How To Use Free-Surface Flows in OpenFOAM v.1812

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Training level: Intermediate

Session type: Lecture with examples

Software stack: OpenFOAM v.1812

https://unicfd.ru

Plan of training course

- 1. Introduction
- 2. Key points of training course
- 3. interFoam solver: how it works
 - Governing equations
 - Volume of Fluid method
 - Solution process
 - Boundary conditions
- 4. Basic case: Spillway tutorial
 - Problem statement
 - Physical properties setup
 - Mesh generation

- Boundary conditions setup
- Numerical schemes and time advancement settings.
 Running.
- Results
- 5. Additional case: RT tutorial
 - Problem statement
 - Settings in OpenFOAM. Running.
 - Results. Comparison with linear theory.
- 6. Conclusions and discussion

Introduction

Applicability

- printing;
- engines;
- ecological cases;
- dams, spillways;
- etc.



Ladybower Reservoir, England

Complexities

- large deformations of the interface;
- creation of different subregions (droplets, bubbles...);
- solution should:
 - be stable:
 - have small diffusivity in the interface region;
 - satisfy to conservation laws;
 - be correct in different scales;
 - require not so much resources for computations.

Key points of training course

- Look inside the standard solver for free-surface flows
- Study how to set boundary conditions in different versions of OpenFOAM
- Look to all stages of modelling of free-surface flows in OpenFOAM v.
 1812: from mesh generation to post-processing

Boundary conditions are critically important in the successful modelling. There are strong differences between OpenFOAM 2.2.x and 2.3.0+.

The main tool: an interFoam solver in OF v. 1812. We will study it with Spillway tutorial: the turbulent flow of fluid

Part I Theoretical part

interFoam: how it works

Structure of theoretical part

- 1. Governing equations
- 2. Volume of Fluid method
- 3. Block scheme of interFoam
- 4. Pressure-velocity coupling
- 5. Boundary conditions (most common types):
 - walls and inlets:
 - outlets and open boundaries;
 - planes of symmetry.

Governing equations for incompressible flow

Continuity equation:

$$\nabla \cdot \mathbf{U} = 0;$$

Navier — Stokes equations:

$$\frac{\partial (\rho \mathbf{U})}{\partial t} + \nabla \cdot (\rho \mathbf{U} \otimes \mathbf{U}) = -\nabla p + \nabla \cdot \hat{\tau} + \rho \mathbf{g},$$

where $\hat{\tau} = \mu(\nabla \mathbf{U}^T + \nabla \mathbf{U})$ is the viscous stress tensor;

• boundary conditions on the interface:

$$[-p\mathbf{I} + \hat{\tau}] \cdot \mathbf{n} = \sigma \kappa \mathbf{n}, \quad [\mathbf{U}] = 0;$$

• initial and boundary conditions on the flow region boundaries (different types — walls, inlets, outlets, open boundaries and other).

Volume of Fluid method

Add a volume fraction function:

$$\alpha_1 = \begin{cases} 1 \text{ if cell full of liquid;} \\ 0 \text{ if cell full of gas;} \\ (0;1) \text{ if cell is placed on the interface;} \end{cases}$$

0	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
0.8	0.9	0.5	0	0	0
1	1	1	0.2	0	0
1	1	1	0 .2	0	0

For two phases

$$\alpha_1 + \alpha_2 = 1.$$

Solve a transport equation for this function:

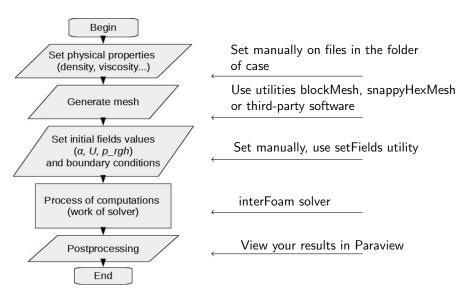
$$\frac{\partial \alpha_1}{\partial t} + \nabla \cdot (\mathbf{U}\alpha_1) + \nabla \cdot (\mathbf{U}_R \alpha_1 \alpha_2) = 0,$$

where $\mathbf{U} = \alpha_1 \mathbf{U}_1 + \alpha_2 \mathbf{U}_2$ — velocity of mixture;

 $\mathbf{U}_R = \mathbf{U}_1 - \mathbf{U}_2$ — velocity field suitable to compress the interface.

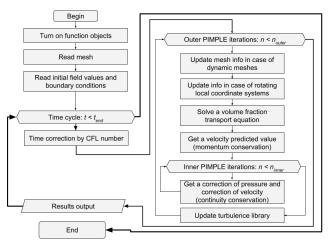
Approximation: Finite Volume Method

Solution process



interFoam solver

Block scheme



see alphaEqn.H¹
see UEqn.H

see pEqn.H

Location: OpenFoam-v1812/applications/solvers/multiphase/VoF

¹see slide 8

interFoam solver

Modified Navier — Stokes equations

Surface tension forces are approximated as an additional term \mathbf{F}_{σ} in Navier — Stokes equation²:

$$\frac{\partial(\rho\mathbf{U})}{\partial t} + \nabla \cdot (\rho\mathbf{U} \otimes \mathbf{U}) = -\nabla p + \nabla \cdot \hat{\tau} + \rho \mathbf{g} + \mathbf{F}_{\sigma}.$$

Use modified pressure:

$$p^* = p - \rho(\mathbf{g} \cdot \mathbf{r}).$$

Its gradient:

$$\nabla p^* = \nabla p - (\nabla \rho)(\mathbf{g} \cdot \mathbf{r}) - \rho \mathbf{g}.$$

Approximation of surface tension forces — by volume fraction gradient:

$$\mathbf{F}_{\sigma} \approx \sigma \kappa \nabla \alpha_1$$
.

²see slide 7

interFoam solver I

Pressure-velocity coupling

Use velocity as sum of prediction and correction parts:

$$\mathbf{U} = \mathbf{U}^* + \mathbf{U}'. \tag{1}$$

Semi-discrete form of momentum equation:

$$A\mathbf{U} = H - \nabla p^* - (\nabla \rho)(\mathbf{g} \cdot \mathbf{r}) + \mathbf{F}_{\sigma}.$$

Here A is the diagonal part of initial matrix system,

H is the non-diagonal part of matrix + r.h.s. without diagonal part of initial matrix system, pressure gradient and terms for gravity and surface tension.

We can write comparing with the velocity splitting (1):

$$\mathbf{U}^* = A^{-1}H;$$

$$\mathbf{U}' = -A^{-1}\nabla p^* - A^{-1}(\nabla \rho)(\mathbf{g} \cdot \mathbf{r}) + A^{-1}\mathbf{F}_{\sigma}.$$

interFoam solver II

Pressure-velocity coupling

Continuity equation in the discrete form:

$$\int_{V} \nabla \cdot \mathbf{U} \, dV = \int_{S} \mathbf{U} \cdot \mathbf{n} \, dS \approx \sum_{f} \underbrace{\mathbf{U}_{f} \cdot \mathbf{S}_{f}}_{\varphi_{f}} = 0, \tag{2}$$

consequently,

$$\sum_{f} \varphi_f = 0. \tag{3}$$

Let's calculate fluxes through one face f:

$$\underbrace{\mathbf{U}_{f} \cdot \mathbf{S}_{f}}_{\varphi} = \underbrace{\mathbf{U}_{f}^{*} \cdot \mathbf{S}_{f}}_{\varphi_{H/A}} - \underbrace{(A^{-1})_{f}}_{D_{p}} (\nabla p^{*})_{f} \cdot \mathbf{S}_{f} - \underbrace{(A^{-1}(\nabla \rho)(\mathbf{g} \cdot \mathbf{r}))_{f} \cdot \mathbf{S}_{f} + (A^{-1}\mathbf{F}_{\sigma})_{f}}_{\varphi_{\sigma}}. \quad (4)$$

interFoam solver III

Pressure-velocity coupling

Create a pressure equation which is derived from continuity equation (3):

$$\sum_{f} (\varphi_{H/A} + \varphi_g) = \sum_{f} D_p(\nabla p^*)_f \cdot \mathbf{S}_f.$$

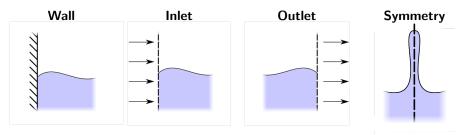
Pressure gradient:

$$(\nabla p^*)_f = \frac{\varphi_{H/A} + \varphi_g - \varphi}{D_p \cdot \mathbf{S}_f}.$$
 (5)

In the source code:

interFoam solver

Types of boundary conditions



Note

For incompressible fluids it is important to calculate correctly the pressure gradient. Absolute value of pressure is calculated up to a constant. So, it is enough to know the pressure reference value only in one point.

Location: OpenFoam-4.1/src/finiteVolume/fields/fvPatchFields

interFoam solver I

Walls & inlets

Boundary condition for volume fraction:

$$\alpha=0$$
 or $\alpha=1$ (fixedValue) — for inlets;
$$\nabla \alpha=0 \ ({\tt zeroGradient}) \ -- \ {\tt for walls}.$$

Boundary condition for velocity:

$$\mathbf{U} = \{U_x; U_y; U_z\}$$
 (fixedValue).

Note

Capillary effects are neglected; to account for these effects — special boundary conditions for volume fraction must be imposed.

Boundary conditions for **pressure** are critically important here. Let's consider the correct boundary condition and changes in OpenFOAM v.2.3.0+.

interFoam solver II

Walls & inlets

On boundaries for walls and inlets:

$$\mathbf{U} = \{U_x; U_y; U_z\}, \quad \mathbf{U}^* = \{U_x; U_y; U_z\} \Rightarrow \mathbf{U}' = \{0; 0; 0\}.$$

According to BC for volume fraction:

$$\mathbf{F}_{\sigma} \approx \sigma \kappa \nabla \alpha_1 = 0$$
 on the boundary.

So, according to expression for volumetric flux (4):

$$-D_p(\nabla p^*)_f \cdot \mathbf{S}_f - (A^{-1}(\nabla \rho)(\mathbf{g} \cdot \mathbf{r}))_f \cdot \mathbf{S}_f) = 0,$$

and, therefore, we can derive boundary condition for pressure:

$$(\nabla p^*)_f = -((\nabla \rho)(\mathbf{g} \cdot \mathbf{r}))_f.$$

interFoam solver III

Walls & inlets

Implementation in OpenFOAM

In OpenFOAM v.2.2.x — buoyantPressure: this expression is in the source code of boundary condition.

In OpenFOAM v.2.3.0+ — fixedFluxPressure: boundary condition is satisfied automatically by pressure gradient (5), calculating in the solver's source code.

interFoam solver I

Outlets

Boundary condition for **volume fraction**:

$$\nabla \alpha = 0$$
 (zeroGradient).

Boundary condition for velocity:

$$\nabla \mathbf{U} = 0$$
 (zeroGradient).

Boundary condition for pressure:

• reference level of pressure — if there are no pressure boundary conditions in any another boundary (typically means "atmosphere"):

$$p_p^* = p_0 - \frac{U^2}{2}$$
 (totalPressure),

where p_0 — total pressure, U — velocity magnitude.

interFoam solver II

Outlets

In the source code we use:

$$p = p0 - 0.5*(1 - pos(phi))*magSqr(U).$$

Here pos() is the boolean function which equals to 1 when the flux phi>0.

• zeroGradient — if you have some another boundary with derived reference level of pressure.

In case of **symmetry** just use slip boundary condition for all variables.

Note

Calculations of patch boundary field on the symmetry planes are performed using the Householder projection on the patch.

Part II Practical part

Basic case: Spillway tutorial

Stages of solution

- 1. Geometry: make STL-surface to draw the dam (in SALOME).
- 2. Liquid/gas properties: write density, kinematic viscosity . . .
- 3. Mesh generation:
 - blockMesh: create a basic mesh box;
 - snappyHexMesh: refine mesh near the dam surface:
 - extrudeMesh: make a 2D-mesh for fast calculations.
- 4. Boundary conditions: describe it in files in 0.org folder.

- 5. Set fields: set initial liquid phase volume fraction.
- 6. Numerical settings:
 - describe interpolation of terms;
 - describe solvers for SLAE;
 - setup turbulence models.
- 7. Time settings: set the end time, CFL-number . . .
- 8. Running: interFoam command.
- Post-processing: open file spillway.foam in Paraview.
- 10. Enjoy!

Problem statement

Input data

Water:

 $\textbf{density} \colon 1000 \text{ kg/m}^3;$

dynamic viscosity:

 $10^{-3} \ \mathrm{Pa} \cdot \mathrm{s}.$

Air:

 $\textbf{density}{:}\ 1\ kg/m^3;$

dynamic viscosity:

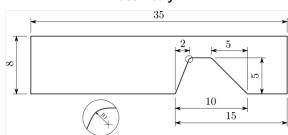
 $1.48 \cdot 10^{-5} \text{ Pa} \cdot \text{s}.$

Surface tension

coefficient: 0.07 N/m.

Inlet velocity: 0.6 m/s.

Geometry



Scheme



Physical properties I

See: folder \constant

File transportProperties:

• Set phases:

```
phases (water air);
```

Set density and kinematic viscosity for each phase:

Physical properties II

Set surface tension:

```
sigma sigma [ 1 0 -2 0 0 0 0 ] 0.07;
```

File g: set the value and direction of gravity

```
dimensions [0 1 -2 0 0 0 0];
value (0 0 -9.81);
```

File turbulenceProperties: set the turbulence model

```
simulationType RAS;

RAS
{
    RASModel     kOmegaSST;
    turbulence     on;
    printCoeffs     on;
}
```

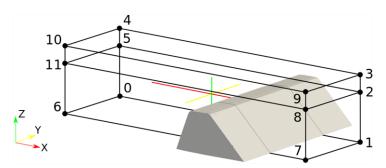
Turbulent intensity: $\approx 2\%$.

blockMesh I

Create basic coarse mesh in the flow region and mark the boundaries.

See: constant/polyMesh/blockMeshDict

Command: blockMesh



Exercise: inspect results in Paraview. You should see the rectangular region with the coarse mesh

blockMesh II

Set scale:

```
convertToMeters 1;
```

Set vertices:

```
vertices (
    (-20 - 0.45 \ 0) // 0
    ( 15 -0.45 0 ) // 1
    (15 - 0.45 6) // 2
    (15 - 0.45 8) // 3
    (-20 - 0.45 8) // 4
    (-20 - 0.45 6) // 5
    (-20 - 0.55 \ 0) // 6
    ( 15 -0.55 0 ) // 7
    ( 15 -0.55 6 ) // 8
    ( 15 -0.55 8 ) // 9
    (-20 - 0.55 8) // 10
    (-20 - 0.55 6) // 11
```

blockMesh III

Create two boxes:

```
blocks
(
    hex (0 1 2 5 6 7 8 11) (70 12 1)
        simpleGrading (1 1 1)
    hex (5 2 3 4 11 8 9 10) (70 4 1)
        simpleGrading (1 1 1)
);
```

Describe boundaries:

```
boundary
(
    outlet
    {
        type patch;
        faces ( (1 2 8 7) (2 3 9 8) );
}
```

blockMesh IV

```
inletAir
   type patch;
   faces ( (4 5 11 10) );
}
inletWater
   type patch;
   faces ( (5 0 6 11) );
atmosphere
   type patch;
   faces ( (3 4 10 9) );
```

blockMesh V

```
bottomWall
   type wall;
    faces ( (0 1 7 6) );
}
front
    type empty;
    faces ( (1 0 5 2) (2 5 4 3) );
}
back
    type empty;
    faces ( (6 7 8 11) (11 8 9 10) );
```

snappyHexMesh I

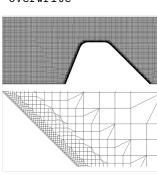
See: constant/system/snappyHexMeshDict **Command**: snappyHexMesh -overwrite

Stage 1. Refine mesh near the surface of dam. Three stages of meshing:

- refinement (see CastellatedMeshControl section);
- smoothing (see SnapControls section);
- set of layers (see addLayersControls section).

Use STL-surface (from constant/triSurface):

```
dam.stl {
    type triSurfaceMesh;
    name dam;
```



snappyHexMesh II

Stage 2. Add two refinement regions where the surface of water will flow. Use two boxes and plane to do it:

```
surface
   type searchableBox;
   min (-15 -1 4.5);
   max ( 4 0 7 );
aroundDam
   type
         searchablePlane;
   planeType pointAndNormal;
   pointAndNormalDict {
      basePoint (7.5 -0.5 2.5);
      normalVector (1 0 1);
   };
```

snappyHexMesh III

```
outlet
{
    type searchableBox;
    min ( 10 -1 0 );
    max ( 15 0 1 );
}
```

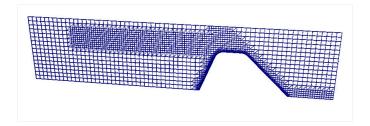
Exercise: try to run snappyHexMesh with different studies of remeshing. Watch differences.



extrudeMesh

See: constant/system/extrudeMeshDict
Command: extrudeMesh

blockMesh and snappyHexMesh construct 3D-mesh. extrudeMesh creates a 2D-mesh based one the planar surface (in our case — from patch).



Exercise: run checkMesh utility before running extrudeMesh and after that. Compare numbers of cells.

Boundary conditions

See: folder 0.org/. Change needed files and copy it to folder 0/.

Name	α	k	ω	p^*	U
inletAir	fixedValue 0	fixedValue 2.16e-4	fixedValue 0.1470	fixedFlux Pressure	fixedValue (0 0 0)
inletWater	fixedValue 1	fixedValue 2.16e-4	fixedValue 0.1470	fixedFlux Pressure	fixedValue (0.6 0 0)
outlet	zero Gradient	zero Gradient	zero Gradient	fixedFlux Pressure	zero Gradient
walls	kqRWall Function	omegaWall Function	zero Gradient	fixedFlux Pressure	fixedValue (0 0 0)
atmosphere	inletOutlet	inletOutlet 2.16e-4	inletOutlet 0.1470	total Pressure	pressure Inlet Outlet Velocity
front,back, defaultFaces	empty	empty	empty	empty	empty

setFields

Set an initial distribution of fields (alpha.water) in regions. Files in 0/ folder will be modified.

```
defaultFieldValues (
    volScalarFieldValue alpha.water 0
);

regions (
   boxToCell {
    box (-20 -1 0) (3 1 5);
    fieldValues (
        volScalarFieldValue alpha.water 1
    );
   }
);
```



Numerical schemes and time settings. Running

See system/controlDict to create time settings:

- time interval,
- CFL number.
- write interval,
- time precision.

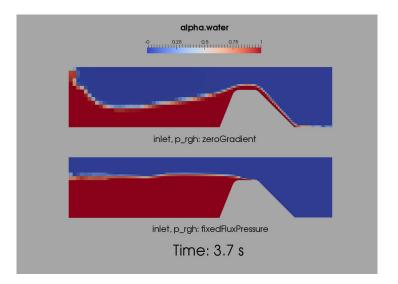
Settings for numerical schemes (use default settings): see system/fvSchemes and system/fvSolution.

Start application by interFoam command.

Scripts

Sequence of all commands is placed in the script file ./Allrun. Clean results: ./Allclean.

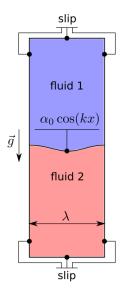
Results



Part II **Practical part**

Additional case: Rayleigh — Taylor instability

Problem statement



Input data

Fluid 1:

density: 1.255 kg/m^3 ;

dynamic viscosity: $3.13 \cdot 10^{-3}$ Pa·s.

Fluid 2:

density: 0.032 kg/m^3 ;

dynamic viscosity: $3.13 \cdot 10^{-3}$ Pa·s.

Surface tension coefficient: 0.01 N/m.

Interface form: $\alpha_0 = 0.05$ m, $k = 2\pi$.

Wave length: $\lambda = 1$ m.

Linear theory

Instability conditions

- 1. Initial perturbation: $\alpha > 0$, $\alpha \ll \lambda$.
- 2. Surface tension coefficient: $\sigma < \sigma_c, \sigma_c = \frac{\Delta \rho g}{k^2}$.
- 3. Dynamic viscosities: $\mu_1 = \mu_2 = \mu$.

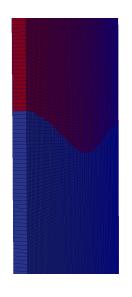
Law for growth of amplitude instabitily

$$\alpha(t) = \alpha_0 \cosh(\Gamma t),$$

where Γ — growth rate (1/s), A — Atwood number (non-dimensional):

$$\Gamma = \sqrt{kg\left(A - \frac{k^2\sigma}{g(\rho_1 + \rho_2)}\right)}; \quad A = \frac{\rho_2 - \rho_1}{\rho_2 + \rho_1}.$$

OpenFOAM case



General settings

Mesh: one block, uniform mesh, no refinement.

Boundary conditions: slip for all variables.

Transport properties: set density and kinematic viscosity for two fluids.

Turbulence properties: laminar flow.

Numerical settings: standard interFoam settings.

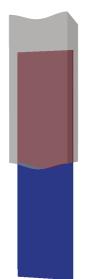
How to set up the interface

Different ways to set up the initial perturbation:

- use STL surface in standard setFields utility;
- use funkySetFields utility from swak4Foam library.

OpenFOAM case

setFields

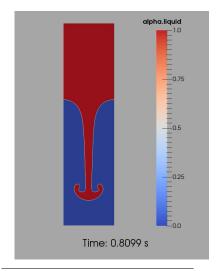


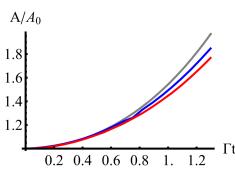
Source code for STL in setFields

```
regions (
  surfaceToCell {
                   "liquid.stl";
   file
   useSurfaceOrientation false;
   outsidePoints ((1e-4 0 -1.04));
   includeCut
                 true:
       includeInside true;
       includeOutside false;
       nearDistance -1;
       curvature
                      -100;
   fieldValues (
      volScalarFieldValue alpha.liquid 1
      volVectorFieldValue U
                                (0\ 0\ 0)
```

STL surface should be placed in the case folder.

Results





Gray color — linear theory Blue color — Gerris³ Red color — OpenFOAM

³open-source code for free-surface flows, see http://gfs.sourceforge.net/wiki/index.php/Main_Page

Summary

- We looked how interFoam works (look in the source code).
- We learned how to set boundary conditions for free-surface flows.
- We studied how to solve cases for free-surface flows step-by-step on the basic example — Spillway tutorial.
- We get the first experience in linear theory of hydrodynamic instabilities and run the additional case — RT instability

Let's talk about training track. Some questions?