# Implicit handling of multilayered material substrates in full-wave SCUFF-EM calculations

Homer Reid

August 16, 2017

## ${\bf Contents}$

$$\epsilon_1, \mu_1$$
 $z=z_1$ 
 $\epsilon_2, \mu_2$ 
 $\epsilon_3, \mu_3$ 
 $z=z_{N-1}$ 
 $\epsilon_N, \mu_N$ 
 $\epsilon_N, \mu_N$ 
 $\epsilon_N, \mu_N$ 
 $\epsilon_N, \mu_N$ 

Figure 1: Geometry of the layered substrate. The *n*th layer has relative permittivity and permeability  $\epsilon_n, \mu_n$ , and its lower surface lies at  $z = z_n$ . The ground plane, if present, lies at  $z = z_{\text{GP}}$ .

#### 1 Overview

In a previous memo<sup>1</sup> I considered SCUFF-STATIC electrostatics calculations in the presence of a multilayered dielectric substrate. In this memo I extend that discussion to the case of *full-wave* (i.e. nonzero frequencies beyond the quasistatic regime) scattering calculations in the SCUFF-EM core library.

#### Substrate geometry

As shown in Figure 1, I consider a multilayered substrate consisting of N material layers possibly terminated by a perfectly-conducting ground plane. The uppermost layer (layer 1) is the infinite half-space above the substrate. The nth layer has relative permittivity and permeability  $\epsilon_n, \mu_n$ , and its lower surface lies at  $z=z_n$ . The ground plane, if present, lies at  $z\equiv z_{\rm N}\equiv z_{\rm GP}$ . If the ground plane is absent, layer N is an infinite half-space.<sup>2</sup>

#### Definition of the substrate DGF

I will use the symbol  $\Gamma(\omega; \mathbf{x}_{\text{D}}, \mathbf{x}_{\text{S}})$  for the *total* 6×6 dyadic Green's function relating time-harmonic fields at  $\mathbf{x}_{\text{D}}$  to sources at  $\mathbf{x}_{\text{S}}$ : thus, if  $\mathcal{S} \equiv \begin{pmatrix} \mathbf{J} \\ \mathbf{M} \end{pmatrix}$  is the 6-vector distribution of free electric and magnetic currents in the presence of the substrate, then the 6-vector of electric and magnetic fields  $\mathcal{F} \equiv \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$  is given by

$$m{\mathcal{F}}(\mathbf{x}_{ exttt{ iny D}}) = \int m{\Gamma}(\mathbf{x}_{ exttt{ iny D}}, \mathbf{x}_{ exttt{ iny S}}) \cdot m{\mathcal{S}}(\mathbf{x}_{ exttt{ iny S}}) d\mathbf{x}_{ exttt{ iny S}}.$$

 $<sup>^1\,\</sup>mathrm{``Implicit}$  handling of multilayered dielectric substrates in SCUFF-STATIC''

<sup>&</sup>lt;sup>2</sup>As in the electrostatic case, this means that a finite-thickness substrate consisting of N material layers is described as a stack of N+1 layers in which the bottommost layer is an infinite half-space  $(z_{N+1} = -\infty)$  with the material properties of vacuum  $(\epsilon_{N+1} = \mu_{N+1} = 1)$ .

The  $6 \times 6$  tensor  $\Gamma$  has a  $2 \times 2$  block structure:

$$\Gamma = \begin{pmatrix} \Gamma^{\text{EE}} & \Gamma^{\text{EM}} \\ \Gamma^{\text{ME}} & \Gamma^{\text{MM}} \end{pmatrix}$$
 (1a)

with the  $3 \times 3$  subblocks defined by

$$\Gamma_{ij}^{PQ}(\omega, \mathbf{x}_{D}, \mathbf{x}_{S}) = \begin{pmatrix} i\text{-component of P-type field at } \mathbf{x}_{D} \text{ due to } j\text{-directed} \\ Q\text{-type point current source at } \mathbf{x}_{S}, \text{ all fields and} \\ \text{sources having time dependence } \sim e^{-i\omega t} \end{pmatrix} (1b)$$

**Homogeneous DGF** In an infinite *homogeneous* medium with relative permittivity and permeability  $\{\epsilon^r, \mu^r\}$ ,  $\Gamma$  reduces to its homogeneous form, for which I will use the symbol  $\Gamma^{0r}$  (where the r index labels the medium, which in this case will be one of the layers in Figure 1, i.e.  $r \in \{1, 2, \dots, N\}$ ):

 $\mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}} \in \text{infinite homogeneous medium } r \implies \Gamma(\omega; \mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}}) = \Gamma^{0r}(\omega; \mathbf{x}_{\mathrm{D}} - \mathbf{x}_{\mathrm{S}})$ 

where $^3$ 

$$\mathbf{\Gamma}^{0r}(\omega, \mathbf{r}) \equiv \begin{pmatrix} ik_r Z_0 Z^r \mathbf{G}(k_r, \mathbf{r}) & ik_r \mathbf{C}(k_r, \mathbf{r}) \\ -ik_r \mathbf{C}(k_r, \mathbf{r}) & \frac{ik_r}{Z_0 Z^r} \mathbf{G}(k_r, \mathbf{r}) \end{pmatrix}$$

$$k_r \equiv \sqrt{\epsilon_0 \epsilon^r \mu_0 \mu^r} \cdot \omega, \quad Z_0 Z^r \equiv \sqrt{\frac{\mu_0 \mu^r}{\epsilon_0 \epsilon^r}},$$

$$G_{ij} = \left(\delta_{ij} - \frac{1}{k^2} \partial_i \partial_j\right) \frac{e^{ik|\mathbf{r}|}}{4\pi |\mathbf{r}|}, \quad C_{ij} = \frac{\varepsilon_{i\ell m}}{ik} \partial_\ell G_{mj}$$
(2)

Inhomogeneous DGF On the other hand, in the presence of the multilayered substrate the full DGF  $\Gamma$  receives corrections, which may be thought of as the fields radiated by surface currents induced on the interfacial surfaces of the substrate, and which I will denote by the symbol  $\mathcal{G}$ :

$$\Gamma(\mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}}) = \mathcal{G}(\mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}}) + \begin{cases} \Gamma^{0r}(\mathbf{x}_{\mathrm{D}} - \mathbf{x}_{\mathrm{S}}), & \mathbf{x}_{\mathrm{S}} \in \text{layer r} \\ 0, & \text{otherwise} \end{cases}$$
(3)

Like  $\Gamma$ ,  $\mathcal{G}$  is a  $6 \times 6$  matrix with a  $2 \times 2$  block structure:

$$\mathcal{G}(\omega; \mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}}) = \begin{pmatrix} \mathcal{G}^{\mathrm{EE}} & \mathcal{G}^{\mathrm{EM}} \\ \mathcal{G}^{\mathrm{ME}} & \mathcal{G}^{\mathrm{MM}} \end{pmatrix}$$
(4)

with the  $3 \times 3$  subblocks defined by

$$\mathcal{G}_{ij}^{\text{\tiny PQ}} = \begin{pmatrix} i\text{-component of P-type field at }\mathbf{x}_{\text{\tiny D}} \text{ due to surface currents on substrate interface layers induced by } j\text{-directed Q-type source at }\mathbf{x}_{\text{\tiny S}}. \end{pmatrix}$$

LIBSUBSTRATE is a code for numerical computation of  $\mathcal{G}$ .

 $<sup>^3</sup>$ Cf. Section 3 of the companion memo "LIBSCUFF implementation and Technical Details," http://homerreid.github.io/scuff-em-documentation/tex/lsInnards.pdf

#### Organization of SCUFF-EM implementation and this memo

The full-wave substrate implementation in SCUFF-EM consists of multiple working parts that fit together in a somewhat modular fashion.

Roughly speaking, the computational problem may be divided into two parts:

- (a) For given source and evaluation (or "destination") points  $\{\mathbf{x}_{\mathrm{S}}, \mathbf{x}_{\mathrm{D}}\}$  at a given angular frequency  $\omega$  in the presence of a multilayer substrate, numerically compute the substrate DGF correction  $\mathcal{G}(\omega, \mathbf{x}_{\mathrm{D}}, \mathbf{x}_{\mathrm{S}})$ . This task is independent of SCUFF-EM and is implemented by a standalone library called LIBSUBSTRATE, described in Section 2 of this memo.
- (b) For a SCUFF-EM geometry in the presence of a substrate, compute the substrate corrections to the BEM system matrix M and RHS vector v, as well as the substrate corrections to post-processing quantities such as scattered fields. This is done by the file Substrate.cc in LIBSCUFF and is described in Section ?? of this memo.

## 2 LIBSUBSTRATE: Numerical computation of substrate Green's functions

Numerical evaluation of substrate contributions to dyadic Green's functions is handled by a C++ library called LIBSUBSTRATE. Although this library is packaged and distributed with SCUFF-EM and depends on other support libraries in the SCUFF-EM distribution, it is independent of the particular integral-equation formulation implemented by LIBSCUFF, and thus should be of general utility beyond SCUFF-EM.

#### 2.1 Overview of computational strategy

LIBSUBSTRATE decomposes the problem of computing  ${\cal G}$  into several logical steps, as follows:

- 1. Solve a linear system to obtain the Fourier-space representation  $\widetilde{\mathcal{G}}(\mathbf{q})$ . Here  $\mathbf{q} = (q_x, q_y)$  is a 2D Fourier variable. (Section ??.)
- **2.** Reduce the two-dimensional integral over  $\mathbf{q}$  to a one-dimensional integral over  $|\mathbf{q}| \equiv q$ . (Section ??.)
- **3.** Evaluate the q integral using established methods for evaluating Sommerfeld integrals. (Section  $\ref{eq:section}$ .)

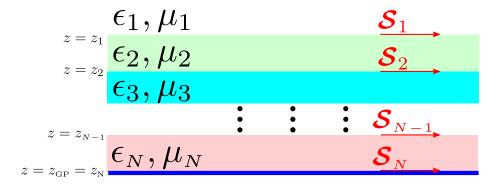


Figure 2: Effective surface-current approach to treatment of multilayer substrate. External field sources induce a distribution of electric and magnetic surface currents  $S_n = \binom{\mathbf{K}_n}{\mathbf{N}_n}$  on the *n*th material interface, and the fields radiated by these effective currents account for the disturbance presented by the substrate.

## 2.2 Computation of Fourier-space DGF $\widetilde{\mathcal{G}}(\mathbf{q})$

To compute the substrate correction to the fields of external sources, I consider the effective tangential electric and magnetic surface currents  ${\bf K}$  and  ${\bf N}$  induced on the interfacial layers by the external field sources (Figure ??). This is the direct extension to full-wave problems of the formalism I used in the electrostatic case, and it comports well with the spirit of surface-integral-equation methods.

More specifically, on the material interface layer at  $z=z_n$  I have a four-vector surface-current density  $\mathcal{S}_n(\rho)$ , where  $\rho=(x,y)$  and the components of  $\mathcal{S}$  are

$$\boldsymbol{\mathcal{S}}_{n}(\boldsymbol{\rho}) = \begin{pmatrix} K_{x}(\boldsymbol{\rho}) \\ K_{y}(\boldsymbol{\rho}) \\ N_{x}(\boldsymbol{\rho}) \\ N_{y}(\boldsymbol{\rho}) \end{pmatrix}. \tag{5}$$

Fields in layer interiors. I will adopt the convention that the lower (upper) bounding surface for each region is the positive (negative) bounding surface for that region in the usual sense of SCUFF-EM regions and surfaces (in which the sign of a {surface,region} pair  $\{S, \mathcal{R}\}$  is the sign with which surface currents on S contribute to fields in  $\mathcal{R}$ ). Thus, at a point  $\mathbf{x} = (\boldsymbol{\rho}, z)$  in the interior of layer  $n \ (z_{n-1} > z > z_n)$ , the six-vector of total fields  $\mathcal{F} = \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$  reads

$$\mathcal{F}_n(\boldsymbol{\rho}, z) = -\Gamma^{0n}(z_{n-1}) \star \mathcal{S}_{n-1} + \Gamma^{0n}(z_n) \star \mathcal{S}_n + \mathcal{F}_n^{\text{ext}}(\boldsymbol{\rho}, z)$$
 (6)

where  $\mathcal{F}_n^{\mathrm{ext}}$  are the externally-sourced (incident) fields due to sources in layer n,  $\Gamma^{0n}$  is the  $6 \times 6$  homogeneous dyadic Green's function for material layer n,

and  $\star$  is shorthand for the convolution operation

"
$$\mathcal{F}(\boldsymbol{\rho}, z) \equiv \Gamma(z') \star \mathcal{S}'' \implies \mathcal{F}(\boldsymbol{\rho}, z) = \int \Gamma(\boldsymbol{\rho} - \boldsymbol{\rho}', z - z') \cdot \mathcal{S}(\boldsymbol{\rho}') d\boldsymbol{\rho}'$$
 (7)

where the integral extends over the entire interfacial plane. I will evaluate convolutions of this form using the 2D Fourier representation of  $\Gamma^{0n}$ :

$$\mathbf{\Gamma}^{0n}(\boldsymbol{\rho}, z) = \int \frac{d^2 \mathbf{q}}{(2\pi)^2} \widetilde{\mathbf{\Gamma}^{0n}}(\mathbf{q}, z) e^{i\mathbf{q}\cdot\boldsymbol{\rho}}$$
(8a)

$$\widetilde{\mathbf{\Gamma}^{0n}}(\mathbf{q}, z) = \frac{1}{2} \begin{pmatrix} -\frac{\omega\mu_0\mu_n}{q_{zn}}\widetilde{\mathbf{G}}^{\pm} & +\widetilde{\mathbf{C}}^{\pm} \\ -\widetilde{\mathbf{C}}^{\pm} & -\frac{\omega\epsilon_0\epsilon_n}{q_{zn}}\widetilde{\mathbf{G}}^{\pm} \end{pmatrix} e^{iq_z|z|}$$
(8b)

$$\widetilde{\mathbf{G}}^{\pm}(\mathbf{q},k) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} - \frac{1}{k^2} \begin{pmatrix} q_x^2 & q_x q_y & \pm q_x q_z \\ q_y q_x & q_y^2 & \pm q_y q_z \\ \pm q_z q_x & \pm q_z q_y & q_z^2 \end{pmatrix}$$
(8c)

$$\widetilde{\mathbf{C}}^{\pm}(\mathbf{q}, k) = \begin{pmatrix} 0 & \mp 1 & +q_y/q_z \\ \pm 1 & 0 & -q_x/q_z \\ -q_y/q_z & +q_x/q_z & 0 \end{pmatrix}$$
(8d)

$$k_n \equiv \sqrt{\epsilon_0 \epsilon_n \mu_0 \mu_n} \cdot \omega, \qquad q_z \equiv \sqrt{k^2 - |\mathbf{q}|^2}, \qquad \pm = \text{sign } z.$$
 (8e)

With this representation, convolutions like (??) become products in Fourier space:

$$\Gamma(z') \star \mathcal{S} = \mathcal{F}(\rho, z) = \int \frac{d^2 \mathbf{q}}{(2\pi)^2} \widetilde{\mathcal{F}}(\mathbf{q}, z) e^{i\mathbf{q}\cdot\rho}, \text{ with } \widetilde{\mathcal{F}}(\mathbf{q}, z) = \widetilde{\Gamma}(\mathbf{q}, z - z') \widetilde{\mathcal{S}}(\mathbf{q})$$

Surface currents from incident fields. To determine the surface currents induced by given incident-field sources, I apply boundary conditions. The boundary condition at  $z = z_n$  is that the tangential  $\mathbf{E}, \mathbf{H}$  fields be continuous: in Fourier space, we have

$$\widetilde{\mathcal{F}}_{\parallel}(\mathbf{q}, z = z_n^+) = \widetilde{\mathcal{F}}_{\parallel}(\mathbf{q}, z = z_n^-)$$
 (9)

The fields just **above** the interface  $(z \to z_n^+)$  receive contributions from three sources:

- Surface currents at  $z = z_{n-1}$ , which contribute with a minus sign and via the Green's function for region n;
- Surface currents at  $z = z_n$ , which contribute with a plus sign and via the Green's function for region n; and
- external field sources in region n.

The fields just **below** the interface  $(z=z_n^-)$  receive contributions from three sources:

- Surface currents at  $z=z_n$ , which contribute with a minus sign and via the Green's function for region n + 1;
- Surface currents at  $z = z_{n+1}$ , which contribute with a plus sign and via the Green's function for region n+1; and
- external field sources in region n+1.

Then equation (??) reads (temporarily omitting **q** arguments)

$$-\widetilde{\mathbf{\Gamma}^{0n}}_{\parallel}(z_{n}-z_{n-1})\cdot\widetilde{\boldsymbol{\mathcal{S}}}_{n-1}+\widetilde{\mathbf{\Gamma}^{0n}}_{\parallel}(0^{+})\cdot\widetilde{\boldsymbol{\mathcal{S}}}_{n}+\widetilde{\boldsymbol{\mathcal{F}}}_{n\parallel}^{\mathrm{ext}}(z_{n})$$

$$=-\widetilde{\mathbf{\Gamma}^{0,n+1}}_{\parallel}(0^{-})\cdot\widetilde{\boldsymbol{\mathcal{S}}}_{n}+\widetilde{\mathbf{\Gamma}^{0,n+1}}_{\parallel}(z_{n}-z_{n+1})\cdot\widetilde{\boldsymbol{\mathcal{S}}}_{n+1}+\widetilde{\boldsymbol{\mathcal{F}}}_{n+1\parallel}^{\mathrm{ext}}(z_{n})$$

$$\mathbf{M}_{n,n-1} \cdot \widetilde{\boldsymbol{\mathcal{S}}}_{n-1} + \mathbf{M}_{n,n} \cdot \widetilde{\boldsymbol{\mathcal{S}}}_n + \mathbf{M}_{n,n+1} \cdot \widetilde{\boldsymbol{\mathcal{S}}}_{n+1} = \widetilde{\boldsymbol{\mathcal{F}}}_{n+1\parallel}^{\mathrm{ext}}(z_n) - \widetilde{\boldsymbol{\mathcal{F}}}_{n\parallel}^{\mathrm{ext}}(z_n) \quad (10)$$

with the  $4 \times 4$  matrix blocks<sup>4</sup>

$$\mathbf{M}_{n,n-1} = -\widetilde{\mathbf{\Gamma}^{0n}}_{\parallel}(z_n - z_{n-1}) \tag{13a}$$

$$\mathbf{M}_{n,n} = +\widetilde{\mathbf{\Gamma}^{0n}}_{\parallel}(0^{+}) + \widetilde{\mathbf{\Gamma}^{0,n+1}}_{\parallel}(0^{-})$$
(13b)

$$\mathbf{M}_{n,n+1} = -\widetilde{\mathbf{\Gamma}^{0,n+1}}_{\parallel}(z_n - z_{n+1}) \tag{13c}$$

Writing down equation (??) equation for all N dielectric interfaces yields a  $4N \times 4N$  system of linear equations, with triadiagonal  $4 \times 4$  block form, relating the surface currents on all layers to the external fields due to sources in all regions:

$$\mathbf{M} \cdot \mathbf{s} = \mathbf{f} \tag{14}$$

$$\mathbf{M}_{n,n} = \sum_{r \in \{n,n+1\}} \frac{1}{2} \begin{pmatrix} -\frac{\omega \epsilon_r}{Z_0 q_{zr}} \mathbf{g}(k_r, \mathbf{q}) & 0 \\ 0 & -\frac{\omega \mu_r Z_0}{q_{zr}} \mathbf{g}(k_r, \mathbf{q}) \end{pmatrix}$$

$$\mathbf{M}_{n,n\pm 1} = \frac{1}{2} \begin{pmatrix} -\frac{\omega \epsilon_r}{Z_0 q_{zr}} \mathbf{g}(k_r, \mathbf{q}) & \mathbf{c}^{\pm} \\ -\mathbf{c}^{\pm} & -\frac{\omega \mu_r Z_0}{q_{zn}^*} \mathbf{g}(k_r, \mathbf{q}) \end{pmatrix} e^{iq_{zr}|z_n - z_{n\pm 1}|}$$

$$(12)$$

$$\mathbf{M}_{n,n\pm 1} = \frac{1}{2} \begin{pmatrix} -\frac{\omega \epsilon_r}{Z_0 q_{zr}} \mathbf{g}(k_r, \mathbf{q}) & \mathbf{c}^{\pm} \\ -\mathbf{c}^{\pm} & -\frac{\omega \mu_r Z_0}{q_{zn}*} \mathbf{g}(k_r, \mathbf{q}) \end{pmatrix} e^{iq_{zr}|z_n - z_{n\pm 1}|}$$
(12)

where I put  $r \equiv \begin{cases} n, & \text{for } \mathbf{M}_{n,n-1} \\ n+1, & \text{for } \mathbf{M}_{n,n+1} \end{cases}$  and

$$\mathbf{g}(k; \mathbf{q}) = \mathbf{1} - \frac{\mathbf{q}\mathbf{q}^{\top}}{k^2}, \qquad \mathbf{c}^{\pm} = \begin{pmatrix} 0 & \mp 1 \\ \pm 1 & 0 \end{pmatrix}$$

<sup>&</sup>lt;sup>4</sup>The  $4 \times 4$  M blocks here have  $2 \times 2$  block structure:

where **M** is the  $4N \times 4N$  block-tridiagonal matrix (??) and where the 4N-vectors **s**, **f** read

$$\mathbf{s} = \left(egin{array}{c} \widetilde{oldsymbol{\mathcal{S}}}_1 \ \widetilde{oldsymbol{\mathcal{S}}}_2 \ \widetilde{oldsymbol{\mathcal{S}}}_3 \ dots \ \widetilde{oldsymbol{\mathcal{S}}}_N \end{array}
ight), \qquad \mathbf{f} = \left(egin{array}{c} -\widetilde{oldsymbol{\mathcal{F}}}_{1\parallel}(z_1) + \widetilde{oldsymbol{\mathcal{F}}}_{2\parallel}(z_1) \ -\widetilde{oldsymbol{\mathcal{F}}}_{2\parallel}(z_2) + \widetilde{oldsymbol{\mathcal{F}}}_{3\parallel}(z_2) \ -\widetilde{oldsymbol{\mathcal{F}}}_{3\parallel}(z_3) + \widetilde{oldsymbol{\mathcal{F}}}_{3\parallel}(z_4) \ dots \ -\widetilde{oldsymbol{\mathcal{F}}}_{N-1,\parallel}(z_{N-1}) + \widetilde{oldsymbol{\mathcal{F}}}_{N\parallel}(z_{N-1}) \end{array}
ight).$$

Solving (??) yields the induced surface currents on all layers in terms of the incident fields:

$$\mathbf{s} = \mathbf{W} \cdot \mathbf{f}$$
 where  $\mathbf{W} \equiv \mathbf{M}^{-1}$ 

or, more explicitly,

$$\widetilde{\boldsymbol{\mathcal{S}}}_n = \sum_m W_{nm} \mathbf{f}_m \tag{15}$$

#### Surface currents induced by point sources

For DGF computations the incident fields arise from a single point source—say, a *j*-directed source in region s. Then the only nonzero length-4 blocks of the RHS vector in (??) are  $\mathbf{f}_{s-1}, \mathbf{f}_s$  with components  $(\ell = \{1, 2, 4, 5\})$ 

$$\left(\mathbf{f}_{s-1}\right)_{\ell} = -\widetilde{\Gamma}_{\ell j}^{0s}(z_{s-1} - z_{s}), \qquad \left(\mathbf{f}_{s}\right)_{\ell} = +\widetilde{\Gamma}_{\ell j}^{0s}(z_{s} - z_{s}) \tag{16}$$

and the surface currents on interface layer n are obtained by solving (??):

$$\widetilde{\mathbf{S}}_{n} = \mathbf{W}_{n,s-1} \mathbf{f}_{s-1} + \mathbf{W}_{n,s} \mathbf{f}_{s}$$

$$= \sum_{p=0}^{1} (-1)^{p+1} \mathbf{W}_{n,s-1+p} \cdot \widetilde{\mathbf{\Gamma}^{0s}}_{\parallel,j} (z_{s} - z_{s-1+p})$$

$$(17)$$

#### Fields due to surface currents

Given the surface currents induced by a j-directed point source at  $\mathbf{x}_s$ , I evaluate the fields due to these currents to get the substrate DGF contribution  $\mathcal{G}$ . If the evaluation point  $\mathbf{x}_D$  lies in region d, then the fields receive contributions from the surface currents at  $z_{d-1}$  and  $z_D$ , propagated by the homogeneous DGF for region d:

$$\widetilde{\mathcal{F}}(z_{\mathrm{D}}) = -\widetilde{\Gamma^{0d}}(z_{\mathrm{D}} - z_{d-1}) \cdot \widetilde{\mathcal{S}}_{d-1} + \widetilde{\Gamma^{0d}}(z_{\mathrm{D}} - z_{\mathrm{D}}) \cdot \widetilde{\mathcal{S}}_{d}$$

$$= \sum_{q=0}^{1} (-1)^{q+1} \widetilde{\Gamma^{0d}}(z_{\mathrm{D}} - z_{d+q-1}) \cdot \widetilde{\mathcal{S}}_{d+q-1}$$
(18)

(The minus sign in the first term arises because, in my convention, surface currents on the upper surface of a region contribute to the fields in that region with a minus sign). Inserting (??), the i component here—which is the ij component of the substrate DGF—is

$$\widetilde{\mathcal{G}}_{ij}(z_{D}, z_{S}) = \sum_{p,q=0}^{1} (-1)^{p+q} \widetilde{\mathbf{\Gamma}^{0d}}_{i,\parallel}(z_{D} - z_{d-1+q}) \mathbf{W}_{d-1+q,s-1+p} \widetilde{\mathbf{\Gamma}^{0s}}_{\parallel,j}(z_{s-1+p} - z_{S}).$$
(19)

The calculation of equation (??) is carried out by the routine GetGTwiddle in LIBSUBSTRATE.

#### Green's functions for potentials

In equation (??) I am computing the 6 components of the **E** and **H** fields produced by the induced surface currents. If instead I compute the *potentials* produced by those currents I obtain a slightly different Green's function. Thus, let  $\mathbf{A}^{\mathrm{E}}, \Phi^{\mathrm{E}}$  be the usual vector and scalar potential of an electric-current source in a homogeneous region, and let  $\mathbf{A}^{\mathrm{M}}, \Phi^{\mathrm{M}}$  be their counterparts for magnetic-current sources, i.e. if the electric and magnetic volume currents are **J** and **M** then

$$\mathbf{A}^{\mathrm{E}}(\mathbf{x}_{\mathrm{D}}) = \mu \int \mathbf{J}(\mathbf{x}_{\mathrm{S}}) G_{0}(\mathbf{x}_{\mathrm{DS}}) d\mathbf{x}_{\mathrm{S}}, \quad \Phi^{\mathrm{E}}(\mathbf{x}_{\mathrm{D}}) = \frac{1}{i\omega\epsilon} \int (\nabla \cdot \mathbf{J}) G_{0}(\mathbf{x}_{\mathrm{DS}}) d\mathbf{x}_{\mathrm{S}}$$

$$(20a)$$

$$\mathbf{A}^{\mathrm{M}}(\mathbf{x}_{\mathrm{D}}) = \epsilon \int \mathbf{M}(\mathbf{x}_{\mathrm{S}}) G_{0}(\mathbf{x}_{\mathrm{DS}}) d\mathbf{x}_{\mathrm{S}}, \quad \Phi^{\mathrm{M}}(\mathbf{x}_{\mathrm{D}}) = \frac{1}{i\omega\mu} \int (\nabla \cdot \mathbf{M}) G_{0}(\mathbf{x}_{\mathrm{DS}}) d\mathbf{x}_{\mathrm{S}}$$

$$(20b)$$

with  $\mathbf{x}_{DS} \equiv \mathbf{x}_{D} - \mathbf{x}_{S}$  and

$$G_0(k; \mathbf{r}) = \frac{e^{ik|\mathbf{r}|}}{4\pi|\mathbf{r}|} = \int \frac{d^2\mathbf{q}}{(2\pi)^2} \widetilde{G}_0(\mathbf{q}, z) e^{i\mathbf{q}\cdot\boldsymbol{\rho}}, \qquad \widetilde{G}_0 = \frac{i}{2q_z} e^{iq_z|z|}.$$

I write

## 2.3 Reduction of 2D Fourier integrals to 1D (Sommerfeld) integrals

The real-space DGF correction is the inverse Fourier transform of (??):

$$oldsymbol{\mathcal{G}}(oldsymbol{
ho},z_{ ext{ iny D}},z_{ ext{ iny S}}) = \int rac{d^2 \mathbf{q}}{(2\pi)^2} \widetilde{oldsymbol{\mathcal{G}}}(\mathbf{q};z_{ ext{ iny D}};z_{ ext{ iny S}}) e^{i \mathbf{q} \cdot oldsymbol{
ho}}$$

or, in polar coordinates with  $(q_x, q_y) = (q \cos \theta_q, q \sin \theta_q), (\rho_x, \rho_y) = (\rho \cos \theta_\rho, \rho \sin \theta_\rho),$ 

$$\mathcal{G}(\boldsymbol{\rho}) = \int_0^\infty \frac{q \, dq}{2\pi} \int_0^{2\pi} \frac{d\theta_q}{2\pi} \widetilde{\mathcal{G}}(\mathbf{q}) e^{iq\rho \cos(\theta_q - \theta_\rho)}. \tag{21}$$

(Here and for much of this section I suppress  $z_{\text{D,S}}$  arguments, but one must remember that they are always there.<sup>5</sup>) The goal of this section is to integrate out the angular variable  $\theta_q$  to reduce the 2D integral over  $\mathbf{q}$  to a 1D integral over  $q = |\mathbf{q}|$ . In abbreviated form this proceeds as follows:

1. Separate variables by writing  $\widetilde{\mathcal{G}}(\mathbf{q})$  as a sum of products of  $\theta_q$ -independent scalar functions  $\widetilde{g}(q)$  times q-independent matrix-valued functions  $\Lambda(\theta_q)$  (Section ??):

$$\widetilde{\mathcal{G}}(\mathbf{q}) = \sum_{n=1}^{18} \widetilde{g}^{(n)}(q) \mathbf{\Lambda}^{(n)}(\theta_q)$$

2. Evaluate integrals over  $\theta_q$  analytically to yield Bessel functions  $J_{\nu}(q\rho)$  multiplying q-independent matrix-valued functions  $\Lambda(\theta_{\rho})$  (Section ??). After this step (??) reads

$$\mathcal{G}(\rho) = \sum_{m=1}^{22} \underbrace{\left[ \int_0^\infty \widetilde{\mathfrak{g}}^{(m)}(q,\rho) \, dq \right]}_{\mathfrak{g}^{(m)}(\rho)} \mathbf{\Lambda}^{(m)}(\theta_\rho)$$
 (22)

where the  $\widetilde{\mathfrak{g}}(q,\rho)$  functions are linear combinations of the  $\widetilde{g}(q)$  functions times Bessel functions in  $q\rho$  and other factors.

3. Evaluate the remaining integrals over q numerically using sophisticated tricks for evaluating Sommereld integrals (Section  $\ref{eq:soft}$ ).

#### 2.3.1 Factor $\hat{\mathcal{G}}$ into q-independent and $\theta_q$ -independent terms

I begin by noting that  $\widetilde{\mathcal{G}}(\mathbf{q})$  may be decomposed as a sum of scalar functions of  $q = |\mathbf{q}|$  times q-independent matrix-valued functions of  $\theta_{\mathbf{q}}$ :

$$\widetilde{\mathcal{G}}(\mathbf{q}) = \sum_{n=1}^{18} \widetilde{g}^{(n)}(q) \mathbf{\Lambda}^{(n)}(\theta_{\mathbf{q}})$$
(23)

<sup>&</sup>lt;sup>5</sup>More specifically, the "g-like" quantities  $\mathcal{G}(\rho)$ ,  $\widetilde{\mathcal{G}}(\mathbf{q})$ ,  $\widetilde{\mathfrak{g}}(q)$ ,  $\widetilde{\mathfrak{g}}(q)$ , and  $\mathfrak{g}(\rho)$  all depend on  $z_{\mathrm{S,D}}$ , but the matrix-valued functions  $\Lambda_n(\theta)$  do not.

For example, the upper two quadrants read

$$\begin{split} \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EE}}(\mathbf{q}) = & \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EEO}\parallel}(q) \underbrace{\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\boldsymbol{\Lambda}^{0\parallel}} + \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EEO}z}(q) \underbrace{\begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix}}_{\boldsymbol{\Lambda}^{0z}} \\ + & \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EE1}}(q) \underbrace{\begin{pmatrix} 0 & 0 & \cos\theta_{\mathbf{q}} \\ 0 & 0 & \sin\theta_{\mathbf{q}} \\ 0 & 0 & 0 \end{pmatrix}}_{\boldsymbol{\Lambda}^{1}(\theta_{\mathbf{q}})} + & \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EE1}}(q) \underbrace{\begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ \cos\theta_{\mathbf{q}} & \sin\theta_{\mathbf{q}} & 0 \end{pmatrix}}_{\boldsymbol{\Lambda}^{1\top}(\theta_{\mathbf{q}})} \\ + & \widetilde{\boldsymbol{\mathcal{G}}}^{\text{EE2}}(q) \underbrace{\begin{pmatrix} \cos^{2}\theta_{\mathbf{q}} & \cos\theta_{\mathbf{q}}\sin\theta_{\mathbf{q}} & 0 \\ \cos\theta_{\mathbf{q}}\sin\theta_{\mathbf{q}} & \sin^{2}\theta_{\mathbf{q}} & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\boldsymbol{\Lambda}^{2}(\theta_{\mathbf{q}})} \end{split}$$

$$\begin{split} \widetilde{\mathcal{G}^{\text{EM}}}(\mathbf{q}) = & \widetilde{g}^{\text{EM0}\parallel}(q) \underbrace{\begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{0\times}} + & \widetilde{g}^{\text{EM2}}(q) \underbrace{\begin{pmatrix} \cos\theta_{\mathbf{q}}\sin\theta_{\mathbf{q}} & \sin^2\theta_{\mathbf{q}} & 0 \\ -\cos^2\theta_{\mathbf{q}} & -\cos\theta_{\mathbf{q}}\sin\theta_{\mathbf{q}} & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\mathbf{\Lambda}^{2\times}} \\ + & \widetilde{g}^{\text{EM1}}(q) \underbrace{\begin{pmatrix} 0 & 0 & -\sin\theta_{\mathbf{q}} \\ 0 & 0 & +\cos\theta_{\mathbf{q}} \\ 0 & 0 & 1 \end{pmatrix}}_{\mathbf{\Lambda}^{2\times}} + & \widetilde{g}^{\text{EM1}\top}(q) \underbrace{\begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ -\sin\theta_{\mathbf{q}} & \cos\theta_{\mathbf{q}} & 1 \end{pmatrix}}_{\mathbf{\Lambda}^{2\times}} \end{split}$$

where the  $\top$  superscript indicates matrix transpose. The expressions for  $\widetilde{\boldsymbol{\mathcal{G}}}^{^{\mathrm{ME}}}$  and  $\widetilde{\boldsymbol{\mathcal{G}}}^{^{\mathrm{MM}}}$  are similar, involving the same  $\Lambda$  matrices with different  $\widetilde{g}$  prefactors.

#### 2.3.2 Evaluate $\theta_q$ integrals

Using Table ??, the  $\theta_{\mathbf{q}}$  integral in (??) may be evaluated analytically to yield Bessel-function factors  $J_{\nu}(q\rho)$  ( $\nu \in \{0,1,2\}$ ) times  $\Lambda$  matrices, now evaluated

$$\frac{1}{2\pi} \int_0^{2\pi} e^{iq\rho\cos(\theta_q - \theta_\rho)} \left\{ \begin{array}{c} 1 \\ \cos\theta_q \\ \sin\theta_q \\ \cos^2\theta_q \\ \cos\theta_q\sin\theta_q \\ \sin^2\theta_q \end{array} \right\} d\theta_q = \left\{ \begin{array}{c} J_0(q\rho) \\ iJ_1(q\rho)\cos\theta_\rho \\ iJ_1(q\rho)\sin\theta_\rho \\ -J_2(q\rho)\cos^2\theta_\rho + \frac{J_1(q\rho)}{q\rho} \\ -J_2(q\rho)\sin^2\theta_\rho + \frac{J_1(q\rho)}{q\rho} \end{array} \right\},$$

Figure 3: Table of integrals used to reduce 2D integrals over  $\mathbf{q}$  to 1D integrals over |q|.

at  $\theta_{\rho}$ . For example, one term in the expansion of  $\mathcal{G}(\rho)$  is

$$\int_{0}^{\infty} \frac{q dq}{2\pi} \widetilde{g}^{\text{EE1}}(q) \underbrace{\int_{0}^{2\pi} \frac{d\theta_{q}}{2\pi} \mathbf{\Lambda}^{1}(\theta_{q}) e^{iq\rho \cos(\theta_{q} - \theta_{\rho})}}_{iJ_{1}(q\rho)\mathbf{\Lambda}^{1}(\theta_{\rho})}$$

$$= \underbrace{\left\{ \int_{0}^{\infty} dq \underbrace{\left[ \frac{q}{2\pi} \widetilde{g}^{\text{EE1}}(q) \cdot iJ_{1}(q\rho) \right]}_{\widetilde{\mathfrak{g}}^{\text{EE1}}(\rho)} \right\} \mathbf{\Lambda}^{1}(\theta_{\rho})}_{\mathbf{g}^{\text{EE1}}(\rho)}$$

The second line here defines some new symbols:  $\tilde{\mathfrak{g}}$  are functions of q and  $\rho$  defined as products of  $\tilde{g}(q)$  factors times  $J_{\nu}(q\rho)$  factors and other factors, while  $\mathfrak{g}$  are functions of  $\rho$  obtained by integrating out the q dependence of  $\mathfrak{g}(q,\rho)$ . The

full set of rules defining the  $\widetilde{\mathfrak{g}}$  is

$$\widetilde{\mathfrak{g}}^{\text{EEO}\parallel}(q,\rho) \equiv \frac{q}{2\pi} \left[ \widetilde{g}^{\text{EEO}\parallel}(q) J_0(q\rho) + \widetilde{g}^{\text{EE2}}(q) \frac{J_1(q\rho)}{q\rho} \right]$$
(24a)

$$\widetilde{\mathfrak{g}}^{\text{EEOz}}(q,\rho) \equiv \frac{q}{2\pi} \widetilde{g}^{\text{EEOz}}(q) J_0(q\rho)$$
 (24b)

$$\widetilde{\mathfrak{g}}^{\text{EE1}}(q,\rho) \equiv i \frac{q}{2\pi} \widetilde{g}^{\text{EE1}}(q) J_1(q\rho)$$
 (24c)

$$\widetilde{\mathfrak{g}}^{\text{EE1T}}(q,\rho) \equiv i \frac{q}{2\pi} \widetilde{\mathfrak{g}}^{\text{EE1T}}(q) J_1(q\rho)$$
 (24d)

$$\widetilde{\mathfrak{g}}^{\text{EE2}}(q,\rho) \equiv -\frac{q}{2\pi} \widetilde{g}^{\text{EE2}}(q) J_2(q\rho) \tag{24e}$$

$$\widetilde{\mathfrak{g}}^{\text{EMO}\parallel\times}(q,\rho) \equiv \frac{q}{2\pi} \left[ \widetilde{g}^{\text{EMO}\parallel}(q) J_0(q\rho) + \widetilde{g}^{\text{EM2}}(q) \frac{J_1(q\rho)}{q\rho} \right]$$
(24f)

$$\widetilde{\mathfrak{g}}^{\text{EM1}\times}(q,\rho) \equiv i \frac{q}{2\pi} \widetilde{\mathfrak{g}}^{\text{EM1A}}(q) J_1(q\rho)$$
 (24g)

$$\widetilde{\mathfrak{g}}^{\text{EM1}\times\top}(q,\rho) \equiv i\frac{q}{2\pi}\widetilde{g}^{\text{EM1B}}(q)J_1(q\rho)$$
 (24h)

$$\widetilde{\mathfrak{g}}^{\text{EM2}\times}(q,\rho) \equiv -\frac{q}{2\pi}\widetilde{g}^{\text{EM2}}J_2(q\rho)$$
 (24i)

#### 2.3.3 Evaluate Sommerfeld integrals over q

Assembling the above pieces, the substrate DGF correction  ${\cal G}$  is a sum of 22 terms:

$$\mathcal{G}(\rho) = \sum_{m=1}^{22} \mathfrak{g}^{(m)}(\rho) \mathbf{\Lambda}^{(m)}(\theta_{\rho}),$$

where the  $\mathfrak{g}^{(m)}(\rho)$  functions are defined by Sommerfeld integrals:

$$\mathfrak{g}^{(m)}(\rho) \equiv \int_0^\infty \widetilde{\mathfrak{g}}^{(m)}(q,\rho) \, dq. \tag{25}$$

<sup>&</sup>lt;sup>6</sup>This tally treats the integrals of the two integrand terms on the RHS of (??a) as two separate integrals [and similarly for (??f) and the corresponding equations for the ME and MM quadrants]. If the terms are lumped together then the number of distinct g functions is 18.

## 3 SCUFF-EM integration: Substrate contributions to BEM matrix and RHS vector

#### 3.1 Fields of individual basis functions

$$\mathcal{G}^{ ext{EE}} =$$

#### 3.2 SIE matrix elements: Panel-panel integrals

If  $S_{\alpha}, S_{\beta}$  are two RWGSurfaces exposed to the outermost (ambient) region in a SCUFF-EM geometry, then the elements of the SIE matrix elements corresponding to any pair of basis functions  $\{\mathbf{b}_a \in \mathcal{S}_{\alpha}, \mathbf{b}_b \in \mathcal{S}_{\beta}\}$  receive corrections of the form

$$\Delta M_{ab}^{PQ} = \left\langle \mathbf{b}_a \middle| \mathbf{\mathcal{G}}^{PQ} \middle| \mathbf{b}_b \right\rangle$$

$$\equiv \iint \mathbf{b}_a(\mathbf{x}_a) \cdot \mathbf{\mathcal{G}}^{PQ}(\mathbf{x}_a, \mathbf{x}_b) \cdot \mathbf{b}_b(\mathbf{x}_b) \, d\mathbf{x}_b \, d\mathbf{x}_a$$
(26)

I will consider two different approaches for evaluating the panel-panel integrals here:

1. The spectral inner approach: In this case I simply evaluate the panel-panel cubature in  $(\ref{eq:condition})$ , with values of  $\mathcal G$  at each cubature point computed via the methods of LIBSUBSTRATE as described in the previous section (possibly accelerated via interpolation tables). I call this the "spectral inner" method because in this case the q integral in the definition of  $\mathcal G$  is the innermost of 3 integrals. Indeed, inserting equation  $(\ref{eq:condition})$  we have

$$\Delta M_{ab}^{PQ} \equiv \iint \mathbf{b}_a(\mathbf{x}_a) \left\{ \sum \mathfrak{g}^{(m)}(\rho) \mathbf{\Lambda}^{(m)}(\theta_\rho) \right\} \mathbf{b}_b(\mathbf{x}_b) d\mathbf{x}_b d\mathbf{x}_a$$

[where  $\rho = (\mathbf{x}_a - \mathbf{x}_b)_{\parallel} = (\rho \cos \theta_{\rho}, \rho \sin \theta_{\rho})$ ]. Recalling the definition (??), this is a sum of triple integrals:

$$\equiv \iint \mathbf{b}_{a}(\mathbf{x}_{a}) \left\{ \sum \left[ \int_{0}^{\infty} \widetilde{\mathfrak{g}}^{(m)}(q,\rho) dq \right] \mathbf{\Lambda}^{(m)}(\theta_{\rho}) \right\} \cdot \mathbf{b}_{b}(\mathbf{x}_{b}) d\mathbf{x}_{b} d\mathbf{x}_{a}.$$
(27)

2. The spectral outer approach: In this case I rearrange the order of integration in (??) so that the q integral is the outermost integral, with an integrand defined for each q by a panel-panel integral involving the spectral-domain GF:

$$\Delta M_{ab}^{PQ} = \int_0^\infty \left\{ \iint \mathbf{b}_a(\mathbf{x}_a) \left[ \sum \widetilde{\mathfrak{g}}^{(m)}(q,\rho) \mathbf{\Lambda}^{(m)}(\theta_\rho) \right] \mathbf{b}_b(\mathbf{x}_b) \, d\mathbf{x}_b \, d\mathbf{x}_a \right\} dq$$
(28)

<sup>&</sup>lt;sup>7</sup>I refer to 4-dimensional integrals like (??) as "panel-panel integrals" because they are a sum of contributions of integrals over pairs of flat triangular panels.

$$\mathcal{G}_{ij}^{ ext{ iny EE}} = \delta_{ij}$$

### 4 Unit-test framework

The LIBSUBSTRATE standalone library comes with a unit-test suite to test core functionality related to calculation of substrate DGFs. Separately, the unit-test suite for LIBSCUFF includes tests to check the integration of LIBSUBSTRATE into LIBSCUFF.

#### 4.1 LIBSUBSTRATE unit tests

#### 4.1.1 tGTwiddle

The unit-test code tGTwiddle.cc tests that the full Fourier-space DGF  $\widetilde{\Gamma}(\mathbf{q}, z_{\text{D}}, z_{\text{S}})$  satisfies the appropriate boundary conditions at each layer of the layered substrate, namely

$$C^{+}(\mathbf{P}, i, \ell)\widetilde{\Gamma}_{ij}^{\mathrm{PQ}}(\mathbf{q}, z_{\ell} + \eta, z_{\mathrm{S}})C^{-}(\mathbf{P}, i, \ell)\widetilde{\Gamma}_{ij}^{\mathrm{PQ}}(\mathbf{q}, z_{\ell} - \eta, z_{\mathrm{S}})$$
(29)

where

$$C^{\pm}(P, i, \ell) = \begin{cases} 1, & i \in \{x, y\} \\ \epsilon_{\ell}^{\pm}, & i = z, P = E \\ \mu_{\ell}^{\pm}, & i = z, P = H \end{cases}$$

where  $\{\epsilon, \mu\}_{\ell}^{\pm}$  are the material properties for the layer above/below  $z_{\ell}$ , i.e. (Figure  $\ref{eq:condition}$ )

$$\{\epsilon_{\ell}, \mu_{\ell}\}^{+} = \{\epsilon_{\ell}, \mu_{\ell}\}, \qquad \{\epsilon_{\ell}, \mu_{\ell}\}^{-} = \{\epsilon_{\ell+1}, \mu_{\ell+1}\}.$$

If a ground plane is present, we have the additional condition

$$\widetilde{\Gamma}_{ij}^{PQ}(q, z_{GP}, z_{S}) = 0 \quad \text{for} \quad i \in \{x, y\}.$$
(30)

Conditions (??) and (??) must hold independently of the indices  $Q \in \{E, H\}$  and  $j \in \{1, 2, 3\}$  and of the values of  $\mathbf{q}$  and  $z_s$ .

## A Symbols and indices used in this document

### A.1 Symbols

Symbol	Arguments	Description
$\mathcal{F}$	r, geometry	Field six-vector $\mathcal{F} = \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}$
С	r, geometry	Current six-vector $C = {J \choose M}$ or $C = {K \choose N}$
Г	$\rho, z_{\scriptscriptstyle \mathrm{D}}, z_{\scriptscriptstyle \mathrm{S}}, \omega,  \mathrm{geometry}$	Full (bare+scattered) $6 \times 6$ dyadic Green's function, $\mathcal{F} = \Gamma \star \mathcal{C}$
$oldsymbol{\Gamma}^{0r}$	$oldsymbol{ ho}, z_{ exttt{ iny D}}, z_{ exttt{ iny S}}, \omega, \epsilon^r, \mu^r$	Bare (homogeneous) $6 \times 6$ dyadic Green's function in region $r$
$\mathcal{G}$	$\rho, z_{\scriptscriptstyle \mathrm{D}}, z_{\scriptscriptstyle \mathrm{S}}, \omega,  \mathrm{geometry}$	Scattering contribution to $\Gamma$ $(\Gamma = \Gamma^{0r} + \mathcal{G})$
P	r, geometry	$egin{aligned}  ext{Potential eight-vector} \; oldsymbol{\mathcal{P}} = \left(egin{array}{c} \mathbf{A}^{ ext{E}} \ \Phi^{ ext{E}} \ \mathbf{A}^{ ext{M}} \ \Phi^{ ext{M}} \end{array} ight) \end{aligned}$
S	r, geometry	$egin{align*}  ext{Source eight-vector} \; oldsymbol{\mathcal{S}} = \left(egin{array}{c} \mathbf{J} \  ho^{ ext{E}} \ \mathbf{M} \  ho^{ ext{M}} \end{array} ight) \end{aligned}$
Λ	$\rho, z_{\scriptscriptstyle \mathrm{D}}, z_{\scriptscriptstyle \mathrm{S}}, \omega,  \mathrm{geometry}$	Full (bare+scattered) 8 × 8 dyadic Green's function, $\mathcal{P} = \Pi \star \mathcal{S}$
$oldsymbol{\Lambda}^{0r}$	$\rho, z_{\scriptscriptstyle \mathrm{D}}, z_{\scriptscriptstyle \mathrm{S}}, \omega,  \mathrm{geometry}$	Bare (homogeneous) $8 \times 8$ dyadic Green's function for region $r$
L	$\rho, z_{\scriptscriptstyle \mathrm{D}}, z_{\scriptscriptstyle \mathrm{S}}, \omega$ , geometry	Scattering contribution to $\Lambda$ $(\Lambda = \Lambda^{0r} + \mathcal{L})$

## A.2 Indices

Index	Range	Significance
i, j	$\{1, 2, 3\}$	Cartesian directions $x, y, z$
I,J	$\{1, 2, 3, 4, 5, 6\}$	Electric/magnetic field/current components
$\mu,  u$	$\{1, 2, 3, 4, 5, 6, 7, 8\}$	

### B $8 \times 8$ Dyadic Green's Functions

The usual  $6 \times 6$  dyadic Green's function  $\Gamma$  operates on a six-vector of currents to yield a six-vector of fields. It is convenient to consider a slightly different object that operates on an *eight*-vector of sources to yield an *eight*-vector of potentials.

In the presence of magnetic currents, the usual (electric-current-sourced) vector and scalar potentials  $\mathbf{A}^{\text{E}}, \Phi^{\text{E}}$ , are joined by their magnetic-current-sourced counterparts  $\mathbf{A}^{\text{M}}, \Phi^{\text{M}}$ , which are related to the fields according to

$$\begin{split} \mathbf{E} &= i\omega\mu\mathbf{A}^{\mathrm{E}} - \frac{1}{i\omega\epsilon}\nabla\Phi^{\mathrm{E}} - \nabla\times\mathbf{A}^{\mathrm{M}} \\ \mathbf{M} &= \nabla\times\mathbf{A}^{\mathrm{E}} + i\omega\epsilon\mathbf{A}^{\mathrm{M}} - \frac{1}{i\omega\mu}\nabla\Phi^{\mathrm{M}}. \end{split}$$

In a homogeneous region, the potentials  $^8$  produced by given source distributions  $\{{\bf J},{\bf M}\}$  are

$$\begin{split} \mathbf{A}^{\scriptscriptstyle{\mathrm{E}}}(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}}) &= \int G_0(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}} - \mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \mathbf{J}(\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \, d\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}, \qquad \Phi^{\scriptscriptstyle{\mathrm{E}}}(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}}) = \int G_0(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}} - \mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \big[ \nabla \cdot \mathbf{J} \big] \, d\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}} \\ \mathbf{A}^{\scriptscriptstyle{\mathrm{M}}}(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}}) &= \int G_0(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}} - \mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \mathbf{M}(\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \, d\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}, \qquad \Phi^{\scriptscriptstyle{\mathrm{M}}}(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}}) = \int G_0(\mathbf{x}_{\scriptscriptstyle{\mathrm{D}}} - \mathbf{x}_{\scriptscriptstyle{\mathrm{S}}}) \big[ \nabla \cdot \mathbf{M} \big] \, d\mathbf{x}_{\scriptscriptstyle{\mathrm{S}}} \end{split}$$

where

$$G_0(\mathbf{r}) = \frac{e^{ik|\mathbf{r}|}}{4\pi|\mathbf{r}|}.$$

$$\begin{pmatrix} E_x \\ E_y \\ E_z \\ H_x \\ H_y \\ H_z \end{pmatrix} = \begin{pmatrix} i\omega\mu G_0 & 0 & 0 & -\frac{1}{i\omega\epsilon}\partial_x G_0 & 0 & \partial_z G_0 & -\partial_y G_0 & 0 \\ 0 & i\omega\mu G_0 & 0 & -\frac{1}{i\omega\epsilon}\partial_y G_0 & -\partial_z G_0 & 0 & \partial_x G_0 & 0 \\ 0 & 0 & i\omega\mu G_0 & -\frac{1}{i\omega\epsilon}\partial_z G_0 & \partial_y G_0 & -\partial_x G_0 & 0 & 0 \\ 0 & -\partial_z G_0 & \partial_y G_0 & 0 & i\omega\epsilon G_0 & 0 & 0 & -\frac{1}{i\omega\mu}\partial_x G_0 \\ \partial_z G_0 & 0 & \partial_x G_0 & 0 & 0 & i\omega\epsilon G_0 & 0 & -\frac{1}{i\omega\mu}\partial_y G_0 \\ -\partial_y G_0 & \partial_x G_0 & 0 & 0 & 0 & i\omega\epsilon G_0 & -\frac{1}{i\omega\mu}\partial_z G_0 \end{pmatrix} \star \begin{pmatrix} J_x \\ J_y \\ J_z \\ \nabla \cdot \mathbf{J} \\ M_x \\ M_y \\ M_z \\ \nabla \cdot \mathbf{M} \end{pmatrix}$$

<sup>&</sup>lt;sup>8</sup>Note that my  $\Phi^{E,M}$  are  $i\omega$  times the actual scalar potentials due to the charge distributions associated with currents J, M.