y(t+d_0)\} \geq \text{var}\{F(q) e(t+1)\} = \left(1 + f_1^2 + \cdots + f_{d_0-1}^2\right) \sigma^2$$

$$\text{where } F(q) = q^{d_0-1} + f_1 q^{d_0-2} + \cdots + f_{d_0-1}.$$

## Minimum-variance control: General case (cont'd)

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The minimal variance is achieved with:

$$u(t) = -\frac{G(q)}{B(q) F(q)} y(t).$$

## Minimum-variance control: General case (cont'd)

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The closed-loop system is

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

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The minimal variance is achieved with:

$$u(t) = -\frac{G(q)}{B(q) F(q)} y(t).$$

The closed-loop system is

$$A(q) y(t) = B(q) \left( -\frac{G(q)}{B(q) F(q)} y(t) \right) + C(q) e(t)$$

## Minimum-variance control: General case (cont'd)

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$$y(t + d_0) = \underbrace{\frac{q G(q)}{C(q)} y(t) + \frac{q B(q) F(q)}{C(q)} u(t)}_{\text{known and independent from } F(q) e(t+1)} + F(q) e(t + 1)$$

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The minimal variance is achieved with:

$$u(t) = -\frac{G(q)}{B(q) F(q)} y(t).$$

The closed-loop system is

$$B(q) (A(q) F(q) + G(q)) y(t) = B(q) F(q) C(q) e(t)$$

## Minimum-variance control: General case (cont'd)

We have rewritten the process as

$$y(t + d_0) = \underbrace{\frac{q G(q)}{C(q)} y(t) + \frac{q B(q) F(q)}{C(q)} u(t)}_{\text{known and independent from } F(q) e(t+1)} + F(q) e(t + 1)$$

$$\text{var}\{y(t+d_0)\} \geq \text{var}\{F(q) e(t+1)\} = \left(1 + f_1^2 + \cdots + f_{d_0-1}^2\right) \sigma^2$$

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The minimal variance is achieved with:

$$u(t) = -\frac{G(q)}{B(q) F(q)} y(t).$$

The closed-loop system (using:  $q^{d_0-1} C = A F + G$ ) is

$$q^{d_0-1} B(q) C(q) y(t) = B(q) F(q) C(q) e(t)$$

## Minimum-variance control: Remarks

### (1) The closed-loop system

$$q^{d_o-1} B(q) C(q) y(t) = B(q) F(q) C(q) e(t)$$

defines the noise-to-output relation

$$y(t) = \frac{B(q) F(q) C(q)}{q^{d_o-1} B(q) C(q)} e(t)$$



## Minimum-variance control: Remarks

### (1) The closed-loop system

$$q^{d_0-1} B(q) C(q) y(t) = B(q) F(q) C(q) e(t)$$

defines the noise-to-output relation

$$y(t) = \frac{F(q)}{q^{d_0-1}} e(t) = \frac{q^{d_0-1} + f_1 q^{d_0-2} + \dots + f_{d_0-1}}{q^{d_0-1}} e(t)$$

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### (3) The minimum variance controller

$$u(t) = -\frac{G(q)}{B(q) F(q)} y(t)$$

can be interpreted as a **pole-placement** controller.

## Minimum-variance control as pole-placement

Since

$$q^{d_0-1} C(q) = A(q) F(q) + G(q)$$

the closed-loop characteristic polynomial

$$A_c(q) = q^{d_0-1} B(q) C(q) = A(q) \underbrace{B(q) F(q)}_{R(q)} + B(q) \underbrace{G(q)}_{S(q)}$$

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Note that for the Diophantine equation  $A_c = A R + B S$

$$\deg\{S(q)\} = \deg\{G(q)\} = n - 1$$

and  $S/R$  is proper since

$$\deg\{R\} = \deg\{B\} + \deg\{F\} = (n - d_0) + (d_0 - 1) = n - 1.$$

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*Can we use an analogous pole-placement technique for the case when  $B(q)$  has unstable zeros?*



## Moving Average Controller

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Design the controller

$$u(t) = -\frac{S(q)}{R(q)}y(t) \quad \text{for} \quad A(q)y(t) = B(q)u(t) + C(q)e(t)$$

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- Let  $R = R_p B^+$ , where  $\deg\{R_p\} = d - 1$ .

The obtained transfer function for the closed-loop system is

$$y(t) = q^{1-d} R_p(q) e(t) = e(t) + r_1 e(t-1) + \dots + r_{d-1} e(t-d+1)$$

## Example 4.3

Consider the plant described by

$$(q^2 + a_1 q + a_2) y(t) = (b_0 q + b_1) u(t) + (q^2 + c_1 q + c_2) e(t)$$

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1. If  $|b_1/b_0| < 1$  minimum variance (MV) controller can be designed noticing that

$$\frac{q^{1-1} (q^2 + c_1 q + c_2)}{q^2 + a_1 q + a_2} = 1 + \frac{(c_1 - a_1) q + (c_2 - a_2)}{q^2 + a_1 q + a_2}$$

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2. If  $|b_1/b_0| > 1$  minimum variance (MV) controller cannot be designed but we can apply moving average controller (MA) with  $d = 2$  using the solution of the Diophantine equation

$$q (q^2 + c_1 q + c_2) = (q^2 + a_1 q + a_2)(q + r_1) + (b_0 q + b_1)(s_0 q + s_1)$$



## Next Lecture / Assignments:

Next meeting (May 10, 13:00-15:00, in A208Tekn): Recitations.

Homework problems: Consider the process in Example 4.3 with  $a_1 = -1.5$ ,  $a_2 = 0.7$ ,  $b_0 = 1$ ,  $c_1 = -1$ , and  $c_2 = 0.2$ .

Determine the variance of the output in the closed-loop system as a function of  $b_1$  when the Moving Average controller is used. Compare with the lowest achievable variance.