



CCSI Steady State MEA Model

(MEA ssm)

User Manual

Version 3.0.0

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To obtain support for the products within this package, please send an e-mail to   
[ccsi-support@acceleratecarboncapture.org](mailto:ccsi-support@acceleratecarboncapture.org).

1. Reporting Issues

To report a problem, make a suggestion or ask a question, please either open an issue at our GitHub repository at: <https://github.com/CCSI-Toolset/MEA_ssm/issues> or alternatively send an e-mail to our support list: [ccsi-support@acceleratecarboncapture.org](mailto:ccsi-support@acceleratecarboncapture.org).

1. Version Log

| Product | Version Number | Release Date | Description |
| --- | --- | --- | --- |
| Steady State MEA Model | 3.0.0 | 8/31/2019 | New version of model created for compatibility with Aspen Plus V10. Additional new features include a more rigorous flowsheet and instructions for creating FORTRAN user subroutines needed for the model. |
| Steady State MEA Model | 2.0.0 | 3/31/2018 | Initial Open Source release |
| Steady State MEA Model | 2015.10.0 | 10/16/2015 |  |

MEA Steady State Model

1. Model Development

**Management Plan**

**February 28, 2011**

* 1. Model Background

This document describes a solvent-based CO2 capture system using aqueous monoethanolamine (MEA). The model consists of the “CCSIMEAModel.bkp” file with supporting files “ccsi.opt” and “ccsi10.dll,” which contain FORTRAN user models associated with the simulation. This model was developed to be compatible with Aspen Plus® V10.

This model represents the first version of the “gold standard” model for the MEA capture system. It is composed of individually developed submodels for physical properties of CO2-loaded aqueous MEA solutions and hydraulic and mass transfer models for the system of interest. Each submodel is developed and calibrated with relevant data over the full range of process conditions of interest (e.g., temperature, composition). For each submodel, existing models are considered as candidates and are modified to better fit experimental data over the conditions of interest.

* 1. Physical Property Models

Physical property models developed in this work include standalone models and an integrated thermodynamic framework. Standalone models for viscosity, density, and surface tension of the system have been developed, with uncertainty quantification, as described in Morgan et al.,1 and are implemented as FORTRAN user models. The thermodynamic framework of this system is developed using UT Austin’s Phoenix model2 thermodynamic framework as a precursor. Here, the solution thermodynamics are represented by the ELECNRTL method in Aspen Plus, which uses the Redlich-Kwong equation of state to calculate the vapor phase fugacity coefficients and the electrolyte non-random two liquid   
(e-NRTL) model to calculate the activity coefficients in the liquid phase. Model parameters are calibrated by fitting data for VLE, heat capacity, and heat of absorption for the ternary MEA-H2O-CO2 system and VLE data for the binary MEA-H2O system. The kinetic model used in this work is taken from the Phoenix model, in which the overall ionic speciation of the system is simplified into two equilibrium reactions:

|  |  |  |
| --- | --- | --- |
|  |  | (1) |
|  |  | (2) |

The forward reaction rate constants are taken from the Phoenix model, and the overall reaction rate is written in terms of the equilibrium constants which are also calculated as part of the thermodynamic framework of the system. This follows the methodology presented in Mathias and Gilmartin3, and is implemented to ensure that the reaction kinetics are consistent with the thermodynamic framework.

* 1. Mass Transfer and Hydraulic Models

The hydrodynamic models developed in this work include models for pressure drop and hold-up. The Billet and Schultes4 correlation is regressed with data from Tsai5 for MellapakPlus™ 250Y packing, which is similar to MellapakPlus 252Y packing, which is considered in this work. In this work, a novel and integrated methodology to obtain the mass transfer model is proposed. In this integrated mass transfer model, parameters of the interfacial area, mass transfer coefficients, and diffusivity models are regressed using wetted wall column data from Dugas6 and pilot plant data from Tobiesen et al.7 This required simultaneous regression of process model and property parameters, which was accomplished using the CCSI software Framework for Optimization and Quantification of Uncertainty and Sensitivity (FOQUS).

* 1. Development of Process Model

The aforementioned submodels are integrated into this steady state process model, which is representative of the configuration of the National Carbon Capture Center (NCCC) in Wilsonville, Alabama, for which data have been obtained for validation of this model. No parameters are tuned to improve the fit to the fit to the pilot plant data. The model includes both the absorber and stripper columns, although the recycle of the lean solvent from the regenerator outlet to the absorber inlet is not modeled. The columns are modeled as rate based columns using RateSep™.

The various submodels are implemented in Aspen Plus either as built-in models (e.g., ELECNRTL thermodynamic framework) or FORTRAN user models, in cases where built-in models with the appropriate model form are not available. The user models are combined into a dynamic library (“ccsi10.dll” for this model) and a dynamic linking options (DLOPT) file (“ccsi.opt”) is also provided, which has already been specified in the Aspen Plus file for this model. The various user models contained in the linked library include physical property models for viscosity, density, surface tension, and diffusivity, the hydraulics model, the interfacial area model, and the reaction kinetics model.

* 1. Model Features

The “CCSIMEAModel.bkp” file included is representative of a typical operating case at NCCC and some adjustment of operating variables is possible. Table 1 includes some of these variables and suggested ranges for which the model is expected to work, based on the ranges considered in the testing at NCCC.

Table : Suggested Ranges for Variables in Simulation

| Variable | Range |
| --- | --- |
| Lean Solvent Amine Concentration (g MEA/g MEA+H2O) | 0.25 – 0.35 |
| Lean Solvent CO2 Loading (mol CO2/mol MEA) | 0.05 – 0.50 |
| Lean Solvent Flowrate (kg/hr) | 3000 – 12000 |
| Flue Gas Flowrate (kg/hr) | 1250 – 3000 |
| Regenerator Reboiler Duty (kW) | 150 – 700 |

Table 1 includes the major variables that dictate the performance of the process, although the list is not exhaustive. Other variables, including operating temperature and pressure of the equipment, are set at typical values for the MEA-based CO2 capture process, and slight variation of these variables is allowable. As the lean solvent flowrate is decreased, the intercooler flow rates should be adjusted accordingly. **Note:** The apparent mole fractions of molecular species may be calculated from the amine concentration (γ) and CO2 loading (α) using the equations:

|  |  |  |
| --- | --- | --- |
|  |  | (3) |
|  |  | (4) |
|  |  | (5) |

1. Tutorial
   1. Creating Fortran Subroutines

This is an optional tutorial for those users who wish to directly develop the Fortran subroutines used in this model and compile them as a dll file. Otherwise, the user may use the provided ‘ccsi.opt’ and ‘ccsi10.dll’ files and skip to the tutorial in section 2.2. In order to start working on the Fortran files, ensure that a compiler is installed in the machine. The compiler used by the authors of this manual is: “Intel Visual Fortran Composer XE 2011 Update 12 for Windows”. This is an external application that requires a license file (to be obtained by the user). Double click the application file to begin the compiler installation, and complete it by following the instructions on the window.

Once the installation is complete, open the Aspen Application “Set Compiler for V10”, and check the status of the sections. At least one of them must display the status “OK” which would confirm the successful installation of the compiler.

To obtain FORTRAN template *.f* files distributed with Aspen Tech software, navigate to the following folder:

C:\Program Files (x86)\AspenTech\Aspen Plus V10.0\Engine\User

For other versions of AspenTech software, the template files may be found in the folder corresponding to the specific version. The user is now required to make changes to the template files as directed in the subsections.

* + 1. Viscosity Model

For the liquid viscosity model, open the file (*mul2u2.f*). In the section of the code titled ‘DECLARE ARGUMENTS’, add the following code for declaring additional defined variables that are not included in the template. The existing code in this section of the template should not be deleted, as it is needed to declare the major input and output variables of the subroutine.

INTEGER DMS\_KCCIDC,I

INTEGER IH2O,IMEA,IMEACOO,ICO2,IMEAH,IHCO3

REAL\*8 XX(100),SUM,DSUM,DPSUM

REAL\*8 A,B,C,D,E,F,G

REAL\*8 MUW,XCO2T,XMEAT,XH2OT,LDG,WTMEA,MUBLEND

In the ‘BEGIN EXECUTABLE CODE’ section, remove the template code that has been provided. Note that the final section of the template code, in which defines the final liquid viscosity (MUMX), its temperature derivative (DMUMX), and its pressure derivative (DPMUMX), must not be deleted. Insert the following code under the ‘BEGIN EXECUTABLE CODE’:

IH2O = DMS\_KCCIDC('H2O')

IMEA = DMS\_KCCIDC('MEA')

IMEACOO = DMS\_KCCIDC('MEACOO-')

ICO2 = DMS\_KCCIDC('CO2')

IMEAH = DMS\_KCCIDC('MEA+')

IHCO3 = DMS\_KCCIDC('HCO3-')

DO I=1,100

XX(I) = 0

END DO

DO I=1,N

IF (IDX(I). EQ. IH2O) XX(IH2O) = Z(I)

IF (IDX(I). EQ. IMEA) XX(IMEA) = Z(I)

IF (IDX(I). EQ. IMEACOO) XX(IMEACOO) = Z(I)

IF (IDX(I). EQ. ICO2) XX(ICO2) = Z(I)

IF (IDX(I). EQ. IMEAH) XX(IMEAH) =Z(I)

IF (IDX(I). EQ. IHCO3) XX(IHCO3) = Z(I)

END DO

A = MULU2A(1,IMEA)

B = MULU2A(2,IMEA)

C = MULU2A(3,IMEA)

D = MULU2A(4,IMEA)

E = MULU2A(5,IMEA)

F = MULU2A(1,IH2O)

G = MULU2A(2,IH2O)

MUW = 1.002

MUW=MUW\*10\*\*(1.3272\*(293.15-T-0.001053\*(T-293.15)\*\*2)/(T-168.15))

XCO2T = XX(IMEACOO) + XX(IHCO3) + XX(ICO2)

XMEAT = XX(IMEACOO) + XX(IMEAH) + XX(IMEA)

XH2OT = XX(IHCO3) + XX(IH2O)

LDG = XCO2T/XMEAT

WTMEA = XMEAT\*XMW(IMEA) + XH2OT\*XMW(IH2O)

WTMEA = 100\*((XMEAT\*XMW(IMEA))/WTMEA)

MUBLEND=(A\*WTMEA+B)\*T+(C\*WTMEA+D)

MUBLEND=MUBLEND\*(LDG\*(E\*WTMEA+F\*T+G)+1)\*WTMEA

MUBLEND=DEXP(MUBLEND/T\*\*2)

IF (XMEAT.EQ.0) THEN

SUM=MUI(IH2O)

ELSE IF (XH2OT.EQ.0) THEN

SUM=DEXP(-102.07+7992.1/T+13.724\*LOG(T))/1000

ELSE

SUM=MUBLEND\*MUW/1000

END IF

The existing RETURN & END statements at the end of the code must be retained. Ensure that the inserted code lines do not get commented.

* + 1. Molar Volume Model

For the liquid molar volume model, the process is analogous to that used for the viscosity model. In the folder that contains the Fortran templates, select ‘*vl2u2.f*’. The following code should be added to the ‘DECLARE ARGUMENTS’ section without deleting the existing code:

INTEGER DMS\_KCCIDC,I

INTEGER IH2O,IMEA,IMEACOO,ICO2,IMEAH,IHCO3

REAL\*8 XX(100),SUM,DSUM,DPSUM

REAL\*8 A,B,C,D,E

REAL\*8 AM,BM,CM,AW,BW,CW

REAL\*8 VH2O,VMEA

REAL\*8 XCO2T,XMEAT,XH2OT,XTOT

REAL\*8 XCO2,XMEA,XH2O

In the section marked ‘BEGIN EXECUTABLE CODE’, remove the template code and replace with the code given below. Note that the final section of the template code, in which defines the final liquid molar volume (VMX), its temperature derivative (DVMX), and its pressure derivative (DPVMX), must not be deleted.

IH2O = DMS\_KCCIDC('H2O')

IMEACOO = DMS\_KCCIDC('MEACOO-')

ICO2 = DMS\_KCCIDC('CO2')

IMEAH = DMS\_KCCIDC('MEA+')

IHCO3 = DMS\_KCCIDC('HCO3-')

IMEA = DMS\_KCCIDC('MEA')

DO I=1,100

XX(I) = 0

END DO

DO I=1,N

IF (IDX(I). EQ. IH2O) XX(IH2O) = Z(I)

IF (IDX(I). EQ. IMEA) XX(IMEA) = Z(I)

IF (IDX(I). EQ. IMEACOO) XX(IMEACOO) = Z(I)

IF (IDX(I). EQ. ICO2) XX(ICO2) = Z(I)

IF (IDX(I). EQ. IMEAH) XX(IMEAH) =Z(I)

IF (IDX(I). EQ. IHCO3) XX(IHCO3) = Z(I)

END DO

A = VL2U2A(1,IMEA)

B = VL2U2A(2,IMEA)

C = VL2U2A(3,IMEA)

D = VL2U2A(4,IMEA)

E = VL2U2A(5,IMEA)

AM=-0.000000535162

BM=-0.000451417

CM=1.19451

AW=-0.00000324839

BW=0.00165311

CW=0.793041

VH2O = XMW(IH2O)/(AW\*T\*\*2+BW\*T+CW)

VMEA = XMW(IMEA)/(AM\*T\*\*2+BM\*T+CM)

XCO2T = XX(IMEACOO) + XX(IHCO3) + XX(ICO2)

XMEAT = XX(IMEACOO) + XX(IMEAH) + XX(IMEA)

XH2OT = XX(IHCO3) + XX(IH2O)

XTOT = XCO2T+XMEAT+XH2OT

XCO2 = XCO2T/XTOT

XMEA = XMEAT/XTOT

XH2O = XH2OT/XTOT

SUM = XMEA\*VMEA + XH2O\*VH2O + XCO2\*A + XMEA\*XH2O\*(B+C\*XMEA)

SUM = SUM+XMEA\*XCO2\*(D+E\*XMEA)

IF (XMEA.EQ.0) THEN

SUM=VI(IH2O)

ELSE IF (XH2O.EQ.0) THEN

SUM=VMEA/1000

ELSE

SUM=SUM/1000

END IF

DSUM=0D0

DPSUM=0D0

The existing RETURN & END statements at the end of the code must be retained.

* + 1. Surface Tension Model

The process for creating the surface tension model is very similar to the process used for the viscosity and molar volume models. In the folder containing the Fortran templates, select ‘*sig2u2.f*’. The following code should be added to the ‘DECLARE ARGUMENTS’ section without deleting the existing code:

INTEGER DMS\_KCCIDC,I

INTEGER IH2O,IMEA,IMEACOO,ICO2,IMEAH,IHCO3

REAL\*8 XX(100),SUM,DSUM,DPSUM

REAL\*8 A,B,C,D,E,F,G,H,K,J

REAL\*8 S1,S2,S3,S4,S5,S6

REAL\*8 C1W,C1M,C2W,C2M,C3W,C3M,C4W,C4M,TCW,TCM

REAL\*8 XMEAT,XCO2T,XH2OT

REAL\*8 XMEA,XCO2,XH2O,LDG,WTMEA

REAL\*8 FXNF,FXNG,SIGCO2,SIGH2O,SIGMEA

In the ‘BEGIN EXECUTABLE CODE’ section, remove the template code and replace with the code given below. Note that the final section of the template code, in which defines the final liquid surface tension (STMX), its temperature derivative (DSTMX), and its pressure derivative (DPSTMX), must not be deleted.

IH2O = DMS\_KCCIDC('H2O')

IMEA = DMS\_KCCIDC('MEA')

IMEACOO = DMS\_KCCIDC('MEACOO-')

ICO2 = DMS\_KCCIDC('CO2')

IMEAH = DMS\_KCCIDC('MEA+')

IHCO3 = DMS\_KCCIDC('HCO3-')

DO I=1,100

XX(I) = 0

END DO

DO I=1,N

IF (IDX(I). EQ. IH2O) XX(IH2O) = Z(I)

IF (IDX(I). EQ. IMEA) XX(IMEA) = Z(I)

IF (IDX(I). EQ. IMEACOO) XX(IMEACOO) = Z(I)

IF (IDX(I). EQ. ICO2) XX(ICO2) = Z(I)

IF (IDX(I). EQ. IMEAH) XX(IMEAH) =Z(I)

IF (IDX(I). EQ. IHCO3) XX(IHCO3) = Z(I)

END DO

A=SIGU2A(1,IMEA)

B=SIGU2A(2,IMEA)

C=SIGU2A(3,IMEA)

D=SIGU2A(4,IMEA)

E=SIGU2A(5,IMEA)

F=SIGU2A(1,IH2O)

G=SIGU2A(2,IH2O)

H=SIGU2A(3,IH2O)

K=SIGU2A(4,IH2O)

J=SIGU2A(5,IH2O)

S1=-5.987

S2=3.7699

S3=-0.43164

S4=0.018155

S5=-0.01207

S6=0.002119

C1W=0.18548

C1M=0.09945

C2W=2.717

C2M=1.067

C3W=-3.554

C3M=0

C4W=2.047

C4M=0

TCW=647.13

TCM=614.45

XCO2T=XX(IMEACOO)+XX(IHCO3)+XX(ICO2)

XMEAT=XX(IMEACOO)+XX(IMEAH)+XX(IMEA)

XH2OT=XX(IH2O)+XX(IHCO3)

WTMEA=(XMW(IMEA)\*XMEAT)/(XMW(IMEA)\*XMEAT+XMW(IH2O)\*XH2OT)

LDG=XCO2T/XMEAT

XMEA=(1+LDG+(XMW(IMEA)/XMW(IH2O))\*(1-WTMEA)/WTMEA)\*\*(-1)

XCO2=XMEA\*LDG

XH2O=1-XMEA-XCO2

FXNF=A+B\*LDG+C\*LDG\*\*2+D\*WTMEA+E\*WTMEA\*\*2

FXNG=F+G\*LDG+H\*LDG\*\*2+K\*WTMEA+J\*WTMEA\*\*2

SIGCO2=S1\*WTMEA\*\*2+S2\*WTMEA+S3+T\*(S4\*WTMEA\*\*2+S5\*WTMEA+S6)

SIGH2O=C1W\*(1-T/TCW)\*\*(C2W+C3W\*(T/TCW)+C4W\*(T/TCW)\*\*2)

SIGMEA=C1M\*(1-T/TCM)\*\*(C2M+C3M\*(T/TCM)+C4M\*(T/TCM)\*\*2)

SUM=SIGH2O+(SIGCO2-SIGH2O)\*FXNF\*XCO2+(SIGMEA-SIGH2O)\*FXNG\*XMEA

IF (XMEAT.EQ.0) THEN

SUM=STI(IH2O)

ELSE IF (XH2OT.EQ.0) THEN

SUM=SIGMEA

ELSE

SUM=SUM

END IF

DSUM=0D0

DPSUM=0D0

The existing RETURN & END statements at the end of the code must be retained.

* + 1. Liquid Diffusivity Model

Select the template ‘dl0u.f’ and add the following statement, required for accessing component data stored in the labeled common DMS\_PLEX, to the end of the ‘DECLARE VARIABLES USED IN DIMENSIONING’ section.

#include "dms\_plex.cmn"

Ensure that the other # include statements are retained.

The following code should be added to the ‘DECLARE ARGUMENTS’ section of the subroutine without deleting the existing code:

INTEGER DMS\_KCCIDC,DMS\_IFCMNC,NBOPST(6),NAME(2)

INTEGER IH2O,IMEA,IMEACOO,ICO2,IMEAH,IHCO3,IN2,IO2

REAL\*8 VISC,MUMX

REAL\*8 E,MU0,THET,A,BB,C,R,HG,MUW

REAL\*8 B(1)

EQUIVALENCE (B(1),IB(1))

INTEGER DFACT\_IDX,EFACT\_IDX

REAL\*8 DFACTCO2,DFACTMEA,EFACT,CO2DW,CO2D,MEAD

Remove all code given in the template’s ‘BEGIN EXECUTABLE CODE’ section, leaving only the final ‘END’ statement. Replace this code with the following:

IH2O = DMS\_KCCIDC('H2O')

IMEA = DMS\_KCCIDC('MEA')

IMEACOO = DMS\_KCCIDC('MEACOO-')

ICO2 = DMS\_KCCIDC('CO2')

IMEAH = DMS\_KCCIDC('MEA+')

IHCO3 = DMS\_KCCIDC('HCO3-')

IN2 = DMS\_KCCIDC('N2')

IO2 = DMS\_KCCIDC('O2')

CALL PPUTL\_GOPSET(NBOPST,NAME)

CALL PPMON\_VISCL (T, P, X, N, IDX, NBOPST, KDIAG, VISC, KER)

MUMX = VISC

E = 4.753D0

MU0 = 0.000024055D0

THET = 139.7D0

A = 0.000442D0

BB = 0.0009565D0

C = 0.0124D0

R = 0.008314D0

P = P / 100000D0

HG = A \* P +((E - BB \* P)/(R \* (T - THET - C \* P)))

MUW = (MU0 \* EXP(HG))

DFACT\_IDX = DMS\_IFCMNC('DFACT1')

EFACT\_IDX = DMS\_IFCMNC('EFACT')

DFACTCO2 = B(DFACT\_IDX+IDX(ICO2))

DFACTMEA = B(DFACT\_IDX+IDX(IMEA))

EFACT = B(EFACT\_IDX+IDX(ICO2))

CO2DW = 0.00000235D0\*EXP(-2119D0/T)

CO2D = CO2DW \* (MUW / MUMX)\*\*(0.8D0)\*((T/313.15)\*\*(EFACT))

CO2D = CO2D \* DFACTCO2

CO2D = ((DFACTCO2)\*\*2)/DFACTMEA \* (MUW/MUMX)\*\*0.8

CO2D = CO2D\*(T/313.15)\*\*(EFACT)

MEAD = (1/((MUMX/MUW)\*\*0.8D0))\*((T/313.15)\*\*(EFACT))

MEAD = MEAD \* DFACTMEA

DO 200 I = 1, N

DO 100 J = 1, N

IF (I.EQ.J) THEN

QBIN(I,J) = 0D0

ELSE

QBIN(I,J) = MEAD

IF (I.EQ.ICO2)QBIN(I,J) = CO2D

IF (J.EQ.ICO2)QBIN(I,J) = CO2D

IF (I.EQ.IN2)QBIN(I,J) = CO2D

IF (J.EQ.IN2)QBIN(I,J) = CO2D

END IF

100 CONTINUE

200 CONTINUE

* + 1. Reaction Kinetics Model

The template to be used for the reaction kinetics model is titled ‘usrknt.f’, which is designed specifically for use with reaction kinetics in rate-based columns (REACT-DIST type reaction). The following code should be placed at the end of the ‘DECLARE VARIABLES USED IN DIMENSIONING’ section, after the code lines EQUIVALENCE (RMISS, USER\_RUMISS) & EQUIVALENCE (IMISS, USER\_IUMISS):

#include "dms\_rglob.cmn"

#include "dms\_lclist.cmn"

#include "pputl\_ppglob.cmn"

#include "dms\_ipoff3.cmn"

#include "dms\_plex.cmn"

EQUIVALENCE(IB(1),B(1))

The following code should be placed in the ‘DECLARE ARGUMENTS’ section without deleting the existing code:

INTEGER I,K,FN,L\_GAMMA,L\_GAMUS,GAM,US,DMS\_KFORMC,KPHI,KER

INTEGER DMS\_ALIPOFF3,IHELGK

REAL\*8 B(1)

REAL\*8 N\_H2O,N\_CO2,N\_MEA,N\_MEAH,N\_MEAC,N\_HCO3

REAL\*8 PHI(100),DPHI(100),GAMMA(100),COEFFCO2,COEFFMEA

REAL\*8 ACCO2,ACMEA,ACH2O,ACMEAH,ACMEAC,ACHCO3,R,STOI(100),LNRKO

REAL\*8 DUM,KEQ1,KEQ2,RXNRATES(100)

The following code should be placed in the ‘BEGIN EXECUTABLE CODE’ section:

FN(I) = I+LCLIST\_LBLCLIST

L\_GAMMA(I) = FN(GAM) + I

L\_GAMUS(I) = FN(US) + I

N\_H2O = DMS\_KFORMC('H2O')

N\_CO2 = DMS\_KFORMC('CO2')

N\_MEA = DMS\_KFORMC('C2H7NO')

N\_MEAH = DMS\_KFORMC('C2H8NO+')

N\_MEAC = DMS\_KFORMC('C3H6NO3-')

N\_HCO3 = DMS\_KFORMC('HCO3-')

T = TLIQ

KPHI = 1

CALL PPMON\_FUGLY(T,P,X,Y,NCOMP,IDX,NBOPST,KDIAG,KPHI,PHI,DPHI,KER)

GAM = DMS\_ALIPOFF3(24)

DO I=1,NCOMP

GAMMA(I)=1.D0

IF (INT(1).EQ.1) GAMMA(I) = DEXP(B(L\_GAMMA(I)))

END DO

US = DMS\_ALIPOFF3(29)

COEFFCO2 = DEXP(B(L\_GAMUS(N\_CO2)))

COEFFMEA = DEXP(B(L\_GAMUS(N\_MEA)))

ACCO2 = COEFFCO2\*X(N\_CO2,1)

ACMEA = COEFFMEA\*X(N\_MEA,1)

ACH2O = GAMMA(N\_H2O)\*X(N\_H2O,1)

ACMEAH = GAMMA(N\_MEAH)\*X(N\_MEAH,1)

ACMEAC = GAMMA(N\_MEAC)\*X(N\_MEAC,1)

ACHCO3 = GAMMA(N\_HCO3)\*X(N\_HCO3,1)

R = PPGLOB\_RGAS/1000

DO I=1,100

STOI(I) = 0D0

END DO

DO I=1,NCOMP

IF (IDX(I).EQ.N\_MEA) STOI(I)=-2D0

IF (IDX(I).EQ.N\_CO2) STOI(I)=-1D0

IF (IDX(I).EQ.N\_MEAH) STOI(I)=1D0

IF (IDX(I).EQ.N\_MEAC) STOI(I)=1D0

END DO

LNRKO = RGLOB\_RMISS

CALL PPELC\_ZKEQ(T,1,1,0,STOI,0D0,NCOMP,IDX,0,1,1,NBOPST,KDIAG,

2 LNRKO,P,IHELGK,DUM,0,0,0)

KEQ1 = DEXP(LNRKO)

DO I=1,100

STOI(I) = 0D0

END DO

DO I=1,NCOMP

IF (IDX(I).EQ.N\_MEA) STOI(I)=-1D0

IF (IDX(I).EQ.N\_CO2) STOI(I)=-1D0

IF (IDX(I).EQ.N\_H2O) STOI(I)=-1D0

IF (IDX(I).EQ.N\_MEAH) STOI(I)=1D0

IF (IDX(I).EQ.N\_HCO3) STOI(I)=1D0

ENDDO

LNRKO = RGLOB\_RMISS

CALL PPELC\_ZKEQ(T,1,1,0,STOI,0D0,NCOMP,IDX,0,1,1,NBOPST,KDIAG,

2 LNRKO,P,IHELGK,DUM,0,0,0)

KEQ2 = DEXP(LNRKO)

RXNRATES(1)=REAL(1)\*DEXP(-REAL(3)/R\*(1/TLIQ-1/298.15))\*

2 (ACMEA\*\*2\*ACCO2-ACMEAC\*ACMEAH/KEQ1)

RXNRATES(2)=REAL(2)\*DEXP(-REAL(4)/R\*(1/TLIQ-1/298.15))\*

2 (ACMEA\*ACCO2-ACMEAH\*ACHCO3/(KEQ2\*ACH2O))

DO K=1,NRL(1)

RXNRATES(K) = RXNRATES(K)\*HLDLIQ

RATEL(K) = RXNRATES(K)

END DO

DO I=1,NCOMP

RATES(I)=0.D0

END DO

DO K=1,NRL(1)

DO I=1,NCOMP

IF (DABS(STOIC(I,K)).GE.RGLOB\_RMIN) RATES(I) = RATES(I) +

2 STOIC(I,K)\*RXNRATES(K)

END DO

END DO

The existing RETURN & END statements at the end of the code must be retained.

* + 1. Interfacial Area Model

The template to be used for the interfacial area model is titled ‘*usrintfa.f*’. The following should be added to the section stating ‘Declare local variables used in the user correlations’:

REAL\*8 Aa,Bb

Remove the equations defining the variable ‘dTemp’ and replace with the following:

Aa = REAL(2)

Bb = REAL(3)

dTemp = Aa\*((WeL\*FrL\*\*(-1/3))\*\*Bb)

The existing RETURN & END statements at the end of the code must be retained.

* + 1. Holdup Model

The template to be used for the liquid and vapor holdup in the RateSep routine is titled ‘usrhldup.f’. No additional variable names need to be declared. Remove the code between the statements {IF (COLTYP .EQ. 1) THEN} and {ELSE IF (COLTYP .EQ. 2) THEN}. Insert the following replacement code:

IF (USRCOR .EQ. 1) THEN

RHOL = AVMWLI\*DENMXL

UL = FRATEL/DENMXL/TWRARA

HT=REAL(1)\*(3.185966\*(VISCML/RHOL)\*\*0.3333\*(UL))

+\*\*REAL(2)

LHLDUP = HT \* TWRARA \* HTPACK

VHLDUP = (1D0 - HT - VOIDFR) \* TWRARA \* HTPACK

END IF

The existing RETURN & END statements at the end of the code must be retained.

* + 1. Creation of dll and opt files

Once the updated Fortran subroutines are ready to be implemented in Aspen, open “Customize Aspen Plus V10”. Within the simulation window, navigate to the directory containing all the updated .f files. Enter *aspcomp \*.f* which creates a .obj file for each .f file in the current directory. An obj file is a more compiled version of .f files that Aspen can use. Once the obj files are created, enter *asplink ccsi10*, which will create a dll file named ‘ccsi10.dll’ in the current directory. The ‘ccsi10.dll’ file is called within the ‘ccsi.opt’ file distributed with the model. The opt file may be created as a text file by entering the name of the dll file that it points to, and changing the file extension to opt. The opt file is specified within the Aspen model for accessing the Fortran subroutines. For users who choose not to create the dll file, a version will be provided with the release notes in the GitHub repository.

Note: In case of a compilation error, the Aspen Plus Linker Diagnostics (.ld) file created within the current directory needs to be opened using Notepad, and the link message displayed towards the end of the file needs to be analyzed, followed by an appropriate code correction in the .f files. The process of creating a new dll needs to be repeated thereafter.

* 1. Predicting System VLE

1. Place the “CCSIMEAModel.bkp” file and the supporting files “ccsi.opt” and “ccsi10.dll” in the same directory. Open the “CCSIMEAModel.bkp” file. When prompted with the “Column Sizing/Rating Detected” box, select the “Use Legacy Hydraulics” option. If the Model Palette is not visible, it may be selected from the “View” tab at the top of the window. In the Model Palette, navigate to the “Manipulators” tab and then select “Mult” to create a multiplier block, which will be referred to by its default name “B1.” Double-click “B1” and then set the multiplication factor to “1.” Add an inlet stream to the block by clicking “Material” in the Model Palette, the red arrow on the inlet of B1, and then elsewhere in the flowsheet. Repeat the procedure for the outlet stream of B1. Name the inlet and outlet streams as “IN” and “OUT,” respectively. **Note:** The streams may be renamed by double clicking the default name and typing the new name.
2. Double-click “IN” and configure it as follows:
   1. Select “Temperature” and “Vapor Fraction” as the “Flash Type” specifications.
   2. Temperature: 40°C.
   3. Vapor Fraction: 0.0001.
   4. Select “Mass-flow” in “gm/hr” as the composition basis. Set the values for “H2O” and “MEA” as “7” and “3,” respectively.
3. In the left navigation pane, navigate to “Model Analysis Tools” → “Sensitivity,” and then click “New.” The new sensitivity block may be named “PCO2.” Under “Manipulated variable” in the “Vary” tab, select “New,” select “Mole Flow” as “type,” “IN” as “stream,” “CO2” as “component,” and “mol/hr” as the “units.” Under “Manipulated variable limits,” specify “0.0005” and “0.03” as the “lower” and “upper limits,” respectively, and “10” as the “number of points.” Navigate to the “Define” tab and then create a new measured variable named “PCO2.” Under “Edit selected variable,” select “Streams” as the “category,” “Stream-Prop” as the “type,” “IN” as the “stream,” and “PPCO2” as the “prop set”. Change the units to “kPa”. Navigate to the “Tabulate” tab and then click “Fill Variables.” Navigate to the “Options” tab and select the “Do not execute base case,” option under “Execution options.”
4. Run the simulation by clicking the “Run” arrow or pressing “F5.” The results of the “PCO2” sensitivity block should be consistent with what is shown in Table 2. **Note:** All of the warnings that appear in the “Control Panel” while running the simulation may be ignored.

Table : Results of PCO2 Sensitivity Block

|  |  |  |  |
| --- | --- | --- | --- |
| Row/ Case | Status | CO2 MOLEFLOW (MOL/HR) | PCO2 (KPA) |
| 1 | OK | 0.0005 | 2.24E-5 |
| 2 | OK | 0.003778 | 0.00097 |
| 3 | OK | 0.007056 | 0.00363 |
| 4 | OK | 0.010333 | 0.00955 |
| 5 | OK | 0.013611 | 0.02339 |
| 6 | OK | 0.016889 | 0.06171 |
| 7 | OK | 0.020167 | 0.21295 |
| 8 | OK | 0.023444 | 1.47244 |
| 9 | OK | 0.026722 | 18.5729 |
| 10 | OK | 0.03 | 103.162 |

1. From this example, the vapor-liquid equilibrium (VLE) of the ternary MEA-H2O-CO2 system as a function of temperature and CO2 loading may be determined for 30 wt% MEA. The CO2 loading (mol CO2/mol MEA) may be calculated by multiplying the CO2 molar flow by the molecular weight of MEA and dividing by the mass flow of MEA. For example,

|  |  |  |
| --- | --- | --- |
|  |  | (6) |

Following this procedure and evaluating the sensitivity block for temperatures of 80 and 120°C, by changing the temperature of the stream “IN” and re-running the simulation, a plot similar to Figure 1 may be generated.

Figure : CO2 partial pressure as a function of loading and temperature (30 wt% MEA).

* 1. CO2 Capture Process Simulation Base Case Setup

The base case model that is set up in the file “CCSIMEAModel.bkp” has operating variables and equipment configurations as specified in Table 3.

Table : Variables for Base Case Simulation

| Variable | Value |
| --- | --- |
| **ABSLEAN Stream (Absorber Solvent Inlet)** | |
| Temperature (°C) | 40.97 |
| Pressure (kPa) | 245.94 |
| Mass Flow (kg/hr) | 6803.7 |
| **Component Mole Fractions** | |
| H2O | 0.87457 |
| CO2 | 0.01585 |
| MEA | 0.10958 |
| **GASIN Stream (Absorber Gas Inlet)** | |
| Temperature (°C) | 42.48 |
| Pressure (kPa) | 108.82 |
| Mass Flow (kg/hr) | 2266.1 |
| **Component Mass Fractions** | |
| H2O | 0.04623 |
| CO2 | 0.17314 |
| N2 | 0.71165 |
| O2 | 0.06898 |
| **Absorber** | |
| Intercooler #1 Flowrate (kg/hr) | 7364.83 |
| Intercooler #1 Return Temperature (°C) | 40.13 |
| Intercooler #2 Flowrate (kg/hr) | 7421.57 |
| Intercooler #2 Flowrate (°C) | 43.32 |
| Absorber Top Pressure (kPa) | 108.82 |
| Absorber Packing Diameter (m) | 0.64135 |
| Absorber Packing Height (ft) | 60.7184 |
| **Regenerator** | |
| Inlet Temperature (°C) | 104.81 |
| Inlet Pressure (kPa) | 183.87 |
| Top Pressure (kPa) | 183.7 |
| Reboiler Duty (kW) | 430.61 |
| Packing Diameter (in) | 23.25 |
| Packing Height (ft) | 39.6837 |

The variables described in Table 3 may be varied within reason, although abrupt changes in certain variables may results in failure of the simulation to converge. In the simulation provided in the example file, the variables for the “ABSLEAN” and “GASIN” streams can be located by double-clicking the respective streams. The variables for the absorber intercoolers can be located from the navigation pane by selecting “Blocks” → “ABSORBER” → “Configuration” → “Pumparounds,” and the first and second intercoolers are referred to as “P-1” and “P-2,” respectively. The top pressure of the absorber and regenerator can be located by double-clicking the “ABSORBER” and “REGEN” blocks and selecting the “Pressure” tab. Moreover, the reboiler duty for “REGEN” is located under the “Configuration” tab. The column packing diameters and height can be located by selecting “Blocks” → “ABOSRBER” or “REGEN” → “Sizing and Rating” → “Packing Rating” → “1” → “Setup.” The values of the regenerator inlet pressure and temperature are specified in the “PUMP” and “EXCHANGE” blocks, respectively. **Note:** A sensitivity block, referred to as “FLOW” in the simulation, is used to set the flowrate of the inlet solvent stream, as the simulation will not automatically converge for such a low flow rate.

* 1. CO2 Capture Process Simulation Example

In this example, the CO2 capture process, which includes the absorber and regenerator columns, is evaluated for two sets of operating conditions.

1. Open the “CCSIMEAModel.bkp” file. In the navigation pane, right-click “Blocks,” select “Activate,” right-click “Streams,” and then select “Activate.” Run the simulation. **Note:** All streams and blocks have been deactivated to reduce the time required to obtain the results for the test in Section 2.2 Predicting System VLE. If block “B1” and streams “IN” and “OUT” have already been created in the same file, they need to be deactivated by right-clicking them and selecting “Deactivate” before activating all streams with the aforementioned procedure.
2. In the flowsheet, right-click stream “ABSRICH,” select “Results,” and then select “STRIPOUT” from the drop-down arrow at the top of the right column. Ensure that the results obtained match those given in Table 4, noting that only selected rows are included in the table.

Table : Selected Stream Table Results

|  |  |  |
| --- | --- | --- |
| Mole Flow mol/hr | ABSRICH | STRIPOUT |
| H2O | 259990 | 256374 |
| CO2 | 0.342210 | 0.976323 |
| MEA | 8702.45 | 26273.15 |
| MEA+ | 12183.51 | 3270.13 |
| MEACOO- | 11816.96 | 3152.56 |
| HCO3- | 366.55 | 117.57 |
| N2 | 33.63 | 1.64E-20 |
| O2 | 5.49 | 8.18E-17 |
| Temperature C | 52.01 | 120.94 |
| Pressure kPa | 108.82 | 183.7 |
| Enthalpy J/kmol | -301827235 | -281379164 |

1. Reinitialize the simulation by clicking “Reset” or pressing “Shift+F5,” and then selecting “OK.” In the navigation pane, navigate to “Blocks” → “Absorber” → “Configuration” → “Pumparounds” → “P-1,” and then change the “flow rate” to “3000 kg/hr.” Navigate to “P-2” and then change the “flow rate” to the same value.
2. Navigate to “Model Analysis Tools” and activate the “FLOW” sensitivity block, which is used to determine the CO2 capture percentage in the absorber and the required reboiler duty for the stripper as a function of the lean solvent flowrate. Execute the model, navigate to the results of the sensitivity block, and verify that the results are similar to those shown in Figure 2.

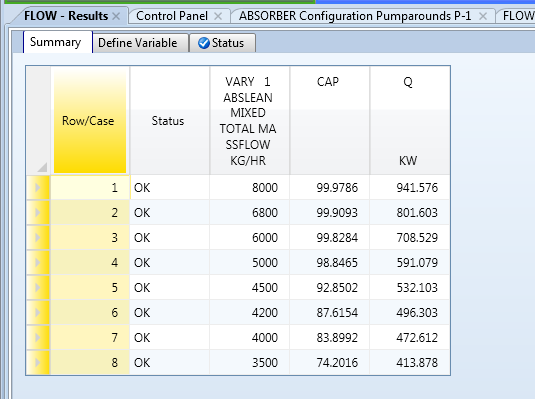


Figure : Results of the “FLOW” sensitivity block for the case study.

1. Navigate to “Blocks” → “Absorber” → “Profiles” and then highlight the columns labeled “Vapor Temperature” and “Liquid Temperature.” Under “Plot” on the “Home” tab, select “Custom,” and then verify that the resulting plot resembles Figure 3. **Note:** These temperature profiles correspond to the last simulation executed (Case 8).

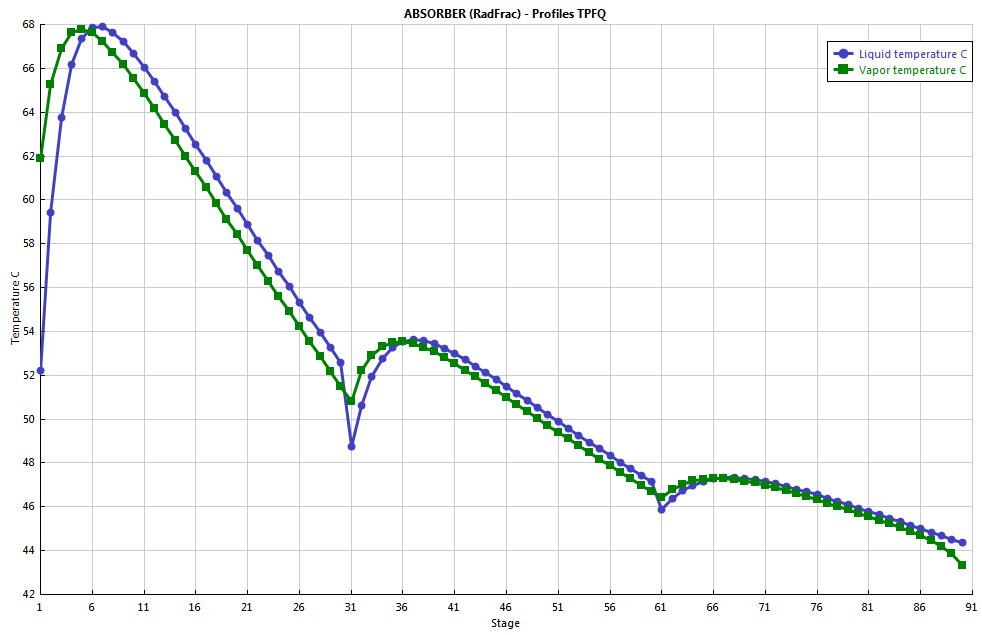


Figure : Absorber temperature profile for the case study.

1. Navigate to “Blocks” → “Regen” → “Profiles” and then repeat the procedure described in Step 5. Verify that the temperature profile resembles what is shown in Figure 4.

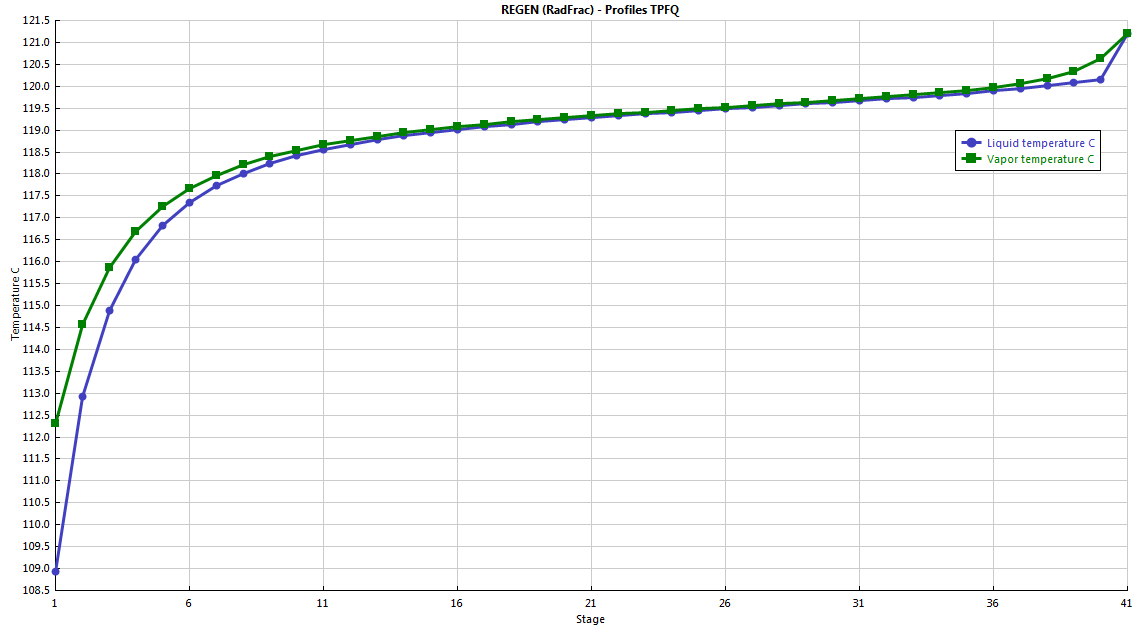


Figure : Regenerator temperature profile for the case study.

1. Usage Information
   1. Environment/Prerequisites

This product requires Aspen Plus V10 or newer with an Aspen Rate-Based Distillation license.

* 1. Support

Support can be obtained from the email support list [ccsi-support@acceleratecarboncapture.org](mailto:ccsi-support@acceleratecarboncapture.org) or by opening an issue at our GitHub repository: <https://github.com/CCSI-Toolset/MEA_ssm/issues>

1. References

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