

## 2.2. Signal Model.

~~Base~~ Bandpass signal: carrier frequency  
 $\downarrow$

$$s(t) = S_1(t) \cdot \cos 2\pi f_c t - S_2(t) \cdot \sin 2\pi f_c t$$

Equivalent baseband / Lowpass signal:  
 complex envelope  
 $u(t) = S_1(t) + j S_2(t)$

$$\Rightarrow s(t) = \operatorname{Re} \{ u(t) e^{j 2\pi f_c t} \}$$

$$= \operatorname{Re} \{ S_1(t) \cdot e^{j 2\pi f_c t} + j S_2(t) \cdot e^{j 2\pi f_c t} \}$$

$$= S_1(t) \cdot \cos 2\pi f_c t - S_2(t) \cdot \sin 2\pi f_c t$$

Let  $h(t)$  be the channel impulse response

$$r(t) = s(t) * h(t)$$

Let  $R(f)$ ,  $S(f)$ ,  $H(f)$  be F.T. of  
~~s(t)~~  $r(t)$ ,  $s(t)$ ,  $h(t)$ , respective.

$$R(f) = S(f) \cdot H(f)$$

Remark:

SUSTech

Let  $P_t$ ,  $P_u$  be the power of  $s(t)$ ,  $u(t)$ ,

$$P_t = \frac{1}{T} \int_0^T s^2(t) dt, \quad P_u = \frac{1}{T} \int_0^T |u(t)|^2 dt$$

$$\Rightarrow P_t = P_u/2$$

Actual signal power = Baseband power / 2.

Equivalent LP Channel Impulse Response:  $h_c(t)$   
bandpass:  $y(t) = s(t) * h_c(t)$   
 $\Downarrow$   $\Downarrow$   $\Downarrow$   
baseband:  $v(t) = u(t) * h_c(t)$  ←

$$\begin{aligned} r(t) &= \operatorname{Re} \{ v(t) e^{j2\pi f_c t} \} \\ s(t) &= \operatorname{Re} \{ u(t) e^{j2\pi f_c t} \} \\ * h_c(t) &= 2 \operatorname{Re} \{ h_c(t) \cdot e^{j2\pi f_c t} \} \end{aligned}$$

A factor of 2 for channel.

$$\text{If } h_c(t) = h_{c,1}(t) + j h_{c,2}(t)$$

$$\text{Then } h(t) = 2 h_{c,1}(t) \cos 2\pi f_c t - 2 h_{c,2}(t) \sin 2\pi f_c t$$

Let  $V(f)$ ,  $U(f)$ ,  $H_L(f)$  be the F.T. of  $v(t)$ ,  $u(t)$ ,  $h_L(t)$ ,

$$V(f) = U(f) \cdot H_L(f)$$

Moreover,

$$S(f) = \frac{1}{2} [U(f-f_c) + U^*(f-f_c)]$$

$$H_L(f) = H_L(f-f_c) + H_L^*(-f-f_c)$$

$$R(f) = \frac{1}{2} [V(f-f_c) + V^*(-f-f_c)]$$

$$\uparrow_{Tx: P_t} \quad \text{Path Loss} \quad \downarrow_{Rx: P_r}$$

Linear Path Loss  $P_L = P_t / P_r$

Path Loss (in decibel)

$$P_L \text{ dB} = 10 \log_{10} \frac{P_t}{P_r} \text{ dB}$$

Path gain (in decibel)

$$P_G = -P_L$$

## 2.3 Free-Space Path Loss

$$v(t) = \frac{\lambda \sqrt{G_L}}{4\pi d} \underbrace{e^{-j2\pi d/\lambda}}_{\text{phase shift}} \cdot u(t)$$

$$\frac{P_r}{P_t} = \frac{\frac{1}{T} \int_0^T |v(t)|^2 dt}{\frac{1}{T} \int_0^T |u(t)|^2 dt} = \left[ \frac{\lambda \sqrt{G_L}}{4\pi d} \right]^2$$

$P_r$  dBm

$$= 10 \cdot \log_{10} P_r - 30$$

$$= 10 \log_{10} \left[ \frac{\lambda \sqrt{G_L}}{4\pi d} \right]^2 + 10 \log_{10} P_t - 30$$

$$= P_t \text{ dBm} + 20 \log_{10} \lambda + 10 \log_{10} G_L \\ - 20 \log_{10} (4\pi) - 20 \log_{10} d$$

$$P_G \text{ dB} = 10 \log_{10} \frac{P_r}{P_t} = P_r \text{ dBm} - P_t \text{ dBm} \\ = 20 \log_{10} \lambda + 10 \log_{10} G_L - 20 \log_{10} (4\pi) - 20 \log_{10} d$$

## 2.4 Ray Tracing

Use finite # of rays to approximate the signal propagation from Tx to Rx

⇒ The received signal is the summation of the signals along the rays

⇒ Scenario-dependent.

### 2.4.1 Two-Ray Model.

Open space: LoS + single reflection off the ground.