

4.

Using voltage division,  $\frac{V_c(s)}{V_i(s)} = \frac{\frac{1}{RC}}{s + \frac{1}{RC}} = \frac{1}{s+1}$ . Since  $V_i(s) = \frac{5}{s}$

$$V_c(s) = \frac{5}{s} \left( \frac{1}{s+1} \right) = \frac{5}{s} - \frac{5}{s+1}.$$

Therefore:  $v_c(t) = 5 - 5e^{-t}$ .

Also,  $T = \frac{1}{1} = 1 \text{ sec}$ ;  $T_r = \frac{2.2}{1} = 2.2 \text{ sec}$ ;  $T_s = \frac{4}{1} = 4 \text{ sec}$ .

25.

a. Adding impedances  $(5s^2 + 2s + 20)X(s) = F(s)$ . So the transfer function is

$$\frac{X(s)}{F(s)} = \frac{1}{5s^2 + 2s + 20} = \frac{0.2}{s^2 + 0.4s + 4}.$$

b. Follows that  $\omega_n^2 = 4$ , or  $\omega_n = 2$ .  $2\zeta\omega_n = 0.4$ , so  $\zeta = 0.1$ .  $\%OS = 100e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}} = 72.93\%$ .  $T_s = \frac{4}{\zeta\omega_n} = 20$

sec.  $T_p = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}} = 1.58 \text{ sec}$ . To obtain the rise time Figure 4.16 is used  $\omega_n T_r = 1.104$ , or

$T_r = 0.552 \text{ sec}$ . The dc gain of the system is  $c_{max} = \frac{0.2}{4} = 0.05$ .

35. (a) Does not meet the x5 rule (page 184):  $4 < 5*(3)$

Residue is not negligible (section 4.8):

$$0.1 * \sqrt{0.001976^2 + 0.0005427^2} = 0.0002 \text{ (using 10% as cutoff)}$$

$$0.001524 > 0.0002$$

2<sup>nd</sup> order approximation is not valid

(b) Does not meet the x5 rule:  $8 < 5*(6)$

Residue is not negligible (section 4.8):

$$0.1 * \sqrt{0.007647^2 + 0.01309^2} = 0.0015 \text{ (using 10% as cutoff)}$$

$$0.007 > 0.0015$$

## 2<sup>nd</sup> order approximation is not valid

(c) Does not meet the x5 rule ( $5.1 < 5 \cdot 2$ )

Residue is negligible

$$0.1 * \sqrt{0.009990^2 + 0.001942^2} = 0.0022 \text{ (using 10% as cutoff)}$$

$$0.00018 < 0.0022 \text{ (actually is less than 1\%)}$$

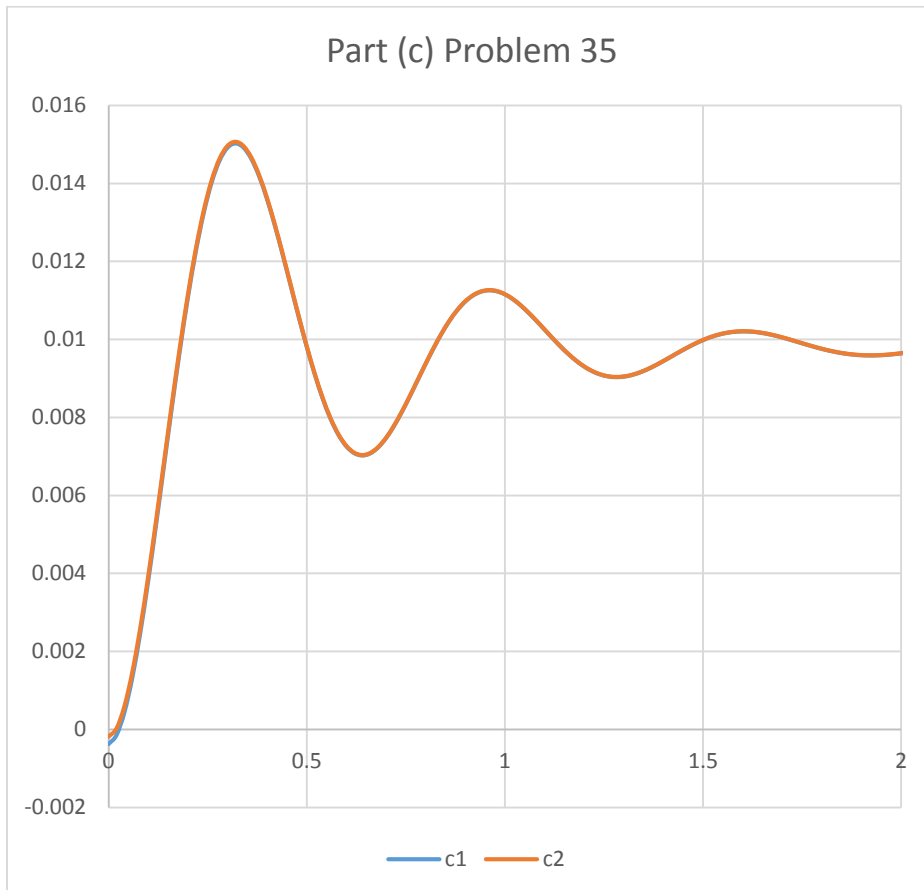
From the oscillatory part of  $c(t)$ , the dominant poles are  $s = -2 \pm j9.796$

The time constant is the reciprocal of the magnitude of the real part,  $\frac{1}{2}$  second. The settling time is four time constants:  $4 \cdot (1/2) = \mathbf{2 \text{ seconds} = T_s}$ . The damped frequency is 9.796 rad/s. The peak time is one half of the period:  $T_p = \pi/\omega_d = \mathbf{0.3207 \text{ seconds} = T_p}$ .

To find damping constant, use  $\zeta\omega_n = 2$  and  $\omega_n\sqrt{1-\zeta^2} = 9.796$ . Rearranging yields

$$\zeta = \sqrt{2^2 / (2^2 + 9.796^2)} = 0.200$$

$$\text{Then \%OS} = e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}} \times 100 = 52.7\%$$



Approximate curve in matlab is:

```
c2 = 0.009804-0.009990*exp(-2*t).*cos(9.796*t)
      -0.001942 *exp(-2*t).*sin(9.796*t);
```

(d) Exactly meets the x5 rule:  $10 = 5 \times 2$

That term also has a smaller residue, but only about five times smaller, so it does not meet the 10% cutoff.

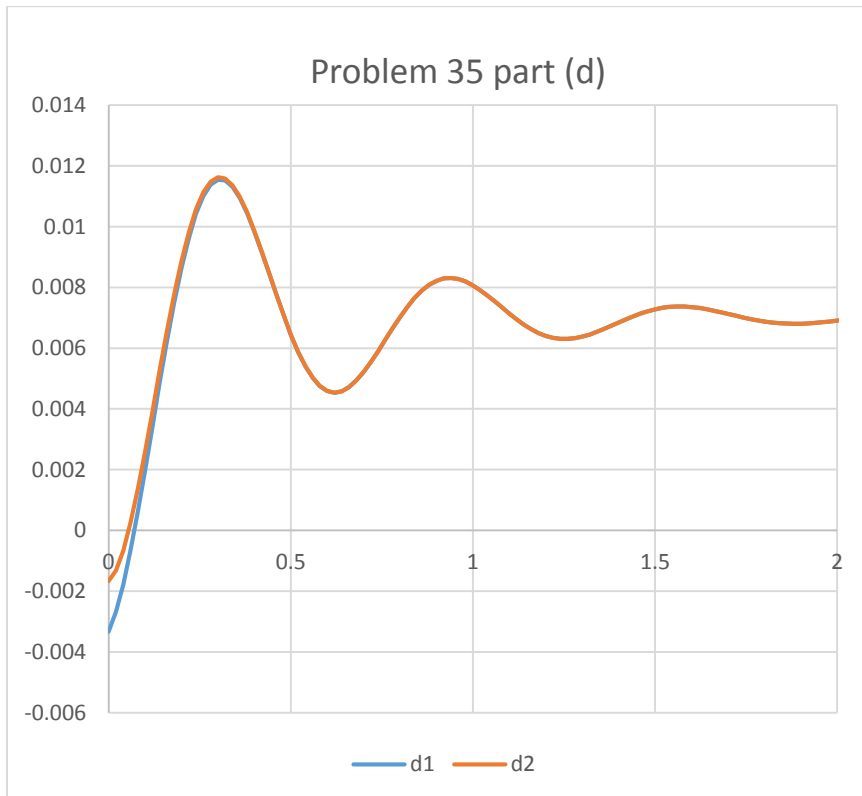
From the oscillatory part of  $c(t)$ , the dominant poles are  $s = -2 \pm j9.951$

The time constant is the reciprocal of the magnitude of the real part,  $\frac{1}{2}$  second. The settling time is four time constants:  $4 \times (1/2) = \mathbf{2 \text{ seconds}} = T_s$ . The damped frequency is 9.951 rad/s. The peak time is one half of the period:  $T_p = \pi/\omega_d = \mathbf{0.3157 \text{ seconds}} = T_p$ .

To find damping constant, use  $\zeta\omega_n = 2$  and  $\omega_n\sqrt{1-\zeta^2} = 9.951$ . Rearranging yields

$$\zeta = \sqrt{2^2 / (2^2 + 9.951^2)} = 0.197$$

$$\text{Then \%OS} = e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}} \times 100 = 53.1\%$$



As in part (c), dropping the term with a small residue and rapid decay rate.

42.

$$\begin{aligned} X(s) &= (sI - A)^{-1}(x(0) + Bu(t)) = \begin{bmatrix} s+3 & 0 \\ 1 & s+1 \end{bmatrix}^{-1} \left[ \begin{bmatrix} 2 \\ 0 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} \frac{1}{s} \right] \\ &= \begin{bmatrix} \frac{1}{s+3} & 0 \\ -\frac{1}{(s+1)(s+3)} & \frac{1}{s+1} \end{bmatrix} \begin{bmatrix} \frac{2s+2}{s} \\ \frac{1}{s} \end{bmatrix} = \begin{bmatrix} \frac{2(s+1)}{s(s+3)} \\ -\frac{s-1}{s(s+1)(s+3)} \end{bmatrix} \end{aligned}$$

$$Y(s) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \frac{2(s+1)}{s(s+3)} \\ -\frac{s-1}{s(s+1)(s+3)} \end{bmatrix} = \frac{2(s+1)}{s(s+3)} = \frac{2}{3} \frac{1}{s} + \frac{5}{3} \frac{1}{s+3}$$

Obtaining the inverse Laplace transform

$$y(t) = \frac{2}{3} + \frac{5}{3} e^{-3t}$$

Let the rotation of the shaft with gear  $N_2$  be  $\theta_L(s)$ . Assuming that all rotating load has been reflected to the  $N_2$  shaft,  $(J_{eqL}s^2 + D_{eqL}s + K)\theta_L(s) + F(s)r = T_{eq}(s)$ , where  $F(s)$  is the force from the translational system,  $r = 2$  is the radius of the rotational member,  $J_{eqL}$  is the equivalent inertia at the  $N_2$  shaft, and  $D_{eqL}$  is the equivalent damping at the  $N_2$  shaft. Since  $J_{eqL} = 1(2)^2 + 1 = 5$  and  $D_{eqL} = 1(2)^2 = 4$ , the equation of motion becomes,  $(5s^2 + 4s + K)\theta_L(s) + 2F(s) = T_{eq}(s)$ . For the translational system

$(Ms^2 + s)X(s) = F(s)$ . Substituting  $F(s)$  into the rotational equation of motion,

$(5s^2 + 4s + K)\theta_L(s) + (Ms^2 + s)2X(s) = T_{eq}(s)$ . But,

$\theta_L(s) = \frac{X(s)}{r} = \frac{X(s)}{2}$  and  $T_{eq}(s) = 2T(s)$ . Substituting these quantities in the equation

above yields  $((5 + 4M)s^2 + 8s + K)\frac{X(s)}{4} = T(s)$ .

Thus, the transfer function is  $\frac{X(s)}{T(s)} = \frac{4/(5 + 4M)}{s^2 + \frac{8}{(5 + 4M)}s + \frac{K}{(5 + 4M)}}$ .

Now,  $T_s = 20 = \frac{4}{R_e} = \frac{4}{\frac{8}{2(5 + 4M)}} = (5 + 4M)$ . Hence,  $M = 15/4$ .

For 16% overshoot,  $\zeta = 0.504$  from Eq. (4.39).

Therefore,  $2\zeta\omega_n = \frac{8}{(5 + 4M)} = 0.4$ . Solving for  $\omega_n$  yields  $\omega_n = 0.3968$ .

But,  $\omega_n = \sqrt{\frac{K}{(5 + 4M)}} = \sqrt{\frac{K}{20}} = 0.3968$ . Thus,  $K = 3.15$ .

85. a.

Substituting  $\Delta F(s) = \frac{2650}{s}$  into the transfer function and solving for  $\Delta V(s)$  gives:

$$\Delta V(s) = \frac{\Delta F(s)}{1908 \cdot s} = \frac{2650}{s(1908 \cdot s + 10)} = \frac{A}{s} + \frac{B}{(1908 \cdot s + 10)}$$

$$\text{Here: } A = \left. \frac{2650}{(1908 \cdot s + 10)} \right|_{s=0} = 265 \text{ and } B = \left. \frac{2650}{s} \right|_{s=-1/190.8} = -505,620$$

Substituting we have:

$$\Delta V(s) = \frac{265}{s} - \frac{505620}{(1908 \cdot s + 10)} = 265 \left( \frac{1}{s} - \frac{1}{(s + 5.24 \times 10^{-3})} \right)$$

Taking the inverse Laplace transform, we have:

$$\Delta v(t) = 265(1 - e^{-5.24 \times 10^{-3} t}) \cdot u(t), \text{ in m/s}$$

b.

```
>> s=tf('s');
>> G=1/(1908*s+10);
>> t=0:0.1:1000;
>> y1=2650*step(G,t);
>> y2=265*(1-exp(-5.24e-3.*t));
>> plot(t,y1,t,y2)
>> xlabel('sec')
>> ylabel('m/s')
```

