Chapter 11: AC Power Analysis

(11.1)Effective or RMS VALUE:

$$X_{\rm rms} = \sqrt{\frac{1}{T} \int_0^T x^2 \, dt}$$

 $X_{rms} = rac{X}{\sqrt{2}}$ (only valid for sinusoidal functions)

If not a sinusoidal then:

$$X_{rms} = \sqrt{\frac{1}{T}} \left(\int_{0}^{T_{1}} (x_{1}^{2}) dt + \int_{T_{1}}^{T_{2}} (x_{2}) dt + ... + \int_{T_{n-1}}^{T_{n}} (x_{n}^{2}) dt \right)$$

The effective value: of a periodic current is the do current that delivers the same average power to a resistor as the sinusoidal periodic current.

(11.2)COMPLEX POWER

Complex power of an Impedance Z:

$$\mathbf{S} = I_{\text{rms}}^2 \mathbf{Z} = \frac{V_{\text{rms}}^2}{\mathbf{Z}^*} = \mathbf{V}_{\text{rms}} \mathbf{I}_{\text{rms}}^*$$

Angle of Impedance:

$$\theta_z = angle(\tilde{Z}) = angle(\tilde{S})$$

Complex Power (for any Circuit Element):

$$\begin{aligned} & \text{Complex Power} = \mathbf{S} = P + jQ = \mathbf{V}_{\text{rms}}(\mathbf{I}_{\text{mas}})^* \\ &= |\mathbf{V}_{\text{rms}}| \ |\mathbf{I}_{\text{rms}}| \frac{\rho_v - \rho_l}{\rho_l} \end{aligned}$$
 Apparent Power = $S = |\mathbf{S}| = |\mathbf{V}_{\text{rms}}| \ |\mathbf{I}_{\text{rms}}| = \sqrt{P^2 + Q^2}$
 Real Power = $P = \text{Re}(\mathbf{S}) = S \cos(\theta_v - \theta_l)$
 Reactive Power = $Q = \text{Im}(\mathbf{S}) = S \sin(\theta_v - \theta_l)$
 Power Factor = $\frac{P}{S} = \cos(\theta_v - \theta_l)$

Lagging power factor when $\ \theta_v-\theta_i>0$ Leading power factor when $\ \theta_v-\theta_i<0$ Reactive factor: $rf=\sin(\theta_z)$

- 1. Q = 0 for resistive loads (unity pf).
- 2. Q < 0 for capacitive loads (leading pf).
- 3. $\widetilde{Q} > 0$ for inductive loads (lagging pf).

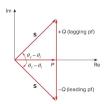


Figure 11.22

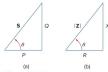


Figure 11.21
(a) Power triangle, (b) impedance triangle

Conservation Of Complex Power:

(assumed using passive sign conv) For Series:

$$\mathbf{V} = \mathbf{V}_1 + \mathbf{V}_2$$

$$\label{eq:S} \begin{split} S &= VI^* = (V_1 + V_2)I^* = V_1I^* + V_2I^* = S_1 + S_2 \\ \text{For parallel:} \end{split}$$

 $\mathbf{I} = \mathbf{I}_1 + \mathbf{I}_2$

$$S = VI^* = V(I_1^* + I_2^*) = VI_1^* + VI_2^* = S_1 + S_2$$

 $\tilde{S}_1 + \tilde{S}_2 + ... + \tilde{S}_n = 0$

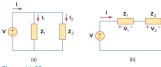


Figure 11.23

An ac voltage source supplied loads connected in: (a) parallel, (b) series.

Maximum Average Power transfer(ALL MAX):



(b)

Figure 11.7

Finding the maximum average power transfer: (a) circuit with a load, (b) the Thevenin equivalent.

$$\tilde{Z_{Th}} = R_{Th} + jX_{Th}$$

$$\tilde{Z_L} = R_L + jX_L$$

$$P = \frac{1}{2}|\mathbf{I}|^2 R_L = \frac{|\mathbf{V}_{\text{Th}}|^2 R_L / 2}{(R_{\text{Th}} + R_L)^2 + (X_{\text{Th}} + X_L)^2}$$

After taking the partial of $P(\tilde{Z_L})$ with respect to R_L and X_L we get:

$$R_L(X_L) = \sqrt{R_{Th}^2 + (X_L + X_{Th})^2}$$

 $X_L = -X_{Th}$

If (
$$ilde{Z_L} = R_L + jX_L$$
): $P_{max} = P(ilde{Z_{Th}}^*) = rac{|V_{Th}|^2}{8R_{Th}}$

If else $(ilde{Z_L}=R_L)$:

$$P_{max} = P(|\tilde{Z_{Th}}|) = \frac{1}{2} \frac{|\tilde{V_{Th}}|^2 |\tilde{Z_{Th}}|}{[[|\tilde{Z_{Th}}| + R_{Th}|^2 + X_{Th}^2]}$$

Chapter 12: Three - Phase Circuits(RMS Eqns)

Balanced phase Voltages: are equal in magnitude and are out of phase with each other by 120

$$V_{an} + V_{bn} + V_{cn} = 0$$

 $V_{an} = V_{bn} = V_{cn}$

Phase Sequence: is the time order in which the voltages pass through their respective maximum values. Positive Sequence(abc):

$$\mathbf{V}_{an} = V_p / \underline{0}^{\circ}$$
 $\mathbf{V}_{bn} = V_p / \underline{-120}^{\circ}$
 $\mathbf{V}_{cn} = V_p / \underline{-240}^{\circ} = V_p / \underline{+120}^{\circ}$

Negative Sequence(acb):

$$\mathbf{V}_{on} = V_p / 0^{\circ}$$
 $\mathbf{V}_{cn} = V_p / -120^{\circ}$
 $\mathbf{V}_{bn} = V_p / -240^{\circ} = V_p / +120^{\circ}$

Balanced load: is one in which the phase impedances are equal in magnitude an in phase.

 $\Delta - > Y$ Transformations:

$$\tilde{Z_Y} = \frac{1}{3}\tilde{Z_\Delta}$$

$$V_{\phi,Y} = rac{1}{\sqrt{3}} V_{\phi,\Delta}$$
 Line-Phase relationship

Phasor diagrams

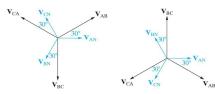


Figure 11.9 Phasor diagrams showing the relationship between line-to-line and line-to-neutral voltages in a balanced system. (a) The abc sequence. (b) The acb sequence.

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For negative sequence:

 $\tilde{V_{AB}} = \sqrt{3}\tilde{V_{AN}}\angle -30$

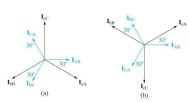


Figure 11.13 Phasor diagrams showing the relationship between line currents and phase currents in a Δ -connected load (a) The positive sequence. (b) The negative sequence.

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For negative sequence:

$$\tilde{I_{AB}} = \sqrt{3}\tilde{I_{aA}}\angle -30$$

EQUATIONS FOR SOLVING 3 - phase

TABLE 12.1

Summary of phase and line voltages/currents for balanced three-phase systems. 1

Connection	Phase voltages/currents	Line voltages/currents
Y-Y	$V_{an} = V_p/0^\circ$	$V_{ab} = \sqrt{3} V_p / 30^{\circ}$
	$V_{bn} = V_p / -120^{\circ}$	$\mathbf{V}_{bc} = \mathbf{V}_{ab} / -120^{\circ}$
	$\mathbf{V}_{cn} = V_p / +120^{\circ}$	$V_{ca} = V_{ab}/+120^{\circ}$
	Same as line currents	$I_a = V_{an}/Z_Y$
		$\mathbf{I}_b = \mathbf{I}_a / -120^\circ$
		$\mathbf{I}_c = \mathbf{I}_a / +120^\circ$
$Y-\Delta$	$V_{an} = V_p / 0^{\circ}$	$\mathbf{V}_{ab} = \mathbf{V}_{AB} = \sqrt{3} V_p / 30^\circ$
	$V_{bn} = V_p / -120^{\circ}$	$\mathbf{V}_{bc} = \mathbf{V}_{BC} = \mathbf{V}_{ab} / -120^{\circ}$
	$\mathbf{V}_{cn} = V_p / +120^{\circ}$	$\mathbf{V}_{ca} = \mathbf{V}_{CA} = \mathbf{V}_{ab} / +120^{\circ}$
	$\mathbf{I}_{AB} = \mathbf{V}_{AB}/\mathbf{Z}_{\Delta}$	$\mathbf{I}_a = \mathbf{I}_{AB}\sqrt{3}/-30^\circ$
	$\mathbf{I}_{BC} = \mathbf{V}_{BC}/\mathbf{Z}_{\Delta}$	$\mathbf{I}_b = \mathbf{I}_a / -120^\circ$
	$I_{CA} = V_{CA}/Z_{\Delta}$	$\mathbf{I}_c = \mathbf{I}_a / +120^{\circ}$
Δ - Δ	$V_{ab} = V_p / 0^{\circ}$	Same as phase voltages
	$\mathbf{V}_{bc} = V_p / -120^{\circ}$	
	$\mathbf{V}_{ca} = V_p / +120^{\circ}$,
	$I_{AB} = V_{ab}/Z_{\Delta}$	$\mathbf{I}_a = \mathbf{I}_{AB}\sqrt{3}/-30^\circ$
	$\mathbf{I}_{BC} = \mathbf{V}_{bc}/\mathbf{Z}_{\Delta}$	$\mathbf{I}_b = \mathbf{I}_a / -120^\circ$
	$I_{CA} = V_{ca}/Z_{\Delta}$	$\mathbf{I}_c = \mathbf{I}_a / +120^{\circ}$
Δ -Y	$V_{ab} = V_p / 0^{\circ}$	Same as phase voltages
	$V_{bc} = V_p / -120^{\circ}$	
	$\mathbf{V}_{ca} = V_p / +120^{\circ}$	$V_p/-30^\circ$
	Same as line currents	$\mathbf{I}_a = \frac{V_p / -30^\circ}{\sqrt{3} \mathbf{Z}_V}$
		$\mathbf{I}_b = \mathbf{I}_a / -120^\circ$
		$\mathbf{I}_c = \mathbf{I}_a / +120^\circ$

Positive or abc sequence is assumed.

Power in a Balanced Load:

Instantaneous power in a three phase balanced system:

$$p_{3\phi} = 3V_{\phi}I_{\phi}cos\theta_z$$

This result is true for either y or delta connected load Per-phase Powers:

$$P_{\phi} = p/3 = V_{1\phi}I_{\phi}cos\theta_{z}$$

$$Q_{\phi} = V_{\phi}I_{\phi}sin\theta_{z}$$

$$\tilde{S}_{\phi} = P_{1\phi} + j * Q_{1\phi} = \tilde{V}_{1\phi} \tilde{I}_{1\phi}^*$$

The total average power is the sum of the average powers in the phases:

$$P_{3\phi} = P_a + P_b + P_c = 3P_\phi = 3V_\phi * I_\phi cos\theta_z = \sqrt{3}V_L I_L cos\theta_z$$

For Y-connected load: $I_L = I_\phi \ but \ V_L = \sqrt{3} V_\phi$

For
$$\Delta$$
 - connected load: $I_L=\sqrt{3}I_\phi~but~V_L=V_\phi$

$$Q_{3\phi} = 3Q_{3\phi} = \sqrt{3}V_L * I_L sin(\theta_\phi)$$

And then total complex power of a 3 phase system:

$$\tilde{S_{3\phi}} = 3\tilde{S_{\phi}} = 3\tilde{V_{\phi}}\tilde{I_{\phi}}^* = 3I_{\phi}^2\tilde{Z_{\phi}} = 3\frac{V_{\phi}^2}{\tilde{Z}^*}$$

OR

$$\tilde{S_{3\phi}} = P_{3\phi} + jQ_{3\phi} = \sqrt{3}V_LI_L\angle\theta_{\phi}$$

Where:

 θ_ϕ is the phase angle of that element or impedance angle

 $\tilde{S_{3\phi}} \neq \tilde{V_L}\tilde{I_L}^* \neq \sqrt{3}V_LI_L \angle \theta_{\phi}$

Power Calculation in 3-phase circuits: (TIPS)

See what is given:

1.) Look what you are given

a.)Case 1: given just impedances or Currents/ Voltages:

Try to change everything to a Y - Y configuration

-> If (there are multiple balanced loads given){
When (L1 and L2 are in parallel):

Transform L1 and L2 to Y forms and connect combine their individual impedances.

Then Make single phase equivalent circuit.

b.)Case 2: given just the a Power quantity

- Notice that $\tilde{S_{\phi,Y}} = \tilde{S_{\phi,\Delta}}$
- That means we can make a single equivalent directly of individual Loads.

c.) case 3: Combination of case 1 and 2

- Try to break this circuit in a single phase equivalent (convert everything to Y)
- For the Load given a Power quantity with a black box use the fact that $S_{\tilde{\phi},Y}=S_{\tilde{\phi},\Delta}^{\tilde{\phi}}$
- -> Next the circuit build the single phase circuit

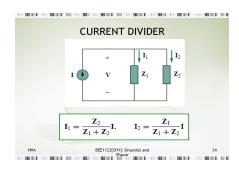
2.)Once you Configured your Circuit. If not given a reference set one:

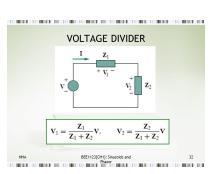
Example: You might be given a magnitude, and there is not way to even solve for a variable need with this magnitude. Therefore give the phasor a reference angle of 0.

If you are given a line voltage but need to use line to neutral voltage make it such that line to voltage phase is your reference.

3.) Solve using or method :

On Calculator function for parallel impedances: $z1(x,y) = x \mid\mid y$





Source Transformations:

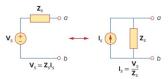


Figure 10.16 Source transformation

$$\mathbf{V}_s = \mathbf{Z}_s \mathbf{I}_s \qquad \Leftrightarrow \qquad \mathbf{I}_s = \frac{\mathbf{V}_s}{\mathbf{Z}_s}$$

Three phase - Circuit visuals (assuming Positive sequence):

Y-Y Balanced circuit:

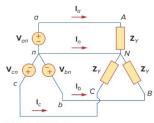


Figure 12.10

Balanced Y-Y connection.

Alternative way of analyzing a balanced Y-Y system:



Figure 12.12

A single-phase equivalent circuit.

Balanced Y - A:

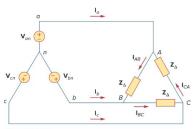
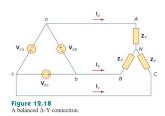


Figure 12.14
Balanced Y-Δ connection.

Alternative way of analyzing a balanced Y- Δ :

Balanced Δ - Y:



Alternative way of analyzing Δ - Y balanced:



Figure 12.20

The single-phase equivalent circuit.

Balanced Δ - Δ :

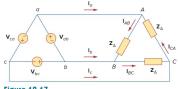
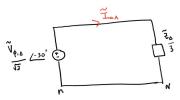
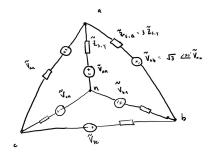


Figure 12.17
A balanced Δ-Δ connection

Alternative way of analyzing $\,\Delta$ - Y $\,$ balanced:



A Three phase source with winding impedance:



Help: (POWER LOSS)

What percentage of the average power at the sending end of the line is delivered to the loads?

% diff =
$$\frac{P_{s,\phi}-P_{\ell,\phi}}{P_{s,\phi}}\cdot 100$$
 %