

# Active Suspensions

Nicola Mimmo

Department of Electric, Electronics, and Information Engineering “G. Marconi”

University of Bologna

# Outline

- Motivations & Goals
- Non-linear 1D Model
- Control Problem Formulation
- Linearisation
- Linear Model Investigation
- Control Architecture
- Control Design
- Performance Evaluation

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# Motivations & Goals

Improve the ride quality and change the setup.



# Motivations & Goals

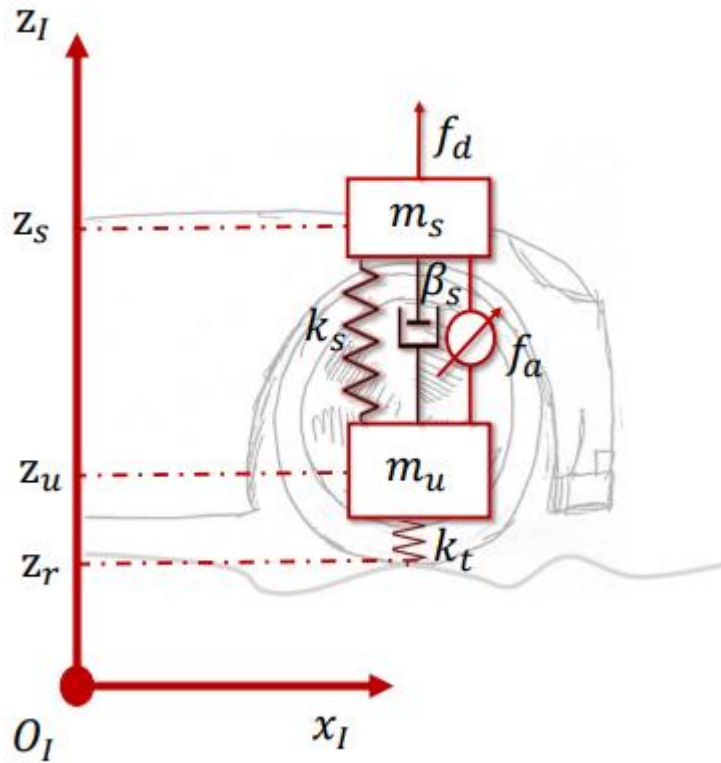
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# Non-linear 1D Model



Sprung mass  $m_s \ddot{z}_s = -m_s g + f_s + f_d$

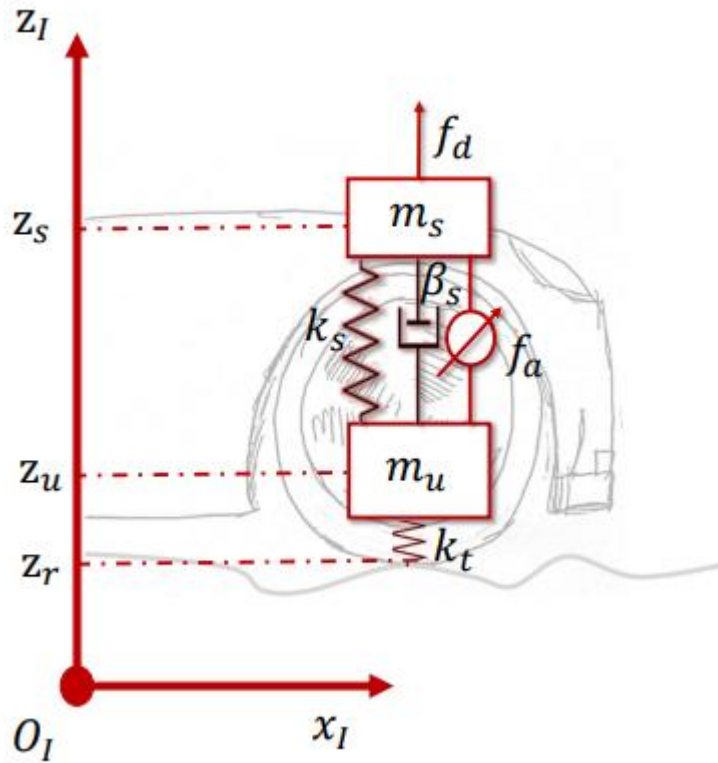
Unsprung mass  $m_u \ddot{z}_u = -m_u g - f_s + f_t(z_u - z_r)$

Tire  $f_t(z_u - z_r) = \begin{cases} 0 & z_u - z_r > \ell_t \\ -k_t(z_u - z_r - \ell_t) & z_u - z_r \leq \ell_t \end{cases}$

Suspension  $f_s := -k_s(z_s - z_u - \ell_s) - \beta_s(\dot{z}_s - \dot{z}_u) + f_a$

Aerodynamics (downforce)  $f_d = \frac{1}{2} \rho S v^2 C_z$

# Non-linear 1D Model



Sensors

Accelerometer (z)

$$y_a = -g - \frac{k_s}{m_s}(z_s - z_u - \ell_s) - \frac{\beta_s}{m_s}(\dot{z}_s - \dot{z}_u) + \frac{f_a + f_d}{m_s} + \nu_a$$

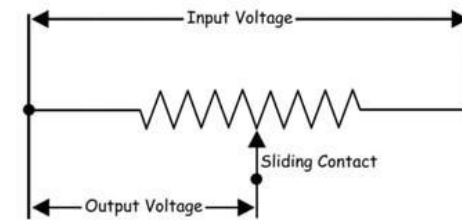
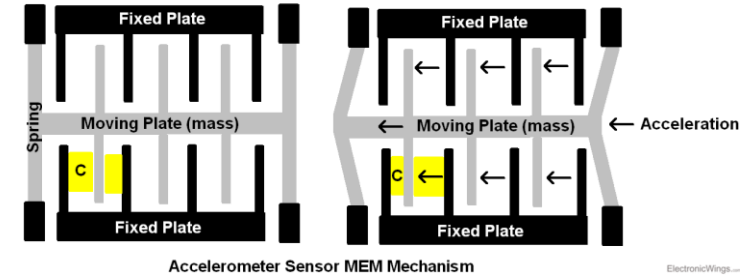
Potentiometer

$$y_p = z_s - z_u + \nu_p$$

Regulated Output

$$e = y_p - r$$

MEMS Based Accelerometer





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# Problem Formulation

let  $\dot{z}_s := v_s$  and  $\dot{z}_u := v_u$

$$\dot{z}_s = v_s$$

$$m_s \dot{v}_s = -m_s g - k_s(z_s - z_u - \ell_s) - \beta_s(v_s - v_u) + f_a + f_d$$

$$\dot{z}_u = v_u$$

$$m_u \dot{v}_u = -m_u g + k_s(z_s - z_u - \ell_s) + \beta_s(v_s - v_u) - f_a + f_t(z_u - z_r)$$

# Problem Formulation

Define

let  $\dot{z}_s := v_s$  and  $\dot{z}_u := v_u$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} := \begin{bmatrix} z_s - z_u \\ v_s - v_u \\ z_u - z_r \\ v_u - \dot{z}_r \end{bmatrix} \quad \begin{array}{l} \dot{z}_s = v_s \\ m_s \dot{v}_s = -m_s g - k_s(z_s - z_u - \ell_s) - \beta_s(v_s - v_u) + f_a + f_d \\ \dot{z}_u = v_u \\ m_u \dot{v}_u = -m_u g + k_s(z_s - z_u - \ell_s) + \beta_s(v_s - v_u) - f_a + f_t(z_u - z_r) \end{array}$$

# Problem Formulation

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -\frac{m_s + m_u}{m_s m_u} k_s (x_1 - \ell_s) - \frac{m_s + m_u}{m_s m_u} \beta_s x_2 + \frac{m_s + m_u}{m_s m_u} f_a + \frac{1}{m_s} f_d - \frac{1}{m_u} f_t(x_3)$$

$$\dot{x}_3 = x_4$$

$$\dot{x}_4 = -g + \frac{k_s}{m_u} (x_1 - \ell_s) + \frac{\beta_s}{m_u} x_2 - \frac{f_a}{m_u} + \frac{1}{m_u} f_t(x_3) - \ddot{z}_r$$

Define

let  $\dot{z}_s := v_s$  and  $\dot{z}_u := v_u$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} := \begin{bmatrix} z_s - z_u \\ v_s - v_u \\ z_u - z_r \\ v_u - \dot{z}_r \end{bmatrix} \quad \begin{array}{l} \dot{z}_s = v_s \\ m_s \dot{v}_s = -m_s g - k_s(z_s - z_u - \ell_s) - \beta_s(v_s - v_u) + f_a + f_d \\ \dot{z}_u = v_u \\ m_u \dot{v}_u = -m_u g + k_s(z_s - z_u - \ell_s) + \beta_s(v_s - v_u) - f_a + f_t(z_u - z_r) \end{array}$$

# Problem Formulation

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -\frac{m_s + m_u}{m_s m_u} k_s (x_1 - \ell_s) - \frac{m_s + m_u}{m_s m_u} \beta_s x_2 + \frac{m_s + m_u}{m_s m_u} f_a + \frac{1}{m_s} f_d - \frac{1}{m_u} f_t(x_3)$$

$$\dot{x}_3 = x_4$$

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$$y_p = x_1 + \nu_p$$

$$y_a = -g - \frac{k_s}{m_s} (x_1 - \ell_s) - \frac{\beta_s}{m_s} x_2 + \frac{f_a + f_d}{m_s} + \nu_a$$

$$e = x_1 + \nu_p - r.$$

# Problem Formulation

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= -\frac{m_s + m_u}{m_s m_u} k_s (x_1 - \ell_s) - \frac{m_s + m_u}{m_s m_u} \beta_s x_2 + \frac{m_s + m_u}{m_s m_u} f_a + \frac{1}{m_s} f_d - \frac{1}{m_u} f_t(x_3) \\ \dot{x}_3 &= x_4 \\ \dot{x}_4 &= -g + \frac{k_s}{m_u} (x_1 - \ell_s) + \frac{\beta_s}{m_u} x_2 - \frac{f_a}{m_u} + \frac{1}{m_u} f_t(x_3) - \ddot{z}_r\end{aligned}$$

$$\begin{aligned}y_p &= x_1 + \nu_p \\ y_a &= -g - \frac{k_s}{m_s} (x_1 - \ell_s) - \frac{\beta_s}{m_s} x_2 + \frac{f_a + f_d}{m_s} + \nu_a\end{aligned}$$

$\mathbf{x} = \text{col}(x_1, x_2, x_3, x_4), \quad u = f_a,$   
 $\mathbf{d} = \text{col}(\ddot{z}_r, f_d),$   
 $\boldsymbol{\nu} = \text{col}(\nu_p, \nu_a),$   
 $\mathbf{w} = \text{col}(\mathbf{d}, \boldsymbol{\nu}, r),$

$$e = x_1 + \nu_p - r.$$

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{f}(\mathbf{x}, u, \mathbf{w}) \\ \mathbf{y} &= \mathbf{h}(\mathbf{x}, u, \mathbf{w}) \\ e &= h_e(\mathbf{x}, u, \mathbf{w}),\end{aligned} \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

# Problem Formulation

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= -\frac{m_s + m_u}{m_s m_u} k_s (x_1 - \ell_s) - \frac{m_s + m_u}{m_s m_u} \beta_s x_2 + \frac{m_s + m_u}{m_s m_u} f_a + \frac{1}{m_s} f_d - \frac{1}{m_u} f_t(x_3) \\ \dot{x}_3 &= x_4 \\ \dot{x}_4 &= -g + \frac{k_s}{m_u} (x_1 - \ell_s) + \frac{\beta_s}{m_u} x_2 - \frac{f_a}{m_u} + \frac{1}{m_u} f_t(x_3) - \ddot{z}_r\end{aligned}$$

$$\begin{aligned}y_p &= x_1 + \nu_p \\ y_a &= -g - \frac{k_s}{m_s} (x_1 - \ell_s) - \frac{\beta_s}{m_s} x_2 + \frac{f_a + f_d}{m_s} + \nu_a\end{aligned}$$

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 $\mathbf{w} = \text{col}(\mathbf{d}, \boldsymbol{\nu}, r),$

$$e = x_1 + \nu_p - r.$$

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{f}(\mathbf{x}, u, \mathbf{w}) \\ \mathbf{y} &= \mathbf{h}(\mathbf{x}, u, \mathbf{w}) \\ e &= h_e(\mathbf{x}, u, \mathbf{w}),\end{aligned}$$

$\mathbf{x}(t_0) = \mathbf{x}_0$

## Control Goals

- 1) Keep all the signals bounded
- 2) Asymptotically steer the regulated output to zero assuming constant disturbances.

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# Linearisation

assume  $u_0 = 0$ ,  $\mathbf{d}_0, \boldsymbol{\nu}_0 = \mathbf{0}$ ,  $\mathbf{x}_0 := \text{col}(x_{1_0}, x_{2_0}, x_{3_0}, x_{4_0})$ ,  $\mathbf{y}_0 := \text{col}(y_{p_0}, y_{a_0})$ , and  $r = r_0$

Impose  $\dot{\mathbf{x}} = \mathbf{0}$

$$0 = x_{2_0}$$

$$0 = -\frac{m_s + m_u}{m_s m_u} k_s (x_{1_0} - \ell_s) + \frac{k_t}{m_u} (x_{3_0} - \ell_t)$$

$$0 = x_{4_0}$$

$$0 = -g + \frac{k_s}{m_u} (x_{1_0} - \ell_s) - \frac{k_t}{m_u} (x_{3_0} - \ell_t)$$

$$y_{p_0} = x_{1_0}$$

$$y_{a_0} = -g - \frac{k_s}{m_s} (x_{1_0} - \ell_s)$$

$$r_0 = x_{1_0},$$

$$\begin{bmatrix} x_{1_0} \\ x_{2_0} \\ x_{3_0} \\ x_{4_0} \end{bmatrix} = \begin{bmatrix} \ell_s - g \frac{m_s}{k_s} \\ 0 \\ \ell_t - g \frac{m_s + m_u}{k_t} \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} y_{p_0} \\ y_{a_0} \end{bmatrix} = \begin{bmatrix} \ell_s - g \frac{m_s}{k_s} \\ 0 \end{bmatrix}$$

$$r_0 = \ell_s - g \frac{m_s}{k_s}.$$

# Linearisation

Define the errors to the equilibrium point as

$$\tilde{\mathbf{x}} := \mathbf{x} - \mathbf{x}_0, \tilde{u} := u - u_0,$$

$$\tilde{\mathbf{d}} := \mathbf{d} - \mathbf{d}_0, \tilde{\boldsymbol{\nu}} = \boldsymbol{\nu} - \boldsymbol{\nu}_0,$$

$$\tilde{r} := r - r_0, \tilde{\mathbf{w}} = \text{col}(\tilde{d}, \tilde{\boldsymbol{\nu}}, \tilde{\mathbf{r}}),$$

$$\tilde{\mathbf{y}} := \mathbf{y} - \mathbf{y}_0$$

$$\tilde{e} := e - 0$$

To obtain

$$\dot{\tilde{\mathbf{x}}} = \mathbf{A}\tilde{\mathbf{x}} + \mathbf{B}_1\tilde{u} + \mathbf{B}_2\tilde{\mathbf{w}} \quad \tilde{\mathbf{x}}(t_0) = \tilde{\mathbf{x}}_0$$

$$\tilde{\mathbf{y}} = \mathbf{C}\tilde{\mathbf{x}} + \mathbf{D}_1\tilde{u} + \mathbf{D}_2\tilde{\mathbf{w}}$$

$$\tilde{e} = \mathbf{C}_e\tilde{\mathbf{x}} + \mathbf{D}_{e2}\tilde{\mathbf{w}}.$$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$\mathbf{B}_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}, \quad \mathbf{B}_2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & m_s^{-1} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}, \quad \mathbf{C}_e = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}$$

$$\mathbf{D}_1 = \begin{bmatrix} 0 \\ m_s^{-1} \end{bmatrix}, \quad \mathbf{D}_2 = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 \\ 0 & m_s^{-1} & 0 & 1 & 0 \end{bmatrix}$$

$$\mathbf{D}_{e2} = \begin{bmatrix} 0 & 0 & 0 & 1 & -1 \end{bmatrix}.$$

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# Linear Model Investigation

Let us study  $\mathbf{A}$

How many eigenvalues?

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

# Linear Model Investigation

Let us study  $A$

How many eigenvalues?

Numerically ...

```
K>> eig(A)
```

```
ans =
```

```
-11.4354 +60.8968i
```

```
-11.4354 -60.8968i
```

```
-1.6757 + 7.5142i
```

```
-1.6757 - 7.5142i
```

$A =$

$1.0e+03 *$

0	0.0010	0	0
-0.4196	-0.0262	3.5556	0
0	0	0	0.0010
0.3556	0.0222	-3.5556	0

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$A =$

$1.0e+03 *$

```
0 0.0010 0 0
-0.4196 -0.0262 3.5556 0
0 0 0 0.0010
0.3556 0.0222 -3.5556 0
```

Let  $\lambda_{1,2} = -\alpha_1 \pm i\beta_1$  and  $\lambda_{3,4} = -\alpha_2 \pm i\beta_2$

$$\begin{bmatrix} z_1(t) \\ z_2(t) \end{bmatrix} = e^{-\alpha_1 t} \begin{bmatrix} \cos(\beta_1 t) & \sin(\beta_1 t) \\ -\sin(\beta_1 t) & \cos(\beta_1 t) \end{bmatrix} \begin{bmatrix} z_1(0) \\ z_2(0) \end{bmatrix}$$

$$\begin{bmatrix} z_3(t) \\ z_4(t) \end{bmatrix} = e^{-\alpha_2 t} \begin{bmatrix} \cos(\beta_2 t) & \sin(\beta_2 t) \\ -\sin(\beta_2 t) & \cos(\beta_2 t) \end{bmatrix} \begin{bmatrix} z_3(0) \\ z_4(0) \end{bmatrix}$$

# Linear Model Investigation

Let us study  $\mathbf{A}$

$$\mathbf{x}(t) = \mathbf{V}\mathbf{z}(t)$$

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-11.4354 + 60.8968i  
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# Linear Model Investigation

Let us study  $\mathbf{A}$

How many eigenvalues?

Numerically ...

```
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```

```
ans =
```

$$\mathbf{x}(t) = \mathbf{V}\mathbf{z}(t)$$

$\mathbf{V} =$

0.0021	0.0114	-0.0279	-0.1251
-0.7162	0	0.9865	0
-0.0027	-0.0109	0.0035	-0.0127
0.6965	-0.0411	0.0893	0.0477

-11.4354	+60.8968i
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$$\begin{array}{l} -11.4354 + 60.8968i \\ -11.4354 - 60.8968i \\ -1.6757 + 7.5142i \\ -1.6757 - 7.5142i \end{array}$$

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# Linear Model Investigation

Let us study  $\mathbf{A}$

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Numerically ...

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-11.4354 + 60.8968i
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$$\mathbf{x}(t) = \mathbf{V}\mathbf{z}(t)$$

$$\mathbf{V} =$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 0.0021 & 0.0114 & -0.0279 & -0.1251 \\ -0.7162 & 0 & 0.9865 & 0 \\ -0.0027 & -0.0109 & 0.0035 & -0.0127 \\ 0.6965 & -0.0411 & 0.0893 & 0.0477 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 1.2816 & 6.8250 & 16.7559 & 75.1375 \\ 42.0622 & 0 & 57.9378 & 0 \\ 9.1364 & 36.6087 & 11.7927 & 42.4622 \\ 79.6353 & 4.7001 & 10.2131 & 5.4516 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

Normalised (by row)

$$\bar{V}(i,:) = \frac{|V(i,:)|}{\sum_j |V(i,j)|}$$

# Linear Model Investigation

Let us study  $A$

How many eigenvalues?

Numerically ...

$$\mathbf{x}(t) = \mathbf{V}\mathbf{z}(t)$$

$$\mathbf{V} =$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 0.0021 & 0.0114 & -0.0279 & -0.1251 \\ -0.7162 & 0 & 0.9865 & 0 \\ -0.0027 & -0.0109 & 0.0035 & -0.0127 \\ 0.6965 & -0.0411 & 0.0893 & 0.0477 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 1.2816 & 6.8250 & 16.7559 & 75.1375 \\ 42.0622 & 0 & 57.9378 & 0 \\ 9.1364 & 36.6087 & 11.7927 & 42.4622 \\ 79.6353 & 4.7001 & 10.2131 & 5.4516 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

Normalised (by row)

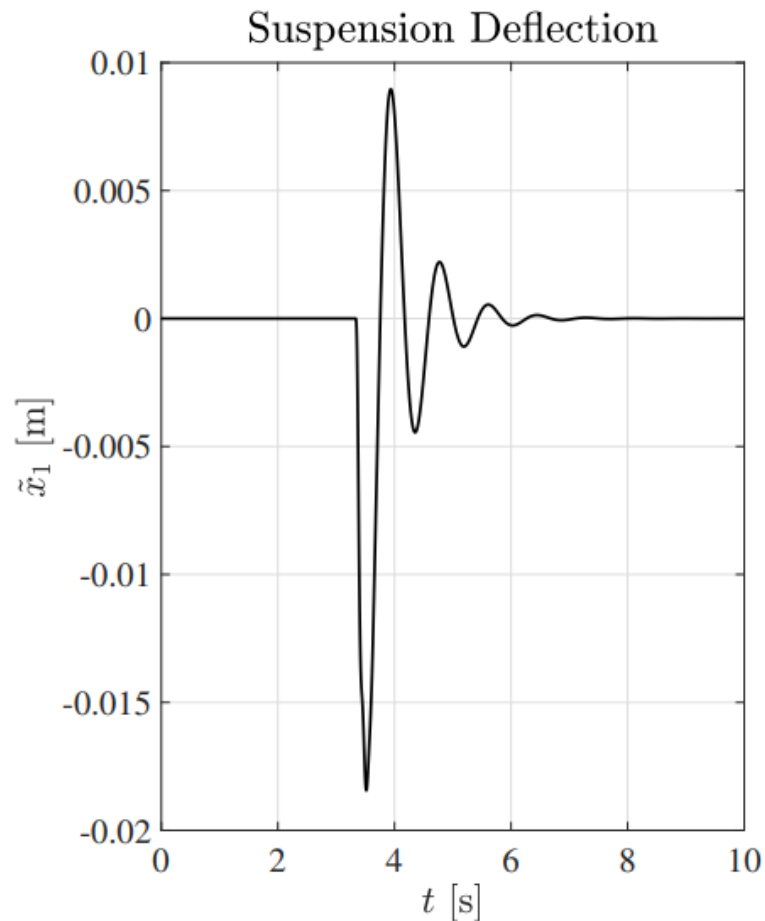
$$\bar{V}(i,:) = \frac{|V(i,:)|}{\sum_j |V(i,j)|}$$

# Linear Model Investigation

Let us study  $A$

How many eigenvalues?

Numerically ...



$$\mathbf{x}(t) = \mathbf{V}\mathbf{z}(t)$$

$$\mathbf{V} =$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 0.0021 & 0.0114 & -0.0279 & -0.1251 \\ -0.7162 & 0 & 0.9865 & 0 \\ -0.0027 & -0.0109 & 0.0035 & -0.0127 \\ 0.6965 & -0.0411 & 0.0893 & 0.0477 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 1.2816 & 6.8250 & 16.7559 & 75.1375 \\ 42.0622 & 0 & 57.9378 & 0 \\ 9.1364 & 36.6087 & 11.7927 & 42.4622 \\ 79.6353 & 4.7001 & 10.2131 & 5.4516 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_4 \\ z_4 \end{bmatrix}$$

Normalised (by row)

$$\bar{V}(i,:) = \frac{|V(i,:)|}{\sum_j |V(i,j)|}$$

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Normalised (by row)

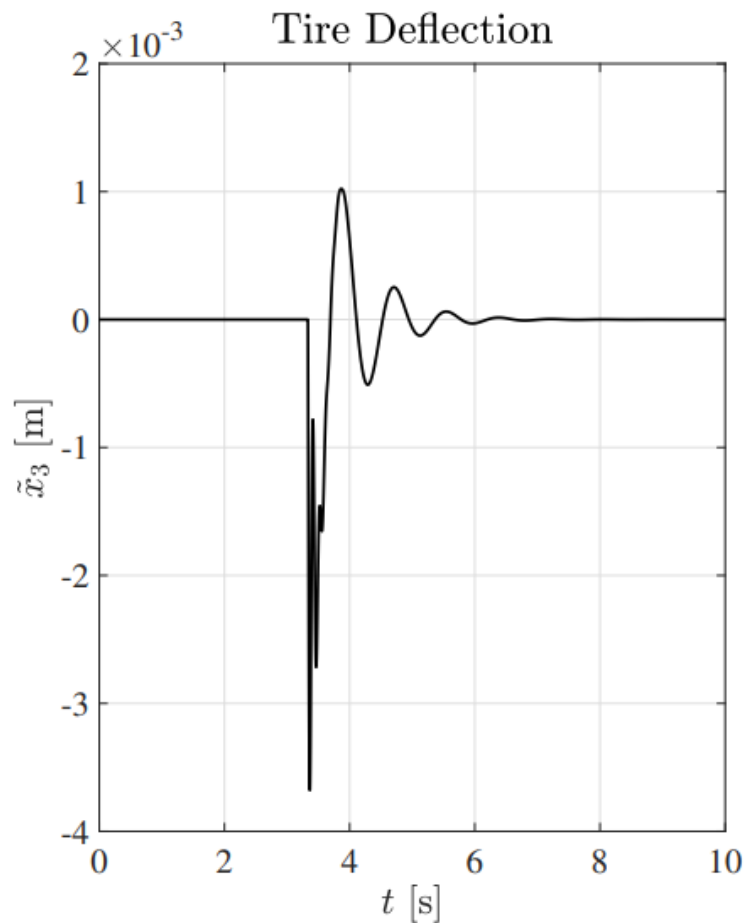
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Normalised (by row)

$$\bar{V}(i,:) = \frac{|V(i,:)|}{\sum_j |V(i,j)|}$$

# Linear Model Investigation

Reachability of  $(\mathbf{A}, \mathbf{B}_1)$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$
$$\mathbf{B}_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}$$

# Linear Model Investigation

Reachability of  $(\mathbf{A}, \mathbf{B}_1)$

$$\mathbf{R} = \begin{bmatrix} \mathbf{B}_1 & \cdots & \mathbf{A}^3 \mathbf{B}_1 \end{bmatrix}$$

$$= \frac{1}{m_u} \begin{bmatrix} 0 & 0 & -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{\bar{m}(2k_t\beta_s m_u + k_s m_u^2 - \bar{m}^3 \beta_s^3)}{m_u^3} \\ \bar{m} & -\frac{\bar{m}^2 \beta_s}{m_u} & \frac{\bar{m}^3 \beta_s^2 - k_t m_u}{m_u^2} & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2 \beta_s^2}{m_u^2} \\ 0 & -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2 \beta_s^2}{m_u^2} & \frac{\bar{m}^3 \beta_s^3 - k_t \beta_s m_u (1 + \bar{m})}{m_u^3} - \frac{k_s}{m_s} \\ -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2 \beta_s^2}{m_u^2} & \frac{\bar{m}^3 \beta_s^3 - k_t \beta_s m_u (1 + \bar{m})}{m_u^3} & -\frac{k_s}{m_s} \end{bmatrix} \text{ Fully reachable}$$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

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# Linear Model Investigation

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Fully  
reachable, on  
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but  
numerically

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# Linear Model Investigation

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$$\mathbf{B}_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}$$

R =

1.0e+03 \*

0	0.0000	-0.0007	-0.0720
0.0000	-0.0007	-0.0720	4.2479
0	-0.0000	0.0006	0.0731
-0.0000	0.0006	0.0731	-3.9160

# Linear Model Investigation

Reachability of  $(\mathbf{A}, \mathbf{B}_1)$

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Fully  
reachable, on  
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$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$\mathbf{B}_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}$$

R =

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# Linear Model Investigation

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

Reachability of  $(A, B_1)$

$$R = [B_1 \quad \dots \quad A^3 B_1]$$

$$= \frac{1}{m_u} \begin{bmatrix} 0 & 0 & -1 & \frac{\bar{m}\beta_s}{m_u} \\ \bar{m} & -\frac{\bar{m}^2\beta_s}{m_u} & \frac{\bar{m}^3\beta_s^2 - k_t m_u}{m_u^2} & \frac{\bar{m}(2k_t\beta_s m_u + k_s m_u^2 - \bar{m}^3\beta_s^3)}{m_u^3} \\ 0 & -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} \\ -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} & \frac{\bar{m}^3\beta_s^3 - k_t\beta_s m_u(1 + \bar{m})}{m_u^3} - \frac{k_s}{m_s} \end{bmatrix}$$

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$$B_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}$$

$$R = \frac{1.0e+03}{\text{Normalised (by column)}} \bar{R}(:, i) = \frac{R(:, i)}{|R(:, i)|}$$

0	0.0000	-0.0007	-0.0720	0	0.0291	-0.0067	-0.0125
0.0000	-0.0007	-0.0720	4.2479	0.7629	-0.7623	-0.7018	0.7351
0	-0.0000	0.0006	0.0731	0	-0.0246	0.0057	0.0126
-0.0000	0.0006	0.0731	-3.9160	-0.6465	0.6461	0.7123	-0.6777

# Linear Model Investigation

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

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$$R = [B_1 \quad \dots \quad A^3 B_1]$$

$$\bar{m} = (m_s + m_u)/m_s$$

$$B_1 = \begin{bmatrix} 0 \\ \frac{m_s + m_u}{m_s m_u} \\ 0 \\ -\frac{1}{m_u} \end{bmatrix}$$

$$= \frac{1}{m_u} \begin{bmatrix} 0 & 0 & -1 & \frac{\bar{m}\beta_s}{m_u} \\ \bar{m} & -\frac{\bar{m}^2\beta_s}{m_u} & \frac{\bar{m}^3\beta_s^2 - k_t m_u}{m_u^2} & \frac{\bar{m}(2k_t\beta_s m_u + k_s m_u^2 - \bar{m}^3\beta_s^3)}{m_u^3} \\ 0 & -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} \\ -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} & \frac{\bar{m}^3\beta_s^3 - k_t\beta_s m_u(1 + \bar{m})}{m_u^3} - \frac{k_s}{m_s} \end{bmatrix}$$

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$$R = 1.0e+03 * \bar{R}(:, i) = \frac{R(:, i)}{|R(:, i)|}$$

Normalised (by column)

0	0.0000	-0.0007	-0.0720	0	0.0291	-0.0067	-0.0125
0.0000	-0.0007	-0.0720	4.2479	0.7629	-0.7623	-0.7018	0.7351
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# Linear Model Investigation

Reachability of  $(\mathbf{A}, \mathbf{B}_1)$

$$\mathbf{R} = [\mathbf{B}_1 \quad \cdots \quad \mathbf{A}^3 \mathbf{B}_1]$$

$$= \frac{1}{m_u} \begin{bmatrix} 0 & 0 & -1 & \frac{\bar{m}\beta_s}{m_u} \\ \bar{m} & -\frac{\bar{m}^2\beta_s}{m_u} & \frac{\bar{m}^3\beta_s^2 - k_t m_u}{m_u^2} & \frac{\bar{m}(2k_t\beta_s m_u + k_s m_u^2 - \bar{m}^3\beta_s^3)}{m_u^3} \\ 0 & -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} \\ -1 & \frac{\bar{m}\beta_s}{m_u} & \frac{k_t m_u - \bar{m}^2\beta_s^2}{m_u^2} & \frac{\bar{m}^3\beta_s^3 - k_t\beta_s m_u(1 + \bar{m})}{m_u^3} - \frac{k_s}{m_s} \end{bmatrix}$$

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# Linear Model Investigation

Observability of  $(\mathbf{A}, \mathbf{C})$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$
$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$



# Linear Model Investigation

Observability of  $(\mathbf{A}, \mathbf{C})$

$$\mathbf{O} = \begin{bmatrix} \mathbf{C} \\ \vdots \\ \mathbf{CA}^3 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{k_s \bar{m}}{m_u} & -\frac{\beta_s \bar{m}}{m_u} & \frac{k_t}{m_u} & 0 \\ \frac{\beta_s k_s \bar{m}^2}{m_u^2} & \frac{\beta_s^2 \bar{m}^2}{m_u^2} - \frac{k_s \bar{m}}{m_u} & -\frac{\beta_s k_t \bar{m}}{m_u^2} & \frac{k_t}{m_u} \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix}$$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

# Linear Model Investigation

Observability of  $(\mathbf{A}, \mathbf{C})$

$$\mathbf{O} = \begin{bmatrix} \mathbf{C} \\ \vdots \\ \mathbf{CA}^3 \end{bmatrix} \quad \text{Fully observable, on the paper ...}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{k_s \bar{m}}{m_u} & -\frac{\beta_s \bar{m}}{m_u} & \frac{k_t}{m_u} & 0 \\ \frac{\beta_s k_s \bar{m}^2}{m_u^2} & \frac{\beta_s^2 \bar{m}^2}{m_u^2} - \frac{k_s \bar{m}}{m_u} & -\frac{\beta_s k_t \bar{m}}{m_u^2} & \frac{k_t}{m_u} \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix}$$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

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# Linear Model Investigation

Observability of  $(A, C)$

$$O = \begin{bmatrix} C \\ \vdots \\ CA^3 \end{bmatrix} \quad \text{Fully observable, on the paper ... but numerically}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{k_s \bar{m}}{m_u} & -\frac{\beta_s \bar{m}}{m_u} & \frac{k_t}{m_u} & 0 \\ \frac{\beta_s k_s \bar{m}^2}{m_u^2} & \frac{\beta_s^2 \bar{m}^2}{m_u^2} - \frac{k_s \bar{m}}{m_u} & -\frac{\beta_s k_t \bar{m}}{m_u^2} & \frac{k_t}{m_u} \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix}$$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

1.0e+07 \*

0.0000	0	0	0
-0.0000	-0.0000	0	0
0	0.0000	0	0
0.0002	0.0000	-0.0014	0
-0.0000	-0.0000	0.0004	0
-0.0017	0.0001	0.0145	-0.0014
0.0011	0.0000	-0.0093	0.0004
-0.5311	-0.0349	5.2723	0.0145

# Linear Model Investigation

Observability of  $(A, C)$

$$O = \begin{bmatrix} C \\ \vdots \\ CA^3 \end{bmatrix} \quad \text{Fully observable, on the paper ... but numerically}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ -\frac{k_s \bar{m}}{m_u} & -\frac{\beta_s \bar{m}}{m_u} & \frac{k_t}{m_u} & 0 \\ \frac{\beta_s k_s \bar{m}^2}{m_u^2} & \frac{\beta_s^2 \bar{m}^2}{m_u^2} - \frac{k_s \bar{m}}{m_u} & -\frac{\beta_s k_t \bar{m}}{m_u^2} & \frac{k_t}{m_u} \\ \vdots & \vdots & \vdots & \vdots \end{bmatrix}$$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

1.0e+07 \*

0.0000	0	0	0
-0.0000	-0.0000	0	0
0	0.0000	0	0
0.0002	0.0000	-0.0014	0
-0.0000	-0.0000	0.0004	0
-0.0017	0.0001	0.0145	-0.0014
0.0011	0.0000	-0.0093	0.0004
-0.5311	-0.0349	5.2723	0.0145

# Linear Model Investigation

Observability of  $(\mathbf{A}, \mathbf{C})$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

$\mathbf{O} =$

1.0000	0	0	0
-0.9981	-0.0624	0	0
0	1.0000	0	0
0.1172	0.0029	-0.9931	0
-0.1172	-0.0073	0.9931	0
-0.1166	0.0041	0.9884	-0.0967
0.1171	0.0029	-0.9924	0.0378
-0.1002	-0.0066	0.9949	0.0027

Normalised (by rows)

$$\bar{O}(i,:) = \frac{O(i,:)}{|O(i,:)|}$$

1.0e+07 \*

0.0000	0	0	0
-0.0000	-0.0000	0	0
0	0.0000	0	0
0.0002	0.0000	-0.0014	0
-0.0000	-0.0000	0.0004	0
-0.0017	0.0001	0.0145	-0.0014
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# Linear Model Investigation

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-0.1002	-0.0066	0.9949	0.0027

Normalised (by rows)

$$\bar{O}(i,:) = \frac{O(i,:)}{|O(i,:)|}$$

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

1.0e+07 \*

0.0000	0	0	0
-0.0000	-0.0000	0	0
0	0.0000	0	0
0.0002	0.0000	-0.0014	0
-0.0000	-0.0000	0.0004	0
-0.0017	0.0001	0.0145	-0.0014
0.0011	0.0000	-0.0093	0.0004
-0.5311	-0.0349	5.2723	0.0145

# Linear Model Investigation

Observability of  $(A, C)$

$O =$

1.0000	0	0	0
-0.9981	-0.0624	0	0
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0.1172	0.0029	-0.9931	0
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Normalised (by rows)

$$\bar{O}(i,:) = \frac{O(i,:)}{|O(i,:)|}$$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k_s \frac{m_s + m_u}{m_s m_u} & -\beta_s \frac{m_s + m_u}{m_s m_u} & \frac{k_t}{m_u} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_s}{m_u} & \frac{\beta_s}{m_u} & -\frac{k_t}{m_u} & 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 \end{bmatrix}$$

1.0e+07 \*

0.0000	0	0	0
-0.0000	-0.0000	0	0
0	0.0000	0	0
0.0002	0.0000	-0.0014	0
-0.0000	-0.0000	0.0004	0
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0.0011	0.0000	-0.0093	0.0004
-0.5311	-0.0349	5.2723	0.0145

# Outline


- Motivations & Goals
- Non-linear 1D Model
- Control Problem Formulation
- Linearisation
- Linear Model Investigation
- Control Architecture
- Control Design
- Performance Evaluation





# Control System Architecture

- Open-loop BIBS (we want to modify the eig.s)
- Const. disturbance/reference
- No time-varying reference
- Non-fully measurable state




# Control System Architecture

- Open-loop BIBS (we want to modify the eig.s) 
  - Const. disturbance/reference
  - No time-varying reference
  - Non-fully measurable state
- Stabiliser





# Control System Architecture

- Open-loop BIBS (we want to modify the eig.s) 
  - Const. disturbance/reference 
  - No time-varying reference
  - Non-fully measurable state
- Stabiliser
  - Integral Action





# Control System Architecture

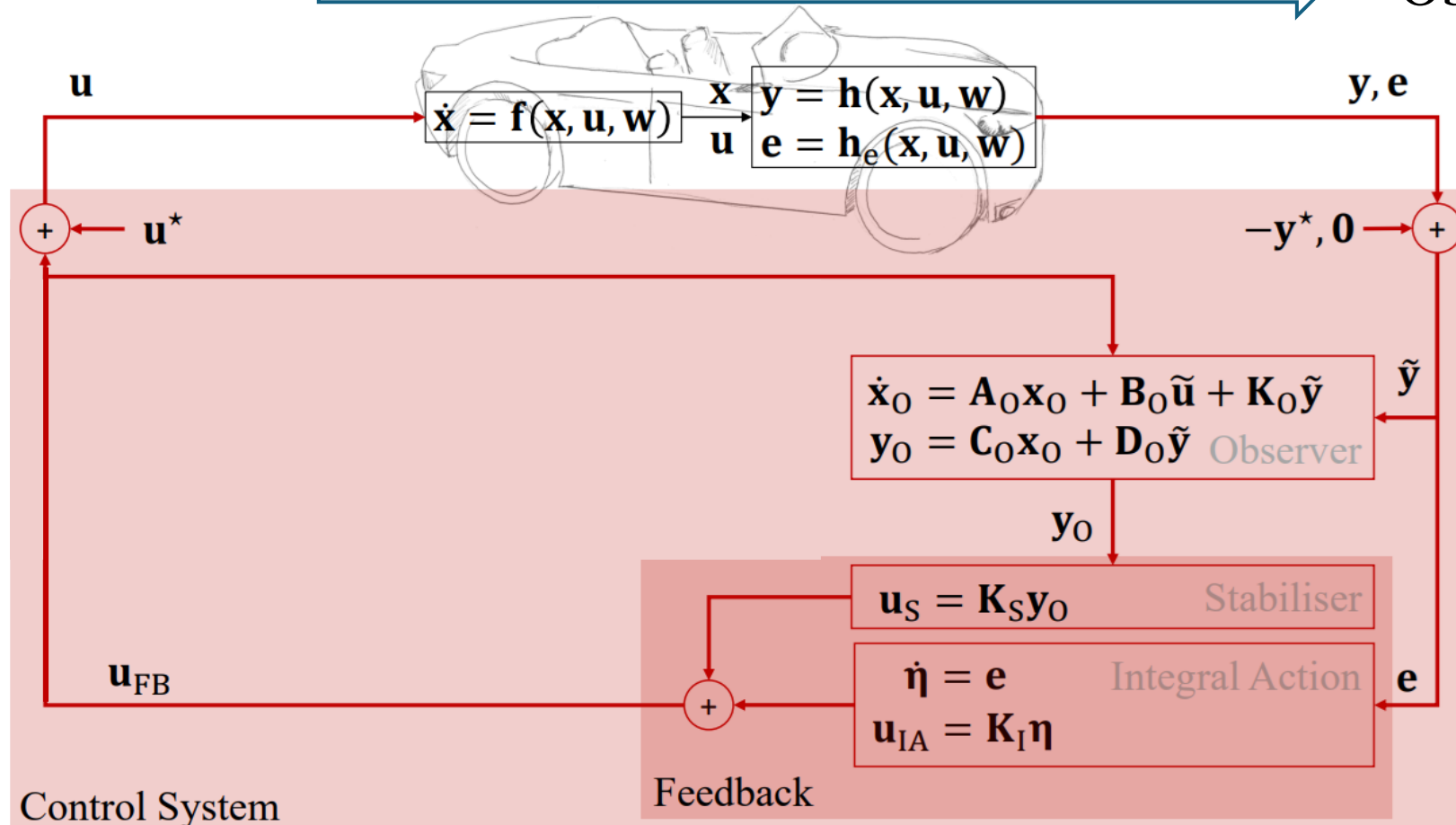
- Open-loop BIBS (we want to modify the eig.s) 
  - Const. disturbance/reference 
  - No time-varying reference 
  - Non-fully measurable state
- Stabiliser
  - Integral Action
  - No Feed-Forward

# Control System Architecture

- Open-loop BIBS (we want to modify the eig.s) 
  - Const. disturbance/reference 
  - No time-varying reference 
  - Non-fully measurable state 
- Stabiliser
  - Integral Action
  - No Feed-Forward
  - Observer

# Control System Architecture

- Open-loop BIBS (we want to modify the eig.s) 
  - Const. disturbance/reference 
  - No time-varying reference 
  - Non-fully measurable state 
- Stabiliser
  - Integral Action
  - No Feed-Forward
  - Observer



# Control System Architecture

Let the plant be

$$\begin{aligned}\dot{\mathbf{x}}_e &= \mathbf{A}_e \mathbf{x}_e + \mathbf{B}_e \tilde{u} \\ \epsilon &= \mathbf{C}_e \mathbf{x}_e + \mathbf{D}_e \tilde{u}\end{aligned}$$

where

$$\mathbf{A}_e = \begin{bmatrix} \mathbf{A} & \mathbf{0} \\ \mathbf{C}_e & \mathbf{0} \end{bmatrix}, \quad \mathbf{B}_e = \begin{bmatrix} \mathbf{B}_1 \\ \mathbf{0} \end{bmatrix} \quad \mathbf{C}_e = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}$$

We stabilise it through  $u_S = \mathbf{K}_e \mathbf{x}_O$ , with  $\mathbf{K}_e := [\mathbf{K}_S \quad k_I]$ , such that  $\mathbf{A}_e + \mathbf{B}_e \mathbf{K}_e$  is Hurwitz.

The integral action is computed as

$$\begin{aligned}\dot{\eta} &= \tilde{e} \\ u_{IA} &= k_I \eta\end{aligned}$$

Finally,  $\tilde{u} = u_S + u_{IA}$ .

The observer takes the form  $\dot{\mathbf{x}}_O = (\mathbf{A} + \mathbf{K}_O \mathbf{C}) \mathbf{x}_O + \mathbf{B}_1 \tilde{u} + \mathbf{K}_O \tilde{y}$

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# Control Design

Let the plant be  $\dot{\mathbf{x}}_e = \mathbf{A}_e \mathbf{x}_e + \mathbf{B}_e \tilde{u}$   
 $\boldsymbol{\epsilon} = \mathbf{C}_e \mathbf{x}_e + \mathbf{D}_e \tilde{u}$

to which we associate the cost function  $J = \int_{t_0}^{\infty} \boldsymbol{\epsilon}^T \mathbf{Q} \boldsymbol{\epsilon} + R \tilde{u}^2 dt$

With  $\mathbf{A}_e = \begin{bmatrix} \mathbf{A} & \mathbf{0} \\ \mathbf{C}_e & \mathbf{0} \end{bmatrix}$ ,  $\mathbf{B}_e = \begin{bmatrix} \mathbf{B}_1 \\ \mathbf{0} \end{bmatrix}$   $\alpha \geq 0$ ,  $R > 0$ , and  $\mathbf{Q} = \mathbf{Q}^T \succeq 0$

Take

1) Comfort  $\boldsymbol{\epsilon}_1 = \begin{bmatrix} -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 & 0 \end{bmatrix} \mathbf{x}_e + m_s^{-1} u$

2) Race  $\boldsymbol{\epsilon}_2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \end{bmatrix} \mathbf{x}_e$

3) Off-road  $\boldsymbol{\epsilon}_3 = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 \end{bmatrix} \mathbf{x}_e.$

# Control Design

Impose  $\epsilon = \text{col}(\epsilon_1, \epsilon_2, x_2, \epsilon_3, x_4, \eta)$

$$\mathbf{C}_\epsilon = \begin{bmatrix} -\frac{k_s}{m_s} & -\frac{\beta_s}{m_s} & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}, \quad \mathbf{D}_\epsilon = \begin{bmatrix} m_s^{-1} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{Q} := 1/6 \text{diag}(|\epsilon_{1\max}|^{-2}, \dots, |\epsilon_{6\max}|^{-2})$$

Take

1) Comfort  $|\epsilon_{1\max}| \ll |\epsilon_{2\max}|, |\epsilon_{3\max}|$

2) Race  $|\epsilon_{2\max}| \ll |\epsilon_{1\max}|, |\epsilon_{3\max}|$

3) Off-road  $|\epsilon_{3\max}| \ll |\epsilon_{1\max}|, |\epsilon_{2\max}|$

Remember  $\bar{R} = R + \mathbf{D}_\epsilon^\top \mathbf{Q} \mathbf{D}_\epsilon$   
 $\bar{R} = R + (1/3)m_s^{-2} |\epsilon_{1\max}|^{-2}$

# Control Design

As for the observer

$$\mathbf{Q}_d := \text{diag}(q_1, q_2, r_1, r_2, 0)$$

$$\mathbf{R}_d = \mathbf{0}$$

Where we assume

$$\begin{aligned} \mathbb{E}[\ddot{z}_r(t)\ddot{z}_r(\tau)] &= q_1\delta(t-\tau) & \mathbb{E}[f_d(t)f_d(\tau)] &= q_2\delta(t-\tau) \\ \mathbb{E}[\nu_p(t)\nu_p(\tau)] &= r_1\delta(t-\tau) & \mathbb{E}[\nu_a(t)\nu_a(\tau)] &= r_2\delta(t-\tau) \end{aligned}$$

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# Performance Evaluation

## Settings

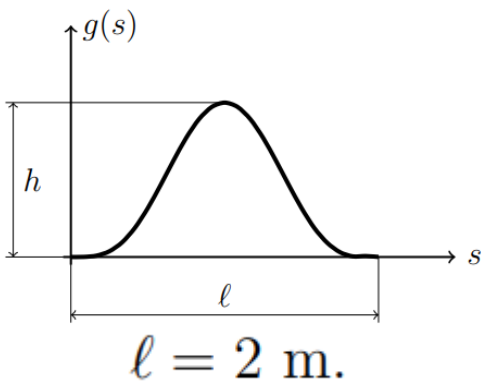
Symbol	Unit	Value		
		Comfort	Race	Off-road
$\epsilon_1$	$\text{m/s}^2$	$0.1g$	$10g$	$10g$
$\epsilon_{2_{\max}}$	m	$10^4$	$10^{-1}$	$10^4$
$\epsilon_{3_{\max}}$	$\text{m/s}$	$10^4$	$10^4$	$5 \cdot 10^{-3}$
$\epsilon_{4_{\max}}$	m	$10^2$	$2.5 \cdot 10^{-3}$	$2.5 \cdot 10^{-3}$
$\epsilon_{5_{\max}}$	$\text{m/s}$	$10^{-1}$	$10^{-2}$	$5 \cdot 10^{-3}$
$\epsilon_{6_{\max}}$	m s	$10^{-1}$	$10^{-2}$	$10^{-2}$
$u_{\max}$	N	$10^3$	$10^3$	$10^3$
$r_1$	$\text{m}^2$	$(10^{-3})^2$	$(10^{-3})^2$	$(10^{-3})^2$
$r_2$	$\text{m}^2/\text{s}^4$	$(0.05g)^2$	$(0.05g)^2$	$(0.05g)^2$
$q_1$	$\text{m}^2/\text{s}^4$	1	1	1
$q_2$	$\text{N}^2$	1	1	1

# Performance Evaluation

Comfort

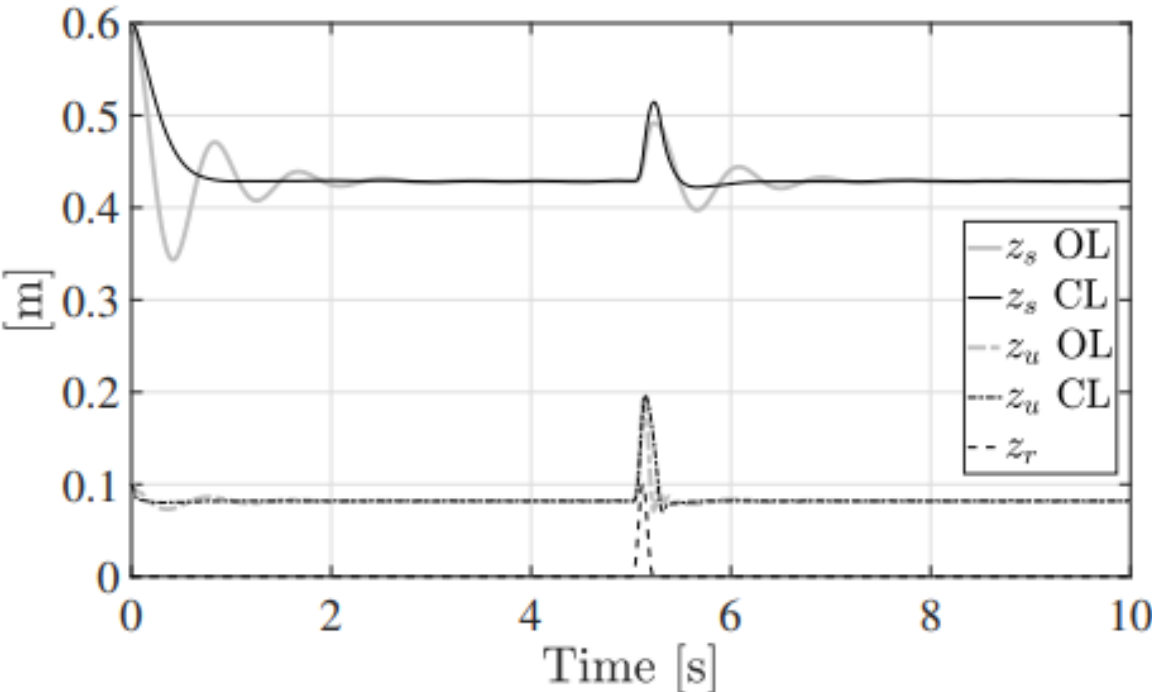
Bump

$v(t) = v_0 = 30 \text{ km/h}, h = 10 \text{ cm}$

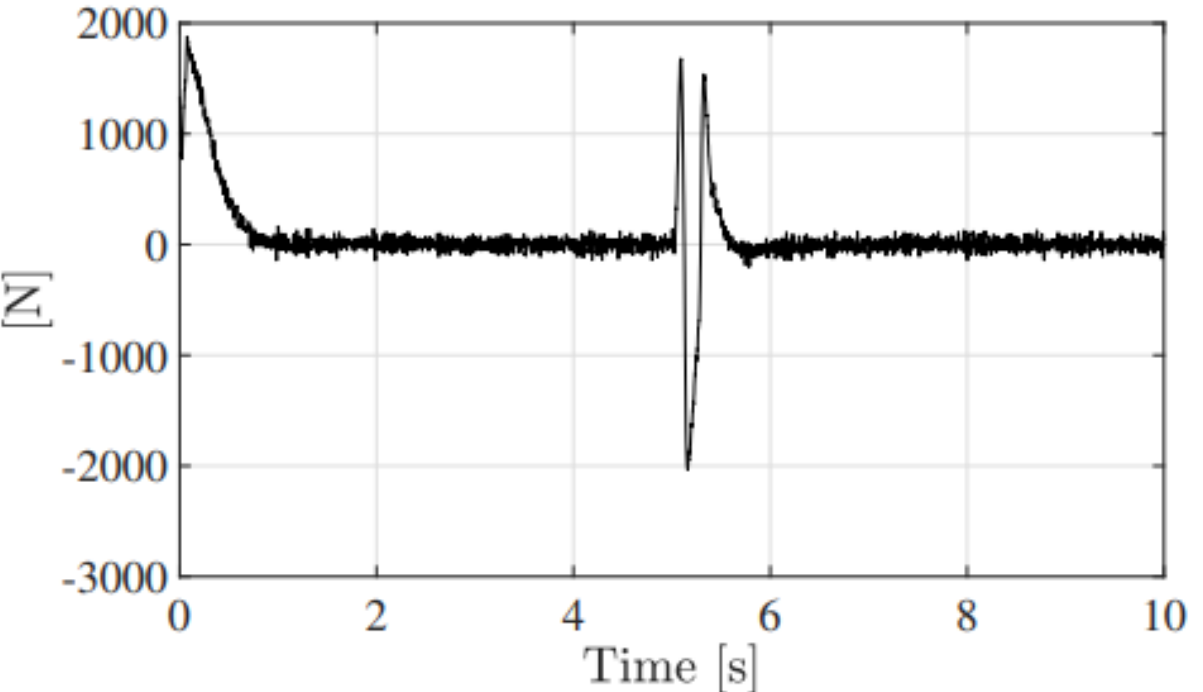


Symbol	Unit	Comfort	Value Race	Off-road
$\epsilon_1$	m/s <sup>2</sup>	0.1g	10g	10g
$\epsilon_{2_{\max}}$	m	10 <sup>4</sup>	10 <sup>-1</sup>	10 <sup>4</sup>
$\epsilon_{3_{\max}}$	m/s	10 <sup>4</sup>	10 <sup>4</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{4_{\max}}$	m	10 <sup>2</sup>	2.5 · 10 <sup>-3</sup>	2.5 · 10 <sup>-3</sup>
$\epsilon_{5_{\max}}$	m/s	10 <sup>-1</sup>	10 <sup>-2</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{6_{\max}}$	m s	10 <sup>-1</sup>	10 <sup>-2</sup>	10 <sup>-2</sup>
$u_{\max}$	N	10 <sup>3</sup>	10 <sup>3</sup>	10 <sup>3</sup>
$r_1$	m <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>
$r_2$	m <sup>2</sup> /s <sup>4</sup>	(0.05g) <sup>2</sup>	(0.05g) <sup>2</sup>	(0.05g) <sup>2</sup>
$q_1$	m <sup>2</sup> /s <sup>4</sup>	1	1	1
$q_2$	N <sup>2</sup>	1	1	1

Non-linear Plant



Control law  $\tilde{u}$

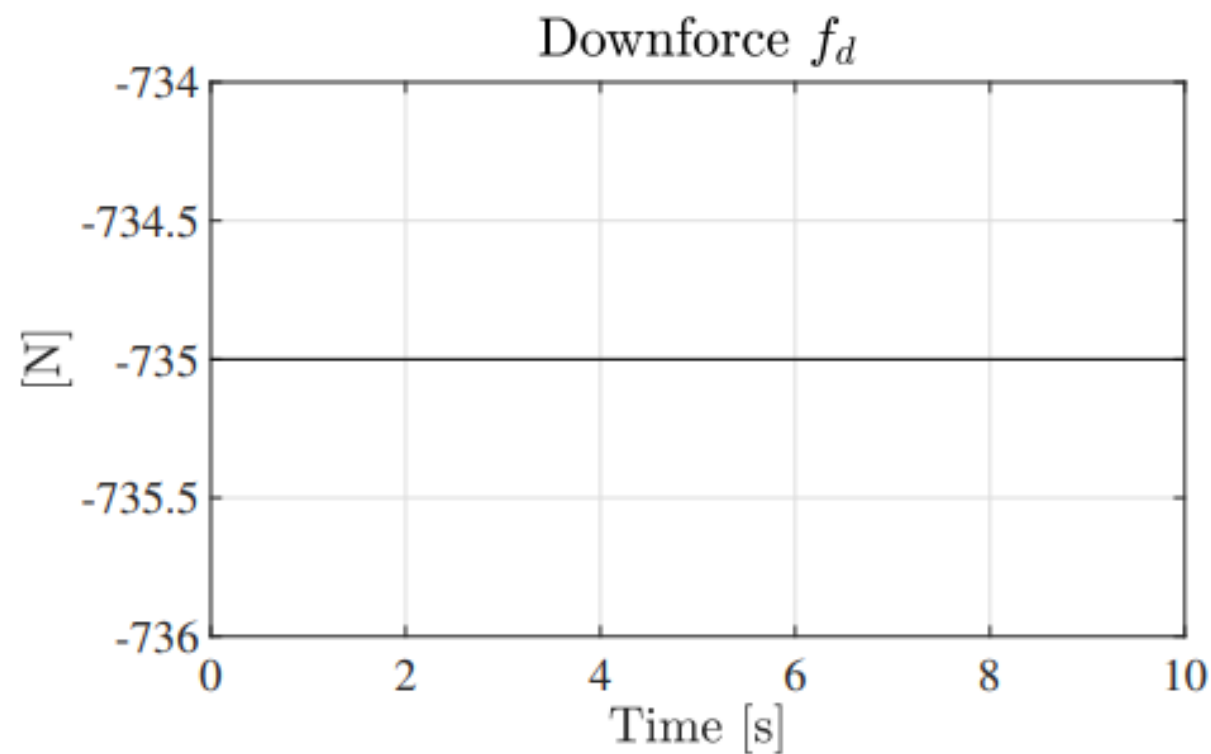
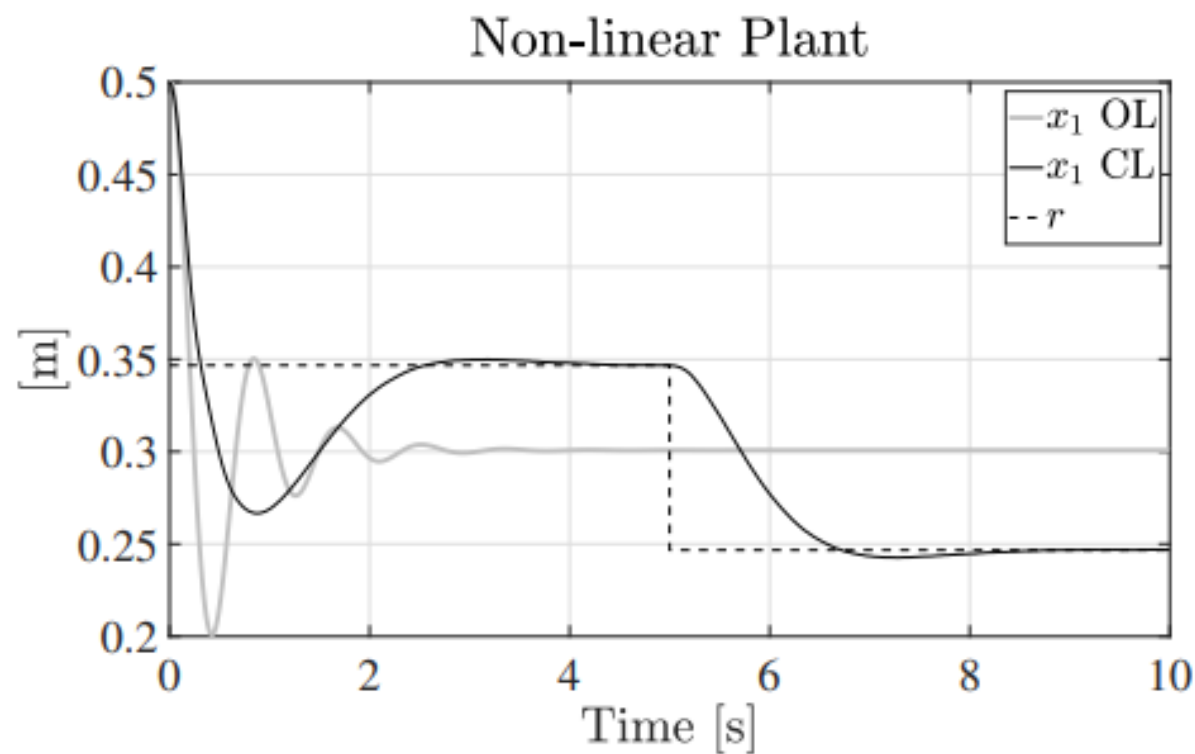


# Performance Evaluation

Race

Target = suspension length (piecewise constant)

Symbol	Unit	Comfort	Value	
			Race	Off-road
$\epsilon_1$	m/s <sup>2</sup>	0.1 <i>g</i>	10 <i>g</i>	10 <i>g</i>
$\epsilon_{2_{\max}}$	m	10 <sup>4</sup>	10 <sup>-1</sup>	10 <sup>4</sup>
$\epsilon_{3_{\max}}$	m/s	10 <sup>4</sup>	10 <sup>4</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{4_{\max}}$	m	10 <sup>2</sup>	2.5 · 10 <sup>-3</sup>	2.5 · 10 <sup>-3</sup>
$\epsilon_{5_{\max}}$	m/s	10 <sup>-1</sup>	10 <sup>-2</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{6_{\max}}$	m s	10 <sup>-1</sup>	10 <sup>-2</sup>	10 <sup>-2</sup>
$u_{\max}$	N	10 <sup>3</sup>	10 <sup>3</sup>	10 <sup>3</sup>
$r_1$	m <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>
$r_2$	m <sup>2</sup> /s <sup>4</sup>	(0.05 <i>g</i> ) <sup>2</sup>	(0.05 <i>g</i> ) <sup>2</sup>	(0.05 <i>g</i> ) <sup>2</sup>
$q_1$	m <sup>2</sup> /s <sup>4</sup>	1	1	1
$q_2$	N <sup>2</sup>	1	1	1

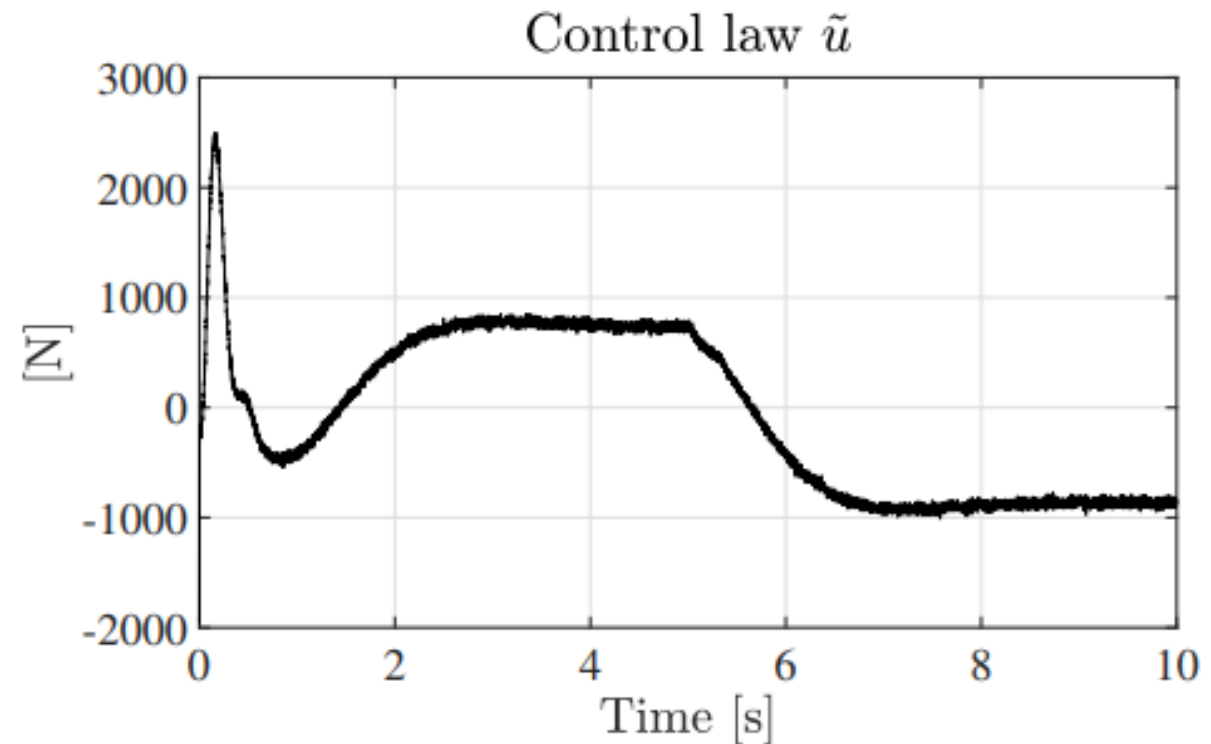
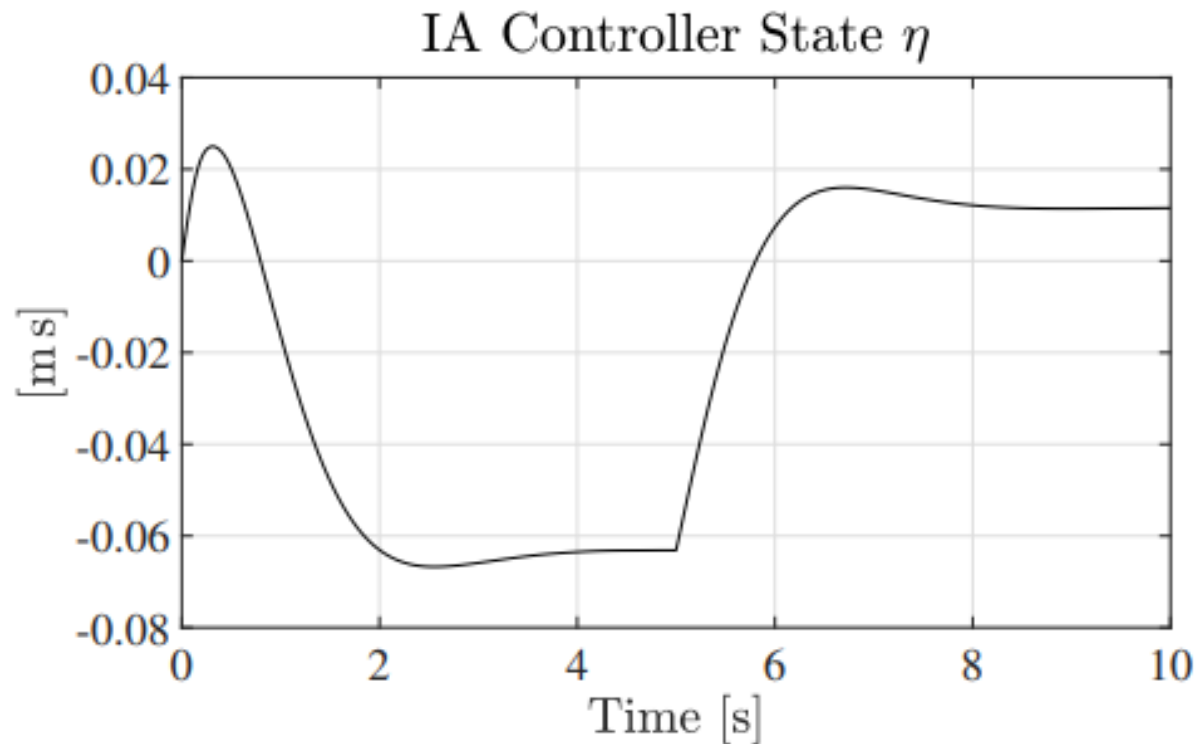


# Performance Evaluation

## Race

Target = suspension length (piecewise constant)

Symbol	Unit	Comfort	Value	
			Race	Off-road
$\epsilon_1$	m/s <sup>2</sup>	0.1g	10g	10g
$\epsilon_{2\max}$	m	10 <sup>4</sup>	10 <sup>-1</sup>	10 <sup>4</sup>
$\epsilon_{3\max}$	m/s	10 <sup>4</sup>	10 <sup>4</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{4\max}$	m	10 <sup>2</sup>	2.5 · 10 <sup>-3</sup>	2.5 · 10 <sup>-3</sup>
$\epsilon_{5\max}$	m/s	10 <sup>-1</sup>	10 <sup>-2</sup>	5 · 10 <sup>-3</sup>
$\epsilon_{6\max}$	m s	10 <sup>-1</sup>	10 <sup>-2</sup>	10 <sup>-2</sup>
$u_{\max}$	N	10 <sup>3</sup>	10 <sup>3</sup>	10 <sup>3</sup>
$r_1$	m <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>	(10 <sup>-3</sup> ) <sup>2</sup>
$r_2$	m <sup>2</sup> /s <sup>4</sup>	(0.05g) <sup>2</sup>	(0.05g) <sup>2</sup>	(0.05g) <sup>2</sup>
$q_1$	m <sup>2</sup> /s <sup>4</sup>	1	1	1
$q_2$	N <sup>2</sup>	1	1	1



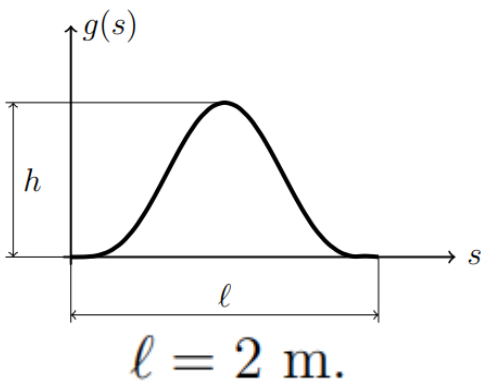


# Performance Evaluation

Off-road

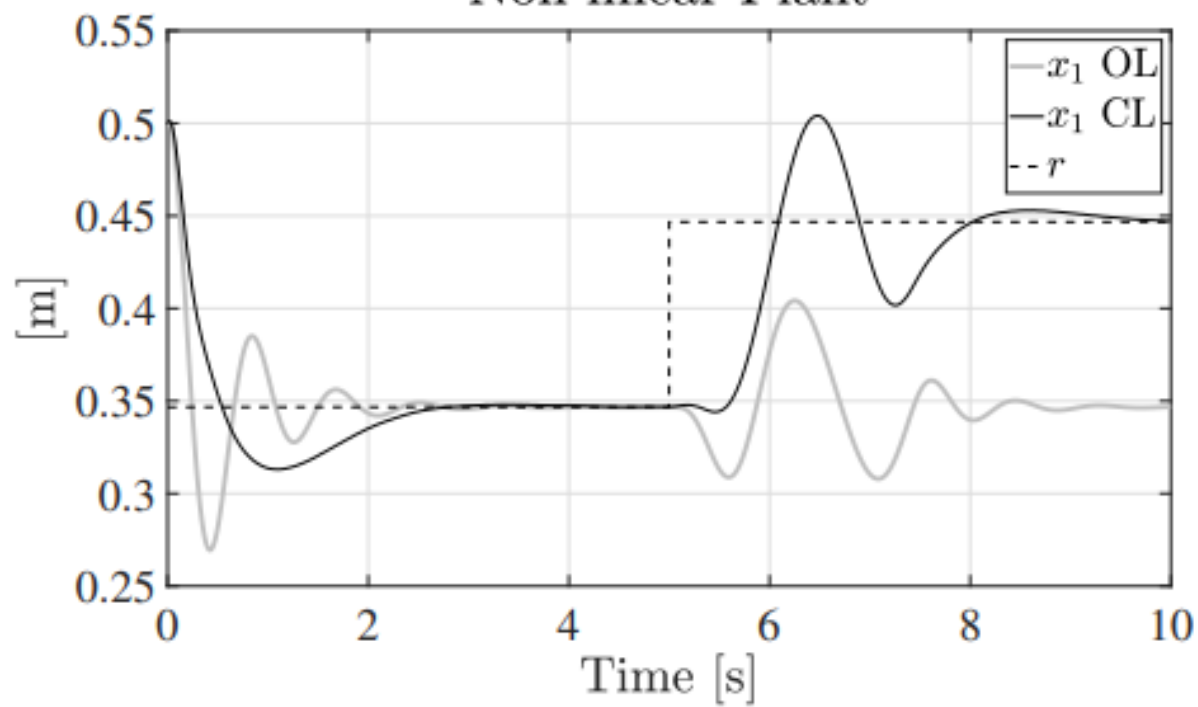
Target = tire deflection  
+ longer suspension (const.)

$v(t) = v_0 = 3 \text{ km/h}, h = 50 \text{ cm}$

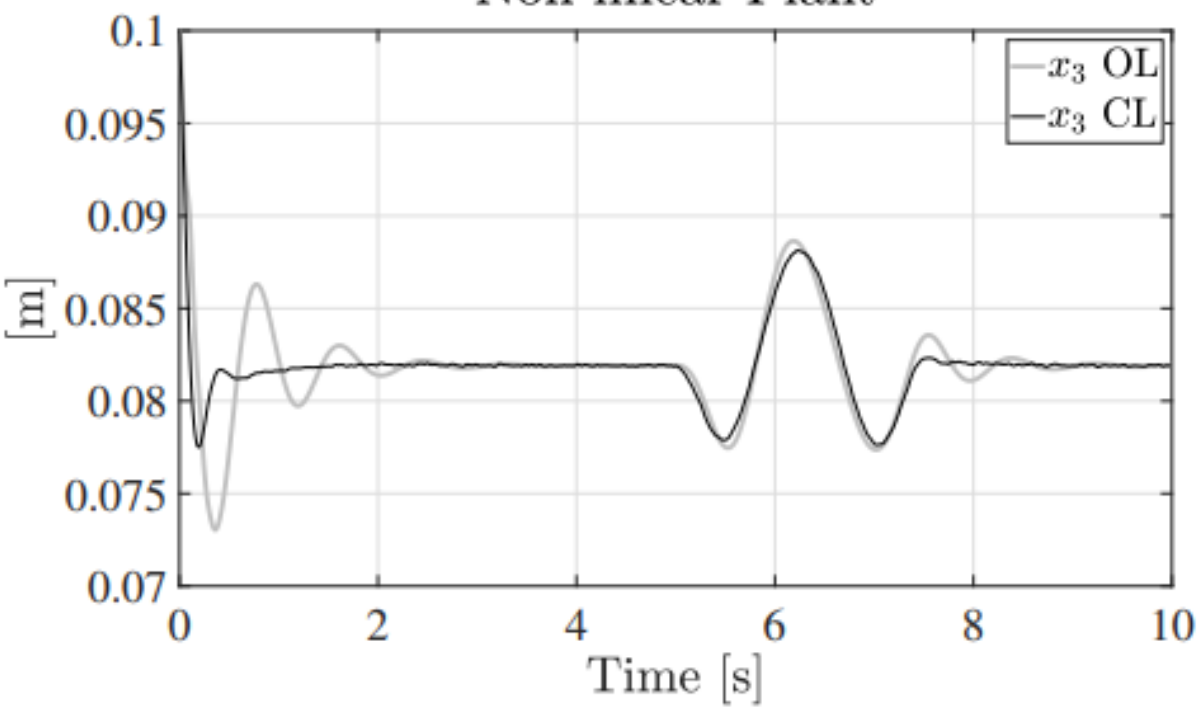


Symbol	Unit	Comfort	Value	Off-road
		Race		
$\epsilon_1$	$\text{m/s}^2$	$0.1g$	$10g$	$10g$
$\epsilon_{2\max}$	m	$10^4$	$10^{-1}$	$10^4$
$\epsilon_{3\max}$	m/s	$10^4$	$10^4$	$5 \cdot 10^{-3}$
$\epsilon_{4\max}$	m	$10^2$	$2.5 \cdot 10^{-3}$	$2.5 \cdot 10^{-3}$
$\epsilon_{5\max}$	m/s	$10^{-1}$	$10^{-2}$	$5 \cdot 10^{-3}$
$\epsilon_{6\max}$	m s	$10^{-1}$	$10^{-2}$	$10^{-2}$
$u_{\max}$	N	$10^3$	$10^3$	$10^3$
$r_1$	$\text{m}^2$	$(10^{-3})^2$	$(10^{-3})^2$	$(10^{-3})^2$
$r_2$	$\text{m}^2/\text{s}^4$	$(0.05g)^2$	$(0.05g)^2$	$(0.05g)^2$
$q_1$	$\text{m}^2/\text{s}^4$	1	1	1
$q_2$	$\text{N}^2$	1	1	1

Non-linear Plant



Non-linear Plant

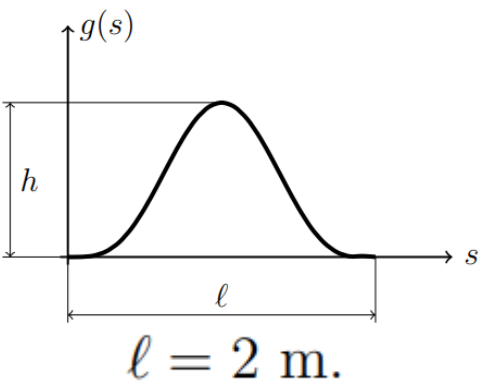


# Performance Evaluation

Off-road

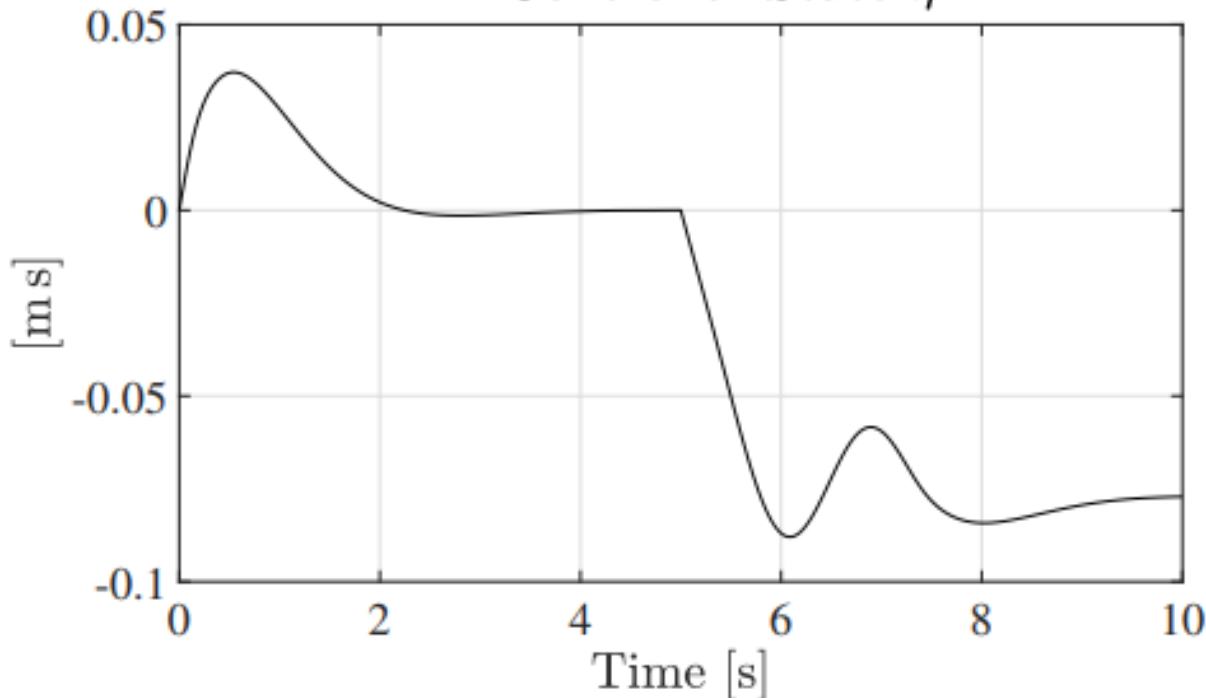
Target = tire deflection  
+ longer suspension (const.)

$v(t) = v_0 = 3 \text{ km/h}$ ,  $h = 50 \text{ cm}$



Symbol	Unit	Comfort	Value	Race	Off-road
$\epsilon_1$	$\text{m/s}^2$	$0.1g$	$10g$		$10g$
$\epsilon_{2\max}$	m	$10^4$	$10^{-1}$		$10^4$
$\epsilon_{3\max}$	$\text{m/s}$	$10^4$	$10^4$		$5 \cdot 10^{-3}$
$\epsilon_{4\max}$	m	$10^2$	$2.5 \cdot 10^{-3}$		$2.5 \cdot 10^{-3}$
$\epsilon_{5\max}$	$\text{m/s}$	$10^{-1}$	$10^{-2}$		$5 \cdot 10^{-3}$
$\epsilon_{6\max}$	m s	$10^{-1}$	$10^{-2}$		$10^{-2}$
$u_{\max}$	N	$10^3$	$10^3$		$10^3$
$r_1$	$\text{m}^2$	$(10^{-3})^2$	$(10^{-3})^2$		$(10^{-3})^2$
$r_2$	$\text{m}^2/\text{s}^4$	$(0.05g)^2$	$(0.05g)^2$		$(0.05g)^2$
$q_1$	$\text{m}^2/\text{s}^4$	1	1		1
$q_2$	$\text{N}^2$	1	1		1

IA Controller State  $\eta$



Control law  $\tilde{u}$

