

Modelling and Networked Control of Water Distribution Networks

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CA733

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Agenda

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Introduction

Modelling of WDN

Fast Dynamics and Graph theory

Slow Dynamics and Linearisation

Slow Dynamics

Linearisation

Control Structure and Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological Synchronisation

References



Introduction

Introduction to Water Distribution Networks

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

2

- ▶ Critical societal infrastructure, responsible for the provision of water to both domestic and industrial consumers.
- ▶ Network pressure must be controlled.
 - ▶ Underpressure → insufficient service pressure → dissatisfied end users.
 - ▶ Overpressure → component failure → repair costs, supply intermittency, etc.
- ▶ Network pressure tied to level in Elevated Water Reservoir(s) (EWR) → level control is key!
- ▶ Other key components are pumps, valves, and pipes.

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Introduction

Test Water Distribution Network Layout

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

3

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

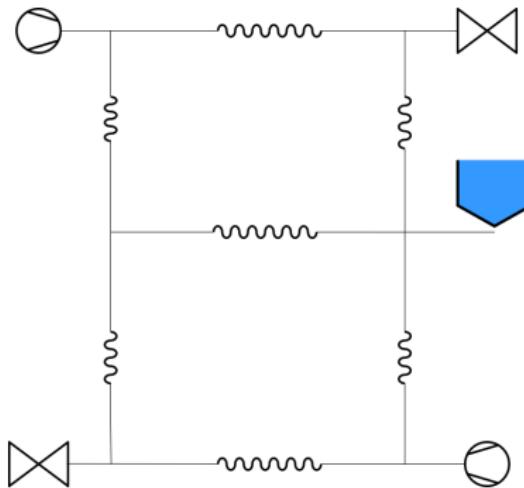
Results

Best-Case Results

Pathological
Synchronisation

References

We analyse a small-scale test WDN with the following layout:



Larger WDNs are typically not amenable to first-principles modelling.



Modelling of Water Distribution Networks

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus
Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results
Pathological
Synchronisation

References

4

- ▶ General principles for modelling fast regime very similar to circuit analysis.
 - ▶ Water flows = currents.
 - ▶ Pressures = voltages.
 - ▶ Network components behave similarly to circuit components, but resistors generally non-linear.
- ▶ Graph theory is combined with physics-induced boundary conditions to yield model of fast regime.

56

Modelling of Water Distribution Networks

Graph Theory

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

5

56

Graph theory describes a system as a directed graph.

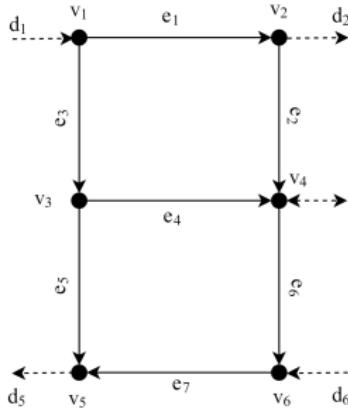


Figure: Graph of simplified WDN network. From [1].

- ▶ Spanning tree
- ▶ Chords



Modelling of Water Distribution Networks

Incidence and Loop matrices

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

6

Auxiliary matrices can be defined to mathematically describe the network:

$$H_{i,j} = \begin{cases} 1 & \text{If } j\text{th edge leaves } i\text{th node} \\ -1 & \text{If } j\text{th edge enters } i\text{th node} \\ 0 & \text{If } j\text{th edge and } i\text{th node unconnected} \end{cases}$$

$$B_{i,j} = \begin{cases} 1 & \text{If direction of } i\text{th loop and } j\text{th edge agree} \\ -1 & \text{If direction of } i\text{th loop and } j\text{th edge disagree} \\ 0 & \text{If } i\text{th loop excludes } j\text{th edge} \end{cases}$$

56



Modelling of Water Distribution Networks

Incidence and Loop matrices: Example

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Example:

$$H = \begin{bmatrix} 1 & 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 1 & 1 & 0 & 0 \\ 0 & -1 & 0 & -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & -1 \\ 0 & 0 & 0 & 0 & 0 & -1 & 1 \end{bmatrix} \quad (1)$$

$$\bar{H} = \begin{bmatrix} 1 & 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 1 & 1 & 0 & 0 \\ 0 & -1 & 0 & -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & -1 \end{bmatrix} \quad (2)$$

$$B = \begin{bmatrix} 1 & 1 & -1 & -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & -1 & 1 & 1 \end{bmatrix} \quad (3)$$



Modelling of Water Distribution Networks

Demand Matrices

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

8

Whether a node is open to atmosphere or not, or connected to a tank, can be described with matrices F and G respectively.

$$F = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, G = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \quad (4)$$

56



Modelling of Water Distribution Networks

General Component Model

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction
Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation
Control Structure and
Root Locus
Optimal Control
Disturbance Estimator
Network Effects
Results
Best-Case Results
Pathological
Synchronisation
References

9

The edges of the WDN can be described with a pressure and flow relationship, analogous to the current and voltage of an electrical component.

This project uses pipes, valves and pumps as edge components.

The general relationship between pressure and flow can be defined as:

$$\Delta p = \mathcal{J}\dot{q} + \lambda(q) + \mu(q, \Theta) + \alpha(q, \omega) - \Delta h \quad (5)$$

56



Modelling of Water Distribution Networks

Pipe Model

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus
Optimal Control

Disturbance Estimator
Network Effects

Results
Best-Case Results
Pathological
Synchronisation

References

10

The pressure drop across a pipe is defined as:

$$\Delta p_k = \mathcal{J} \dot{q} + \lambda(q) + \Delta z \quad (6)$$

where:

$$\lambda_k(q_k) = \left(f \cdot \frac{8 \cdot L \cdot q^2}{\pi^2 \cdot g \cdot D^5} + k_f \cdot \frac{8 \cdot q^2}{\pi^2 \cdot g \cdot D^4} \right) \cdot g \cdot \rho \quad (7)$$

$$\mathcal{J} = \frac{L \cdot \rho}{A} \quad (8)$$

$$\Delta z_k = \rho \cdot g \cdot \Delta h_k \quad (9)$$

56



Modelling of Water Distribution Networks

Valve Model

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

11

The pressure drop across a valve is defined as:

$$\Delta p_k = \mu(q, \Theta) = \frac{1}{K_{valve}(\Theta)^2} \cdot |q| \cdot q \quad (10)$$

where Θ is the opening degree of the valve.

Derivation:

$$\frac{\Delta p_1}{q_1^2} = \frac{\Delta p_2}{q_2^2} \Leftrightarrow q_1 = q_2 \cdot \sqrt{\frac{\Delta p_1}{\Delta p_2}} \quad (11)$$

$$q = q_n(\Theta) \cdot \sqrt{\frac{\Delta p_1}{1}} = K_{valve}(\Theta) \cdot \sqrt{\Delta p_1} \quad (12)$$

56



Modelling of Water Distribution Networks

Pump Model

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

12

The pressure drop across a pump is defined as:

$$\Delta p_k = a_0 \cdot \omega^2 + a_1 \cdot \omega \cdot q - a_2 \cdot |q| \cdot q \quad (13)$$

where $[a_0, a_1, a_2]$ is a tuple of coefficients that describe the pump's characteristic curve, q is the flow rate through the pump, and ω is the rotational velocity of the pump.



Modelling of Water Distribution Networks

Assumptions

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

13

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Kirchhoff's node and mesh law:

$$Hq = d \quad (14)$$

$$B\Delta p = BH^T p = 0 \wedge B\Delta h = BH^T h = 0 \quad (15)$$

Mass conservation:

$$d_n = - \sum_{i=1}^{n-1} d_i \quad (16)$$



Modelling of Water Distribution Networks

Lemmas

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

14

Lemma 4.1:

$$H_T \bar{H}_T^{-1} = \begin{bmatrix} I_{n-1} \\ -\mathbf{1}^T \end{bmatrix} \quad (17)$$

where $\mathbf{1}$ is a vector of ones and $I_{n-1} \in \mathbb{R}^{n-1 \times n-1}$ is an identity matrix.

Lemma 4.2:

$$q = B^T q_C + \begin{bmatrix} 0_{C \times n-1} \\ \bar{H}_T^{-1} \end{bmatrix} \bar{d} \quad (18)$$

56



Modelling of Water Distribution Networks

System Model

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Non linear differential equation:

$$\Phi \mathcal{J} \Phi^T \dot{q} = -\Phi \left(\lambda(q_n) + \mu(q_n) + \alpha(q_n) \right) + \Psi (\bar{h} - \mathbf{1} h_0) + \mathcal{I} (p_\tau - \mathbf{1} p_0) \quad (19)$$

Where the matrices Φ, Ψ, \mathcal{I} are defined as:

$$\Phi \triangleq \begin{bmatrix} I & -\bar{H}_C^T \bar{H}_T^{-T} \\ 0 & \bar{F}^T \bar{H}_T^{-T} \\ 0 & \bar{G}^T \bar{H}_T^{-T} \end{bmatrix}, \quad \Psi \triangleq \begin{bmatrix} 0 \\ \bar{F}^T \\ \bar{G}^T \end{bmatrix}, \quad \mathcal{I} \triangleq \begin{bmatrix} 0 \\ 0 \\ I \end{bmatrix} \quad (20)$$

$$\mathcal{P} : (\Phi \mathcal{J} \Phi^T)^{-1} \quad (21)$$

$$\dot{q}_n = -\mathcal{P} \Phi \left(\lambda(q_n) + \mu(q_n) + \alpha(q_n) \right) + \mathcal{P} \left(\Psi (\bar{h} - \mathbf{1} h_0) + \mathcal{I} (p_\tau - \mathbf{1} p_0) \right) \quad (22)$$

Modelling of Water Distribution Networks

System Model Simulation

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction
Modelling of WDN

Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

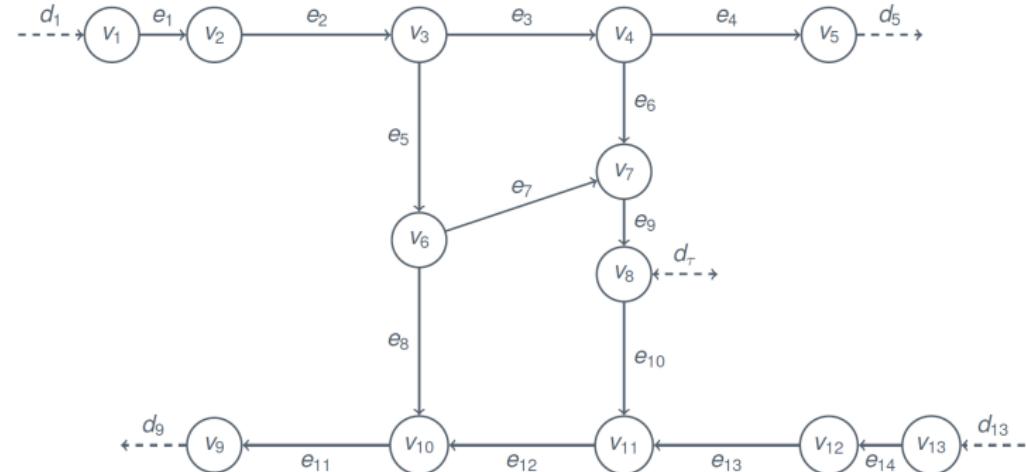
Disturbance Estimator

Network Effects

Results
Best-Case Results
Pathological
Synchronisation

References

56



Modelling of Water Distribution Networks

Slow Dynamics

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

17

► Fundamentals

$$p \propto h$$

$$\dot{V} = q$$

► Assume constant cross sectional area A

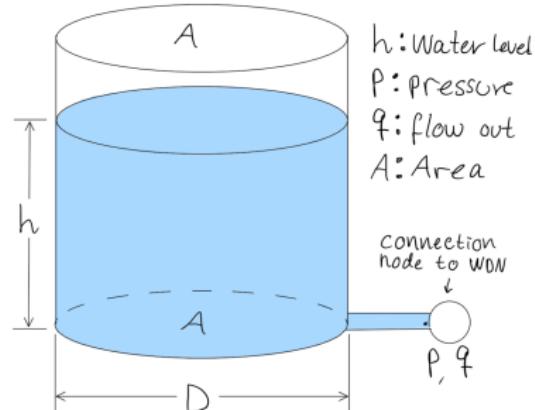
$$V \propto h \implies V \propto p$$

$$\dot{p} \propto \dot{V} \wedge \dot{V} = q \implies \dot{p} \propto q$$

► We arrive at

$$\dot{p} = -\tau q, \text{ where}$$

$$\tau = \rho g \frac{1}{A}$$



56

Modelling of Water Distribution Network

State-space Formulation of Slow Dynamics

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

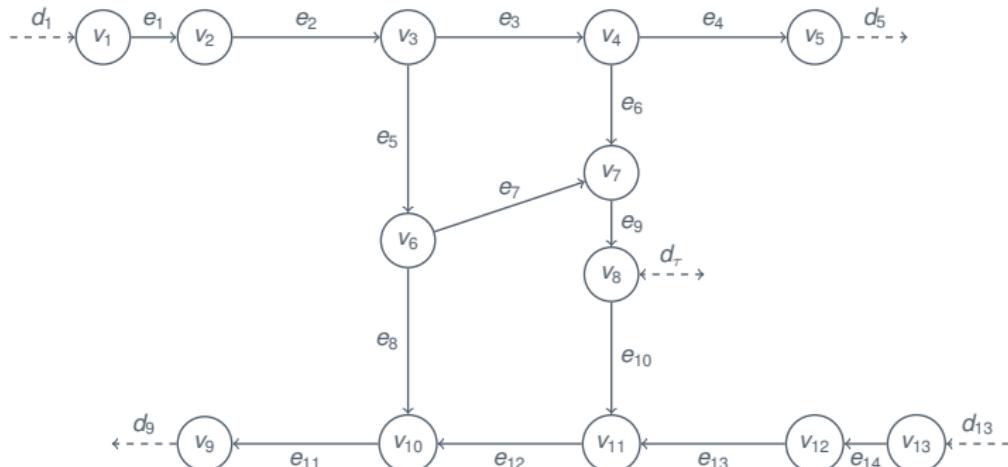
Best-Case Results

Pathological
Synchronisation

References

18

56



In context of WDN we now consider flows to and from network
as external demands d_i



Modelling of Water Distribution Networks

State-space Formulation of Slow Dynamics

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

19

Mass conservation holds, and such

$$d_n = - \sum_{i=1}^{n-1} d_i \implies d_\tau = -(d_p + d_c)$$

$$\dot{p} = -\tau d_\tau = \tau(d_p + d_c)$$

When discretised by forward Euler:

$$p_\tau(k+1) = p_\tau(k) - \tau d_\tau(k) t_s = p_\tau(k) + \tau(d_p(k) + d_c(k)) t_s$$

Which corresponds to a discrete, linear state-space model:

$$p_\tau(k+1) = Ap_\tau(k) + B_p d_p(k) + B_c d_c(k) \quad (23)$$

$$d_p = \begin{bmatrix} d_1 \\ d_{13} \end{bmatrix}, d_c = \begin{bmatrix} d_5 \\ d_9 \end{bmatrix}, B_p = B_c = t_s \begin{bmatrix} \tau & \tau \end{bmatrix}, A = 1$$

56

Modelling of Water Distribution Networks

Linearisation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

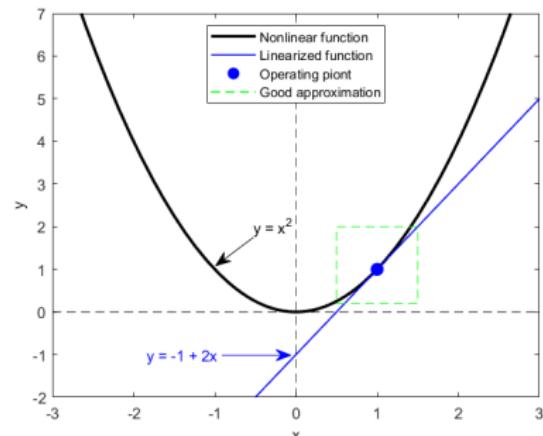
References

20

In near vicinity of
linearisation point x_0 ,

$$\dot{x} \approx f(x_0) + \left. \nabla f \right|_{x_0} (x - x_0)$$

Linearising around
equilibrium point
preferred



56



Modelling of Water Distribution Networks

Linearisation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

21

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Recalling the fast dynamics differential equation is given as

$$\dot{q}_n = -\mathcal{P}\Phi\left(\lambda(q_n) + \mu(q_n, \Theta) + \alpha(q_n, \omega)\right) + \mathcal{P}\left(\Psi(\bar{h} - \mathbf{1}h_0) + \mathcal{I}(p_\tau - \mathbf{1}p_0)\right) \quad (24)$$

The linear model such becomes

$$\dot{q}_n \approx f(x_0) + \frac{\partial f}{\partial q_n} \Big|_{x_0} \tilde{q}_n + \frac{\partial f}{\partial \Theta} \Big|_{x_0} \tilde{\Theta} + \frac{\partial f}{\partial \omega} \Big|_{x_0} \tilde{\omega} + \frac{\partial f}{\partial p_\tau} \Big|_{x_0} \tilde{p}_\tau \quad (25)$$

where $x_0 = \{q_0, \Theta_0, \omega_0, p_{\tau_0}\}$, $\tilde{q} = q - q_0$, likewise for $\tilde{\Theta}$, $\tilde{\omega}$, \tilde{p}_τ



Modelling of Water Distribution Networks

Linearisation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

22

The full linearised model is then obtained as

$$\begin{aligned}\dot{q}_n \approx f(x_0) - \mathcal{P}\Phi & \left(a_1\omega_0 + \left(|q_0| + \text{sign}(q_0)q_0 \right) \right. \\ & \left(K_\lambda + a_2 + \frac{1}{(K_v\Theta_0)^2} \right) \tilde{q}_n \Big) \\ & - \mathcal{P}\Phi \left(\left(-|q_0|q_0 \frac{2}{K_v^2\Theta_0^3} \right) \tilde{\Theta} \right) \\ & - \mathcal{P}\Phi \left(\left(a_1 q_0 + 2a_0\omega_0 \right) \tilde{\omega} \right) \\ & + \mathcal{P}\mathcal{I}\tilde{p}_\tau\end{aligned}\tag{26}$$

The equation can be simplified further making some assumptions

56



Modelling of Water Distribution Networks

Linearisation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

23

Equilibrium disappears, valve and tank dynamics assumed to
be constant disturbances

$$\dot{q}_n \approx -\mathcal{P}\Phi \left(a_1\omega_0 + \left(|q_0| + \text{sign}(q_0)q_0 \right) \left(K_\lambda + a_2 + \frac{1}{(K_v\Theta_0)^2} \right) \tilde{q}_n \right) - \mathcal{P}\Phi \left(\left(a_1 q_0 + 2a_0\omega_0 \right) \tilde{\omega} \right) \quad (27)$$

56

Control Structure

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

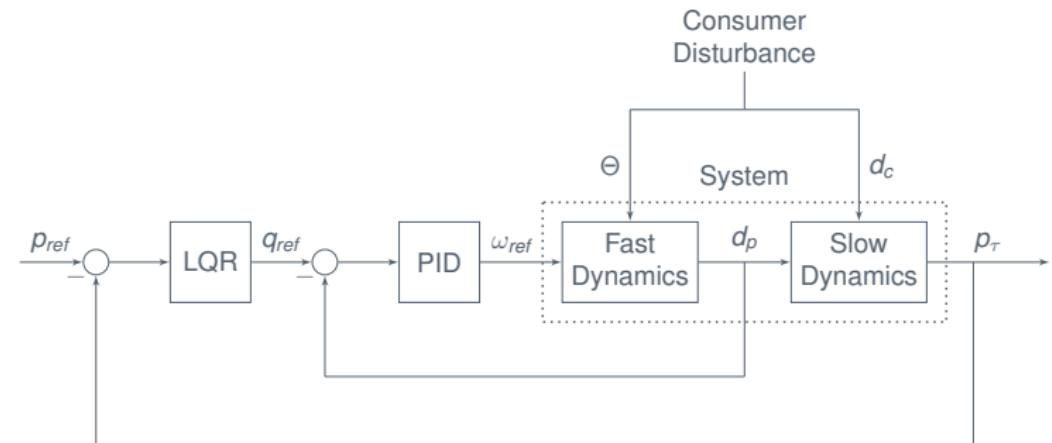
Results

Best-Case Results

Pathological
Synchronisation

References

24



56



Control Structure

The Root Locus Method

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and Root Locus

25

Optimal Control

Disturbance Estimator

Network Effects

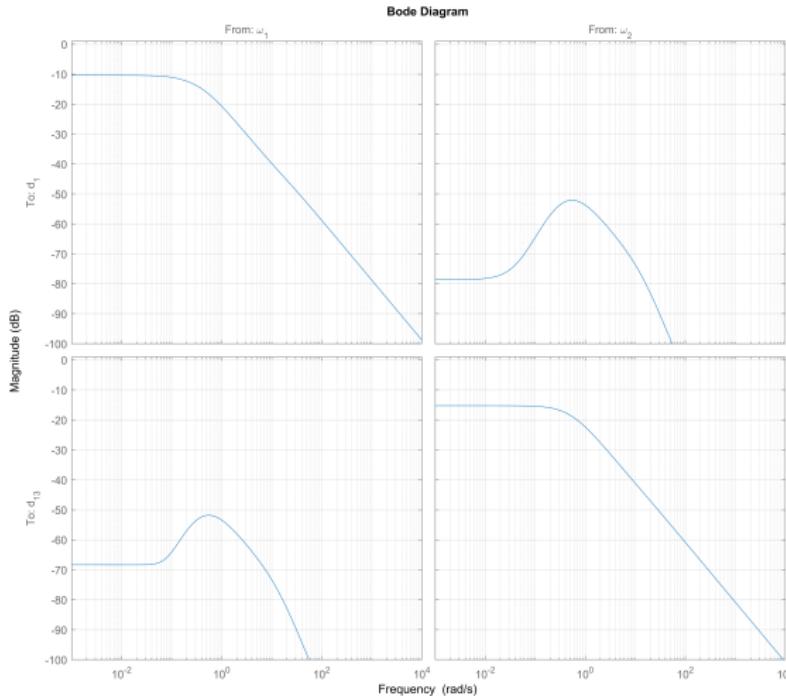
Results

Best-Case Results

Pathological
Synchronisation

References

56



Control Structure

The Root Locus Method

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and Root Locus

26

Optimal Control

Disturbance Estimator

Network Effects

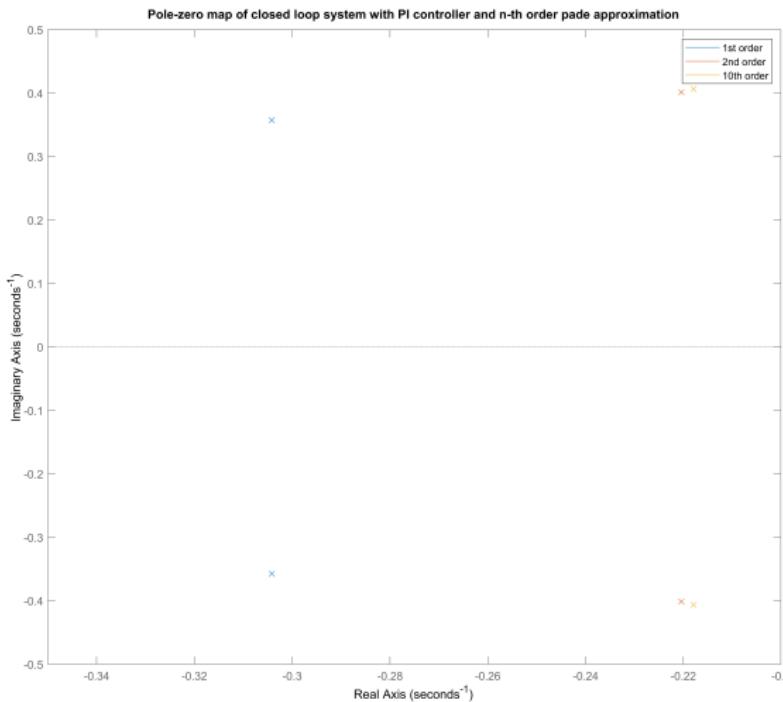
Results

Best-Case Results

Pathological
Synchronisation

References

56



Control Structure

Root Locus and Resulting Controller

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

27

Optimal Control

Disturbance Estimator

Network Effects

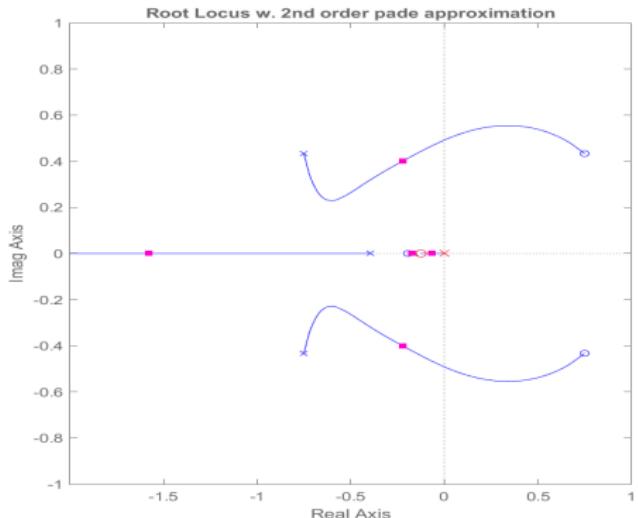
Results

Best-Case Results

Pathological
Synchronisation

References

- ▶ Faster than outer loop.
- ▶ No steady state error.
- ▶ No overshoot, and low amount of oscillation.
- ▶ Stability.



Results in controller transfer function:

$$C(s) = \frac{K_p s + K_i}{s} = \frac{1.8s + 0.225}{s} \quad (28)$$



Control Structure

Step Response

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and Root Locus

28

Optimal Control

Disturbance Estimator

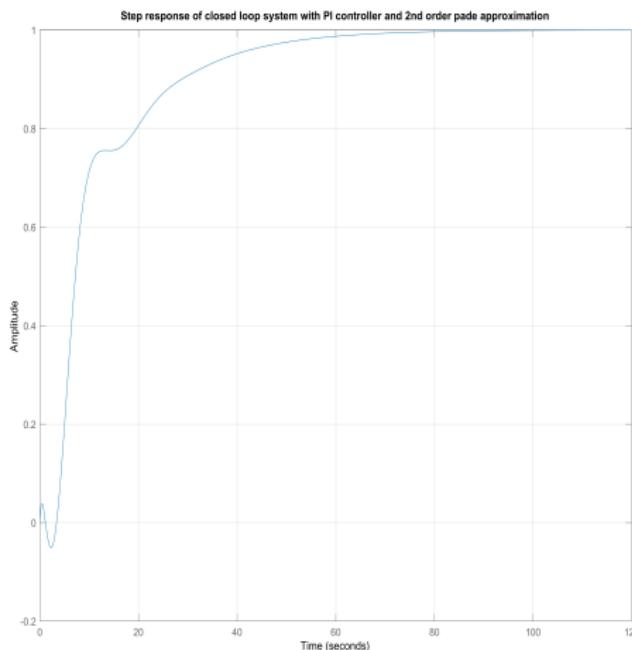
Network Effects

Results

Best-Case Results
Pathological
Synchronisation

References

56





Optimal Control

General Optimal Control Problem

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

29

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

The basic structure of an optimal control problem is sketched in the language of calculus of variations.

$$\dot{x} = f(x, u, t) \quad (29)$$

$$x(t_0) = x_0, x \in \mathbb{R}^n, u \in U \subseteq \mathbb{R}^m \quad (30)$$

where $t \in \mathbb{R}$ is the time and x, u are functions of t , with U the set of admissible controls.

Cost functional:

$$J = \mathcal{M}(x(T)) + \int_0^T \mathcal{L}(x(t), u(t)) dt \quad (31)$$



Infinite-Horizon Linear-Quadratic Regulator

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction
Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation
Control Structure and
Root Locus

Optimal Control
30
Disturbance Estimator
Network Effects
Results
Best-Case Results
Pathological
Synchronisation
References

The LQR time-invariant case with no terminal cost.
System Dynamics:

$$\dot{x}(t) = Ax(t) + Bu(t) \quad (32)$$

Cost functional:

$$J = \int_{t_0}^{\infty} (x^T(t)Qx(t) + u^T(t)Ru(t)) dt \quad (33)$$

State feedback control law:

$$u^*(t) = -R^{-1}B^T Px^*(t) \quad (34)$$

P is time-invariant and fulfills the *algebraic Riccati equation*:

$$PA + A^T P + Q - PBR^{-1}B^T P = 0 \quad (35)$$



Tracking LQR and Integral Action

Tracking LQR

Modelling and
Networked Control of
Water Distribution
Networks
CA733

- Introduction
- Modelling of WDN
- Fast Dynamics and Graph theory
- Slow Dynamics and Linearisation
- Slow Dynamics Linearisation
- Control Structure and Root Locus
- Optimal Control
- Disturbance Estimator
- Network Effects
- Results
 - Best-Case Results
 - Pathological Synchronisation
- References

Let $\hat{x} = x - x_r$ and $\hat{u} = u - u_r$. Shifted coordinate system cost functional framed as an output tracking problem:

$$J = \int_{t_0}^{\infty} ((C^T \hat{x}^T) Q_y (C \hat{x}) + \hat{u}^T R \hat{u}) dt = \int_{t_0}^{\infty} (\hat{y}^T Q_y \hat{y} + \hat{u}^T R \hat{u}) dt \quad (36)$$

- ▶ If linearised around some equilibrium point, these can be used as reference.



Tracking LQR and Integral Action

Integral Action

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

32

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

States are extended with integral state x_i

$$u = -\bar{K}\bar{x} \quad (37)$$

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{B}u + B_r r \quad (38)$$

$$y = \bar{C}\bar{x} \quad (39)$$

$$\bar{A} = \begin{bmatrix} A & 0 \\ -C & 0 \end{bmatrix}, \quad \bar{B} = \begin{bmatrix} B \\ 0 \end{bmatrix}, \quad B_r = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad \bar{C} = [C \quad 0] \quad (40)$$

$$\bar{K} = -[K \quad -K_i] \quad (41)$$

K_i can be an awkward weight to choose.



Velocity-Form LQR

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

33

Disturbance Estimator

Network Effects

Results

Best-Case Results
Pathological
Synchronisation

References

Deviation variables:

$$\Delta x_k = x_k - x_{k-1}, \quad \Delta y_k = y_k - r_k, \quad \Delta u_k = u_k - u_{k-1} \quad (42)$$

Extended vectors and matrices:

$$\begin{aligned}\tilde{\zeta}_k &= \begin{bmatrix} \Delta x_k \\ \Delta y_k \end{bmatrix}, \quad \tilde{u}_k = \Delta u_k, \\ \tilde{A} &= \begin{bmatrix} A & 0 \\ CA & I \end{bmatrix}, \quad \tilde{B} = \begin{bmatrix} B \\ CB \end{bmatrix}, \quad \tilde{C} = [0 \quad I]\end{aligned} \quad (43)$$

Cost functional:

$$J = \sum_{k_0}^{\infty} (\tilde{\zeta}^T Q \tilde{\zeta} + \tilde{u}^T R \tilde{u}) \quad (44)$$

Origin regulation! If $\tilde{\zeta} \rightarrow 0 \Rightarrow \Delta y \rightarrow 0 \Rightarrow y \rightarrow r$.



Velocity-Form LQR

Feedback Law

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

34

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Control input applied at time k is:

$$u^*(k) = \sum_{i=1}^k \Delta u^*(i) = \sum_{i=1}^k \tilde{K} \zeta^*(i) \quad (45)$$

with

$$\tilde{K} = (\tilde{B}^T P \tilde{B} - R)^{-1} (\tilde{B}^T P \tilde{A}) \quad (46)$$

See e.g. Pannocchia et al. [2] for details.



Velocity-Form LQR

Disturbance-accommodating VF-LQR

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

35

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Standard LQR does not accommodate exogenous inputs (such as the model of the consumer demand flows) but can be modified to do so [3]:

$$u(k) = \sum_{i=1}^k \Delta u^*(i) - B^\dagger \mathcal{B} \delta(i) \quad (47)$$

where B^\dagger is the Moore-Penrose pseudoinverse of B and \mathcal{B} is the disturbance input matrix.



Disturbance Estimation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

36

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

Objectives with the use of disturbance estimation

- ▶ VF-LQR controller needs an estimate of the consumer demand.
- ▶ The optimal estimator is the **Kalman Filter**.



Disturbance Estimation

The Kalman Filter

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

37

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

- ▶ Need a linear model of consumer behaviour for the Kalman Filter
- ▶ Under normal circumstances the Kalman gain is found recursively.
- ▶ In the case of LTI system the Kalman filter itself becomes time invariant → constant Kalman gain.
ARE:

$$\begin{aligned}\Pi &= A(\Pi^{-1} + C^T R^{-1} C)^{-1} A^T + Q \\ K &= \Pi C^T (C \Pi C^T + R)^{-1}\end{aligned}\tag{48}$$

- ▶ Kalman filter is also very interesting from a leakage detection POV.

Disturbance Estimation

Water Consumption Data

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

38

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

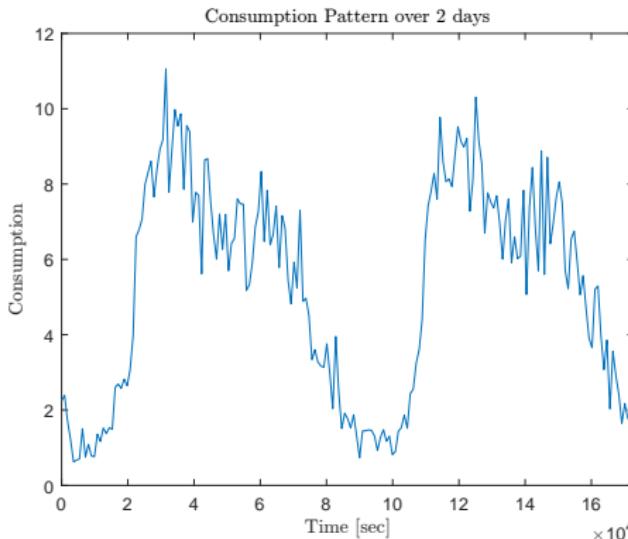


Figure: Consumption pattern over two days

Disturbance Estimation

FFT of Consumption Pattern

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

39

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

- ▶ Frequency analysis of the data.

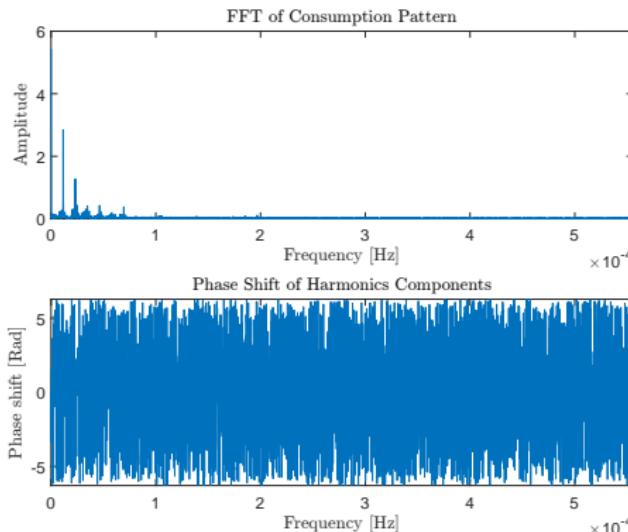


Figure: Amplitude and phase content of full consumption pattern

We want a sparse representation. Largest frequency components are: DC, 24.05hr, 12.03hr, 8.02hr and 5.99hr.



Disturbance Estimation

Approximation of Consumption

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

40

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

- ▶ Fourth-order Fourier approximation of consumer demand:

$$d_c(t) \approx k_0 + k_1 \cos(\omega_1 t + \phi_1) + k_2 \cos(\omega_2 t + \phi_2) \\ + k_3 \cos(3\omega_3 t + \phi_3) + k_4 \cos(4\omega_4 t + \phi_4) \quad (49)$$

- ▶ We wish to model equation 49 as a state-space model:

$$\dot{x} = Ax$$

$$y = Cx$$



Disturbance Estimation

State-space Representation

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

41

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

- ▶ Need to represent the evolution of the "states" in the approximation as a linear combination of states.
- ▶ This can not be achieved using the current states.

$$\dot{x} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -\omega_1 & 0 & 0 \\ 0 & \omega_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -\omega_2 \\ 0 & 0 & 0 & \omega_2 & 0 \end{bmatrix} \begin{bmatrix} k_0 \\ k_1 \cos(\omega_1 t) \\ k_1 \sin(\omega_1 t) \\ k_2 \cos(\omega_2 t) \\ k_2 \sin(\omega_2 t) \end{bmatrix} \quad (50)$$

$$C = [1 \ 1 \ 0 \ 1 \ 0], \quad \dot{x} = \begin{bmatrix} 0 \\ -k_1 \omega_1 \sin(\omega_1 t) \\ k_1 \omega_1 \cos(\omega_1 t) \\ -k_2 \omega_2 \sin(\omega_2 t) \\ k_2 \omega_2 \cos(\omega_2 t) \end{bmatrix} \quad (51)$$

- ▶ Fourth order doesn't fit the page!

Disturbance Estimation

Model vs. Data

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

42

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

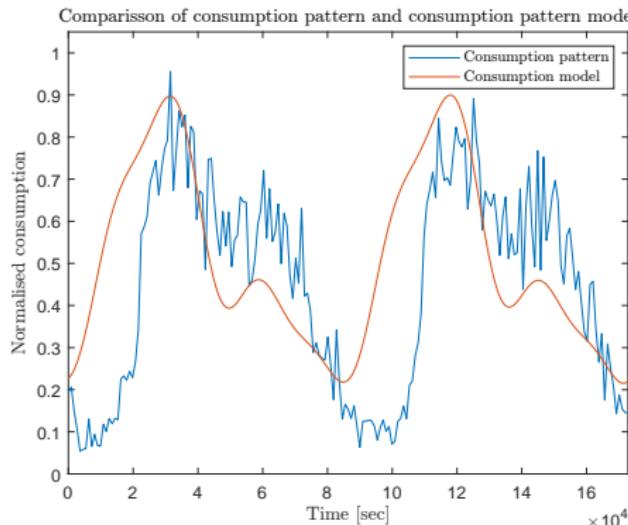


Figure: Comparison of raw historical data, and model

- The model follows the visual trend in real data.

56



Disturbance Estimation

Kalman Filter Design

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus
Optimal Control

Disturbance Estimator

43

Network Effects

Results

Best-Case Results
Pathological
Synchronisation

References

Considerations when designing the KF.

- ▶ In practice the Kalman gain is found using lqr in matlab.
- ▶ Stiffness of the filter is decided by Q-R ratio.
- ▶ Big R means uncertainty concerning observation and that we trust model much → stiff filter.

56

Network Effects

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

44

Results

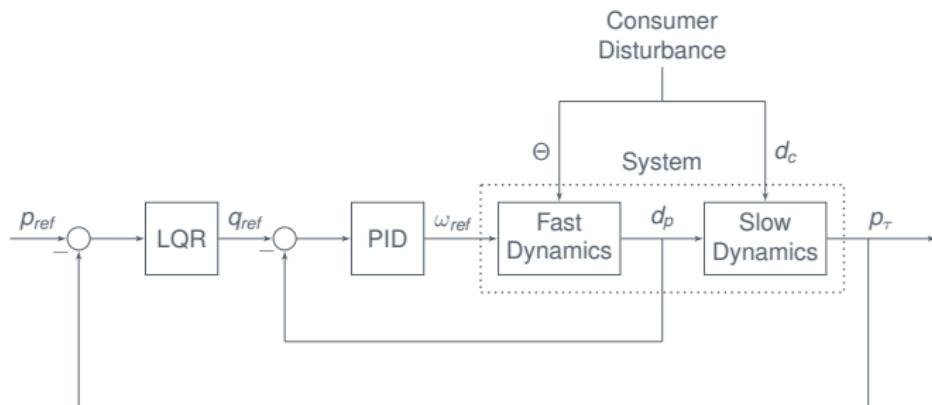
Best-Case Results

Pathological
Synchronisation

References

56

- ▶ Outer loop
 - ▶ Central control unit
 - ▶ Transmit data
- ▶ Urban environment
 - ▶ Packet loss scaling with distance
 - ▶ 60% or more expected at 20 km [4]
- ▶ Try-Once-Discard protocol used
 - ▶ Packet loss → assume states = 0





Network Effects

For Specific Packet Loss

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus
Optimal Control
Disturbance Estimator

Network Effects
Results
Best-Case Results
Pathological
Synchronisation
References

45

- ▶ Packet loss is stochastic, must think in terms of mean-square stability:

$$\lim_{k \rightarrow \infty} E[x(k)^2] = 0 \quad (52)$$

- ▶ Assuming 60% as upper bound for loss, α , the condition for mean-square stability is [5]:

$$S \left(\alpha A \otimes A + (1 - \alpha)(A - BK) \otimes (A - BK) \right) < 1 \quad (53)$$

- ▶ This is because propagation matrix of the state covariance is:

$$\alpha A \otimes A + (1 - \alpha)(A - BK) \otimes (A - BK) \quad (54)$$

- ▶ We get $S = 0.9453$



Network Effects

Upper Loss Bound

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus
Optimal Control

Disturbance Estimator

Network Effects

Results
Best-Case Results
Pathological
Synchronisation
References

46

- ▶ Upper bound on packet loss Ξ . All values $\alpha < \Xi$ will also be stable.

$$\Xi = \frac{1}{\|\sigma_+(V)\|_\infty}$$

$$V = \begin{bmatrix} (S \otimes \hat{S} + \hat{S} \otimes S)(I - S \otimes S)^{-1} & \hat{S} \otimes \hat{S} \\ (I - S \otimes S)^{-1} & 0 \end{bmatrix} \quad (55)$$

$$S = (A - BK) \otimes (A - BK), \quad \hat{S} = A \otimes A - S$$

- ▶ In the limit of zero control:

$$\begin{aligned} \lim_{\tilde{K} \rightarrow 0} & \left(\alpha \tilde{A} \otimes \tilde{A} + (1 - \alpha)(\tilde{A} - \tilde{B}\tilde{K}) \otimes (\tilde{A} - \tilde{B}\tilde{K}) \right) \\ &= \left(\alpha \tilde{A} \otimes \tilde{A} + (1 - \alpha)\tilde{A} \otimes \tilde{A} \right) \end{aligned} \quad (56)$$

56



Network Effects

Upper Loss Bound - Continued

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

47

Thus *any* EWR is marginally stable in the zero limit of control
for any packet loss as $\mathcal{S}(1, 1, 1, 1) = 1$.

$$\begin{aligned} \forall \alpha \in \{0 \dots 1\} : & \left(\alpha \tilde{\mathbf{A}} \otimes \tilde{\mathbf{A}} + (1 - \alpha) \tilde{\mathbf{A}} \otimes \tilde{\mathbf{A}} \right) \\ &= \tilde{\mathbf{A}} \otimes \tilde{\mathbf{A}} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 1 & 0 & 1 & 0 \\ 1 & 1 & 1 & 1 \end{bmatrix} \end{aligned} \quad (57)$$

References

Results

SWIL Laboratory Setup

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results
Pathological
Synchronisation

References



Results

Level Control

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

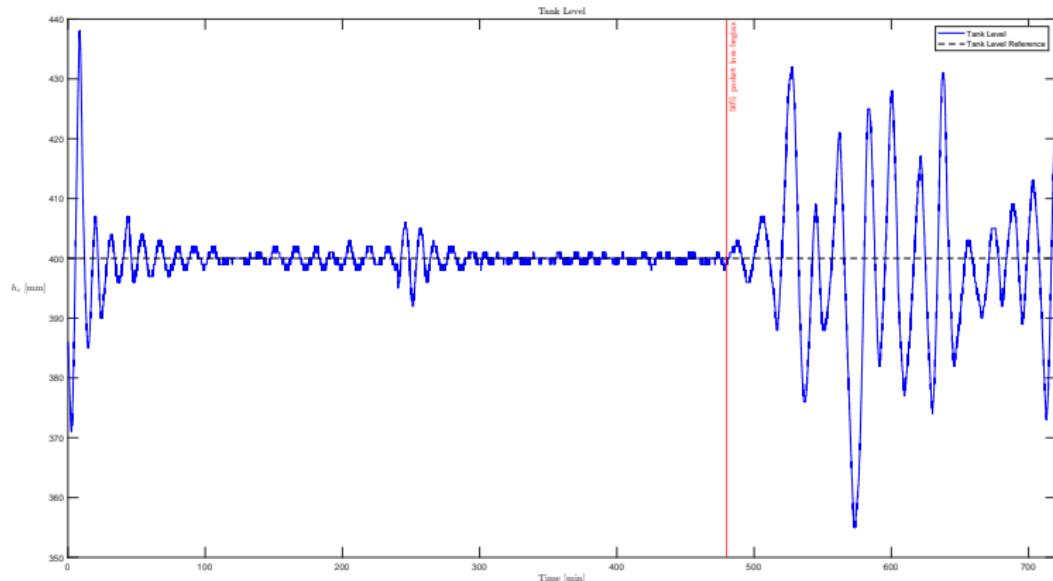
Results

Best-Case Results

Pathological
Synchronisation

References

49



56

Results

Flow Control

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

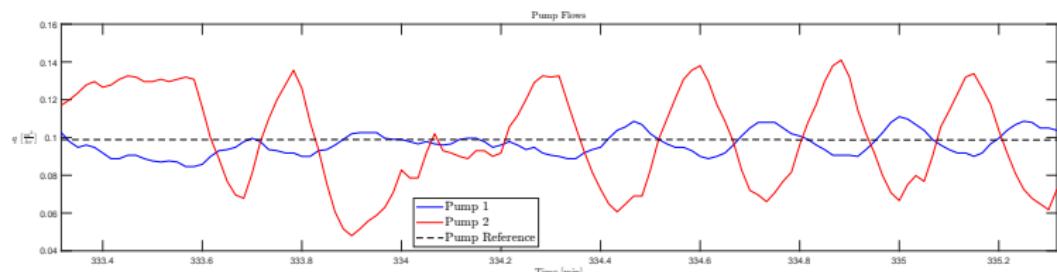
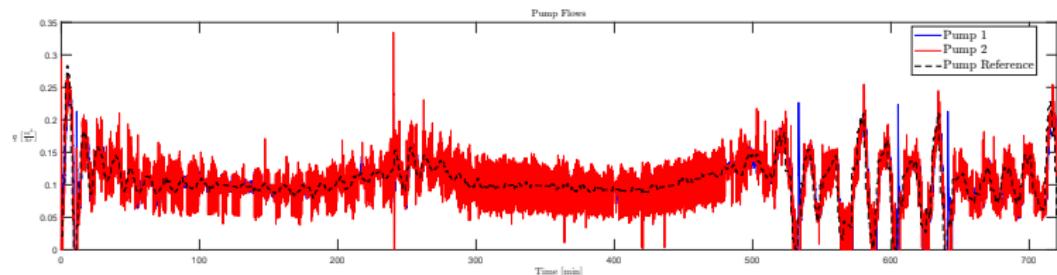
Results

Best-Case Results

Pathological
Synchronisation

References

50



56

Results

Disturbance Estimation

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

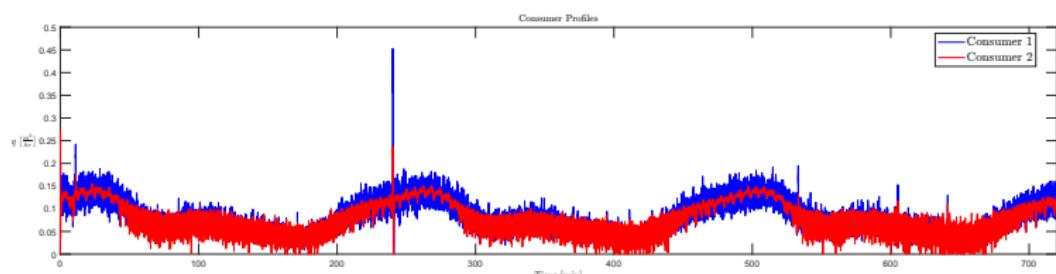
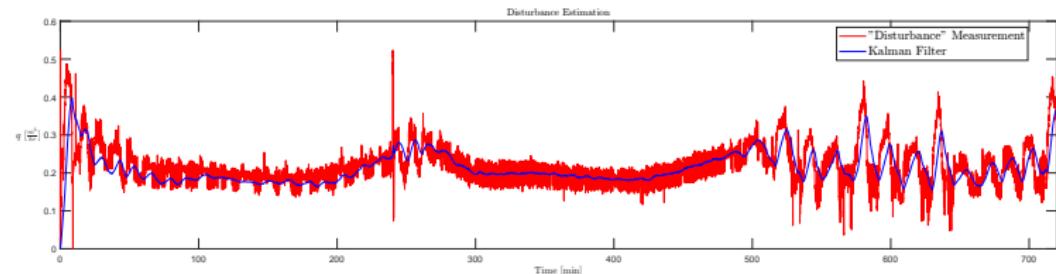
Results

Best-Case Results

Pathological
Synchronisation

References

51





Results

Leakage Detection

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

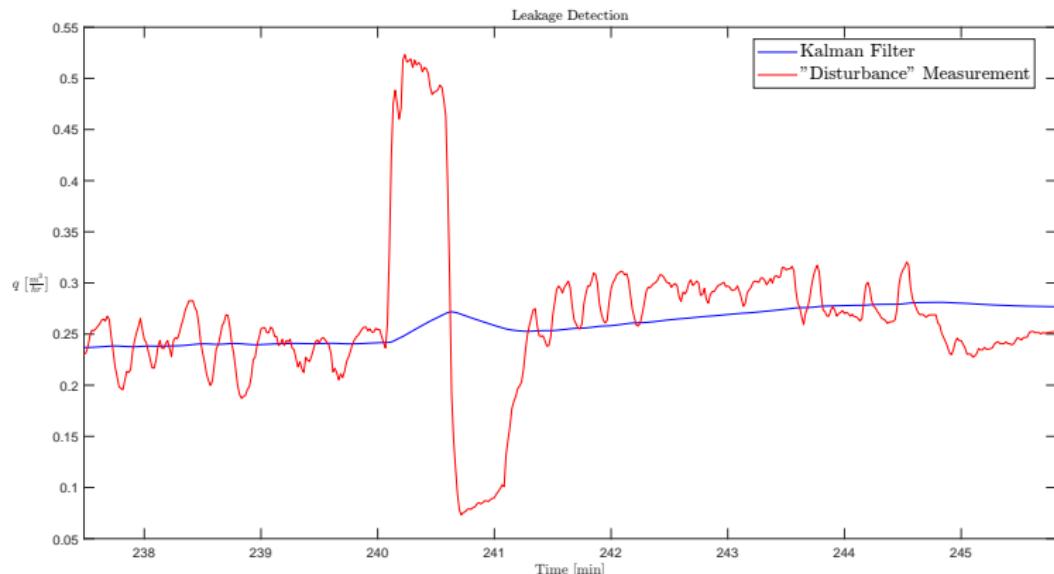
Results

Best-Case Results

Pathological
Synchronisation

References

52



56

Results

Level Control - Pathological Behaviour

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

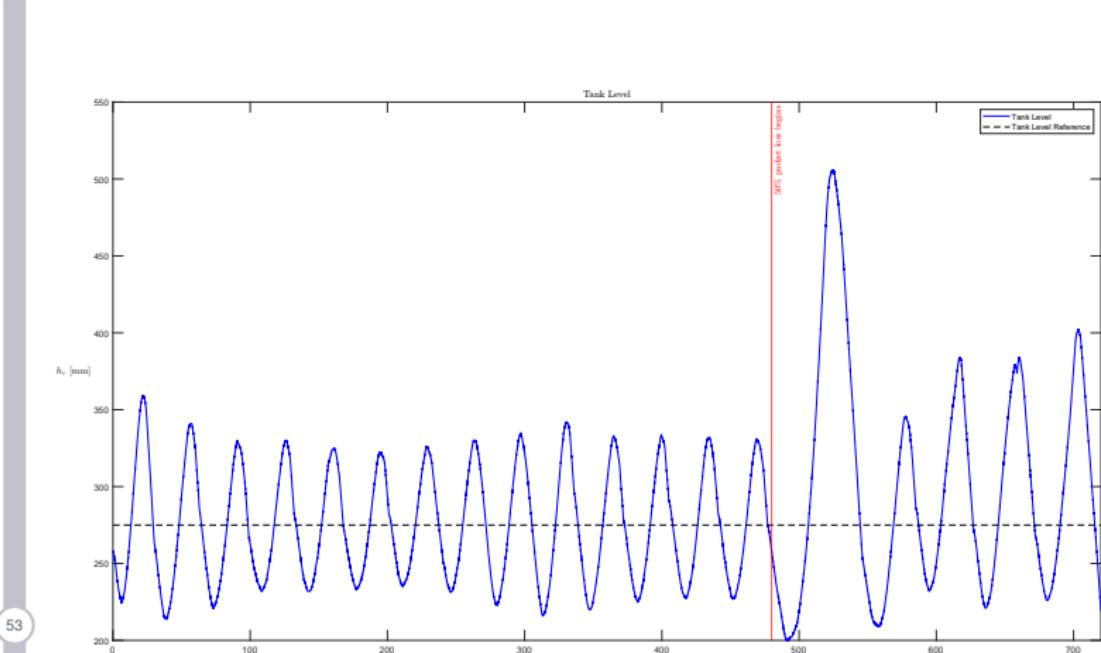
Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References



53

56

Results

Flow Control - Pathological Behaviour

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and Root Locus

Optimal Control

Disturbance Estimator

Network Effects

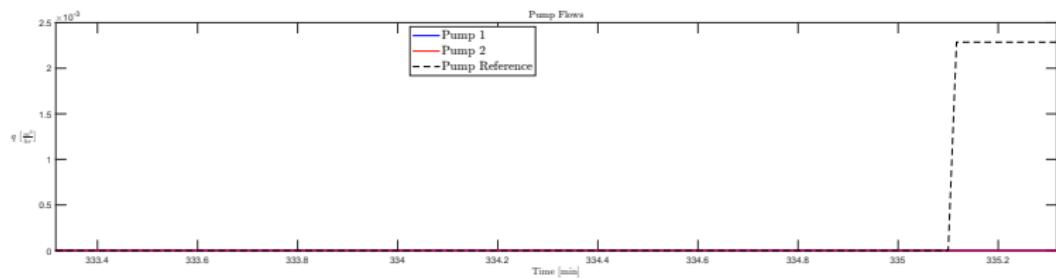
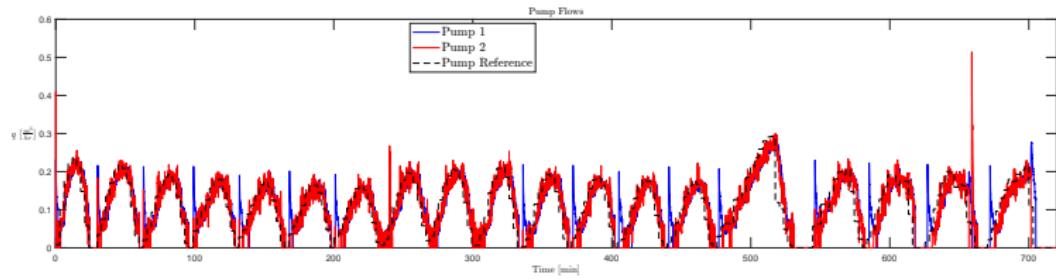
Results

Best-Case Results

Pathological Synchronisation

References

54



Results

Disturbance Estimation - Pathological Behaviour

Modelling and
Networked Control of
Water Distribution
Networks

CA733

Introduction

Modelling of WDN

Fast Dynamics and Graph
theory

Slow Dynamics and
Linearisation

Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

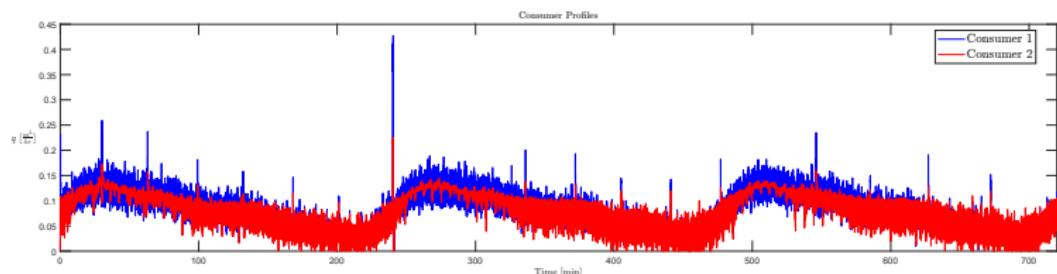
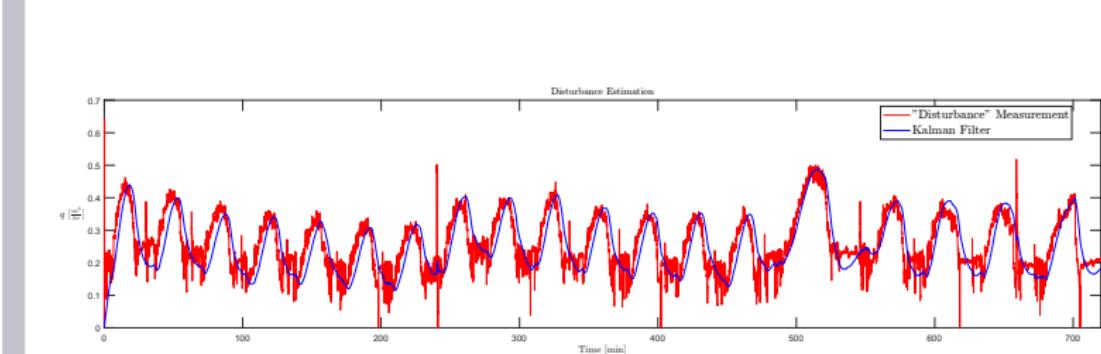
Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References





References

Modelling and
Networked Control of
Water Distribution
Networks
CA733

Introduction

Modelling of WDN
Fast Dynamics and Graph
theory
Slow Dynamics and
Linearisation
Slow Dynamics
Linearisation

Control Structure and
Root Locus

Optimal Control

Disturbance Estimator

Network Effects

Results

Best-Case Results

Pathological
Synchronisation

References

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Open for questions!



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