# Near-field profile in the Kretschmann configuration with gaussian-beam illumination

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We consider a planar interface, possibly with multiple layers, illuminated under total internal reflection by a gaussian beam from an incident medium (i). We seek to calculate the near-field profile in the outer medium (o).

# 1 Gaussian beam illumination

Following Novotny, we start with the angular spectrum representation of the incident beam with wavevector  $\mathbf{k}_i$ . In a frame  $F_1$  attached to the central ray as depicted in Fig. 1, the electric field at a point  $\mathbf{r}_1$ , is written as a collection of plane waves (Novotny Eq. 3.9 p. 47, Eq. 3.27, p.54),

$$\mathbf{E}_1(\mathbf{r}_1) = \iint a(k_{i1x}, k_{i1y}) \exp\left(i\mathbf{k}_{i1} \cdot \mathbf{r}_1\right) \hat{\mathbf{e}}_1(\mathbf{r}_1, \mathbf{k}_{i1}) \mathrm{d}k_{i1x} \mathrm{d}k_{i1y},$$

where

$$a(\mathbf{k}_1) = \frac{w_0^2}{4\pi} e^{-\frac{w_0^2}{4}(k_{1x}^2 + k_{1y}^2)}$$

describes the gaussian field profile with waist  $w_0$ , and  $\hat{\mathbf{e}}_1 = (\cos \psi; \sin \psi; 0)^t$  keeps track of the electric field direction (for a focused beam, see Eq. 3 of Burghardt et al.).

### 2 Reference frame

The results should be expressed in a reference frame attached to the planar interface, we thus define a ro-

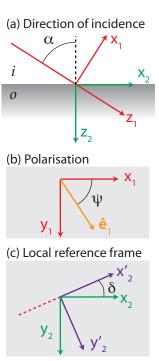


Figure 1: Illustration of the different reference frames used in the derivation. (a) The central ray of the gaussian beam makes an angle  $\alpha$  with the normal to the interface. (b) The polarisation is described by the angle  $\Psi$  between the electric field and the  $x_1$  axis; values of  $\Psi=0,90$  correspond to p- and s- polarisations, respectively. (c) A rotation of angle  $\delta$  brings the frame of reference  $F_2'$  to coincide with the plane of incidence of a given plane wave.

tation matrix around the axis  $y_1$ .

$$R_y(\alpha) = \begin{bmatrix} \cos(\alpha) & 0 & \sin(\alpha) \\ 0 & 1 & 0 \\ -\sin(\alpha) & 0 & \cos(\alpha) \end{bmatrix}. \tag{1}$$

For each individual plane wave in the kernel, a second rotation is performed around the  $z_2$  axis, that brings the new reference frame  $(x'_2, y'_2, z'_2)$  to coincide with the plane of incidence of that particular plane wave,

$$R_z(\delta) = \begin{bmatrix} \cos(\delta) & \sin(\delta) & 0 \\ -\sin(\delta) & \cos(\delta) & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

The angle of rotation  $\delta$  is given by

$$\delta = \sin^{-1} \frac{s_{2y}}{\sqrt{s_{2x}^2 + s_{2y}^2}}$$

where  $\hat{\mathbf{s}}_2 = R_y(\alpha)\hat{\mathbf{s}}_1$  is obtained by rotation of the normalised incident wavevector  $\hat{\mathbf{s}}_1 = \mathbf{k}_{i1}/|\mathbf{k}_{i1}|$ . Each plane wave, expressed in this dedicated frame of reference, is now written

$$\mathbf{E}_{i2'}(\mathbf{r}_{2'}) = \hat{\mathbf{e}}_{i2'} \exp\left(i\mathbf{k}_{i2'} \cdot \mathbf{r}_{2'}\right).$$

# 3 Transmission at the interface

We consider an individual plane wave incident on the interface, and express the amplitude in the frame  $F'_2$  of the electric field  $\mathbf{E}_{o2'}$  on the outer side using the Fresnel coefficients  $t^p$  and  $t^s$  (Etchegoin, Le Ru, App. F.3),

$$\mathbf{E}_{o2'}(\mathbf{r}_{2'}) = \begin{bmatrix} \left(\frac{n_i}{n_o}\right)^2 \frac{k_{o2z}}{k_{i2'z}} t^p E_{i2'x} \\ t^s E_{2'y} \\ \left(\frac{n_i}{n_o}\right)^2 t^p E_{i2'z} \end{bmatrix} \exp\left(i\mathbf{k}_{o2'} \cdot \mathbf{r}_{2'}\right).$$

The wave vector of this inhomogeneous plane wave is given by  $\mathbf{k}_{o2'} = \left(k_{i2'x}, k_{i2'y}, \sqrt{k_o^2 - (k_{i2'x}^2 + k_{i2'x}^2)}\right)$ .

The electric field is finally transformed back into the reference frame  $F_2$  by a rotation of  $R_z(-\delta)$ , before the integration is performed, in polar coordinates,

$$\mathbf{E}_{o2}(\mathbf{r}_2) = \iint a(\rho, \theta) \mathbf{E}_{o2}(\mathbf{r}_2) \rho d\rho d\theta,$$

with

$$\begin{cases} \rho = \sqrt{k_{ix1}^2 + k_{iy1}^2} \\ \theta = \tan^{-1} \frac{k_{iy1}}{k_{ix1}} \end{cases}$$
 (2)