



ELEKTRONIČKI ELEMENTI I SKLOPOVI

Predavanje 6

**BIPOLARNI TRANZISTOR – Ebers-Mollov
model**

UNIPOLARNI TRANZISTOR

Ebers-Mollove jednadžbe i model tranzistora

$$I_E = a_{11} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] + a_{12} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$
$$I_C = a_{21} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] + a_{22} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$

$$a_{11} = S \cdot q \cdot \left(\frac{D_{nB} \cdot n_{0B}}{w_B} + \frac{D_{pE} \cdot p_{0E}}{L_{pE}} \right)$$

$$a_{22} = S \cdot q \cdot \left(\frac{D_{nB} \cdot n_{0B}}{w_B} + \frac{D_{pC} \cdot p_{0C}}{L_{pC}} \right)$$

$$a_{12} = a_{21} = -S \cdot q \cdot D_{nB} \cdot \frac{n_{0B}}{w_B}$$

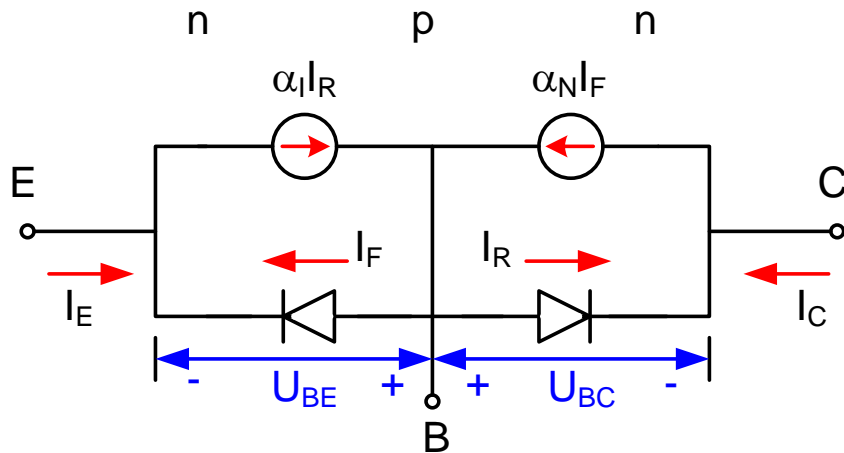
(svojstvo recipročnosti!)

a_{11} jest struja $I_E = I_{ES}$ pri $U_{BC}=0$ i $U_{BE}<0$

a_{22} jest struja $I_C = I_{CS}$ pri $U_{BE}=0$ i $U_{BC}<0$



Injekcijski Ebers-Mollov model



$$I_E - \alpha_I I_R + I_F = 0 \quad (1)$$

$$I_C - \alpha_N I_F + I_R = 0 \quad (2)$$

$$I_F = I_{ES} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] \quad (3)$$

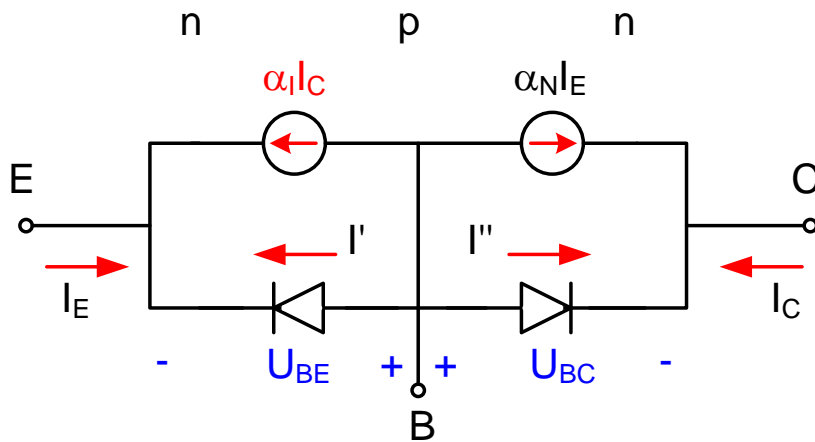
$$I_R = I_{CS} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right] \quad (4)$$

$$I_E = -I_{ES} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] + \alpha_I I_{CS} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$

$$I_C = \alpha_N I_{ES} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] - I_{CS} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$



Ebers-Mollov model npn tranzistora



$$I_E + \alpha_I I_C + I' = 0$$

$$I_C + \alpha_N I_E + I'' = 0$$

$$I' = I_{EB0} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right]$$

$$I'' = I_{CB0} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$

$$I_E = -\frac{I_{EB0}}{1 - \alpha_I \alpha_N} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] + \frac{\alpha_I I_{CB0}}{1 - \alpha_I \alpha_N} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$

$$I_C = \frac{\alpha_N I_{EB0}}{1 - \alpha_I \alpha_N} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] - \frac{I_{CB0}}{1 - \alpha_I \alpha_N} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right]$$

$$I_{ES} = \frac{I_{EB0}}{1 - \alpha_I \alpha_N} \quad I_{CS} = \frac{I_{CB0}}{1 - \alpha_I \alpha_N}$$

$$I_C = \alpha_N I_E + I_{CB0}$$

$$I_E = \alpha_I I_C + I_{EB0}$$

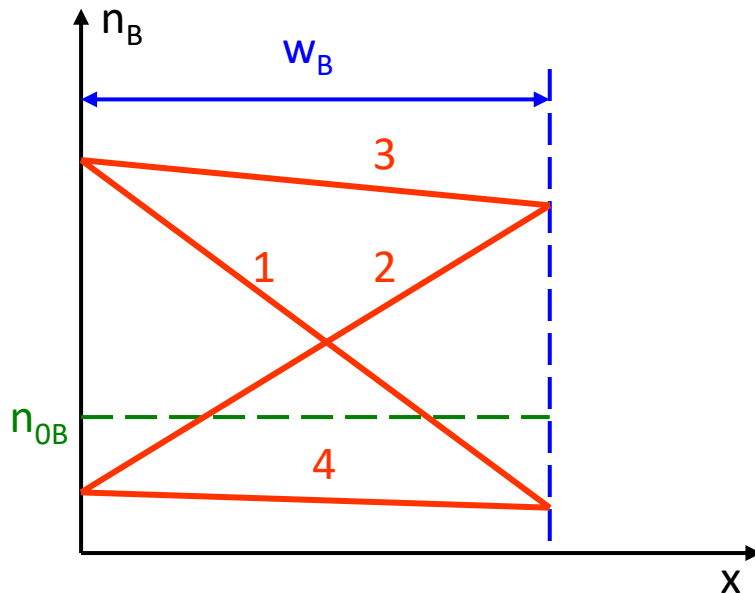
$$I_{CB0} = I_C \quad (uz \ I_E = 0)$$

$$I_{EB0} = I_E \quad (uz \ I_C = 0)$$



Područja rada tranzistora

- Raspodjela manjinskih nosilaca u bazi npn tranzistora u različitim područjima rada:



- 1 – normalno aktivno područje
- 2 – inverzno aktivno područje
- 3 – područje zasićenja
- 4 – zaporno područje



Normalno aktivno područje

$$U_{BE} \gg U_T, U_{BC} < 0$$

$$I_E = -I_{ES} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] - \alpha_I I_{CS} \quad (1)$$

$$I_C = \alpha_N I_{ES} \left[\exp\left(\frac{U_{BE}}{U_T}\right) - 1 \right] + I_{CS} \quad (2)$$

Iz (1) i (2) slijedi funkcija $I_C = f(I_E)$:

$$I_C = -\alpha_N I_E + \underbrace{I_{CS}(1 - \alpha_N \alpha_I)}_{I_{CB0}}$$

$$I_C = -\alpha_N I_E + I_{CB0}$$



Inverzno aktivno područje

$$U_{BE} < 0, U_{BC} > U_T$$

$$I_E = I_{ES} + \alpha_I I_{CS} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right] \quad (1)$$

$$I_C = \alpha_N I_{ES} - I_{CS} \left[\exp\left(\frac{U_{BC}}{U_T}\right) - 1 \right] \quad (2)$$

Iz (1) i (2) slijedi funkcija $I_E = f(I_C)$:

$$I_E = -\alpha_I I_C + I_{EB0}$$

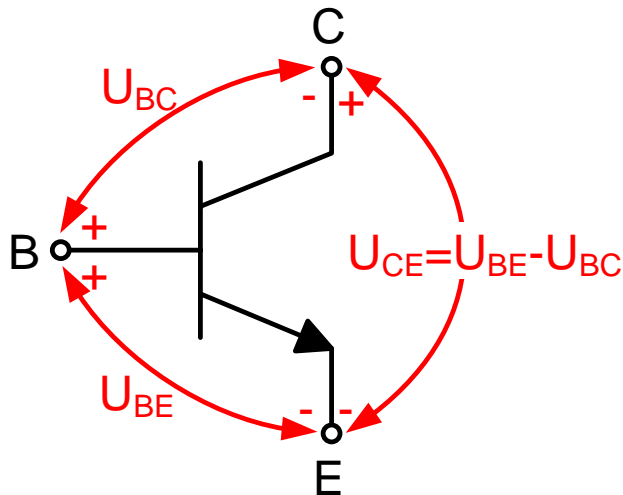


Područje zasićenja

$$U_{BE} > 0, U_{BC} > 0$$

$$U_{BC} = U_T \cdot \ln \frac{I_C + \alpha_N I_E - I_{CB0}}{-I_{CB0}}$$

$$U_{BE} = U_T \cdot \ln \frac{I_E + \alpha_I I_C - I_{EB0}}{-I_{EB0}}$$



$$U_{CE} = U_T \cdot \ln \frac{(I_E + \alpha_I I_C - I_{EB0}) \cdot \alpha_N}{(I_C + \alpha_N I_E - I_{CB0}) \cdot \alpha_I}$$



Zaporno područje

$$U_{BE} < 0, U_{BC} < 0$$

$$I_E = \frac{I_{EB0}}{1 - \alpha_N \alpha_I} (1 - \alpha_N)$$

$$I_C = \frac{I_{CB0}}{1 - \alpha_N \alpha_I} (1 - \alpha_I)$$

Unatoč nepropusnoj polarizaciji kroz oba spojišta teku male struje emitera i kolektora.

Stoga se zaporno područje definira uvjetom: $I_E = 0$; $U_{BC} < 0$ te je $I_C = I_{CB0}$

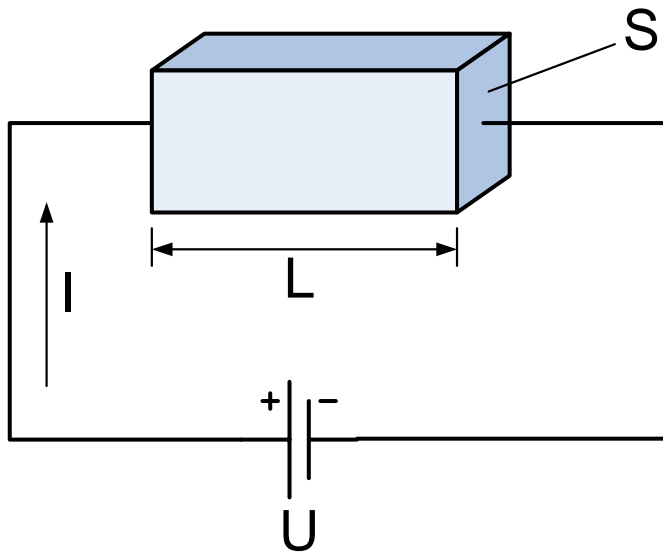
Uz ove uvjete iz Ebers-Mollovih jednadžbi dobiva se odgovarajući napon U_{BE} :

$$U_{BE} = U_T \cdot \ln(1 - \alpha_N) \quad \text{Npr. za } \alpha = 0,9 \text{ pri } T = 300 \text{ K}$$

$$U_{BE} = -59,5 \text{ mV}$$



UNIPOLARNI TRANZISTOR



$$R = \rho \cdot \frac{L}{S}$$

$$I = \frac{U}{R}$$

$$\frac{1}{\rho} = \sigma = n \cdot q \cdot \mu$$

Field Effect Transistor (**FET**)

Metal Oxide Semiconductor FET (**MOSFET**)

Insulated Gate FET (**IGFET**)

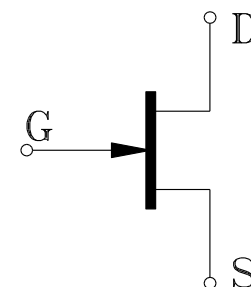
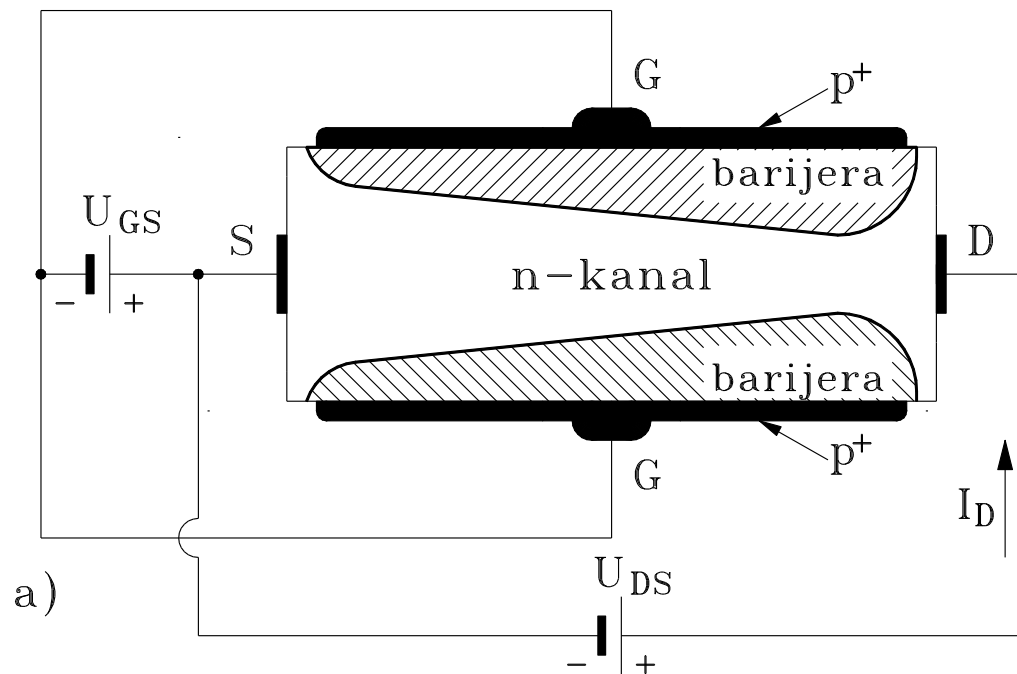


Unipolarni tranzistor (Tranzistor s efektom polja)

- U vođenju struje sudjeluju ili **elektroni** ili **šupljine**.
- Dio poluvodiča kroz koji teče struja naziva se KANAL:
 - p-kanalni
 - n-kanalni
- Protjecanjem struje kroz kanal upravlja se vanjskim naponom, tj. električnim poljem – tranzistor s efektom polja.
- Prvi unipolarni tranzistori bili su **spojni** unipolarni tranzistori – JFET (Junction Field Effect Transistor).

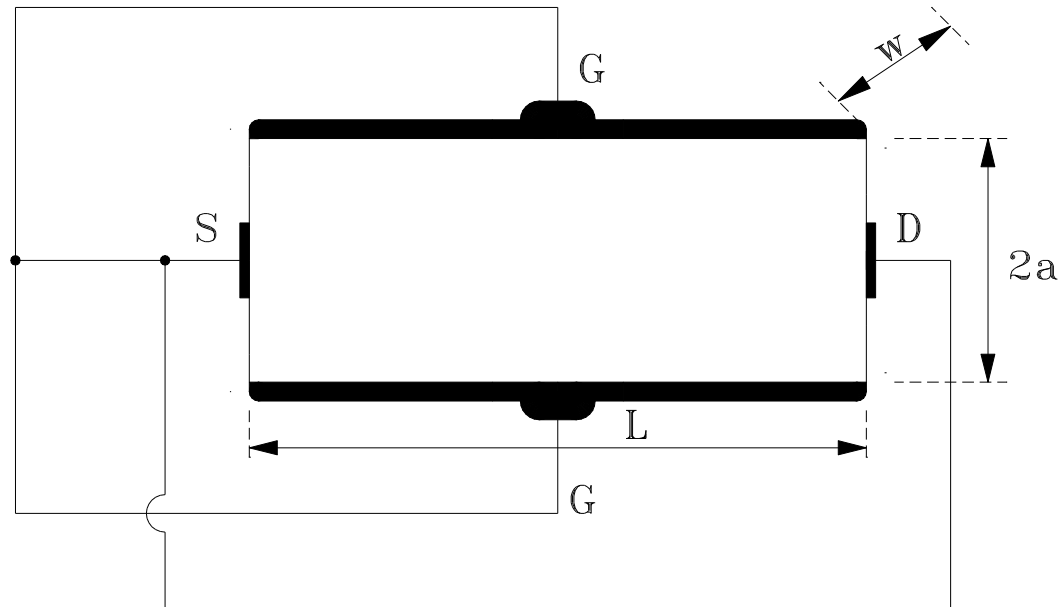


Tranzistor s efektom polja (JFET)



a) n-kanalni spojni FET; b) električni simbol za n-kanalni spojni FET

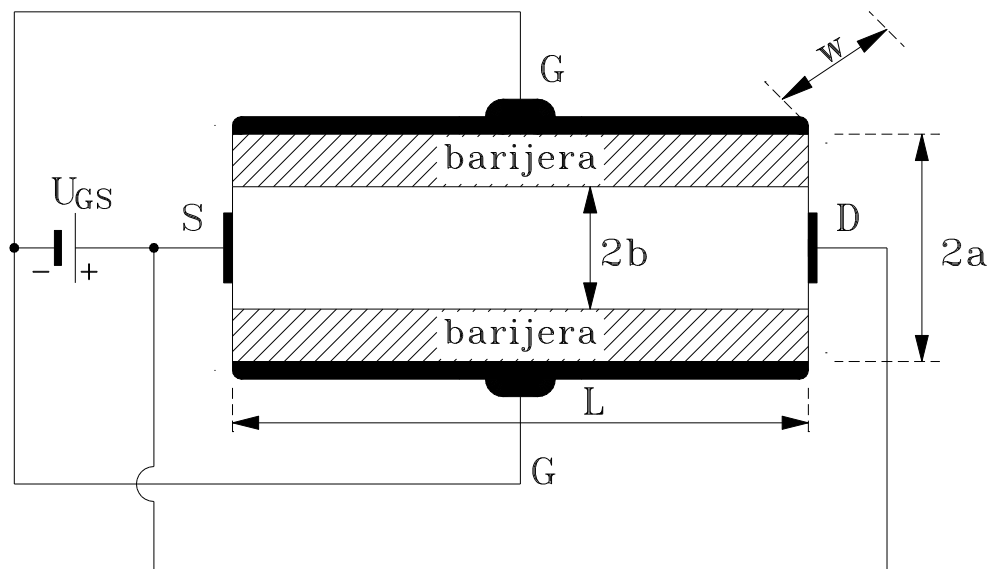




Širina potpuno otvorenog kanala pri $U_{DS}=0$ i $U_{GS}=0$

$$G_0 = \frac{1}{R_0} = \frac{q \cdot \mu_n \cdot N_D \cdot 2a \cdot w}{L} = \sigma \cdot \frac{2a \cdot w}{L}$$





Širina kanala pri nekom naponu U_{GS} i $U_{DS}=0$

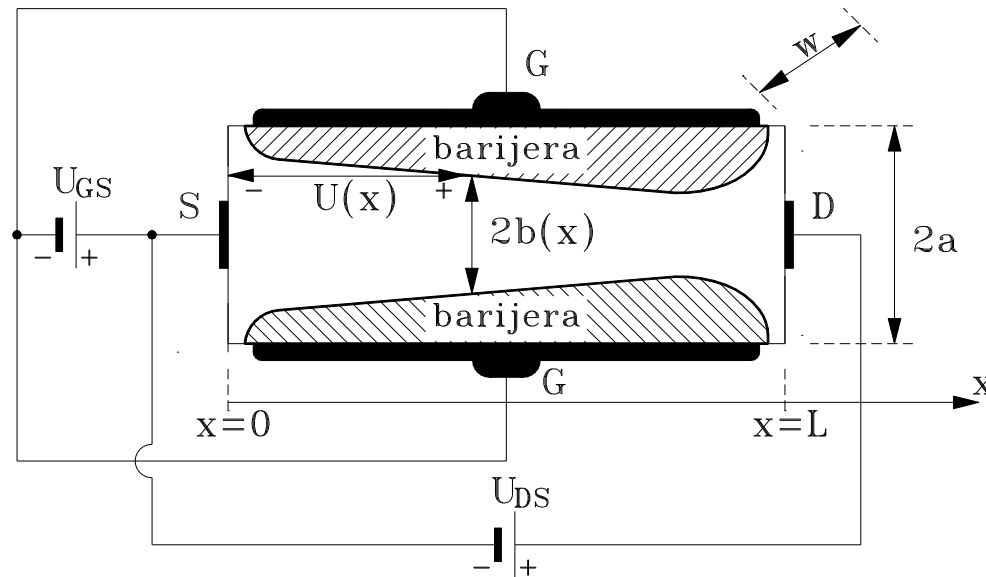
$$a - b = \sqrt{\frac{2 \cdot \varepsilon \cdot (U_k - U_{GS})}{q \cdot N_D}}$$

$$U_{GS0} = U_k - \frac{a^2 \cdot q \cdot N_D}{2 \cdot \varepsilon}$$

$$a^2 = \frac{2 \cdot \varepsilon \cdot (U_k - U_{GS0})}{q \cdot N_D}$$

$$b = a \cdot \left(1 - \sqrt{\frac{U_k - U_{GS}}{U_k - U_{GS0}}} \right)$$





Širina kanala pri nekom naponu $U_{GS} \neq 0$ i $U_{DS} \neq 0$

$$b(x) = a \cdot \left(1 - \sqrt{\frac{U_k - U_{GS} + U(x)}{U_k - U_{GS0}}} \right)$$

$$I_D(x) = I_D = 2b(x) \cdot w \cdot q \cdot N_D \frac{dU(x)}{dx}$$



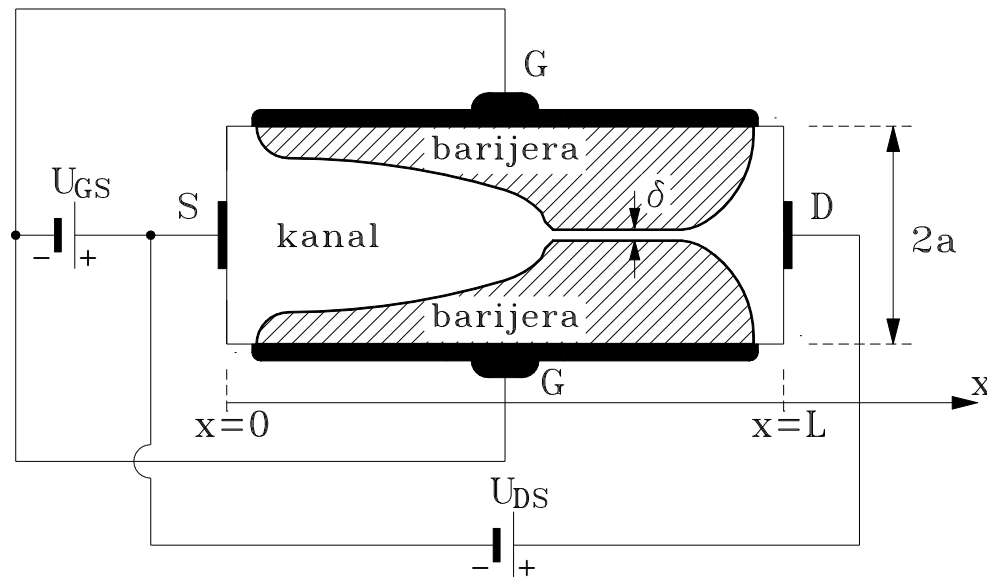
$$I_D = 2a \cdot w \cdot q \cdot N_D \cdot \mu_n \cdot \left(1 - \sqrt{\frac{U_k - U_{GS} + U(x)}{U_k - U_{GS0}}} \right) \cdot \frac{dU(x)}{dx}$$

$$I_D \cdot dx = 2a \cdot w \cdot q \cdot N_D \cdot \mu_n \cdot \left(1 - \sqrt{\frac{U_k - U_{GS} + U(x)}{U_k - U_{GS0}}} \right) \cdot dU(x)$$

$$I_D = G_0 \cdot \left[U_{DS} - \frac{2}{3} \cdot \frac{(U_k - U_{GS} + U_{DS})^{\frac{3}{2}} - (U_k - U_{GS})^{\frac{3}{2}}}{\sqrt{U_k - U_{GS0}}} \right]$$

$$G_0 = \frac{2a \cdot w \cdot q \cdot N_D \cdot \mu_n}{L}$$





Širina kanala uz napon $U_{DS} > U_{GS} - U_{GS0}$

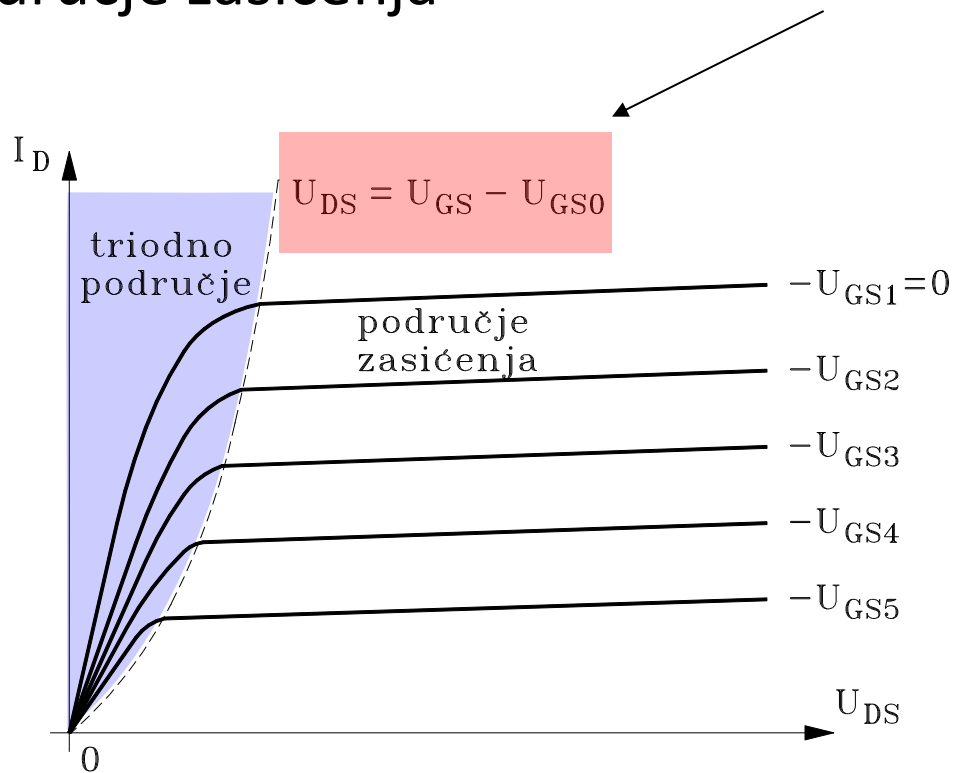
$$I_{Dzas} = G_0 \cdot \left[U_{GS} - U_{GS0} - \frac{2}{3} \cdot \frac{(U_k - U_{GS0})^{\frac{3}{2}} - (U_k - U_{GS})^{\frac{3}{2}}}{\sqrt{U_k - U_{GS0}}} \right]$$



Izlazne karakteristike FET-a

- Dva područja rada:
 - Triodno područje
 - Područje zasićenja

Jednadžba krivulje koja odvaja triodno i područje zasićenja



Dinamički parametri FET-a

- Strmina g_m :

$$g_m = \left. \frac{\partial I_D}{\partial U_{GS}} \right|_{U_{DS} = konst.}$$

$$g_m = G_0 \cdot \frac{\sqrt{U_k - U_{GS} + U_{DS}} - \sqrt{U_k - U_{GS}}}{\sqrt{U_k - U_{GS0}}} \quad \text{Triodno područje}$$

$$g_m = G_0 \cdot \left(1 - \frac{\sqrt{U_k - U_{GS}}}{\sqrt{U_k - U_{GS0}}} \right) \quad \text{Područje zasićenja}$$

- Izlazna dinamička vodljivost g_d :

$$g_d = \left. \frac{\partial I_D}{\partial U_{DS}} \right|_{U_{GS} = konst.}$$

$$g_d = G_0 \cdot \left[1 - \sqrt{\frac{U_k - U_{GS} + U_{DS}}{U_k - U_{GS0}}} \right] \quad \text{Triodno područje}$$



U području zasićenja može se upotrijebiti empirijski izraz za struju odvoda I_D : $I_D = I_{Dzas} \cdot (1 + \lambda \cdot U_{DS})$

pa je tada izlazna dinamička vodljivost:

$g_{dzas} = \lambda \cdot I_{Dzas}$, gdje je λ parametar iznosa između 0,01 i 0,001 V⁻¹

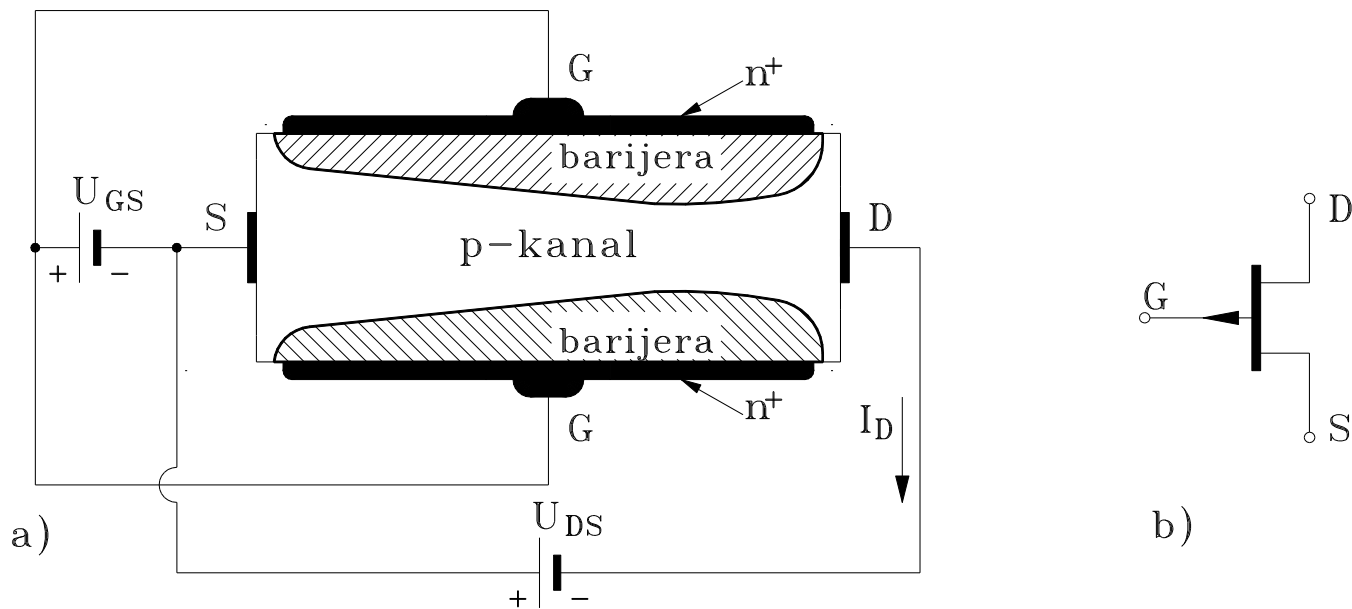
- Dinamički otpor r_d je recipročna veličina g_d .
- Faktor pojačanja μ :

$$\mu = \left. \frac{\partial U_{DS}}{\partial U_{GS}} \right|_{I_D = konst.}$$

$$\mu = \frac{\partial U_{DS}}{\partial U_{GS}} = \frac{\partial U_{DS}}{\partial I_D} \cdot \frac{\partial I_D}{\partial U_{GS}} = \frac{g_m}{g_d} = r_d \cdot g_m$$



p-kanalni JFET



a) p-kanalni spojni FET; b) električni simbol za p-kanalni spojni FET



$$a - b = \sqrt{\frac{2 \cdot \varepsilon \cdot (U_k + U_{GS})}{q \cdot N_A}}$$

$$U_{GS0} = \frac{a^2 \cdot q \cdot N_A}{2 \cdot \varepsilon} - U_k$$

$$b = a \cdot \left(1 - \sqrt{\frac{U_k + U_{GS}}{U_k + U_{GS0}}} \right)$$

$$-I_D = G_0 \cdot \left[-U_{DS} - \frac{2}{3} \cdot \frac{(U_k + U_{GS} - U_{DS})^{\frac{3}{2}} - (U_k + U_{GS})^{\frac{3}{2}}}{\sqrt{U_k + U_{GS0}}} \right]$$

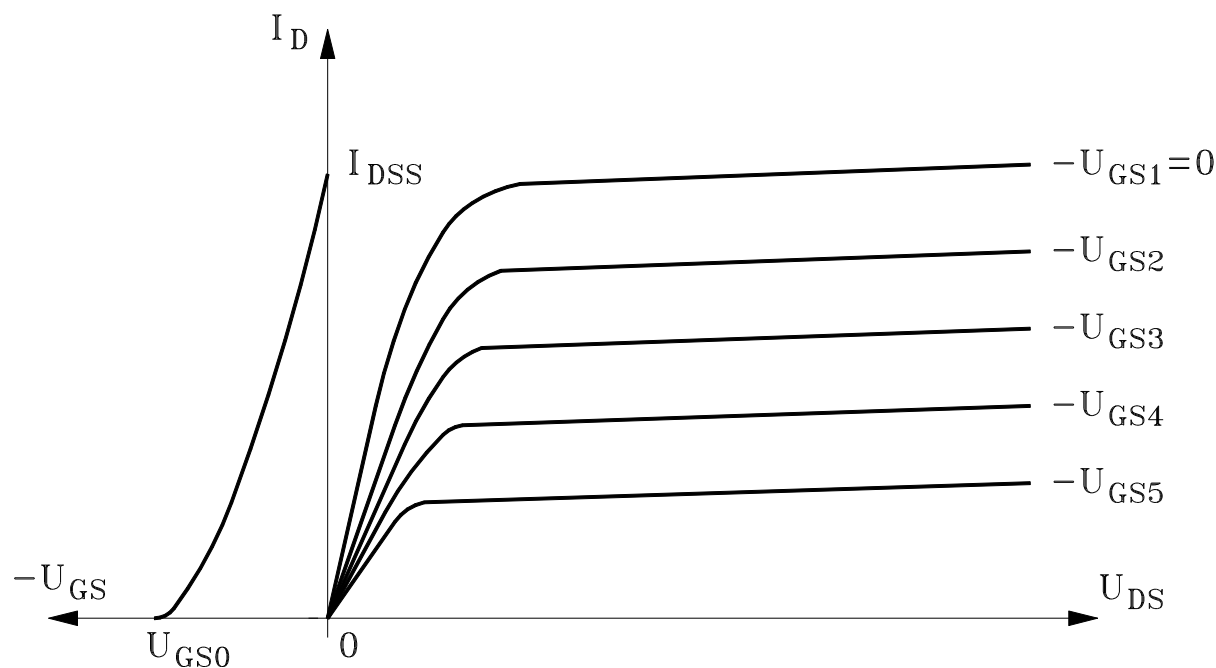
$$|U_{DS}| = |U_{GS} - U_{GS0}|$$

$$-I_{Dzas} = G_0 \cdot \left[-U_{GS} + U_{GS0} - \frac{2}{3} \cdot \frac{(U_k + U_{GS0})^{\frac{3}{2}} - (U_k + U_{GS})^{\frac{3}{2}}}{\sqrt{U_k + U_{GS0}}} \right]$$



Statičke karakteristike JFET-a

$$I_D = I_{DSS} \cdot \left(1 - \frac{U_{GS}}{U_{GS0}}\right)^2$$



Statičke karakteristike n-kanalnog FET-a

