

## **Lecture 10:** Indirect Minimum-Variance / Stochastic STR.

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- Indirect Minimum Variance Adaptive Control.
- Stochastic Self Tuning Regulators.

## Stochastic Linear Models

Assume the plant is represented by special ARMAX model

$$A(q) y(t) = B(q) u(t) + C(q) e(t)$$

where  $\{e(t)\}$  – white noise,  $d_0 = 1$ ,

$$A(q) = q^n + a_1 q^{n-1} + \dots + a_n, \quad \deg\{A\} = n$$

$$B(q) = b_1 q^{n-1} + \dots + b_n, \quad \deg\{B\} = n - 1$$

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Equivalently,

$$\begin{aligned} y(t) = & -a_1 y(t-1) - \dots - a_n y(t-n) \\ & + b_1 u(t-1) + \dots + b_n u(t-n) \\ & + e(t) + c_1 e(t-1) + \dots + c_n e(t-n) \end{aligned}$$

## Example: approximate regression for dynamic noise

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Consider the model

$$y(t) = -a y(t-1) + b u(t-1) + c e(t-1) + e(t)$$

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$$f(k) = y(k) + a y(k-1) - b u(k-1)$$

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## Extended Least Square (ELS)

For the model

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with  $\theta^0 = \left[ a_1, \dots, a_n, b_1, \dots, b_n, c_1, \dots, c_n \right]^T$

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with  $\theta^0 = \begin{bmatrix} a_1, \dots, a_n, b_1, \dots, b_n, c_1, \dots, c_n \end{bmatrix}^T$

Define the prediction error

$$\varepsilon(t) = y(t) - \phi(t-1)^T \hat{\theta}(t-1)$$

with the regression vector

$$\phi(t-1)^T = \begin{bmatrix} -y(t-1), \dots, u(t-n), \varepsilon(t-1), \dots, \varepsilon(t-n) \end{bmatrix}$$

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$$\phi(t-1)^T = \begin{bmatrix} -y(t-1), \dots, u(t-n), \varepsilon(t-1), \dots, \varepsilon(t-n) \end{bmatrix}$$

and apply standard RLS for the approximate regression model

$$y(t) = \phi(t-1)^T \theta + e(t)$$

## ELS / RML

The **ELS** algorithm is given by RLS

$$\hat{\theta}(t) = \hat{\theta}(t-1) + P(t) \phi(t-1)^T \varepsilon(t)$$

$$P(t)^{-1} = P(t-1)^{-1} + \phi(t-1) \phi(t-1)^T$$

$$\varepsilon(t) = y(t) - \phi(t-1)^T \hat{\theta}(t-1)$$

with  $e(\cdot)$  approximated by  $\varepsilon(\cdot)$  in  $\phi(t-1)$

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with  $e(\cdot)$  approximated by  $\varepsilon(\cdot)$  in  $\phi(t-1)$

Another possible choice is Recursive Maximum Likelihood method (**RML**):

$$\begin{aligned}\hat{\theta}(t) &= \hat{\theta}(t-1) + P(t) \phi_f(t-1)^T \varepsilon(t) \\ P(t)^{-1} &= P(t-1)^{-1} + \phi_f(t-1) \phi_f(t-1)^T \\ \varepsilon(t) &= y(t) - \phi_f(t-1)^T \hat{\theta}(t-1) \\ \hat{C}(q) \phi_f(t) &= \phi(t)\end{aligned}$$

## Example 4.4 (MV+ELS)

Consider the plant from previous lecture described by

$$y(t) = -a y(t-1) + b u(t-1) + c e(t-1) + e(t)$$



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Suppose the real parameters  $a = 0.9$ ,  $b = 3$ ,  $c = -0.3$  are not known and so the minimum variance controller

$$u(t) = \frac{a - c}{b} y(t) = s_0 y(t), \quad s_0 = (-0.3 - (-0.9))/3 = 0.2$$

cannot be applied directly.

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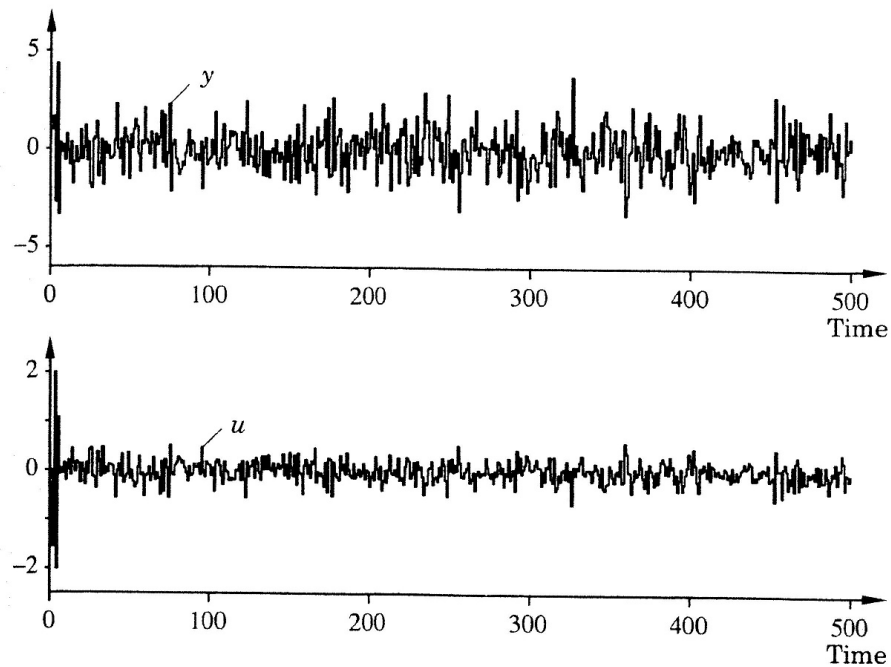
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Let us combine **MV** controller

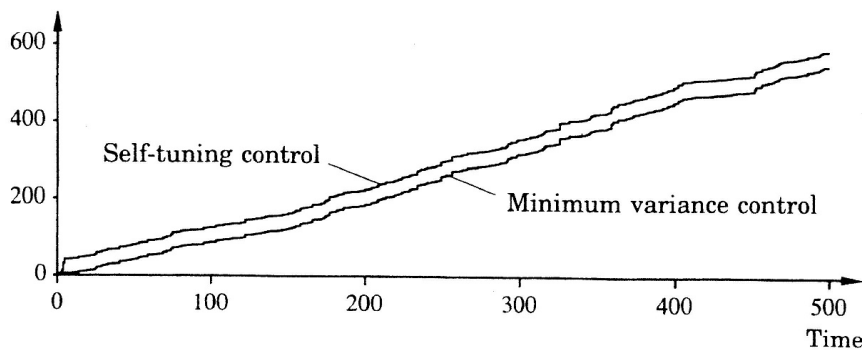
$$u(t) = \hat{s}_0(t) y(t), \quad \hat{s}_0(t) = \frac{\hat{a}(t) - \hat{c}(t)}{\hat{b}(t)}$$

with **ELS** estimator for  $\hat{\theta}(t) = [\hat{a}(t), \hat{b}(t), \hat{c}(t)]$  using

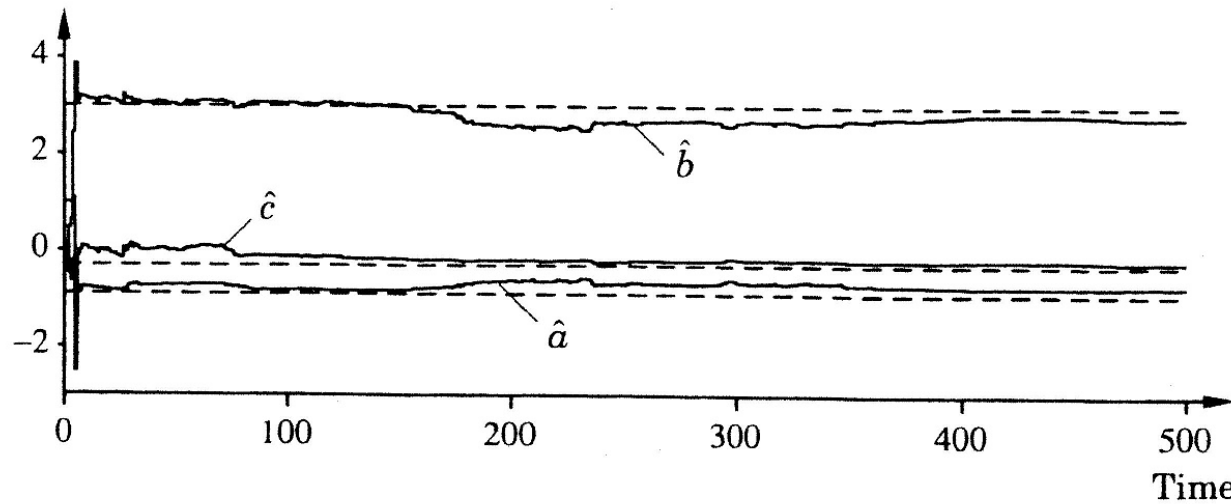
$$\phi(t-1)^T = [-y(t-1), u(t-1), \varepsilon(t-1)]$$



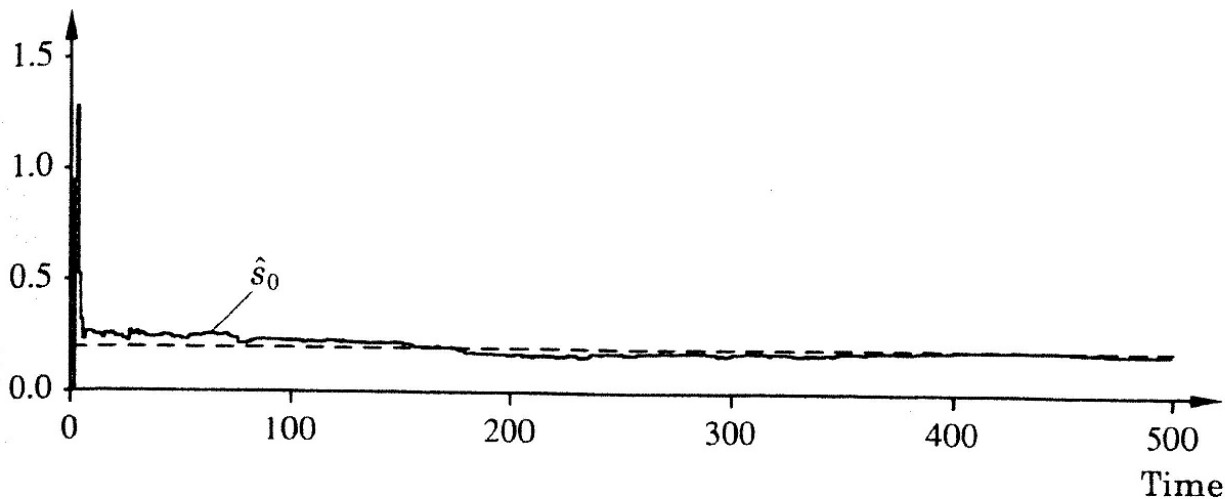
**Figure 4.2** Output and input when an indirect self-tuning regulator based on minimum-variance control is used to control the system in Example 4.4.



**Figure 4.3** The accumulated loss when a self-tuning regulator and the optimal minimum-variance controller are used on the system in Example 4.4.



**Figure 4.4** The estimated parameters  $\hat{a}(t)$ ,  $\hat{b}(t)$ , and  $\hat{c}(t)$  when the system in Example 4.4 is controlled. The dashed lines correspond to the true parameter values.



**Figure 4.5** The controller parameter  $\hat{s}_0(t)$  when the system in Example 4.4 is controlled. The dashed line is the optimal parameter for the minimum-variance controller.

## Direct Minimum Variance Controller

The closed-loop system under **MV** controller

$$u = -\frac{S(q)}{R(q)} y(t), \quad R(q) = B(q) F(q), \quad S(q) = G(q)$$

can be written in the form

$$y(t+d_0) = \frac{q G(q)}{C(q)} y(t) + \frac{q B(q) F(q)}{C(q)} u(t) + q^{1-d_0} F(q) e(t+d_0)$$

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Let us introduce the polynomials with backward shifts as

$$\frac{q R}{C} = \frac{r_0 q^n + \dots + r_{n-1} q}{q^n + c_1 q^{n-1} + \dots + c_n} = \frac{r_0 + \dots + r_{n-1} q^{-n+1}}{1 + c_1 q^{-1} + \dots + c_n q^{-n}} = \frac{R^*}{C^*}$$

to rewrite the system in the *direct form* for adaptation

$$y(t+d_0) = \frac{R^*(q^{-1})}{C^*(q^{-1})} u(t) + \frac{S^*(q^{-1})}{C^*(q^{-1})} y(t) + R_p^*(q^{-1}) e(t+d_0)$$

## Moving Average Self-Tuning Controller

The **MA** controller is defined by

$$u = -\frac{S(q)}{R(q)} y(t), \quad R = R_p B^+, \quad q^{d-1} C = A R_p + B^- S$$



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$$C y(t + d) = q R_p B^- B^+ u(t) + q R_p C e(t) + q B^- S y(t)$$

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Using the polynomials with backward shifts

$$C^* = 1 + \dots + c_n q^{-n}, \quad R^* = r_0 + \dots + r_{n-1} q^{-n+1}, \quad S^* = \dots$$

we obtain the system in the *direct form* for adaptation

$$y(t+d_0) = \frac{B^{-*}}{C^*} \left( R^*(q^{-1}) u(t) + S^*(q^{-1}) y(t) \right) + R_p^*(q^{-1}) e(t+d_0)$$

## Adding Parameter Estimation

The closed-loop system under MV and MA controllers is

$$y(t+d) = \frac{Q^*}{P^*} \left( R^*(q^{-1})u(t) + S^*(q^{-1})y(t) \right) + R_p^*(q^{-1})e(t+d)$$

with  $d = d_0$  and  $Q^*/P^* = 1/C^*$  for MV and

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The fact that the denominator  $C^*(q^{-1})$  is unknown is an obstacle to obtaining the standard regression form and using ELS or RML with over parametrization might be heavy.

However, standard **RLS** can be used for the approximate model

$$\varepsilon(t) = y(t) - R^* u_f(t-d) - S^* y_f(t-d) = y(t) - \phi(t-d)^T \hat{\theta}(t-1)$$

with a stable filter  $Q^*/P^*$  for the signals:

$$y_f(t) = \frac{Q^*(q^{-1})}{P^*(q^{-1})} y(t), \quad u_f(t) = \frac{Q^*(q^{-1})}{P^*(q^{-1})} u(t)$$

## Stochastic Self-Tuning Regulators

Surprisingly, adaptive controllers with sufficiently high degree of the polynomials with incorrect filters  $P^*/Q^*$ ,

$$u(t) = -\frac{\hat{S}^*(q^{-1})}{\hat{R}^*(q^{-1})} y(t)$$

recover MV (no zero cancellations) for  $d = d_0$  and

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MA (with correct number of canceled zeros) for  $d > d_0$ .

The modification to include feedforward term is often useful:

$$y(t+d) = R^*(q^{-1}) u(t) + S^*(q^{-1}) y(t) - T^*(q^{-1}) v(t) + \varepsilon(t+d)$$

where  $v(t)$  can be a measurable disturbance and

$$u(t) = -\frac{\hat{S}^*(q^{-1})}{\hat{R}^*(q^{-1})} y(t) + \frac{\hat{T}^*(q^{-1})}{\hat{R}^*(q^{-1})} v(t)$$

## Example 4.5 (Direct MV STR)

Consider the plant from Example 4.4

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The closed-loop system with MV controller can be approximated by the process

$$y(t+1) = r_0 u(t) + s_0 y(t) + \varepsilon(t+1), \quad \frac{s_0}{r_0} = \frac{a-c}{b} = 0.2$$

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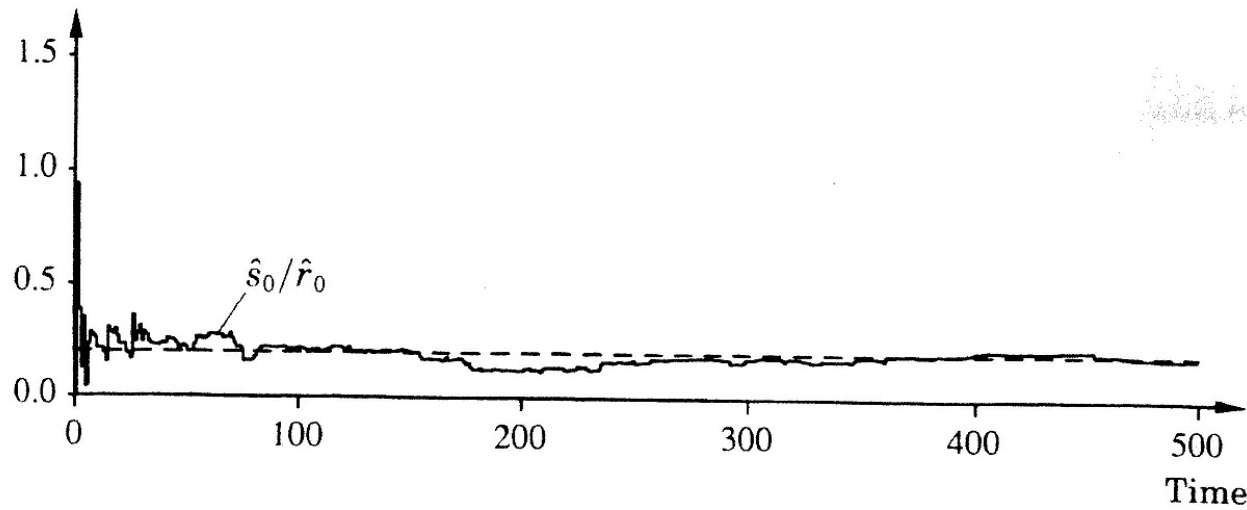
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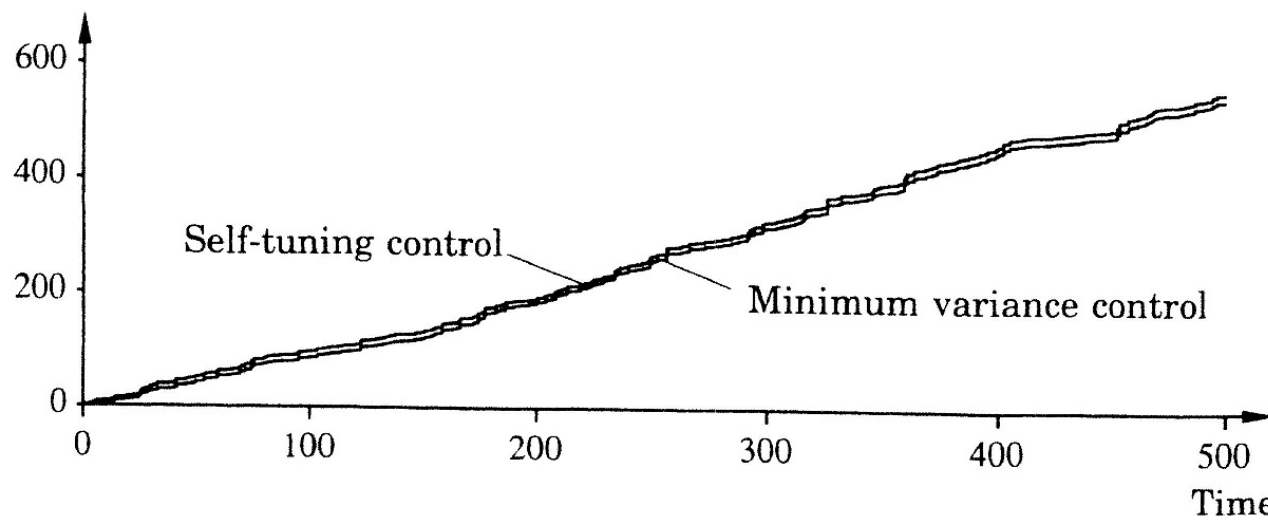
Let us use STR with  $\hat{r}_0 = 1$  and

$$u(t) = -\frac{\hat{s}_0(t)}{\hat{r}_0} y(t),$$

with **RLS** estimator for  $\hat{\theta}(t) = \hat{s}_0(t)$



**Figure 4.6** The parameter  $\hat{s}_0/\hat{r}_0$  in the controller, when the process in Example 4.5 is controlled by using the direct minimum-variance self-tuning controller.



**Figure 4.7** The loss function when the direct self-tuning regulator and the optimal minimum-variance controller are used on the system in Example 4.5.



## Example 4.6 (Direct MV/MA STR)

Consider a sampled model of a delayed integrator

$$(q^2 - q) y(t) = (h - \tau)(q + b) u(t) + (q^2 + c q) e(t), \quad b = \frac{\tau}{h - \tau}$$

with  $c = 0.8$  and  $h = 1$ .

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Let us use STR with  $d = 1$  or  $d = 2$

$$u(t) = -\hat{s}_0(t) y(t) \quad \text{or} \quad u(t) = -\hat{s}_0(t) y(t) - \hat{r}_1(t) u(t - 1)$$

with **RLS** estimator for  $\hat{\theta}(t) = \hat{s}_0(t)$  or  $\hat{\theta}(t) = [\hat{s}_0(t), \hat{r}_1(t)]^T$ .

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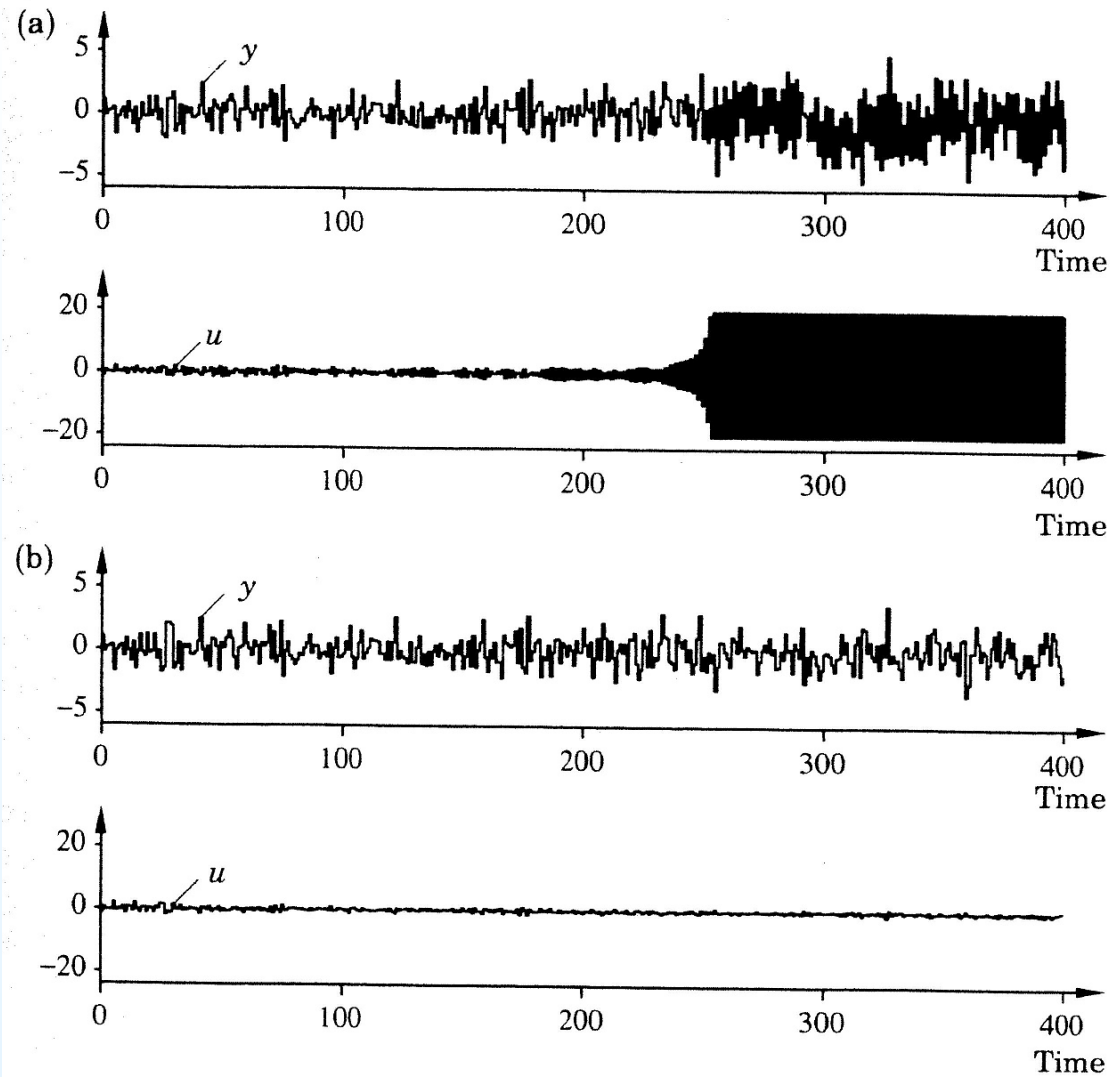
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with **RLS** estimator for  $\hat{\theta}(t) = \hat{s}_0(t)$  or  $\hat{\theta}(t) = [\hat{s}_0(t), \hat{r}_1(t)]^T$ .

Note that since  $|b| < 1 \Leftrightarrow \tau < h/2$ ,  $d = d_0 = 1$  (MV) should not be used for  $\tau > h/2 = 0.5$ .



**Figure 4.8** Simulation of the self-tuning algorithm on the integrator with time delay in Example 4.6. At  $t = 100$  the delay is changed from 0.4 to 0.6. (a)  $d = 1$ ; (b)  $d = 2$ .

## Next Lecture / Assignments:

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Next meeting (**May 14, 10:00-12:00, in A206Tekn**):  
Model-Reference Adaptive Systems.

Homework problem: Reproduce the simulation results given on  
Figure 4.8.