

# Implicit handling of multilayered material substrates in full-wave SCUFF-EM calculations

Homer Reid

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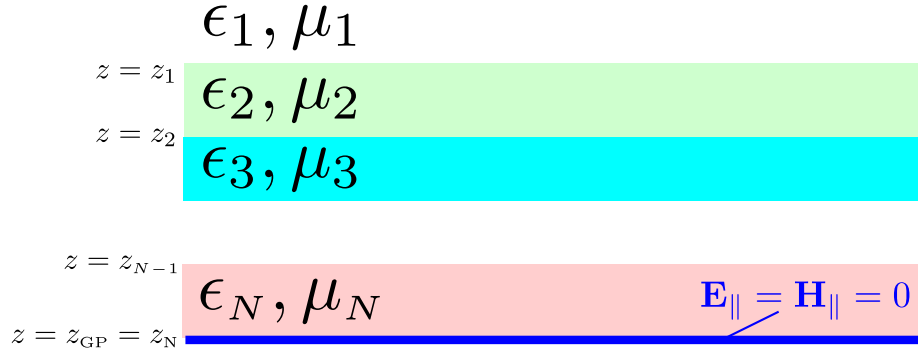


Figure 1: Geometry of the layered substrate. The  $n$ th layer has relative permittivity and permeability  $\epsilon_n, \mu_n$ , and its lower surface lies at  $z = z_n$ . The ground plane, if present, lies at  $z = z_{GP}$ .

## 1 Overview

In a previous memo<sup>1</sup> I considered SCUFF-STATIC electrostatics calculations in the presence of a multilayered dielectric substrate. In this memo I extend that discussion to the case of *full-wave* (i.e. nonzero frequencies beyond the quasi-static regime) scattering calculations in the SCUFF-EM core library.

### Substrate geometry

As shown in Figure 1, I consider a multilayered substrate consisting of  $N$  material layers possibly terminated by a perfectly-conducting ground plane. The uppermost layer (layer 1) is the infinite half-space above the substrate. The  $n$ th layer has relative permittivity and permeability  $\epsilon_n, \mu_n$ , and its lower surface lies at  $z = z_n$ . The ground plane, if present, lies at  $z \equiv z_N \equiv z_{GP}$ . If the ground plane is absent, layer  $N$  is an infinite half-space.<sup>2</sup>

### Definition of the substrate DGF

I will use the symbol  $\mathbf{\Gamma}(\omega; \mathbf{x}_D, \mathbf{x}_S)$  for the *total*  $6 \times 6$  dyadic Green's function relating time-harmonic fields at  $\mathbf{x}_D$  to sources at  $\mathbf{x}_S$ : thus, if  $\mathcal{S} \equiv \begin{pmatrix} \mathbf{J} \\ \mathbf{M} \end{pmatrix}$  is the 6-vector distribution of free electric and magnetic currents in the presence of the substrate, then the 6-vector of electric and magnetic fields  $\mathcal{F} \equiv \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$  is given by

$$\mathcal{F}(\mathbf{x}_D) = \int \mathbf{\Gamma}(\mathbf{x}_D, \mathbf{x}_S) \cdot \mathcal{S}(\mathbf{x}_S) d\mathbf{x}_S.$$

<sup>1</sup>“Implicit handling of multilayered dielectric substrates in SCUFF-STATIC”

<sup>2</sup>As in the electrostatic case, this means that a finite-thickness substrate consisting of  $N$  material layers is described as a stack of  $N + 1$  layers in which the bottommost layer is an infinite half-space ( $z_{N+1} = -\infty$ ) with the material properties of vacuum ( $\epsilon_{N+1} = \mu_{N+1} = 1$ ).

The  $6 \times 6$  tensor  $\mathbf{\Gamma}$  has a  $2 \times 2$  block structure:

$$\mathbf{\Gamma} = \begin{pmatrix} \mathbf{\Gamma}^{\text{EE}} & \mathbf{\Gamma}^{\text{EM}} \\ \mathbf{\Gamma}^{\text{ME}} & \mathbf{\Gamma}^{\text{MM}} \end{pmatrix} \quad (1a)$$

with the  $3 \times 3$  subblocks defined by

$$\Gamma_{ij}^{\text{PQ}}(\omega, \mathbf{x}_D, \mathbf{x}_S) = \begin{pmatrix} i\text{-component of P-type field at } \mathbf{x}_D \text{ due to } j\text{-directed} \\ \text{Q-type point current source at } \mathbf{x}_S, \text{ all fields and} \\ \text{sources having time dependence } \sim e^{-i\omega t} \end{pmatrix} \quad (1b)$$

**Homogeneous DGF** In an infinite *homogeneous* medium with relative permittivity and permeability  $\{\epsilon^r, \mu^r\}$ ,  $\mathbf{\Gamma}$  reduces to its homogeneous form, for which I will use the symbol  $\mathbf{\Gamma}^{0r}$  (where the  $r$  index labels the medium, which in this case will be one of the layers in Figure 1, i.e.  $r \in \{1, 2, \dots, N\}$ ):

$\mathbf{x}_D, \mathbf{x}_S \in \text{infinite homogeneous medium } r \implies \mathbf{\Gamma}(\omega; \mathbf{x}_D, \mathbf{x}_S) = \mathbf{\Gamma}^{0r}(\omega; \mathbf{x}_D - \mathbf{x}_S)$   
where<sup>3</sup>

$$\mathbf{\Gamma}^{0r}(\omega, \mathbf{r}) \equiv \begin{pmatrix} ik_r Z_0 Z^r \mathbf{G}(k_r, \mathbf{r}) & ik_r \mathbf{C}(k_r, \mathbf{r}) \\ -ik_r \mathbf{C}(k_r, \mathbf{r}) & \frac{ik_r}{Z_0 Z^r} \mathbf{G}(k_r, \mathbf{r}) \end{pmatrix} \quad (2)$$

$$k_r \equiv \sqrt{\epsilon_0 \epsilon^r \mu_0 \mu^r} \cdot \omega, \quad Z_0 Z^r \equiv \sqrt{\frac{\mu_0 \mu^r}{\epsilon_0 \epsilon^r}},$$

$$G_{ij} = \left( \delta_{ij} - \frac{1}{k^2} \partial_i \partial_j \right) \frac{e^{ik|\mathbf{r}|}}{4\pi|\mathbf{r}|}, \quad C_{ij} = \frac{\epsilon_{ilm}}{ik} \partial_l G_{mj}$$

**Inhomogeneous DGF** On the other hand, in the presence of the multilayered substrate the full DGF  $\mathbf{\Gamma}$  receives corrections, which may be thought of as the fields radiated by surface currents induced on the interfacial surfaces of the substrate, and which I will denote by the symbol  $\mathcal{G}$ :

$$\mathbf{\Gamma}(\mathbf{x}_D, \mathbf{x}_S) = \mathcal{G}(\mathbf{x}_D, \mathbf{x}_S) + \begin{cases} \mathbf{\Gamma}^{0r}(\mathbf{x}_D - \mathbf{x}_S), & \mathbf{x}_S \in \text{layer } r \\ 0, & \text{otherwise} \end{cases} \quad (3)$$

Like  $\mathbf{\Gamma}$ ,  $\mathcal{G}$  is a  $6 \times 6$  matrix with a  $2 \times 2$  block structure:

$$\mathcal{G}(\omega; \mathbf{x}_D, \mathbf{x}_S) = \begin{pmatrix} \mathcal{G}^{\text{EE}} & \mathcal{G}^{\text{EM}} \\ \mathcal{G}^{\text{ME}} & \mathcal{G}^{\text{MM}} \end{pmatrix} \quad (4)$$

with the  $3 \times 3$  subblocks defined by

$$\mathcal{G}_{ij}^{\text{PQ}} = \begin{pmatrix} i\text{-component of P-type field at } \mathbf{x}_D \text{ due to surface currents on sub-} \\ \text{strate interface layers induced by } j\text{-directed Q-type source at } \mathbf{x}_S. \end{pmatrix}$$

LIBSUBSTRATE is a code for numerical computation of  $\mathcal{G}$ .

<sup>3</sup>Cf. Section 3 of the companion memo “LIBSCUFF implementation and Technical Details,” <http://homerreid.github.io/scuff-em-documentation/tex/lsInnards.pdf>

### Organization of SCUFF-EM implementation and this memo

The full-wave substrate implementation in SCUFF-EM consists of multiple working parts that fit together in a somewhat modular fashion.

Roughly speaking, the computational problem may be divided into two parts:

- (a) For given source and evaluation (or “destination”) points  $\{\mathbf{x}_s, \mathbf{x}_d\}$  at a given angular frequency  $\omega$  in the presence of a multilayer substrate, numerically compute the substrate DGF correction  $\mathcal{G}(\omega, \mathbf{x}_d, \mathbf{x}_s)$ . This task is independent of SCUFF-EM and is implemented by a standalone library called LIBSUBSTRATE, described in Section 2 of this memo.
- (b) For a SCUFF-EM geometry in the presence of a substrate, compute the substrate corrections to the BEM system matrix  $\mathbf{M}$  and RHS vector  $\mathbf{v}$ , as well as the substrate corrections to post-processing quantities such as scattered fields. This is done by the file `Substrate.cc` in LIBSCUFF and is described in Section 3 of this memo.

## 2 LIBSUBSTRATE: Numerical computation of substrate Green's functions

Numerical evaluation of substrate contributions to dyadic Green's functions is handled by a C++ library called LIBSUBSTRATE. Although this library is packaged and distributed with SCUFF-EM and depends on other support libraries in the SCUFF-EM distribution, it is independent of the particular integral-equation formulation implemented by LIBSCUFF, and thus should be of general utility beyond SCUFF-EM.

### 2.1 Overview of computational strategy

LIBSUBSTRATE decomposes the problem of computing  $\mathcal{G}$  into several logical steps, as follows:

1. Solve a linear system to obtain the Fourier-space representation  $\tilde{\mathcal{G}}(\mathbf{q})$ . Here  $\mathbf{q} = (q_x, q_y)$  is a 2D Fourier variable. (Section 2.2.)
2. Reduce the two-dimensional integral over  $\mathbf{q}$  to a one-dimensional integral over  $|\mathbf{q}| \equiv q$ . (Section 2.3.)
3. Evaluate the  $q$  integral using established methods for evaluating Sommerfeld integrals. (Section ??.)

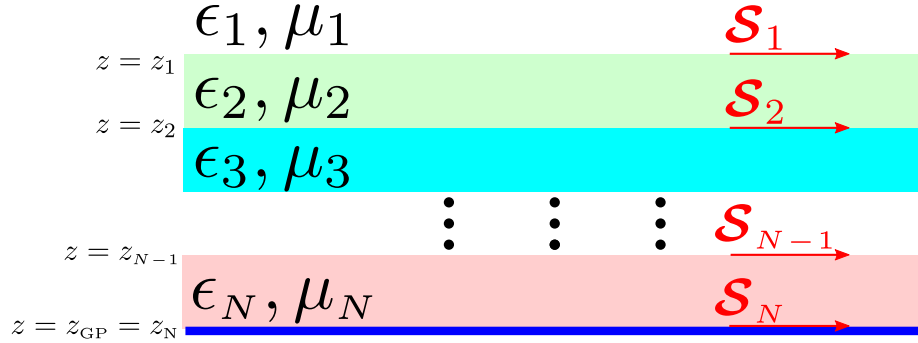


Figure 2: Effective surface-current approach to treatment of multilayer substrate. External field sources induce a distribution of electric and magnetic surface currents  $\mathcal{S}_n = \begin{pmatrix} \mathbf{K}_n \\ \mathbf{N}_n \end{pmatrix}$  on the  $n$ th material interface, and the fields radiated by these effective currents account for the disturbance presented by the substrate.

## 2.2 Computation of Fourier-space DGF $\tilde{\mathcal{G}}(\mathbf{q})$

To compute the substrate correction to the fields of external sources, I consider the effective tangential electric and magnetic surface currents  $\mathbf{K}$  and  $\mathbf{N}$  induced on the interfacial layers by the external field sources (Figure 2). This is the direct extension to full-wave problems of the formalism I used in the electrostatic case, and it comports well with the spirit of surface-integral-equation methods.

More specifically, on the material interface layer at  $z = z_n$  I have a four-vector surface-current density  $\mathcal{S}_n(\boldsymbol{\rho})$ , where  $\boldsymbol{\rho} = (x, y)$  and the components of  $\mathcal{S}$  are

$$\mathcal{S}_n(\boldsymbol{\rho}) = \begin{pmatrix} K_x(\boldsymbol{\rho}) \\ K_y(\boldsymbol{\rho}) \\ N_x(\boldsymbol{\rho}) \\ N_y(\boldsymbol{\rho}) \end{pmatrix}. \quad (5)$$

**Fields in layer interiors.** I will adopt the convention that the lower (upper) bounding surface for each region is the positive (negative) bounding surface for that region in the usual sense of SCUFF-EM regions and surfaces (in which the sign of a {surface, region} pair  $\{\mathcal{S}, \mathcal{R}\}$  is the sign with which surface currents on  $\mathcal{S}$  contribute to fields in  $\mathcal{R}$ ). Thus, at a point  $\mathbf{x} = (\boldsymbol{\rho}, z)$  in the interior of layer  $n$  ( $z_{n-1} > z > z_n$ ), the six-vector of total fields  $\mathcal{F} = \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$  reads

$$\mathcal{F}_n(\boldsymbol{\rho}, z) = -\mathbf{\Gamma}^{0n}(z_{n-1}) \star \mathcal{S}_{n-1} + \mathbf{\Gamma}^{0n}(z_n) \star \mathcal{S}_n + \mathcal{F}_n^{\text{ext}}(\boldsymbol{\rho}, z) \quad (6)$$

where  $\mathcal{F}_n^{\text{ext}}$  are the externally-sourced (incident) fields due to sources in layer  $n$ ,  $\mathbf{\Gamma}^{0n}$  is the  $6 \times 6$  homogeneous dyadic Green's function for material layer  $n$ ,

and  $\star$  is shorthand for the convolution operation

$$“\mathcal{F}(\boldsymbol{\rho}, z) \equiv \Gamma(z') \star \mathcal{S}'' \implies \mathcal{F}(\boldsymbol{\rho}, z) = \int \Gamma(\boldsymbol{\rho} - \boldsymbol{\rho}', z - z') \cdot \mathcal{S}(\boldsymbol{\rho}') d\boldsymbol{\rho}' \quad (7)$$

where the integral extends over the entire interfacial plane. I will evaluate convolutions of this form using the 2D Fourier representation of  $\Gamma^{0n}$ :

$$\Gamma^{0n}(\boldsymbol{\rho}, z) = \int \frac{d^2\mathbf{q}}{(2\pi)^2} \widetilde{\Gamma^{0n}}(\mathbf{q}, z) e^{i\mathbf{q} \cdot \boldsymbol{\rho}} \quad (8a)$$

$$\widetilde{\Gamma^{0n}}(\mathbf{q}, z) = \frac{1}{2} \begin{pmatrix} -\frac{\omega\mu_0\mu_n}{q_{zn}} \tilde{\mathbf{G}}^\pm & +\tilde{\mathbf{C}}^\pm \\ -\tilde{\mathbf{C}}^\pm & -\frac{\omega\epsilon_0\epsilon_n}{q_{zn}} \tilde{\mathbf{G}}^\pm \end{pmatrix} e^{iq_z|z|} \quad (8b)$$

$$\tilde{\mathbf{G}}^\pm(\mathbf{q}, k) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} - \frac{1}{k^2} \begin{pmatrix} q_x^2 & q_x q_y & \pm q_x q_z \\ q_y q_x & q_y^2 & \pm q_y q_z \\ \pm q_z q_x & \pm q_z q_y & q_z^2 \end{pmatrix} \quad (8c)$$

$$\tilde{\mathbf{C}}^\pm(\mathbf{q}, k) = \begin{pmatrix} 0 & \mp 1 & +q_y/q_z \\ \pm 1 & 0 & -q_x/q_z \\ -q_y/q_z & +q_x/q_z & 0 \end{pmatrix} \quad (8d)$$

$$k_n \equiv \sqrt{\epsilon_0\epsilon_n\mu_0\mu_n} \cdot \omega, \quad q_z \equiv \sqrt{k^2 - |\mathbf{q}|^2}, \quad \pm = \text{sign } z. \quad (8e)$$

With this representation, convolutions like (7) become products in Fourier space:

$$\Gamma(z') \star \mathcal{S} = \mathcal{F}(\boldsymbol{\rho}, z) = \int \frac{d^2\mathbf{q}}{(2\pi)^2} \tilde{\mathcal{F}}(\mathbf{q}, z) e^{i\mathbf{q} \cdot \boldsymbol{\rho}}, \quad \text{with} \quad \tilde{\mathcal{F}}(\mathbf{q}, z) = \tilde{\Gamma}(\mathbf{q}, z - z') \tilde{\mathcal{S}}(\mathbf{q})$$

**Surface currents from incident fields.** To determine the surface currents induced by given incident-field sources, I apply boundary conditions. The boundary condition at  $z = z_n$  is that the tangential  $\mathbf{E}, \mathbf{H}$  fields be continuous: in Fourier space, we have

$$\tilde{\mathcal{F}}_\parallel(\mathbf{q}, z = z_n^+) = \tilde{\mathcal{F}}_\parallel(\mathbf{q}, z = z_n^-) \quad (9)$$

The fields just **above** the interface ( $z \rightarrow z_n^+$ ) receive contributions from three sources:

- Surface currents at  $z = z_{n-1}$ , which contribute with a minus sign and via the Green's function for region  $n$ ;
- Surface currents at  $z = z_n$ , which contribute with a plus sign and via the Green's function for region  $n$ ; and
- external field sources in region  $n$ .

The fields just **below** the interface ( $z = z_n^-$ ) receive contributions from three sources:

- Surface currents at  $z = z_n$ , which contribute with a minus sign and via the Green's function for region  $n + 1$ ;
- Surface currents at  $z = z_{n+1}$ , which contribute with a plus sign and via the Green's function for region  $n + 1$ ; and
- external field sources in region  $n + 1$ .

Then equation (9) reads (temporarily omitting  $\mathbf{q}$  arguments)

$$\begin{aligned} & -\widetilde{\mathbf{\Gamma}}^{0n}_{\parallel}(z_n - z_{n-1}) \cdot \widetilde{\mathbf{S}}_{n-1} + \widetilde{\mathbf{\Gamma}}^{0n}_{\parallel}(0^+) \cdot \widetilde{\mathbf{S}}_n + \widetilde{\mathcal{F}}_{n\parallel}^{\text{ext}}(z_n) \\ & = -\widetilde{\mathbf{\Gamma}}^{0,n+1}_{\parallel}(0^-) \cdot \widetilde{\mathbf{S}}_n + \widetilde{\mathbf{\Gamma}}^{0,n+1}_{\parallel}(z_n - z_{n+1}) \cdot \widetilde{\mathbf{S}}_{n+1} + \widetilde{\mathcal{F}}_{n+1\parallel}^{\text{ext}}(z_n) \end{aligned}$$

or

$$\mathbf{M}_{n,n-1} \cdot \widetilde{\mathbf{S}}_{n-1} + \mathbf{M}_{n,n} \cdot \widetilde{\mathbf{S}}_n + \mathbf{M}_{n,n+1} \cdot \widetilde{\mathbf{S}}_{n+1} = \widetilde{\mathcal{F}}_{n+1\parallel}^{\text{ext}}(z_n) - \widetilde{\mathcal{F}}_{n\parallel}^{\text{ext}}(z_n) \quad (10)$$

with the  $4 \times 4$  matrix blocks<sup>4</sup>

$$\mathbf{M}_{n,n-1} = -\widetilde{\mathbf{\Gamma}}^{0n}_{\parallel}(z_n - z_{n-1}) \quad (13a)$$

$$\mathbf{M}_{n,n} = +\widetilde{\mathbf{\Gamma}}^{0n}_{\parallel}(0^+) + \widetilde{\mathbf{\Gamma}}^{0,n+1}_{\parallel}(0^-) \quad (13b)$$

$$\mathbf{M}_{n,n+1} = -\widetilde{\mathbf{\Gamma}}^{0,n+1}_{\parallel}(z_n - z_{n+1}) \quad (13c)$$

Writing down equation (10) equation for all  $N$  dielectric interfaces yields a  $4N \times 4N$  system of linear equations, with triadiagonal  $4 \times 4$  block form, relating the surface currents on all layers to the external fields due to sources in all regions:

$$\mathbf{M} \cdot \mathbf{s} = \mathbf{f} \quad (14)$$

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<sup>4</sup>The  $4 \times 4$   $\mathbf{M}$  blocks here have  $2 \times 2$  block structure:

$$\mathbf{M}_{n,n} = \sum_{r \in \{n, n+1\}} \frac{1}{2} \begin{pmatrix} -\frac{\omega \epsilon_r}{Z_0 q_{zr}} \mathbf{g}(k_r, \mathbf{q}) & 0 \\ 0 & -\frac{\omega \mu_r Z_0}{q_{zr}} \mathbf{g}(k_r, \mathbf{q}) \end{pmatrix} \quad (11)$$

$$\mathbf{M}_{n,n\pm 1} = \frac{1}{2} \begin{pmatrix} -\frac{\omega \epsilon_r}{Z_0 q_{zr}} \mathbf{g}(k_r, \mathbf{q}) & \mathbf{c}^{\pm} \\ -\mathbf{c}^{\pm} & -\frac{\omega \mu_r Z_0}{q_{zn^*}} \mathbf{g}(k_r, \mathbf{q}) \end{pmatrix} e^{iq_{zr}|z_n - z_{n\pm 1}|} \quad (12)$$

where I put  $r \equiv \begin{cases} n, & \text{for } \mathbf{M}_{n,n-1} \\ n+1, & \text{for } \mathbf{M}_{n,n+1} \end{cases}$  and

$$\mathbf{g}(k; \mathbf{q}) = \mathbf{1} - \frac{\mathbf{q}\mathbf{q}^{\top}}{k^2}, \quad \mathbf{c}^{\pm} = \begin{pmatrix} 0 & \mp 1 \\ \pm 1 & 0 \end{pmatrix}$$



where  $\mathbf{M}$  is the  $4N \times 4N$  block-tridiagonal matrix (13) and where the  $4N$ -vectors  $\mathbf{s}$ ,  $\mathbf{f}$  read

$$\mathbf{s} = \begin{pmatrix} \tilde{\mathcal{S}}_1 \\ \tilde{\mathcal{S}}_2 \\ \tilde{\mathcal{S}}_3 \\ \vdots \\ \tilde{\mathcal{S}}_N \end{pmatrix}, \quad \mathbf{f} = \begin{pmatrix} -\tilde{\mathcal{F}}_{1\parallel}(z_1) + \tilde{\mathcal{F}}_{2\parallel}(z_1) \\ -\tilde{\mathcal{F}}_{2\parallel}(z_2) + \tilde{\mathcal{F}}_{3\parallel}(z_2) \\ -\tilde{\mathcal{F}}_{3\parallel}(z_3) + \tilde{\mathcal{F}}_{4\parallel}(z_3) \\ \vdots \\ -\tilde{\mathcal{F}}_{N-1,\parallel}(z_{N-1}) + \tilde{\mathcal{F}}_{N\parallel}(z_{N-1}) \end{pmatrix}.$$

Solving (14) yields the induced surface currents on all layers in terms of the incident fields:

$$\mathbf{s} = \mathbf{W} \cdot \mathbf{f} \quad \text{where} \quad \mathbf{W} \equiv \mathbf{M}^{-1}$$

or, more explicitly,

$$\tilde{\mathcal{S}}_n = \sum_m W_{nm} \mathbf{f}_m \quad (15)$$

### Surface currents induced by point sources

For DGF computations the incident fields arise from a single point source—say, a  $j$ -directed source in region  $s$ . Then the only nonzero length-4 blocks of the RHS vector in (14) are  $\mathbf{f}_{s-1}, \mathbf{f}_s$  with components ( $\ell = \{1, 2, 4, 5\}$ )

$$(\mathbf{f}_{s-1})_\ell = -\tilde{\Gamma}_{\ell j}^{0s}(z_{s-1} - z_s), \quad (\mathbf{f}_s)_\ell = +\tilde{\Gamma}_{\ell j}^{0s}(z_s - z_s) \quad (16)$$

and the surface currents on interface layer  $n$  are obtained by solving (15):

$$\begin{aligned} \tilde{\mathcal{S}}_n &= \mathbf{W}_{n,s-1} \mathbf{f}_{s-1} + \mathbf{W}_{n,s} \mathbf{f}_s \\ &= \sum_{p=0}^1 (-1)^{p+1} \mathbf{W}_{n,s-1+p} \cdot \widetilde{\Gamma}_{\parallel,j}^{0s}(z_s - z_{s-1+p}) \end{aligned} \quad (17)$$

### Fields due to surface currents

Given the surface currents induced by a  $j$ -directed point source at  $\mathbf{x}_s$ , I evaluate the fields due to these currents to get the substrate DGF contribution  $\mathcal{G}$ . If the evaluation point  $\mathbf{x}_d$  lies in region  $d$ , then the fields receive contributions from the surface currents at  $z_{d-1}$  and  $z_d$ , propagated by the homogeneous DGF for region  $d$ :

$$\begin{aligned} \tilde{\mathcal{F}}(z_d) &= -\widetilde{\Gamma}^{0d}(z_d - z_{d-1}) \cdot \tilde{\mathcal{S}}_{d-1} + \widetilde{\Gamma}^{0d}(z_d - z_d) \cdot \tilde{\mathcal{S}}_d \\ &= \sum_{q=0}^1 (-1)^{q+1} \widetilde{\Gamma}^{0d}(z_d - z_{d+q-1}) \cdot \tilde{\mathcal{S}}_{d+q-1} \end{aligned} \quad (18)$$

(The minus sign in the first term arises because, in my convention, surface currents on the upper surface of a region contribute to the fields in that region with a minus sign). Inserting (17), the  $i$  component here—which is the  $ij$  component of the substrate DGF—is

$$\tilde{g}_{ij}(z_D, z_S) = \sum_{p,q=0}^1 (-1)^{p+q} \widetilde{\mathbf{\Gamma}_{i,\parallel}^{0d}}(z_D - z_{d-1+q}) \mathbf{W}_{d-1+q,s-1+p} \widetilde{\mathbf{\Gamma}_{\parallel,j}^{0s}}(z_{s-1+p} - z_S). \quad (19)$$

The calculation of equation (19) is carried out by the routine `GetGTwiddle` in `LIBSUBSTRATE`.

### Green's functions for potentials

In equation (18) I am computing the 6 components of the  $\mathbf{E}$  and  $\mathbf{H}$  fields produced by the induced surface currents. If instead I compute the *potentials* produced by those currents I obtain a slightly different Green's function. Thus, let  $\mathbf{A}^E, \Phi^E$  be the usual vector and scalar potential of an electric-current source in a homogeneous region, and let  $\mathbf{A}^M, \Phi^M$  be their counterparts for magnetic-current sources, i.e. if the electric and magnetic volume currents are  $\mathbf{J}$  and  $\mathbf{M}$  then

$$\mathbf{A}^E(\mathbf{x}_D) = \mu \int \mathbf{J}(\mathbf{x}_S) G_0(\mathbf{x}_{DS}) d\mathbf{x}_S, \quad \Phi^E(\mathbf{x}_D) = \frac{1}{i\omega\epsilon} \int (\nabla \cdot \mathbf{J}) G_0(\mathbf{x}_{DS}) d\mathbf{x}_S \quad (20a)$$

$$\mathbf{A}^M(\mathbf{x}_D) = \epsilon \int \mathbf{M}(\mathbf{x}_S) G_0(\mathbf{x}_{DS}) d\mathbf{x}_S, \quad \Phi^M(\mathbf{x}_D) = \frac{1}{i\omega\mu} \int (\nabla \cdot \mathbf{M}) G_0(\mathbf{x}_{DS}) d\mathbf{x}_S \quad (20b)$$

with  $\mathbf{x}_{DS} \equiv \mathbf{x}_D - \mathbf{x}_S$  and

$$G_0(k; \mathbf{r}) = \frac{e^{ik|\mathbf{r}|}}{4\pi|\mathbf{r}|} = \int \frac{d^2\mathbf{q}}{(2\pi)^2} \tilde{G}_0(\mathbf{q}, z) e^{i\mathbf{q} \cdot \boldsymbol{\rho}}, \quad \tilde{G}_0 = \frac{i}{2q_z} e^{iq_z|z|}.$$

I write

## 2.3 Reduction of 2D Fourier integrals to 1D (Sommerfeld) integrals

The real-space DGF correction is the inverse Fourier transform of (19):

$$\mathcal{G}(\boldsymbol{\rho}, z_D, z_S) = \int \frac{d^2 \mathbf{q}}{(2\pi)^2} \tilde{\mathcal{G}}(\mathbf{q}; z_D; z_S) e^{i\mathbf{q} \cdot \boldsymbol{\rho}}$$

or, in polar coordinates with  $(q_x, q_y) = (q \cos \theta_q, q \sin \theta_q)$ ,  $(\rho_x, \rho_y) = (\rho \cos \theta_\rho, \rho \sin \theta_\rho)$ ,

$$\mathcal{G}(\boldsymbol{\rho}) = \int_0^\infty \frac{q dq}{2\pi} \int_0^{2\pi} \frac{d\theta_q}{2\pi} \tilde{\mathcal{G}}(\mathbf{q}) e^{iq\rho \cos(\theta_q - \theta_\rho)}. \quad (21)$$

(Here and for much of this section I suppress  $z_{D,S}$  arguments, but one must remember that they are always there.<sup>5</sup>) The goal of this section is to integrate out the angular variable  $\theta_q$  to reduce the 2D integral over  $\mathbf{q}$  to a 1D integral over  $q = |\mathbf{q}|$ . In abbreviated form this proceeds as follows:

1. Separate variables by writing  $\tilde{\mathcal{G}}(\mathbf{q})$  as a sum of products of  $\theta_q$ -independent scalar functions  $\tilde{g}(q)$  times  $q$ -independent matrix-valued functions  $\mathbf{\Lambda}(\theta_q)$  (Section 2.3.1):

$$\tilde{\mathcal{G}}(\mathbf{q}) = \sum_{n=1}^{18} \tilde{g}^{(n)}(q) \mathbf{\Lambda}^{(n)}(\theta_q)$$

2. Evaluate integrals over  $\theta_q$  analytically to yield Bessel functions  $J_\nu(q\rho)$  multiplying  $q$ -independent matrix-valued functions  $\mathbf{\Lambda}(\theta_\rho)$  (Section 2.3.2). After this step (21) reads

$$\mathcal{G}(\boldsymbol{\rho}) = \sum_{m=1}^{22} \underbrace{\left[ \int_0^\infty \tilde{\mathbf{g}}^{(m)}(q, \rho) dq \right]}_{\mathbf{g}^{(m)}(\rho)} \mathbf{\Lambda}^{(m)}(\theta_\rho) \quad (22)$$

where the  $\tilde{\mathbf{g}}(q, \rho)$  functions are linear combinations of the  $\tilde{g}(q)$  functions times Bessel functions in  $q\rho$  and other factors.

3. Evaluate the remaining integrals over  $q$  numerically using sophisticated tricks for evaluating Sommerfeld integrals (Section 2.3.3).

### 2.3.1 Factor $\tilde{\mathcal{G}}$ into $q$ -independent and $\theta_q$ -independent terms

I begin by noting that  $\tilde{\mathcal{G}}(\mathbf{q})$  may be decomposed as a sum of scalar functions of  $q = |\mathbf{q}|$  times  $q$ -independent matrix-valued functions of  $\theta_q$ :

$$\tilde{\mathcal{G}}(\mathbf{q}) = \sum_{n=1}^{18} \tilde{g}^{(n)}(q) \mathbf{\Lambda}^{(n)}(\theta_q) \quad (23)$$

---

<sup>5</sup>More specifically, the “ $g$ -like” quantities  $\mathcal{G}(\boldsymbol{\rho})$ ,  $\tilde{\mathcal{G}}(\mathbf{q})$ ,  $\tilde{g}(q)$ ,  $\tilde{\mathbf{g}}(q, \rho)$ , and  $\mathbf{g}(\rho)$  all depend on  $z_{S,D}$ , but the matrix-valued functions  $\mathbf{\Lambda}_n(\theta)$  do not.

For example, the upper two quadrants read

$$\begin{aligned}
\widetilde{\mathcal{G}}^{\text{EE}}(\mathbf{q}) = & \underbrace{\widetilde{g}^{\text{EE}0\parallel}(q) \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{0\parallel}} + \underbrace{\widetilde{g}^{\text{EE}0z}(q) \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix}}_{\mathbf{\Lambda}^{0z}} \\
& + \underbrace{\widetilde{g}^{\text{EE}1}(q) \begin{pmatrix} 0 & 0 & \cos \theta_{\mathbf{q}} \\ 0 & 0 & \sin \theta_{\mathbf{q}} \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^1(\theta_{\mathbf{q}})} + \underbrace{\widetilde{g}^{\text{EE}1\top}(q) \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ \cos \theta_{\mathbf{q}} & \sin \theta_{\mathbf{q}} & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{1\top}(\theta_{\mathbf{q}})} \\
& + \underbrace{\widetilde{g}^{\text{EE}2}(q) \begin{pmatrix} \cos^2 \theta_{\mathbf{q}} & \cos \theta_{\mathbf{q}} \sin \theta_{\mathbf{q}} & 0 \\ \cos \theta_{\mathbf{q}} \sin \theta_{\mathbf{q}} & \sin^2 \theta_{\mathbf{q}} & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^2(\theta_{\mathbf{q}})} \\
\widetilde{\mathcal{G}}^{\text{EM}}(\mathbf{q}) = & \underbrace{\widetilde{g}^{\text{EM}0\parallel}(q) \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{0\times}} + \underbrace{\widetilde{g}^{\text{EM}2}(q) \begin{pmatrix} \cos \theta_{\mathbf{q}} \sin \theta_{\mathbf{q}} & \sin^2 \theta_{\mathbf{q}} & 0 \\ -\cos^2 \theta_{\mathbf{q}} & -\cos \theta_{\mathbf{q}} \sin \theta_{\mathbf{q}} & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{2\times}} \\
& + \underbrace{\widetilde{g}^{\text{EM}1}(q) \begin{pmatrix} 0 & 0 & -\sin \theta_{\mathbf{q}} \\ 0 & 0 & +\cos \theta_{\mathbf{q}} \\ 0 & 0 & 1 \end{pmatrix}}_{\mathbf{\Lambda}^{1\times}} + \underbrace{\widetilde{g}^{\text{EM}1\top}(q) \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ -\sin \theta_{\mathbf{q}} & \cos \theta_{\mathbf{q}} & 1 \end{pmatrix}}_{\mathbf{\Lambda}^{1\times\top}}
\end{aligned}$$

where the  $\top$  superscript indicates matrix transpose. The expressions for  $\widetilde{\mathcal{G}}^{\text{ME}}$  and  $\widetilde{\mathcal{G}}^{\text{MM}}$  are similar, involving the same  $\mathbf{\Lambda}$  matrices with different  $\widetilde{g}$  prefactors.

### 2.3.2 Evaluate $\theta_{\mathbf{q}}$ integrals

Using Table 3, the  $\theta_{\mathbf{q}}$  integral in (21) may be evaluated analytically to yield Bessel-function factors  $J_{\nu}(q\rho)$  ( $\nu \in \{0, 1, 2\}$ ) times  $\mathbf{\Lambda}$  matrices, now evaluated

$$\frac{1}{2\pi} \int_0^{2\pi} e^{iq\rho \cos(\theta_q - \theta_\rho)} \begin{pmatrix} 1 \\ \cos \theta_q \\ \sin \theta_q \\ \cos^2 \theta_q \\ \cos \theta_q \sin \theta_q \\ \sin^2 \theta_q \end{pmatrix} d\theta_q = \begin{pmatrix} J_0(q\rho) \\ iJ_1(q\rho) \cos \theta_\rho \\ iJ_1(q\rho) \sin \theta_\rho \\ -J_2(q\rho) \cos^2 \theta_\rho + \frac{J_1(q\rho)}{q\rho} \\ -J_2(q\rho) \cos \theta_\rho \sin \theta_\rho \\ -J_2(q\rho) \sin^2 \theta_\rho + \frac{J_1(q\rho)}{q\rho} \end{pmatrix},$$

Figure 3: Table of integrals used to reduce 2D integrals over  $\mathbf{q}$  to 1D integrals over  $|q|$ .

at  $\theta_\rho$ . For example, one term in the expansion of  $\mathcal{G}(\rho)$  is

$$\begin{aligned} & \int_0^\infty \frac{q dq}{2\pi} \tilde{g}^{\text{EE1}}(q) \underbrace{\int_0^{2\pi} \frac{d\theta_q}{2\pi} \Lambda^1(\theta_q) e^{iq\rho \cos(\theta_q - \theta_\rho)}}_{iJ_1(q\rho) \Lambda^1(\theta_\rho)} \\ &= \underbrace{\left\{ \int_0^\infty dq \underbrace{\left[ \frac{q}{2\pi} \tilde{g}^{\text{EE1}}(q) \cdot iJ_1(q\rho) \right]}_{\tilde{\mathbf{g}}^{\text{EE1}}(q, \rho)} \right\}}_{\mathbf{g}^{\text{EE1}}(\rho)} \Lambda^1(\theta_\rho) \end{aligned}$$

The second line here defines some new symbols:  $\tilde{\mathbf{g}}$  are functions of  $q$  and  $\rho$  defined as products of  $\tilde{g}(q)$  factors times  $J_\nu(q\rho)$  factors and other factors, while  $\mathbf{g}$  are functions of  $\rho$  obtained by integrating out the  $q$  dependence of  $\mathbf{g}(q, \rho)$ . The

full set of rules defining the  $\tilde{\mathfrak{g}}$  is

$$\tilde{\mathfrak{g}}^{\text{EE0}\parallel}(q, \rho) \equiv \frac{q}{2\pi} \left[ \tilde{g}^{\text{EE0}\parallel}(q) J_0(q\rho) + \tilde{g}^{\text{EE2}}(q) \frac{J_1(q\rho)}{q\rho} \right] \quad (24a)$$

$$\tilde{\mathfrak{g}}^{\text{EE0}z}(q, \rho) \equiv \frac{q}{2\pi} \tilde{g}^{\text{EE0}z}(q) J_0(q\rho) \quad (24b)$$

$$\tilde{\mathfrak{g}}^{\text{EE1}}(q, \rho) \equiv i \frac{q}{2\pi} \tilde{g}^{\text{EE1}}(q) J_1(q\rho) \quad (24c)$$

$$\tilde{\mathfrak{g}}^{\text{EE1}\top}(q, \rho) \equiv i \frac{q}{2\pi} \tilde{g}^{\text{EE1}\top}(q) J_1(q\rho) \quad (24d)$$

$$\tilde{\mathfrak{g}}^{\text{EE2}}(q, \rho) \equiv -\frac{q}{2\pi} \tilde{g}^{\text{EE2}}(q) J_2(q\rho) \quad (24e)$$

$$\tilde{\mathfrak{g}}^{\text{EM0}\parallel \times}(q, \rho) \equiv \frac{q}{2\pi} \left[ \tilde{g}^{\text{EM0}\parallel}(q) J_0(q\rho) + \tilde{g}^{\text{EM2}}(q) \frac{J_1(q\rho)}{q\rho} \right] \quad (24f)$$

$$\tilde{\mathfrak{g}}^{\text{EM1}\times}(q, \rho) \equiv i \frac{q}{2\pi} \tilde{g}^{\text{EM1A}}(q) J_1(q\rho) \quad (24g)$$

$$\tilde{\mathfrak{g}}^{\text{EM1}\times\top}(q, \rho) \equiv i \frac{q}{2\pi} \tilde{g}^{\text{EM1B}}(q) J_1(q\rho) \quad (24h)$$

$$\tilde{\mathfrak{g}}^{\text{EM2}\times}(q, \rho) \equiv -\frac{q}{2\pi} \tilde{g}^{\text{EM2}} J_2(q\rho) \quad (24i)$$

### 2.3.3 Evaluate Sommerfeld integrals over $q$

Assembling the above pieces, the substrate DGF correction  $\mathcal{G}$  is a sum of 22 terms:<sup>6</sup>

$$\mathcal{G}(\rho) = \sum_{m=1}^{22} \mathfrak{g}^{(m)}(\rho) \Lambda^{(m)}(\theta_\rho),$$

where the  $\mathfrak{g}^{(m)}(\rho)$  functions are defined by Sommerfeld integrals:

$$\mathfrak{g}^{(m)}(\rho) \equiv \int_0^\infty \tilde{\mathfrak{g}}^{(m)}(q, \rho) dq. \quad (25)$$

---

<sup>6</sup>This tally treats the integrals of the two integrand terms on the RHS of (24a) as two separate integrals [and similarly for (24f) and the corresponding equations for the ME and MM quadrants]. If the terms are lumped together then the number of distinct  $\mathfrak{g}$  functions is 18.

### 3 SCUFF-EM integration: Substrate contributions to BEM matrix and RHS vector

#### 3.1 Fields of individual basis functions

$$\mathcal{G}^{\text{EE}} =$$

#### 3.2 SIE matrix elements: Panel-panel integrals

If  $\mathcal{S}_\alpha, \mathcal{S}_\beta$  are two `RWGSurfaces` exposed to the outermost (ambient) region in a SCUFF-EM geometry, then the elements of the SIE matrix elements corresponding to any pair of basis functions  $\{\mathbf{b}_a \in \mathcal{S}_\alpha, \mathbf{b}_b \in \mathcal{S}_\beta\}$  receive corrections of the form

$$\begin{aligned} \Delta M_{ab}^{\text{PQ}} &= \langle \mathbf{b}_a | \mathcal{G}^{\text{PQ}} | \mathbf{b}_b \rangle \\ &\equiv \iint \mathbf{b}_a(\mathbf{x}_a) \cdot \mathcal{G}^{\text{PQ}}(\mathbf{x}_a, \mathbf{x}_b) \cdot \mathbf{b}_b(\mathbf{x}_b) d\mathbf{x}_b d\mathbf{x}_a \end{aligned} \quad (26)$$

I will consider two different approaches for evaluating the panel-panel integrals<sup>7</sup> here:

1. The *spectral inner* approach: In this case I simply evaluate the panel-panel cubature in (26), with values of  $\mathcal{G}$  at each cubature point computed via the methods of LIBSUBSTRATE as described in the previous section (possibly accelerated via interpolation tables). I call this the “spectral inner” method because in this case the  $q$  integral in the definition of  $\mathcal{G}$  is the innermost of 3 integrals. Indeed, inserting equation (22) we have

$$\begin{aligned} \Delta M_{ab}^{\text{PQ}} &\equiv \iint \mathbf{b}_a(\mathbf{x}_a) \left\{ \sum \mathfrak{g}^{(m)}(\rho) \mathbf{\Lambda}^{(m)}(\theta_\rho) \right\} \mathbf{b}_b(\mathbf{x}_b) d\mathbf{x}_b d\mathbf{x}_a \\ &\quad \text{[where } \boldsymbol{\rho} = (\mathbf{x}_a - \mathbf{x}_b)_\parallel = (\rho \cos \theta_\rho, \rho \sin \theta_\rho)]. \text{ Recalling the definition (25),} \\ &\quad \text{this is a sum of triple integrals:} \\ &\equiv \iint \mathbf{b}_a(\mathbf{x}_a) \left\{ \sum \left[ \int_0^\infty \tilde{\mathfrak{g}}^{(m)}(q, \rho) dq \right] \mathbf{\Lambda}^{(m)}(\theta_\rho) \right\} \cdot \mathbf{b}_b(\mathbf{x}_b) d\mathbf{x}_b d\mathbf{x}_a. \end{aligned} \quad (27)$$

2. The *spectral outer* approach: In this case I rearrange the order of integration in (28) so that the  $q$  integral is the *outermost* integral, with an integrand defined for each  $q$  by a panel-panel integral involving the spectral-domain GF:

$$\Delta M_{ab}^{\text{PQ}} = \int_0^\infty \left\{ \iint \mathbf{b}_a(\mathbf{x}_a) \left[ \sum \tilde{\mathfrak{g}}^{(m)}(q, \rho) \mathbf{\Lambda}^{(m)}(\theta_\rho) \right] \mathbf{b}_b(\mathbf{x}_b) d\mathbf{x}_b d\mathbf{x}_a \right\} dq \quad (28)$$

---

<sup>7</sup>I refer to 4-dimensional integrals like (26) as “panel-panel integrals” because they are a sum of contributions of integrals over pairs of flat triangular panels.

$$\mathcal{G}_{ij}^{\text{EE}} = \delta_{ij}$$



## 4 Impedance matrix

$$\mathbf{J}_p(\mathbf{x}) = \sum_{a \in \mathcal{P}_p} \left\{ \left[ -\sum_{\alpha\beta} \mathbf{b}_\alpha(\mathbf{x}) M_{\alpha\beta} R_{\beta a} \right] + \mathbf{b}_a(\mathbf{x}) \right\} w_a, \quad \mathbf{E}_q(\mathbf{x}) = \sum_{b \in \mathcal{P}_q} \left\{ \left[ -\sum_{\gamma\delta} \mathbb{E}_\gamma(\mathbf{x}) M_{\gamma\delta} R_{\delta b} \right] + \mathbb{E}_b(\mathbf{x}) \right\} w_b$$

$$\begin{aligned} Z_{pq} &\equiv \frac{1}{2I_p I_q} \int \mathbf{J}_p(\mathbf{x}) \mathbf{E}_q(\mathbf{x}) d\mathbf{x} \\ &= T_1 + T_2 + T_3 + T_4 \\ T_1 &\equiv \sum_{\alpha\beta\gamma\delta} R_{\delta q} M_{\alpha\beta} \underbrace{\left\langle \mathbf{b}_\alpha \middle| \mathbf{E}_\gamma \right\rangle}_{M_{\alpha\gamma}^{-1}} M_{\gamma\delta} R_{\beta p} \\ &= \frac{1}{2} \mathbf{R}_q \mathbf{M} \mathbf{R}_p \\ T_2 &\equiv - \sum_{\alpha\beta} \underbrace{\left\langle \mathbf{b}_\alpha \middle| \mathbf{E}_b \right\rangle}_{R_{\alpha q}} M_{\alpha\beta} R_{\beta p} \qquad \qquad \qquad = -\frac{1}{2} \mathbf{R}_q \mathbf{M} \mathbf{R}_p \end{aligned}$$

## 5 Unit-test framework

The LIBSUBSTRATE standalone library comes with a unit-test suite to test core functionality related to calculation of substrate DGFs. Separately, the unit-test suite for LIBSCUFF includes tests to check the integration of LIBSUBSTRATE into LIBSCUFF.

### 5.1 LIBSUBSTRATE unit tests

#### 5.1.1 tGTwiddle

The unit-test code `tGTwiddle.cc` tests that the full Fourier-space DGF  $\tilde{\Gamma}(\mathbf{q}, z_D, z_S)$  satisfies the appropriate boundary conditions at each layer of the layered substrate, namely

$$C^+(P, i, \ell) \tilde{\Gamma}_{ij}^{\text{PQ}}(\mathbf{q}, z_\ell + \eta, z_S) C^-(P, i, \ell) \tilde{\Gamma}_{ij}^{\text{PQ}}(\mathbf{q}, z_\ell - \eta, z_S) \quad (29)$$

where

$$C^\pm(P, i, \ell) = \begin{cases} 1, & i \in \{x, y\} \\ \epsilon_\ell^\pm, & i = z, P = E \\ \mu_\ell^\pm, & i = z, P = H \end{cases}$$

where  $\{\epsilon, \mu\}_\ell^\pm$  are the material properties for the layer above/below  $z_\ell$ , i.e. (Figure ??)

$$\{\epsilon_\ell, \mu_\ell\}^+ = \{\epsilon_\ell, \mu_\ell\}, \quad \{\epsilon_\ell, \mu_\ell\}^- = \{\epsilon_{\ell+1}, \mu_{\ell+1}\}.$$

If a ground plane is present, we have the additional condition

$$\tilde{\Gamma}_{ij}^{\text{PQ}}(q, z_{\text{GP}}, z_S) = 0 \quad \text{for } i \in \{x, y\}. \quad (30)$$

Conditions (29) and (30) must hold *independently* of the indices  $Q \in \{E, H\}$  and  $j \in \{1, 2, 3\}$  and of the values of  $\mathbf{q}$  and  $z_S$ .

## A Symbols and indices used in this document

### A.1 Symbols

Symbol	Arguments	Description
$\mathcal{F}$	$\mathbf{r}$ , geometry	Field six-vector $\mathcal{F} = \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$
$\mathcal{C}$	$\mathbf{r}$ , geometry	Current six-vector $\mathcal{C} = \begin{pmatrix} \mathbf{J} \\ \mathbf{M} \end{pmatrix}$ or $\mathcal{C} = \begin{pmatrix} \mathbf{K} \\ \mathbf{N} \end{pmatrix}$
$\mathbf{\Gamma}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , geometry	Full (bare+scattered) $6 \times 6$ dyadic Green's function, $\mathcal{F} = \mathbf{\Gamma} \star \mathcal{C}$
$\mathbf{\Gamma}^{0r}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , $\epsilon^r$ , $\mu^r$	Bare (homogeneous) $6 \times 6$ dyadic Green's function in region $r$
$\mathcal{G}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , geometry	Scattering contribution to $\mathbf{\Gamma}$ ( $\mathbf{\Gamma} = \mathbf{\Gamma}^{0r} + \mathcal{G}$ )
$\mathcal{P}$	$\mathbf{r}$ , geometry	Potential eight-vector $\mathcal{P} = \begin{pmatrix} \mathbf{A}^E \\ \Phi^E \\ \mathbf{A}^M \\ \Phi^M \end{pmatrix}$
$\mathcal{S}$	$\mathbf{r}$ , geometry	Source eight-vector $\mathcal{S} = \begin{pmatrix} \mathbf{J} \\ \rho^E \\ \mathbf{M} \\ \rho^M \end{pmatrix}$
$\mathbf{\Lambda}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , geometry	Full (bare+scattered) $8 \times 8$ dyadic Green's function, $\mathcal{P} = \mathbf{\Lambda} \star \mathcal{S}$
$\mathbf{\Lambda}^{0r}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , geometry	Bare (homogeneous) $8 \times 8$ dyadic Green's function for region $r$
$\mathcal{L}$	$\boldsymbol{\rho}$ , $z_D$ , $z_S$ , $\omega$ , geometry	Scattering contribution to $\mathbf{\Lambda}$ ( $\mathbf{\Lambda} = \mathbf{\Lambda}^{0r} + \mathcal{L}$ )

## A.2 Indices

Index	Range	Significance								
$i, j$	$\{1, 2, 3\}$	Cartesian directions $x, y, z$								
$I, J$	$\{1, 2, 3, 4, 5, 6\}$	Electric/magnetic field/current components <table><tr><td>1,2,3</td><td><math>E_{x,y,z}, J_{x,y,z}, K_{x,y,z}</math></td></tr><tr><td>4,5,6</td><td><math>H_{x,y,z}, M_{x,y,z}, N_{x,y,z}</math></td></tr></table>	1,2,3	$E_{x,y,z}, J_{x,y,z}, K_{x,y,z}$	4,5,6	$H_{x,y,z}, M_{x,y,z}, N_{x,y,z}$				
1,2,3	$E_{x,y,z}, J_{x,y,z}, K_{x,y,z}$									
4,5,6	$H_{x,y,z}, M_{x,y,z}, N_{x,y,z}$									
$\mu, \nu$	$\{1, 2, 3, 4, 5, 6, 7, 8\}$	Electric/magnetic potential/source components <table><tr><td>1,2,3</td><td><math>A^{\text{E}}_{x,y,z}, J_{x,y,z}, K_{x,y,z}</math></td></tr><tr><td>4</td><td><math>\Phi^{\text{E}}, \rho^{\text{E}}, \sigma^{\text{E}}</math></td></tr><tr><td>5,6,7</td><td><math>A^{\text{M}}_{x,y,z}, M_{x,y,z}, N_{x,y,z}</math></td></tr><tr><td>8</td><td><math>\Phi^{\text{M}}, \rho^{\text{M}}, \sigma^{\text{M}}</math></td></tr></table>	1,2,3	$A^{\text{E}}_{x,y,z}, J_{x,y,z}, K_{x,y,z}$	4	$\Phi^{\text{E}}, \rho^{\text{E}}, \sigma^{\text{E}}$	5,6,7	$A^{\text{M}}_{x,y,z}, M_{x,y,z}, N_{x,y,z}$	8	$\Phi^{\text{M}}, \rho^{\text{M}}, \sigma^{\text{M}}$
1,2,3	$A^{\text{E}}_{x,y,z}, J_{x,y,z}, K_{x,y,z}$									
4	$\Phi^{\text{E}}, \rho^{\text{E}}, \sigma^{\text{E}}$									
5,6,7	$A^{\text{M}}_{x,y,z}, M_{x,y,z}, N_{x,y,z}$									
8	$\Phi^{\text{M}}, \rho^{\text{M}}, \sigma^{\text{M}}$									

## B $8 \times 8$ Dyadic Green's Functions

The usual  $6 \times 6$  dyadic Green's function  $\mathbf{\Gamma}$  operates on a six-vector of currents to yield a six-vector of fields. It is convenient to consider a slightly different object that operates on an *eight*-vector of sources to yield an *eight*-vector of potentials.

In the presence of magnetic currents, the usual (electric-current-sourced) vector and scalar potentials  $\mathbf{A}^E, \Phi^E$ , are joined by their magnetic-current-sourced counterparts  $\mathbf{A}^M, \Phi^M$ , which are related to the fields according to

$$\begin{aligned}\mathbf{E} &= i\omega\mu\mathbf{A}^E - \frac{1}{i\omega\epsilon}\nabla\Phi^E - \nabla \times \mathbf{A}^M \\ \mathbf{M} &= \nabla \times \mathbf{A}^E + i\omega\epsilon\mathbf{A}^M - \frac{1}{i\omega\mu}\nabla\Phi^M.\end{aligned}$$

In a homogeneous region, the potentials<sup>8</sup> produced by given source distributions  $\{\mathbf{J}, \mathbf{M}\}$  are

$$\begin{aligned}\mathbf{A}^E(\mathbf{x}_D) &= \int G_0(\mathbf{x}_D - \mathbf{x}_S) \mathbf{J}(\mathbf{x}_S) d\mathbf{x}_S, & \Phi^E(\mathbf{x}_D) &= \int G_0(\mathbf{x}_D - \mathbf{x}_S) [\nabla \cdot \mathbf{J}] d\mathbf{x}_S \\ \mathbf{A}^M(\mathbf{x}_D) &= \int G_0(\mathbf{x}_D - \mathbf{x}_S) \mathbf{M}(\mathbf{x}_S) d\mathbf{x}_S, & \Phi^M(\mathbf{x}_D) &= \int G_0(\mathbf{x}_D - \mathbf{x}_S) [\nabla \cdot \mathbf{M}] d\mathbf{x}_S\end{aligned}$$

where

$$G_0(\mathbf{r}) = \frac{e^{ik|\mathbf{r}|}}{4\pi|\mathbf{r}|}.$$

$$\begin{pmatrix} E_x \\ E_y \\ E_z \\ H_x \\ H_y \\ H_z \end{pmatrix} = \begin{pmatrix} i\omega\mu G_0 & 0 & 0 & -\frac{1}{i\omega\epsilon}\partial_x G_0 & 0 & \partial_z G_0 & -\partial_y G_0 & 0 \\ 0 & i\omega\mu G_0 & 0 & -\frac{1}{i\omega\epsilon}\partial_y G_0 & -\partial_z G_0 & 0 & \partial_x G_0 & 0 \\ 0 & 0 & i\omega\mu G_0 & -\frac{1}{i\omega\epsilon}\partial_z G_0 & \partial_y G_0 & -\partial_x G_0 & 0 & 0 \\ 0 & -\partial_z G_0 & \partial_y G_0 & 0 & i\omega\epsilon G_0 & 0 & 0 & -\frac{1}{i\omega\mu}\partial_x G_0 \\ \partial_z G_0 & 0 & \partial_x G_0 & 0 & 0 & i\omega\epsilon G_0 & 0 & -\frac{1}{i\omega\mu}\partial_y G_0 \\ -\partial_y G_0 & \partial_x G_0 & 0 & 0 & 0 & 0 & i\omega\epsilon G_0 & -\frac{1}{i\omega\mu}\partial_z G_0 \end{pmatrix} \star \begin{pmatrix} J_x \\ J_y \\ J_z \\ \nabla \cdot \mathbf{J} \\ M_x \\ M_y \\ M_z \\ \nabla \cdot \mathbf{M} \end{pmatrix}$$

<sup>8</sup>Note that my  $\Phi^{E,M}$  are  $i\omega$  times the actual scalar potentials due to the charge distributions associated with currents  $\mathbf{J}, \mathbf{M}$ .