

CURRENT ON A PLANAR DIELECTRIC PLATE

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A TE_z plane wave is incident on an infinitesimally thin planar dielectric sheet of length L at an angle ϕ_i as shown in Fig. 1. The scattering off the sheet is obtained by applying the *surface equiavalence* theorem where the dielectric sheet is replaced by equivalent surface electric and magnetic currents generating the same fields outside the sheet as the original problem and satisfying boundary conditions. The currents can be expressed in terms of the fields as:

$$\mathbf{J}_s = \hat{\mathbf{n}} \times \mathbf{H} = \hat{\mathbf{z}}J(\rho'), \quad (1a)$$

$$\mathbf{M}_s = -\hat{\mathbf{n}} \times \mathbf{E} = \hat{\mathbf{x}}M(\rho') \quad (1b)$$

where the normal unit vector $\hat{\mathbf{n}}$ is along the positive y direction and ρ' depends x and y . To determine the surface currents, we set up two homogeneous equivalent problems; one external to the dielectric sheet and the other inside the sheet. For the external equivalent, the total electric field \mathbf{E}_1 consists of the plane wave incident field \mathbf{E}_i and scattered field \mathbf{E}_1^{scat} due to the equivalent currents:

$$\mathbf{E}_1 = \mathbf{E}_i + \mathbf{E}_1^{scat} \quad (2)$$

where

$$\mathbf{E}_i = E^0 (\hat{\mathbf{x}} \sin \phi_i - \hat{\mathbf{y}} \cos \phi_i) e^{jk_1(x \cos \phi_i + y \sin \phi_i)} \quad (3)$$

with k_1 being the propagation constant of air and E^0 the amplitude of the incoming plane wave. The scattered electric field due to the equivalent currents can be expressed as:

$$\mathbf{E}_1^{scat} = \left(k_0^2 + \nabla \nabla \cdot \right) \mathbf{A} - \frac{1}{\varepsilon_1} \nabla \times \mathbf{F} \quad (4)$$

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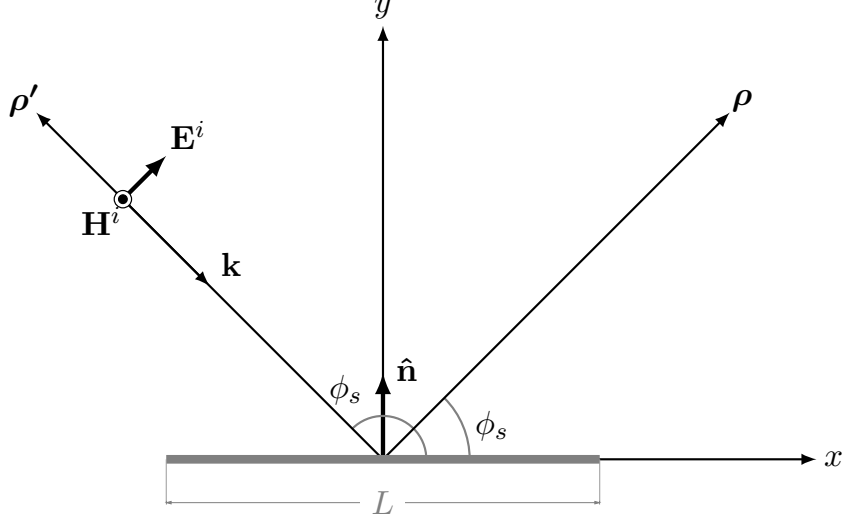


Figure 1: Thin Dielectric sheet with TE_z polarization

where \mathbf{A} and \mathbf{F} are the magnetic and electric vector potentials respectively, given by:

$$\mathbf{A} = \frac{\mu}{4\pi} \iint_S \mathbf{J}_s(\mathbf{r}') \frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} dS', \quad (5a)$$

$$\mathbf{F} = \frac{\varepsilon}{4\pi} \iint_S \mathbf{M}_s(\mathbf{r}') \frac{e^{-jk_0|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} dS'. \quad (5b)$$

with \mathbf{r} and \mathbf{r}' the position vectors for the observation and source point respectively. For a structure extending to infinity in the z direction, (5) can be re-written in its two-dimensional form:

$$\mathbf{A} = \frac{\mu}{4j} \int_l \mathbf{J}_s(\rho') H_0^{(2)}(k_0|\rho - \rho'|) dl', \quad (6a)$$

$$\mathbf{F} = \frac{\varepsilon}{4j} \int_l \mathbf{M}_s(\rho') H_0^{(2)}(k_0|\rho - \rho'|) dl', \quad (6b)$$

where $H_0^{(2)}(k_0|\rho - \rho'|)$ is the zeroth-order Hankel function of the second kind. For a horizontally oriented infinitesimally thin planar sheet, the operator inside the parentheses in (4) becomes:

$$\left(k_0^2 + \nabla \nabla \cdot\right) \longrightarrow \left(k_0^2 + \frac{\partial^2}{\partial x^2}\right) \quad (7)$$

and the argument of the Hankel function reduces to $k_0|x - x'|$. The component of the

scattered electric field tangential to sheet becomes:

$$\begin{aligned} E_{1,x}^{scat} &= -j\omega \left(k_0^2 + \frac{\partial^2}{\partial x^2} \right) A_x \\ &= -\frac{\omega\mu}{4} \left(k_0^2 + \frac{\partial^2}{\partial x^2} \right) \int_l J_x(x') H_0^{(2)}(k_0|x-x'|) dl' \end{aligned} \quad (8)$$

where the partial derivative along the y direction is ignored bearing in mind the thickness of the sheet. In a similar way, the tangential component of the scattered magnetic field can be expressed as:

$$\begin{aligned} \mathbf{H}_{1,z}^{scat} &= -\frac{j\omega}{F} z \\ &= -\frac{\omega\varepsilon_1}{4} \int_l M_z(x') H_0^{(2)}(k_0|x-x'|) dl' \end{aligned} \quad (9)$$

For interior equivalent configuration of the original problem, the same surface currents are used with their signs reversed. With the absence of an incident wave, the tangential components of the electric and magnetic fields valid for the interior region are:

$$E_{2,x}^{scat} = \frac{\omega\mu}{4} \left(k_1^2 + \frac{\partial^2}{\partial x^2} \right) \int_l J_x(x') H_0^{(2)}(k_1|x-x'|) dl' \quad (10a)$$

$$H_{2,z}^{scat} = \frac{\omega\varepsilon_2}{4} \int_l M_z(x') H_0^{(2)}(k_2|x-x'|) dl' \quad (10b)$$

Once the fields in the two regions are expressed in terms of equivalent currents, we apply the boundary conditions ensuring continuity of the tangential fields at the interface thereby obtaining expressions through which the surface currents can be computed. At the interface:

$$\hat{\mathbf{n}} \times (\mathbf{E}_1 - \mathbf{E}_2) = \mathbf{0} \quad (11a)$$

$$\hat{\mathbf{n}} \times (\mathbf{H}_1 - \mathbf{H}_2) = \mathbf{0} \quad (11b)$$

The component of the electric field tangential to the sheet surface is x directed. We therefore, obtain a scalar equation from (3) and (11a):

$$\begin{aligned} E^0 \sin \phi_i e^{jk_1 x \cos \phi_i} &= \frac{\omega\mu}{4k_1^2} \left(k_1^2 + \frac{\partial^2}{\partial x^2} \right) \int_l J_x(x') H_0^{(2)}(k_1|x-x'|) dl' \\ &\quad + \frac{\omega\mu}{4k_2^2} \left(k_2^2 + \frac{\partial^2}{\partial x^2} \right) \int_l J_x(x') H_0^{(2)}(k_2|x-x'|) dl' \end{aligned} \quad (12)$$

For a TE_z polarized incident wave, the magnetic current obtained is:

$$\frac{E^0}{\eta_1} e^{jk_1 x \cos \phi_i} = \frac{\omega}{4} \int_l \varepsilon_1 M_z(x') H_0^{(2)}(k_1 |x - x'|) + \varepsilon_2 M_z(x') H_0^{(2)}(k_2 |x - x'|) dl' \quad (13)$$

where η_1 is the characteristic impedance of external region. Equation (12) is commonly known as *Pocklington Integral equation* where the differential operator written in brackets may be moved inside the integral:

$$\begin{aligned} E^0 \sin \phi_i e^{jk_1 x \cos \phi_i} &= \frac{\omega \mu}{4k_1^2} \int_l J_x(x') \left(k_0^2 + \frac{\partial^2}{\partial x^2} \right) H_0^{(2)}(k_1 |x - x'|) dl' \\ &\quad + \frac{j\omega}{k_2^2} \int_l J_x(x') \left(k_2^2 + \frac{\partial^2}{\partial x^2} \right) H_0^{(2)}(k_2 |x - x'|) dl' \end{aligned} \quad (14)$$

The second order derivative on the Hankel functions can be removed by using the recurrence relations [, p. 361].

$$\frac{dH_0^{(2)}(x)}{dx} = -H_1^{(2)}(x) + \frac{1}{x} H_0^{(2)}(x) \quad (15a)$$

$$H_1^{(2)}(x) = \frac{x}{2} [H_0^{(2)}(x) + H_2^{(2)}(x)] \quad (15b)$$

Moreover, a Hankel function with an argument $k\zeta = k|x - x'|$ may be differentiated by the chain-rule:

$$\begin{aligned} \frac{\partial H_0^{(2)}(k\zeta)}{\partial x} &= \frac{dH_0^{(2)}(k\zeta)}{dk\zeta} \frac{\partial k\zeta}{\partial x} \\ &= \frac{dH_0^{(2)}(k\zeta)}{dk\zeta} \times \frac{k(x - x')}{\zeta} \end{aligned} \quad (16)$$

By differentiating (16) one more time, we obtain:

$$\frac{\partial^2 H_0^{(2)}(k\zeta)}{\partial x^2} = \frac{k}{\zeta} \left[H_2^{(2)}(k\zeta) \frac{k(x - x')^2}{\zeta} - H_1^{(2)}(k\zeta) \right] \quad (17)$$

The differential operator in (14) can now be rewritten as:

$$\begin{aligned} \left(k_i^2 + \frac{\partial^2}{\partial x^2} \right) H_0^{(2)}(k_i \zeta) &= \frac{k_i^2}{2} H_0^{(2)}(k_i \zeta) + k_i^2 \left[\frac{(x - x')^2}{\zeta^2} - \frac{1}{2} \right] H_2^{(2)}(k_i \zeta) \\ &= \frac{k_i^2}{2} H_0^{(2)}(k_i \zeta) + k_i^2 \left(\cos^2 \psi - \frac{1}{2} \right) H_2^{(2)}(k_i \zeta) \\ &= \frac{k_i^2}{2} H_0^{(2)}(k_i \zeta) + k_i^2 \cos(2\psi) H_2^{(2)}(k_i \zeta) \end{aligned} \quad (18)$$

where $i = 1, 2$ and $\cos \psi = (x - x')/\zeta$. The electric current (14) can therefore be expressed

as:

$$E^0 \sin \phi_i e^{jk_1 x \cos \phi_i} = \frac{-j\omega}{2} \int_l J_x(x') \left[H_0^{(2)}(k_1 \zeta) + \cos(2\psi) H_2^{(2)}(k_1 \zeta) \right. \\ \left. + H_0^{(2)}(k_2 \zeta) + \cos(2\psi) H_2^{(2)}(k_2 \zeta) \right] dl' \quad (19)$$

For a flat sheet lying along the x axis, the factor $\cos \psi$ equals 1.

Solution with Method of Moments

The Method of Moments (MoM) is a procedure to reduce the integral equations that may not have an exact solution, like (??) and (13) of the form:

$$L(f) = g \quad (20)$$

where L is the integral operator $\int G(x, x') dx'$, f is the unknown function and g is an excitation source, into a system of linear equations in terms of the unknown function which can be approximated by a finite series of weighted subdomain expansion functions:

$$f(x') \approx \sum_{n=1}^N \alpha_n f_n(x'), \quad (21)$$

where α_n 's are the unknown weighting coefficients. A common choice of the expansion functions $f_n(x')$ is a set of orthogonal pulse functions which results in a staircase approximation of the original function:

$$f_n(x') = \begin{cases} 1, & \text{for } x' \text{ in } \Delta x'_n \\ 0, & \text{otherwise} \end{cases} \quad (22)$$

Introducing a series approximation of the unknown results in a residual:

$$R_N = \sum_{n=1}^N \alpha_n L[f_n(x')] - g \quad (23)$$

In order to minimize the approximation error, a *moment* or an inner product is applied on a suitable choice of testing functions w_m introduced:

$$\sum_{n=1}^N \alpha_n \langle w_m, L[f_n(x')] \rangle - \langle w_m, g \rangle = 0, \text{ for } m = 1, 2, \dots, N. \quad (24)$$

where $\langle \cdot, \cdot \rangle$ represents the inner product operation which is difficult to compute. To circumvent this, delta functions are used as the testing functions and this process is called *Point*

Matching method. With:

$$w_m = \delta(x' - x_m) \quad (25)$$

equation (26) becomes:

$$\sum_{n=1}^N \alpha_n L[f_n(x_m)] = g(x_m), \text{ for } m = 1, 2, \dots, N. \quad (26)$$

The equation set in matrix form can be written as:

$$Z[\alpha_n = g_m] \quad (27)$$

where,

$$Z = \begin{bmatrix} L[f_1(x_1)] & L[f_2(x_1)] & \cdots & L[f_N(x_1)] \\ L[f_1(x_2)] & L[f_2(x_2)] & \cdots & L[f_N(x_2)] \\ \vdots & \vdots & \ddots & \vdots \\ L[f_1(x_N)] & L[f_2(x_N)] & \cdots & L[f_N(x_N)] \end{bmatrix} \quad (28)$$

and the vectors α_n and g_m contain the unknown coefficients and the source respectively. Once α_n is found through matrix inversion in (27), the unknown function f is computed through (21).

The matrix terms for electric and magnetic currents for a dielectric sheet follow from (19) and (13) respectively:

$$Z_{mn}^J = \frac{\omega\mu}{4} \int_{x_n}^{x_{n+1}} \left[H_0^{(2)}(k_1|x_m - x_n|) + H_0^{(2)}(k_2|x_m - x_n|) \right] dx' \quad (29a)$$

$$Z_{mn}^M = \frac{\omega}{8} \int_{x_n}^{x_{n+1}} \left[\varepsilon_1 H_0^{(2)}(k_1|x_m - x_n|) + \varepsilon_2 H_0^{(2)}(k_2|x_m - x_n|) + \varepsilon_1 H_2^{(2)}(k_2|x_m - x_n|) + \varepsilon_2 H_2^{(2)}(k_2|x_m - x_n|) \right] dx' \quad (29b)$$

The the integrals in the Z_{mn} terms can only be evaluated with any quadrature routine except for the self terms ($m = n$) for which small argument approximations of the Hankel

function are used to estimate the integral. For the self terms:

$$Z_{nn}^J = -\frac{\omega\mu\Delta}{8} \left\{ 2 - \frac{j}{\pi} \left[6 + 2 \ln \left(\frac{e^\gamma k_1 \Delta}{4e} \right) + \frac{16}{(k_1 \Delta)^2} + 2 \ln \left(\frac{e^\gamma k_2 \Delta}{4e} \right) + \frac{16}{(k_1 \Delta)^2} \right] \right\} \quad (30a)$$

$$Z_{nn}^M = -\frac{\omega\mu\Delta}{4} \left\{ 2 - \frac{2j}{\pi} \ln \left(\frac{e^\gamma k_1 \Delta}{4e} \right) - \frac{2j}{\pi} \ln \left(\frac{e^\gamma k_2 \Delta}{4e} \right) \right\} \quad (30b)$$