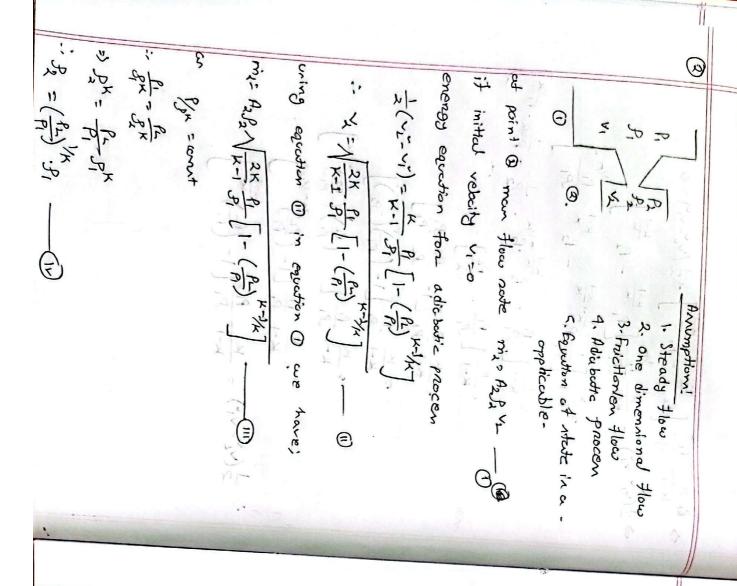
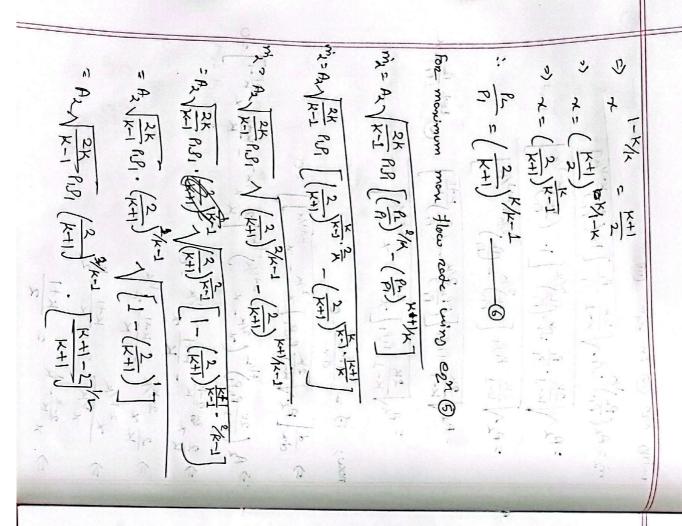
The energy equation of compressible flow for => == == + == + == count >> de + vdv =0 -- 0 => of + 2ml +020 bernoulli's equation; Anumption: 1. Stoody flow adiabatic flow in deriven below. 1+ 2 + 2 = com+ 4. Equation of state in applicable 2. One dimensional flow for adjubedic process ex = comst 0= | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x - 0 | x put = const

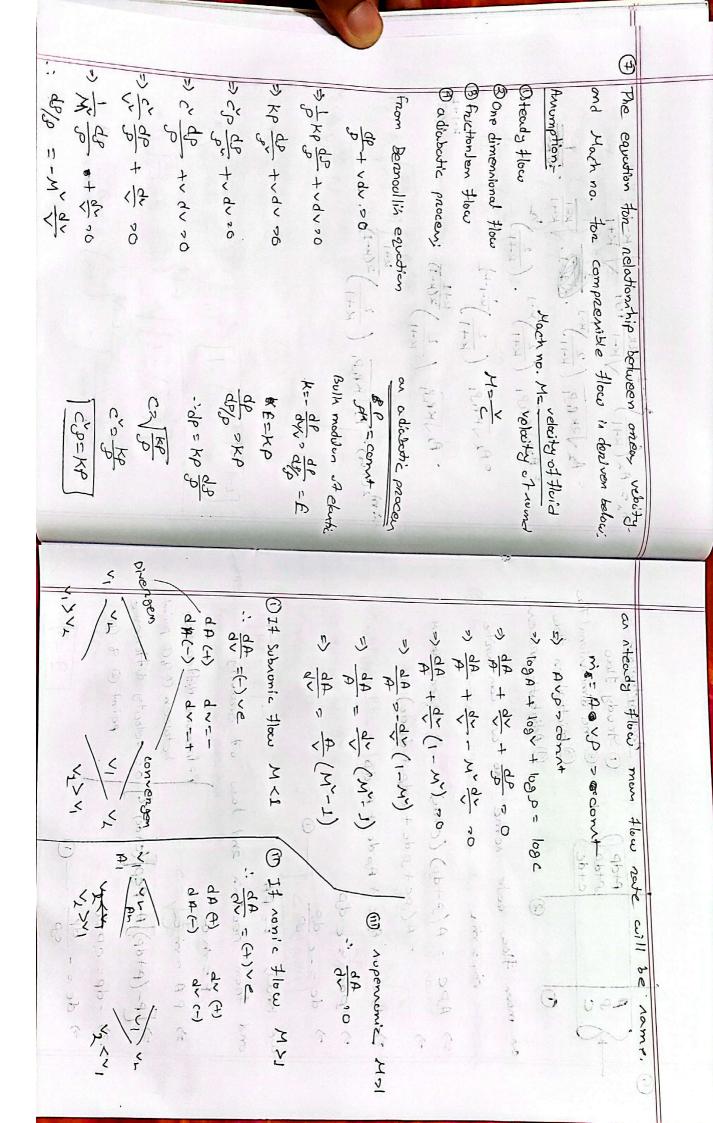


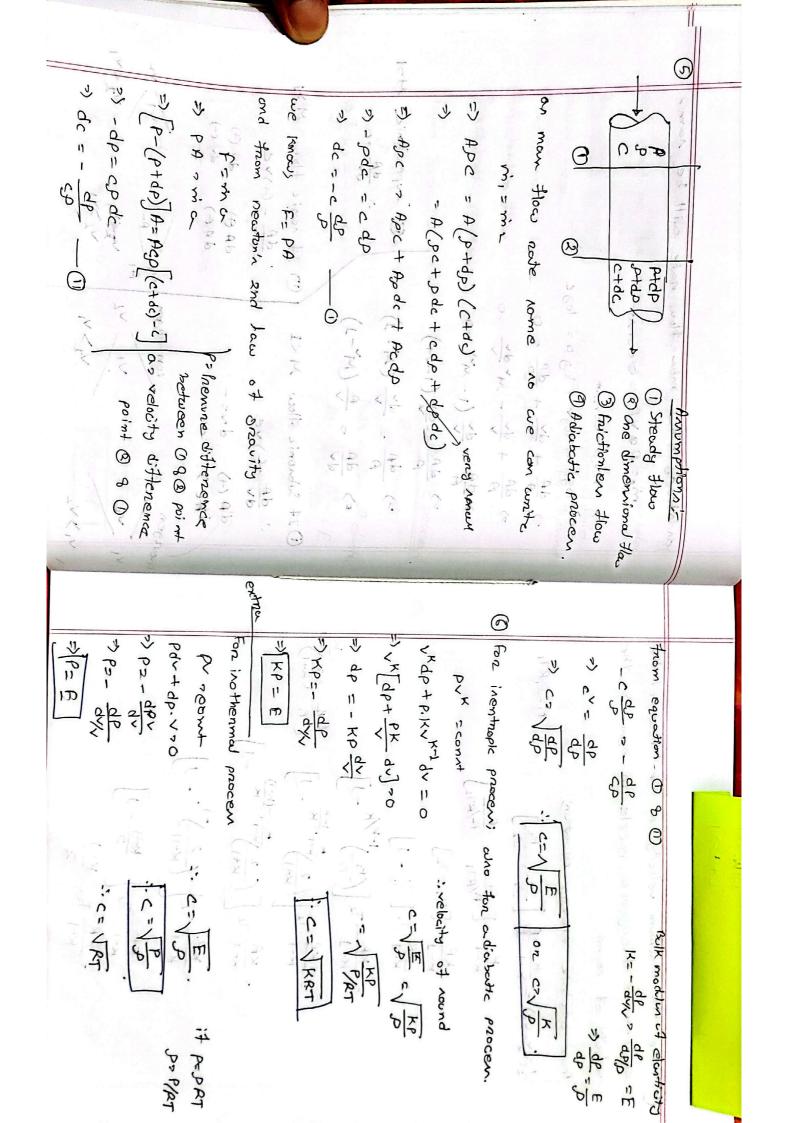
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79. 1 ( Pr.) 1 ( P



 $\frac{1}{100} = A_{\lambda} \left( \frac{1}{K+1} \right)^{1/2} \left( \frac{2}{K+1} \right)^{1/2} \cdot \left( \frac{1}{K+1} \right)^{1/2} \cdot \left( \frac{1}{K+1$ 





Prove that movimum velocity at the throat of the convergence divergence nozzle in equal to the velocity of round. From adiabatic energy equation;  $\frac{1}{2}(v_2^2-v_1^2)=\frac{K}{K-1}\left[\frac{P_1}{P_1}-\frac{P_2}{P_1}\right]$ P\_1=P\_1RT\_1  $N = \frac{K}{K-1} = \frac{P_1}{P_1/RT_1} = \frac{P_2}{P_2/RT_2} = \frac{P_2}{P_2/RT_2} = \frac{P_2}{P_3} = \frac{P_2}{P_3} = \frac{P_3}{P_4} = \frac{P_3}{P_4} = \frac{P_4}{P_4} = \frac{P_4}{P_4}$ broos [KR Hollsti.-T2] O = Vb [-X VXI.9 + 9b\*V 9H = RR TE TI - 1] 0- [-b 49 +9b] 4/ 12 KR - TE (P2) - 1 Vb 9H - = 9b ( > KR TL (2) - 1) +wood w P KR TL K-1 70 96 -99 (1)

1 3 =9/6

17 VIDO 17 VIDO ERTL PARRIDER MISSING WIND SINGER · Y = KRTLO 1 CM/C 588 3 · vo = c Proved from insurfaces condition,  $\frac{12}{2} = \left(\frac{\sqrt{1}}{2}\right)^2 = \left(\frac{\sqrt{1}}{21}\right)^2 = \left(\frac{\sqrt{1$ 7 (4) = 6 (A) -1 -2 0 1 co 528 B = 361.32 KB recently as theren you could be fire of 111 x 288 x 259.1 1 5 822.67 may [3(16-12): KR - [12-13]: KRIL [1-12]