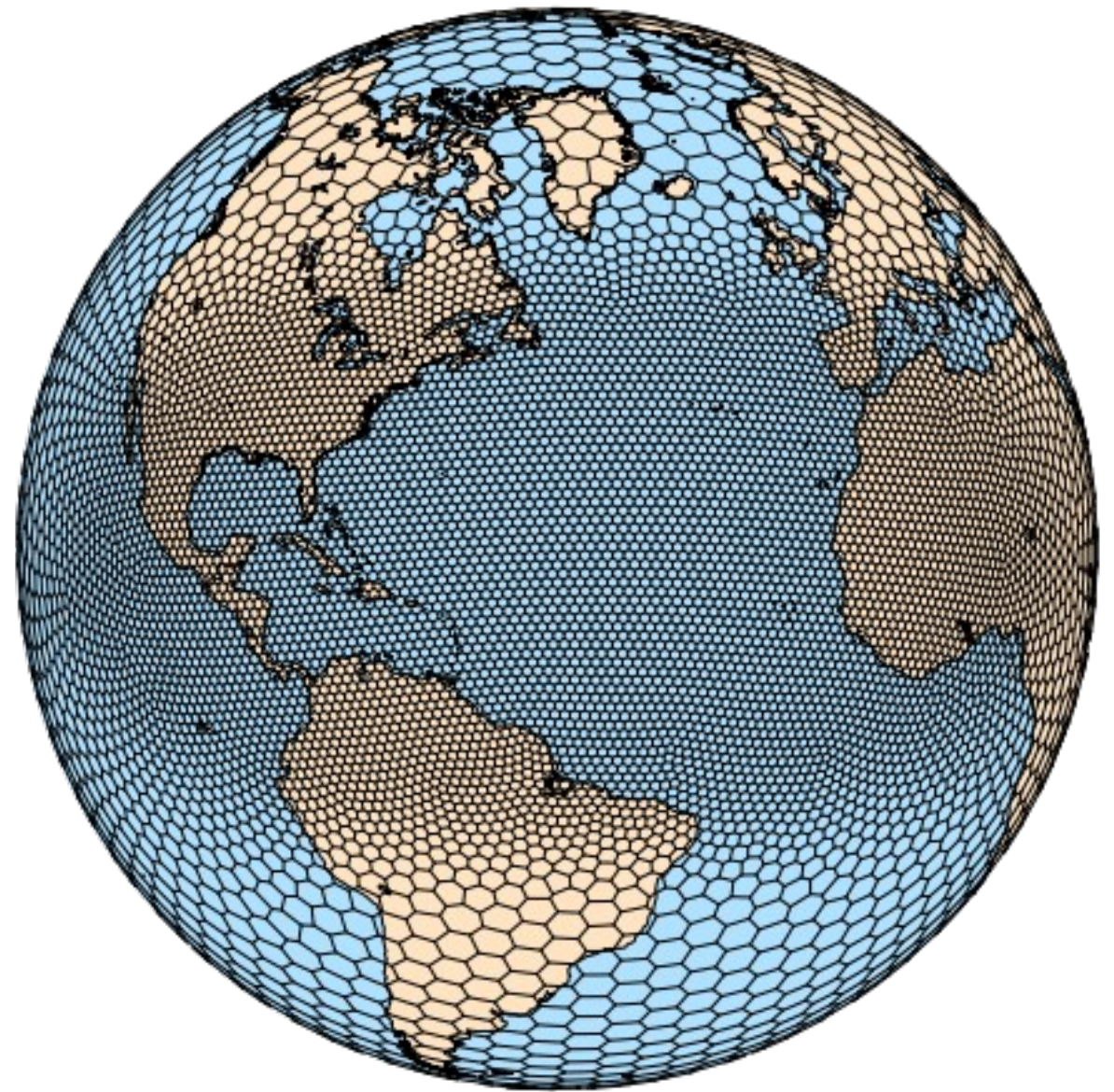


## *Dynamical Core*

- *Spatial discretization*
  - *Transport*
  - *Filters*
  - *Namelist parameters*
  - *References*

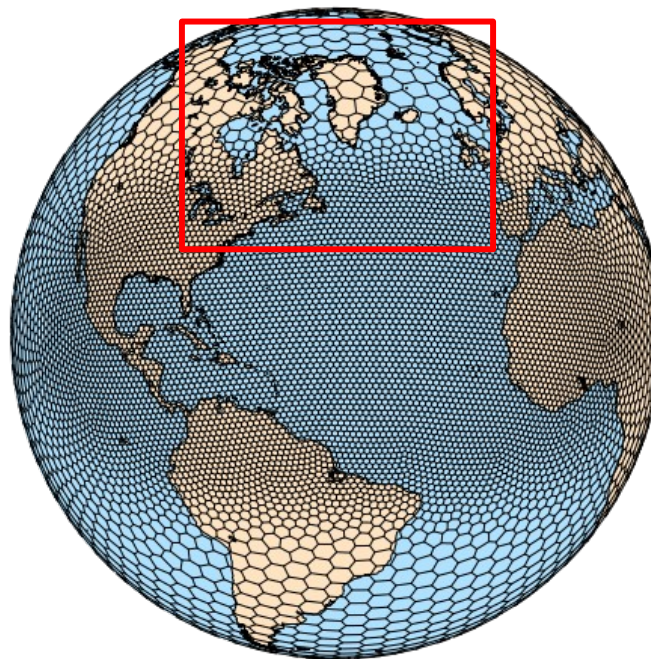
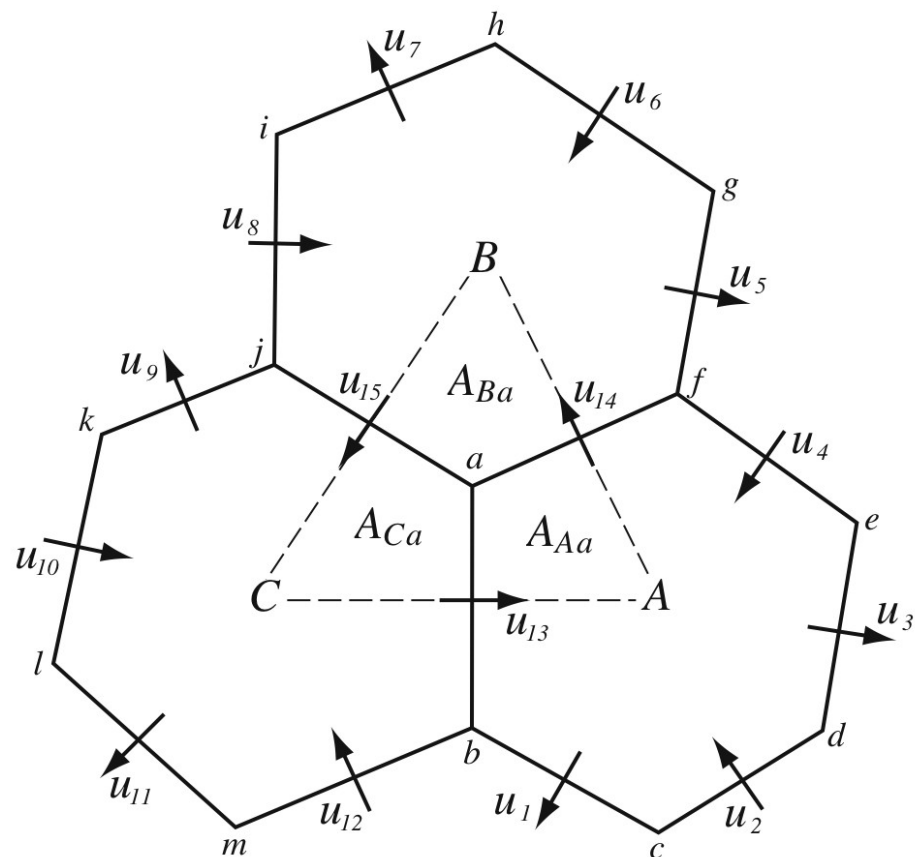




## MPAS Horizontal Mesh

### Unstructured spherical centroidal Voronoi meshes

- Mostly *hexagons*, some pentagons (5-sided cells) and heptagons (7-sided cells).
- Cell centers are at cell center-of-mass (centroidal).
- Cell edges bisect lines connecting cell centers; perpendicular.
- C-grid staggering of velocities (velocities are perpendicular to cell faces).
- Uniform resolution – traditional icosahedral mesh.



## MPAS Nonhydrostatic Atmospheric Solver

### Equations

- Prognostic equations for coupled variables.
- Generalized height coordinate.
- Horizontally vector-invariant equation set.
- Continuity equation for dry air mass.
- Thermodynamic equation for coupled potential temperature.

Variables:  $(U, V, \Omega, \Theta, Q_j) = \tilde{\rho}_d(u, v, \omega, \theta, q_j)$        $\tilde{\rho}_d = \rho_d/\zeta_z$

Vertical coordinate:  $z = \zeta + A(\zeta)h_s(x, y, \zeta)$

Prognostic equations:

$$\frac{\partial \mathbf{V}_H}{\partial t} = -\frac{\rho_d}{\rho_m} \left[ \nabla_\zeta \left( \frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_{Hp}}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{V}_H$$

$$- \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} - \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H}$$

$$\frac{\partial W}{\partial t} = -\frac{\rho_d}{\rho_m} \left[ \frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W$$

$$\frac{\partial \Theta_m}{\partial t} = -(\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m}$$

$$\frac{\partial \tilde{\rho}_d}{\partial t} = -(\nabla \cdot \mathbf{V})_\zeta$$

$$\frac{\partial Q_j}{\partial t} = -(\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j}$$

Dry-air flux divergence

Flux divergence

Diagnostics and definitions:

$$\frac{\rho_m}{\rho_d} = 1 + q_v + q_c + q_r + \dots$$

$$p = p_0 \left( \frac{R_d \zeta_z \Theta_m}{p_0} \right)^\gamma$$

$$\theta_m = \theta [1 + (R_v/R_d)q_v]$$

## Operators on the Voronoi Mesh

### *Flux divergence and transport*

Transport equation,  
conservative form:

$$\frac{\partial(\rho\psi)}{\partial t} = -\nabla \cdot \mathbf{V}(\rho\psi)$$

Finite-Volume formulation,  
Integrate over cell:

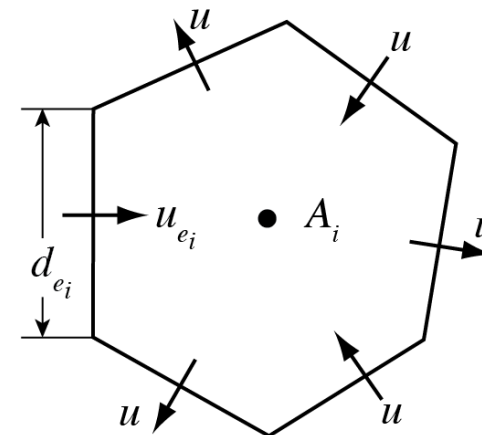
$$\int_D \left[ \frac{\partial}{\partial t}(\rho\psi) = -\nabla \cdot \mathbf{V}(\rho\psi) \right] dV$$

Apply divergence theorem:

$$\frac{\partial(\overline{\rho\psi})}{\partial t} = -\frac{1}{V} \int_{\Sigma} (\rho\psi) \mathbf{V} \cdot \mathbf{n} d\sigma$$

Discretize in time and space:

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\rho \mathbf{V} \cdot \mathbf{n}_{e_i})} \psi$$



Velocity divergence operator is  
2<sup>nd</sup>-order accurate for  
edge-centered velocities.

# Operators on the Voronoi Mesh

## *Flux divergence and transport*

Transport equation,  
conservative form:

$$\frac{\partial(\rho\psi)}{\partial t} = -\nabla \cdot \mathbf{V}(\rho\psi)$$

Finite-Volume formulation,  
Integrate over cell:

$$\int_D \left[ \frac{\partial}{\partial t}(\rho\psi) = -\nabla \cdot \mathbf{V}(\rho\psi) \right] dV$$

Apply divergence theorem:

$$\frac{\partial(\overline{\rho\psi})}{\partial t} = -\frac{1}{V} \int_{\Sigma} (\rho\psi) \mathbf{V} \cdot \mathbf{n} d\sigma$$

In MPAS, the mass flux is a prognostic  
variables at the cell edge.

Scalar mixing ratios are defined at  
cell centers. Their definition at the  
cell edges defines the  
*transport scheme*.

More generally, a transport scheme  
defines the temporally and spatially  
integrated scalar mass flux through  
the edge over timestep  $\Delta t$ .

Discretize in time and space:

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\rho \mathbf{V} \cdot \mathbf{n}_{e_i})} \psi$$



# Operators on the Voronoi Mesh

## *Flux divergence and transport*

Runge-Kutta time integration

$$\phi^t \rightarrow \phi^{t+\Delta t}$$

$$\phi^* = \phi^t + \frac{\Delta t}{3} RHS(\phi^t)$$

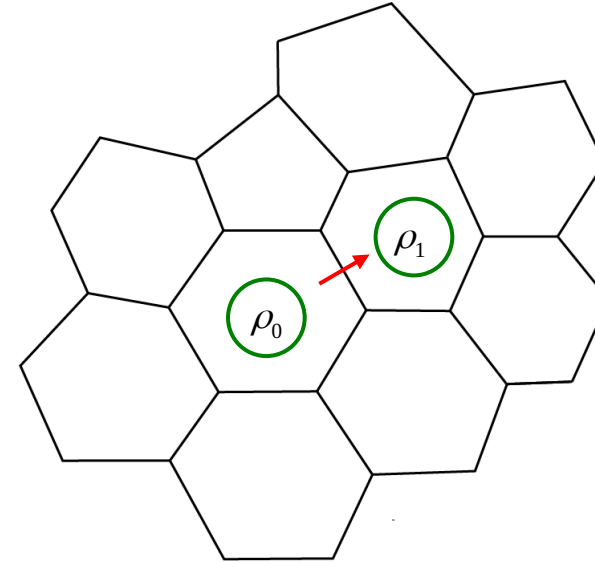
$$\phi^{**} = \phi^t + \frac{\Delta t}{2} RHS(\phi^*)$$

$$\phi^{t+\Delta t} = \phi^t + \Delta t RHS(\phi^{**})$$

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \psi}$$

## Transport – Unstructured MPAS Mesh

$$\begin{aligned}
 \frac{\partial \mathbf{V}_H}{\partial t} &= -\frac{\rho_d}{\rho_m} \left[ \nabla_\zeta \left( \frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_H p}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{V}_H \\
 &\quad - \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} - \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H} \\
 \frac{\partial W}{\partial t} &= -\frac{\rho_d}{\rho_m} \left[ \frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W \\
 \frac{\partial \Theta_m}{\partial t} &= -(\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m} \\
 \frac{\partial \tilde{\rho}_d}{\partial t} &= -(\nabla \cdot \mathbf{V})_\zeta \\
 \frac{\partial Q_j}{\partial t} &= -(\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j} \\
 \mathbf{V} &= \rho \mathbf{v}; \quad \mathbf{v} = (u, w)
 \end{aligned}$$



For the horizontal dry-air mass flux, the value of the density  $\rho_d$  at a cell face is set equal to the average of the densities from the two cells sharing the face:

$$\rho_{\text{edge}} = (\rho_0 + \rho_1)/2, \quad \mathbf{V}_{\text{edge}} = u_e (\rho_0 + \rho_1)/2$$

## MPAS Nonhydrostatic Atmospheric Solver

### Equations

- Prognostic equations for coupled variables.
- Generalized height coordinate.
- Horizontally vector-invariant equation set.
- Continuity equation for dry air mass.
- Thermodynamic equation for coupled potential temperature.

Variables:  $(U, V, \Omega, \Theta, Q_j) = \tilde{\rho}_d(u, v, \omega, \theta, q_j)$        $\tilde{\rho}_d = \rho_d/\zeta_z$

Vertical coordinate:  $z = \zeta + A(\zeta)h_s(x, y, \zeta)$

Prognostic equations:

$$\frac{\partial \mathbf{V}_H}{\partial t} = -\frac{\rho_d}{\rho_m} \left[ \nabla_\zeta \left( \frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_H p}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{V}_H$$

$$- \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} - \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H}$$

$$\frac{\partial W}{\partial t} = -\frac{\rho_d}{\rho_m} \left[ \frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W$$

$$\frac{\partial \Theta_m}{\partial t} = -(\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m}$$

$$\frac{\partial \tilde{\rho}_d}{\partial t} = -(\nabla \cdot \mathbf{V})_\zeta$$

Flux divergence

$$\frac{\partial Q_j}{\partial t} = -(\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j}$$

$$\frac{\rho_m}{\rho_d} = 1 + q_v + q_c + q_r + \dots$$

Diagnostics and definitions:

$$p = p_0 \left( \frac{R_d \zeta_z \Theta_m}{p_0} \right)^\gamma$$

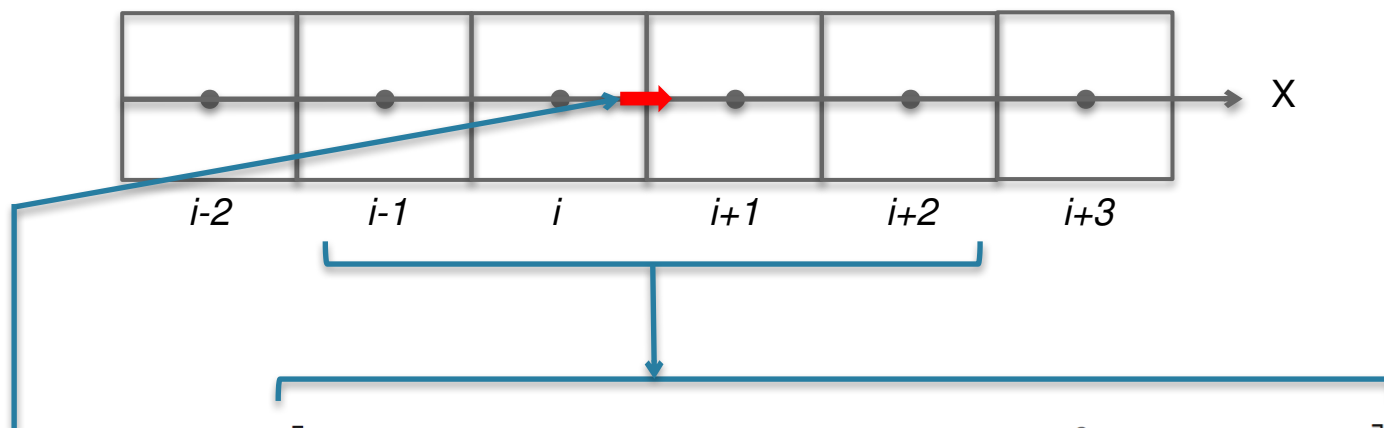
$$\theta_m = \theta [1 + (R_v/R_d) q_v]$$



## Operators on the Voronoi Mesh

### *Flux divergence and transport*

How do we define the edge mixing ratio on the MPAS unstructured mesh?  
First consider a structured mesh - WRF 3rd and 4th-order fluxes



$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

(Hundsdofer et al, 1995; Van Leer, 1985)

$\beta = 0$ , fourth-order;  $\beta = 1$  third order

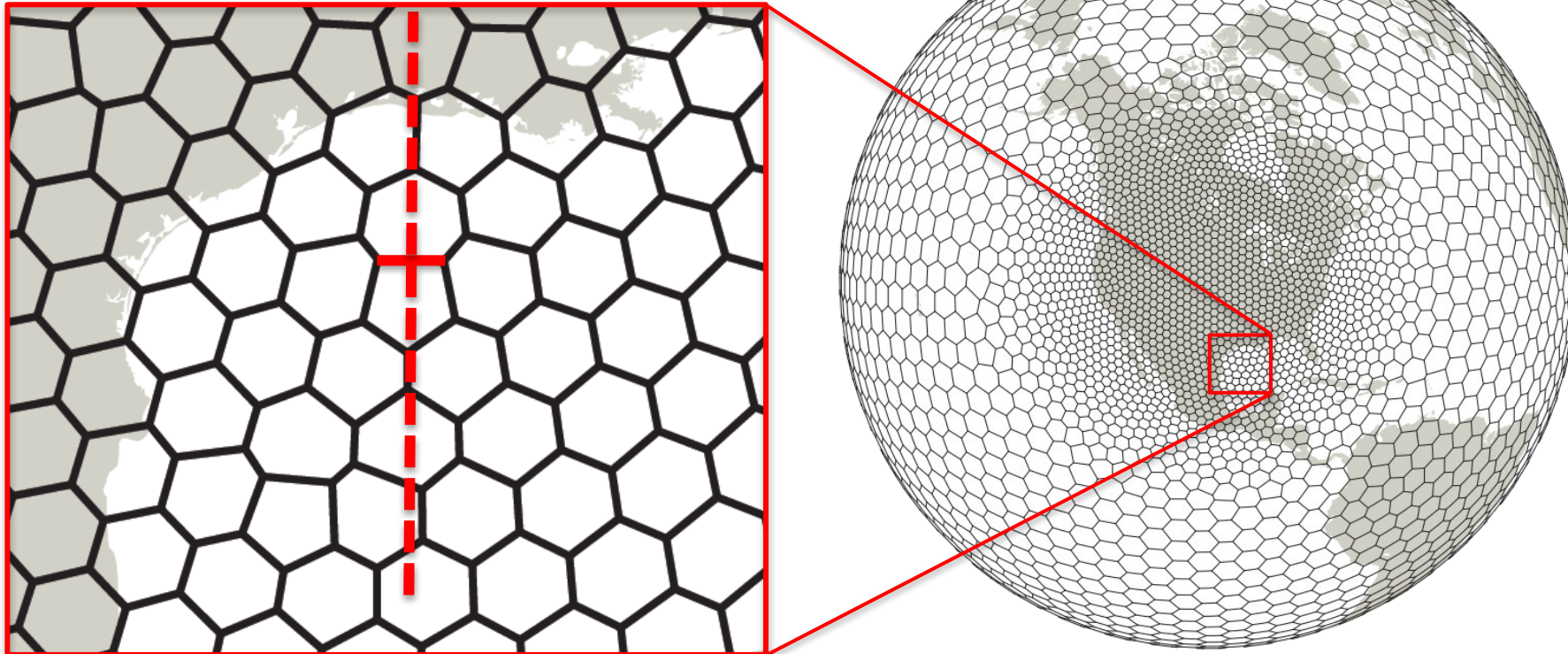
## Operators on the Voronoi Mesh

### *Flux divergence and transport*

3rd and 4th-order WRF fluxes:

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

The coordinates are not continuous in MPAS.



## Transport – Unstructured MPAS Mesh

3rd and 4th-order fluxes (e.g. WRF):

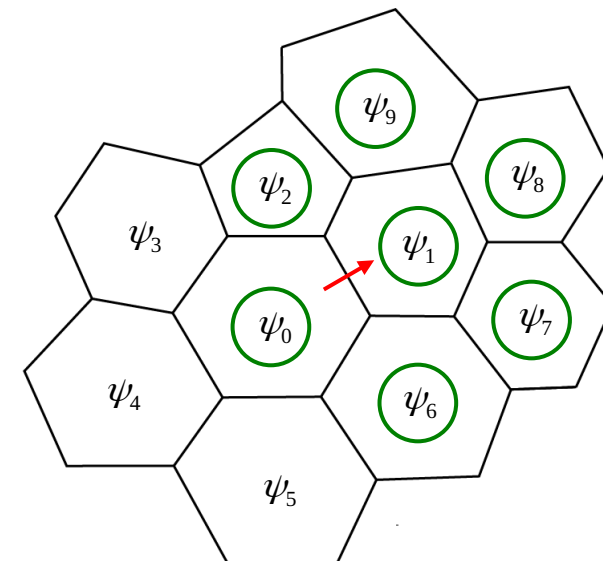
$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

where  $\delta_x^2 \psi_i = \psi_{i-1} - 2\psi_i + \psi_{i+1}$  (Hundsdofer et al, 1995; Van Leer, 1985)

Recognizing  $\delta_x^2 \psi = \Delta x^2 \frac{\partial^2 \psi}{\partial x^2} + O(\Delta x^4)$  we recast the 3rd and 4th order flux as

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} + \text{sign}(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right]$$

where  $x$  is the direction normal to the cell edge and  $i$  and  $i+1$  are cell centers. We use the least-squares-fit polynomial to compute the second derivatives.





## Transport – Unstructured MPAS Mesh

3rd and 4th-order fluxes (e.g. WRF):

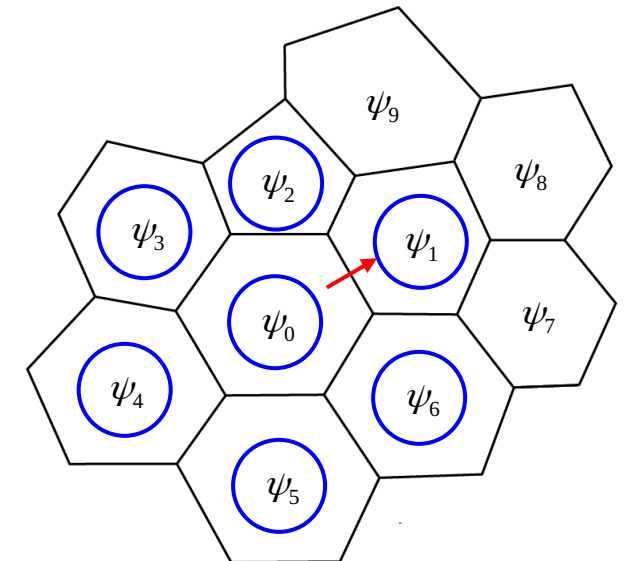
$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

where  $\delta_x^2 \psi_i = \psi_{i-1} - 2\psi_i + \psi_{i+1}$  (Hundsdofer et al, 1995; Van Leer, 1985)

Recognizing  $\delta_x^2 \psi = \Delta x^2 \frac{\partial^2 \psi}{\partial x^2} + O(\Delta x^4)$  we recast the 3rd and 4th order flux as

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right. \\ \left. + \text{sign}(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right]$$

where  $x$  is the direction normal to the cell edge and  $i$  and  $i+1$  are cell centers. We use the least-squares-fit polynomial to compute the second derivatives.

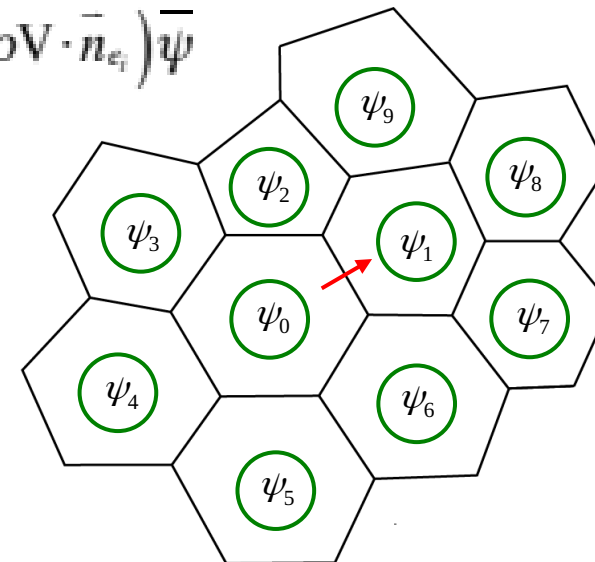


## Flux divergence, transport, and Runge-Kutta time integration

Scalar transport equation for cell  $i$ :

$$\frac{\partial(\rho\psi)_i}{\partial t} = L(\mathbf{V}, \rho, \psi) = -\frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} (\rho \mathbf{V} \cdot \bar{\mathbf{n}}_{e_i}) \bar{\psi}$$

1. Scalar edge-flux value  $\psi$  is the weighted sum of cell values from cells that share edge and all their neighbors.
2. Each edge-flux is used to update the two cells that share the edge.
3. Three edge-flux evaluations and cell updates are needed to complete the Runge-Kutta timestep.
4. Weights are pre-computed and stored for use during the integration.

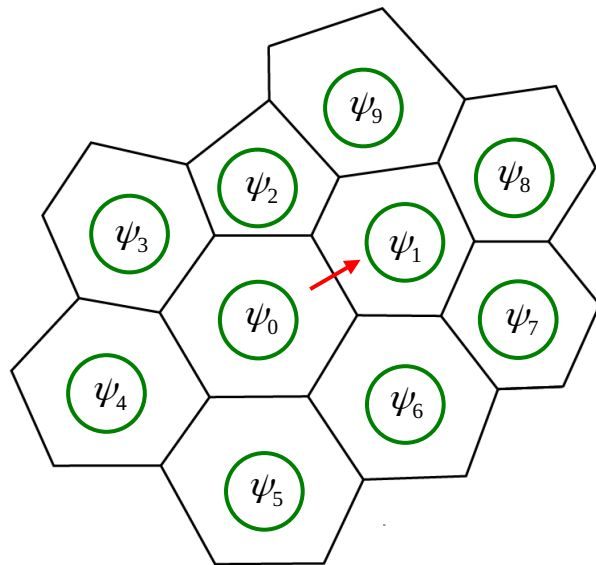


$$(\rho\psi)^* = (\rho\psi)^t + \frac{\Delta t}{3} L(\mathbf{V}, \rho, \psi^t)$$

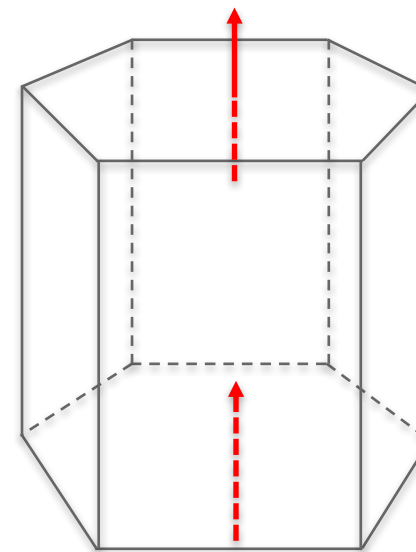
$$(\rho\psi)^{**} = (\rho\psi)^t + \frac{\Delta t}{2} L(\mathbf{V}, \rho, \psi^*)$$

$$(\rho\psi)^{t+\Delta t} = (\rho\psi)^t + \Delta t L(\mathbf{V}, \rho, \psi^{**})$$

## *Flux divergence and transport. Conservation*



Horizontal (scalar) mass fluxes



Vertical (scalar) mass fluxes

*The mass (or scalar mass) flux on a cell edge (face) is used to update both cells sharing that edge (face), thus mass (and scalar mass) is conserved exactly.*



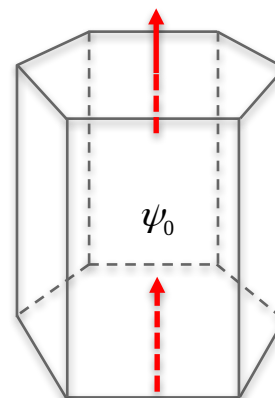
## Scalar transport: Positive-definite and monotonic renormalization

Scalar update, last RK3 step:

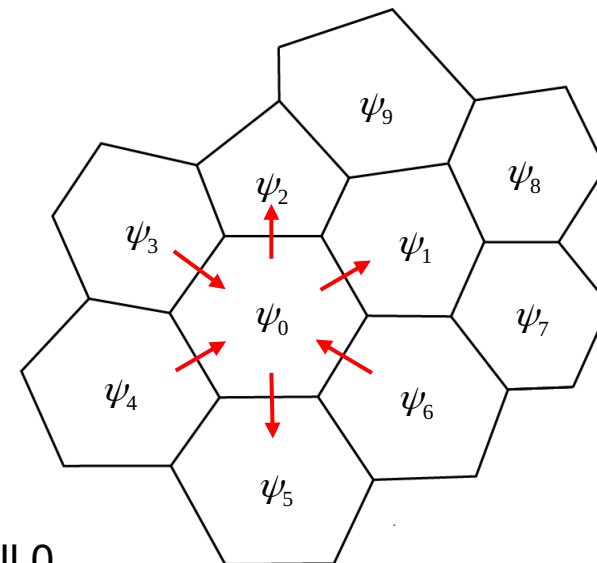
$$(\rho\phi)_i^{t+\Delta t} = (\rho\phi)_i^t - \frac{1}{V_i} \sum_{n_{e_i}} \underbrace{A_{e_i} (\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \phi}_{\text{fluxes } f_i} \quad (1)$$

### Renormalization

- (1) Decompose flux:  $f_i = f_i^{upwind} + f_i^c$
- (2) Renormalize high-order correction fluxes  $f_i^c$  such that solution is positive definite or monotonic:  
 $f_i^c = R(f_i^c)$
- (3) Update scalar equation (1)  
 using  $f_i = f_i^{upwind} + R(f_i^c)$



$n = 8$  in this example, 6 horizontal fluxes and 2 vertical fluxes to update cell 0



## Conservative Transport with RK3 Time Integration: *Examples*

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right. \\ \left. + \text{sign}(u) \Delta x_e^2 \beta \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right]$$

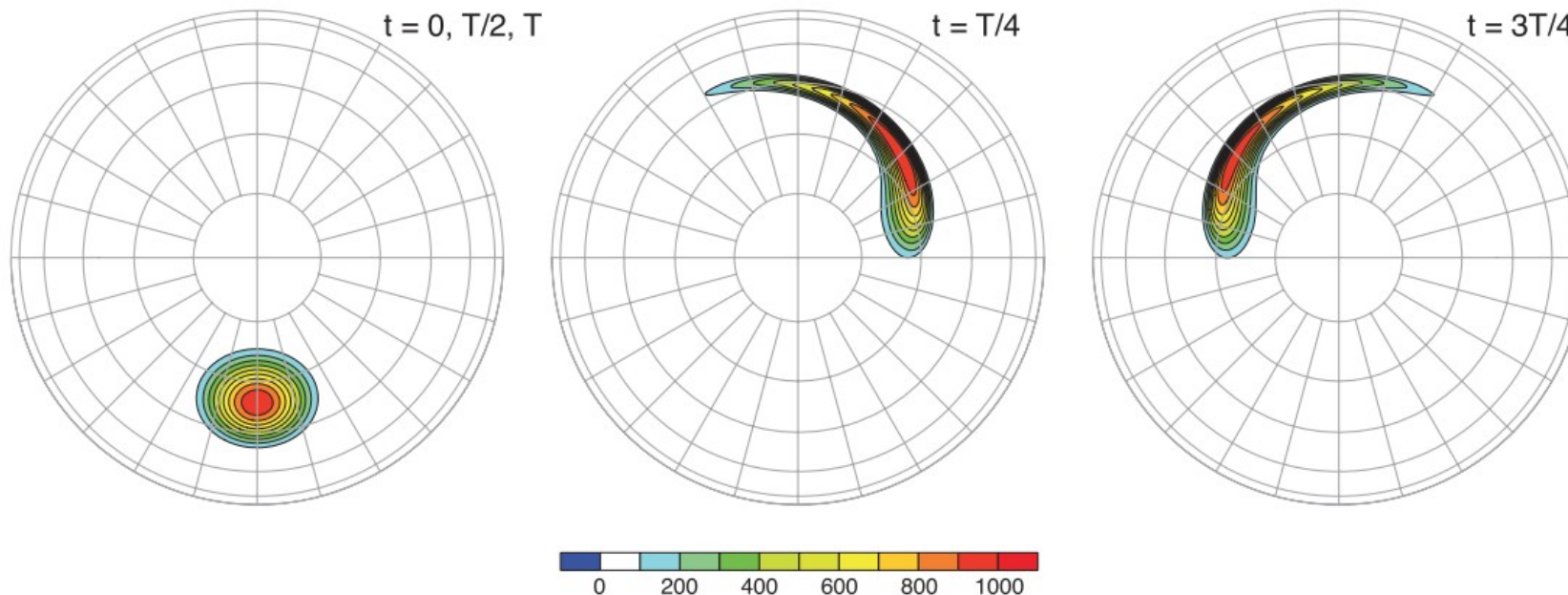


FIG. 5. Exact solution for the Blossey and Durran (deformational flow) test case adapted to the sphere, from Skamarock and Menchaca (2010).

## Conservative Transport with RK3 Time Integration: *Examples*

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[ \frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right. \\ \left. + \text{sign}(u) \Delta x_e^2 \beta \frac{1}{12} \left\{ \left( \frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left( \frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right]$$

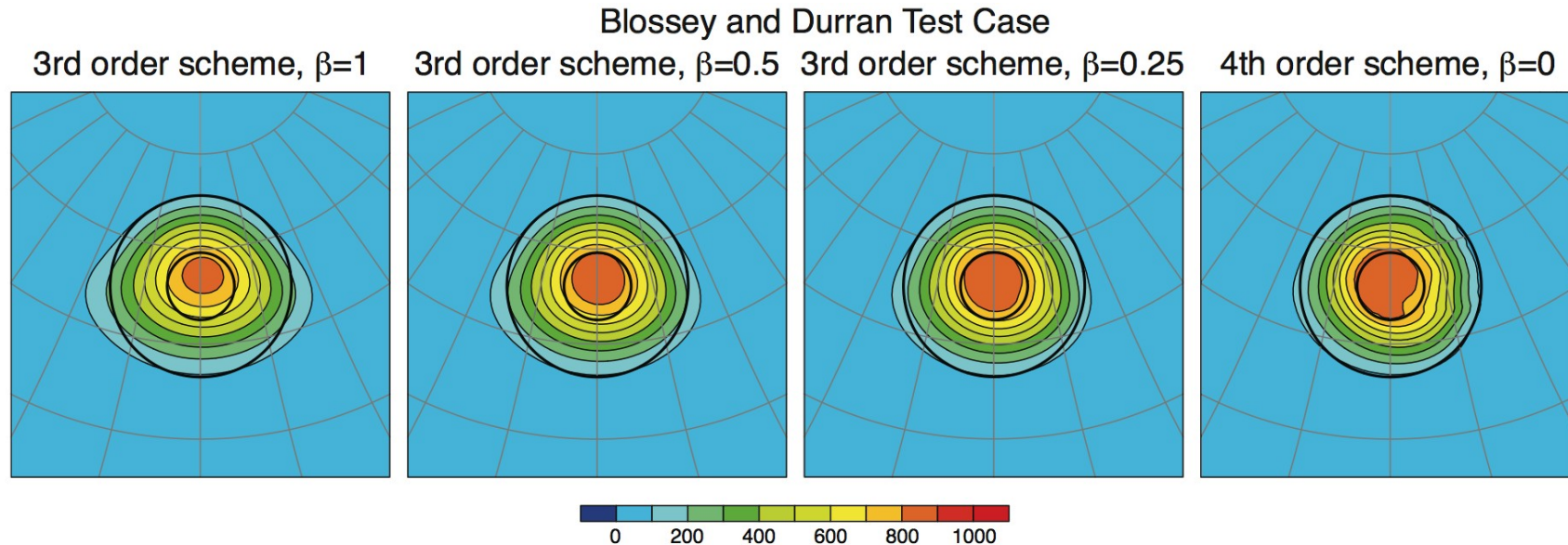
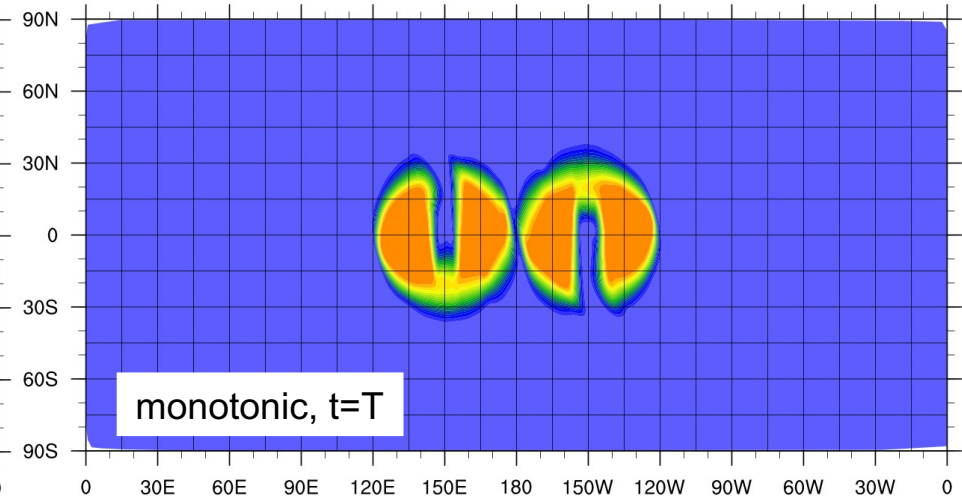
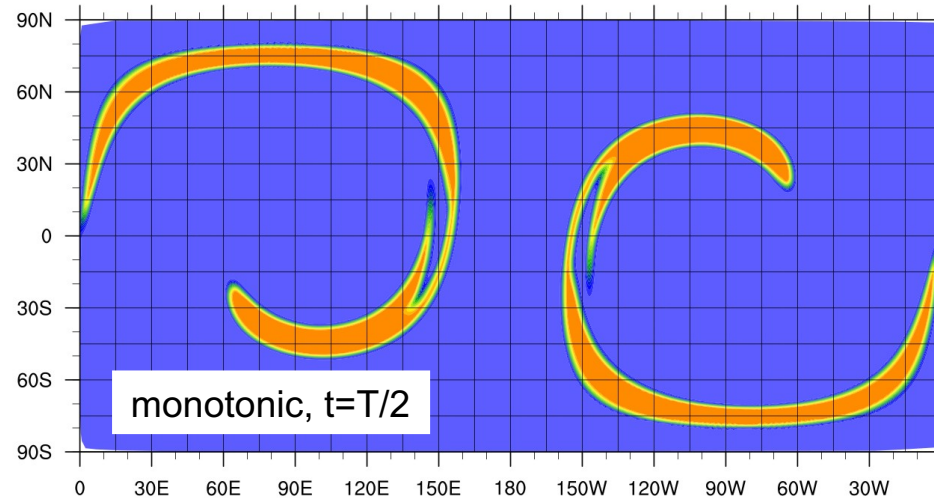
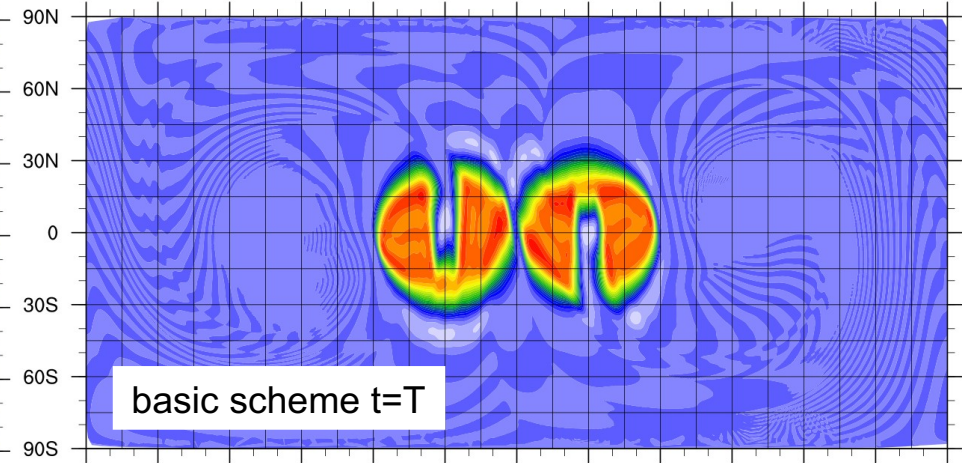
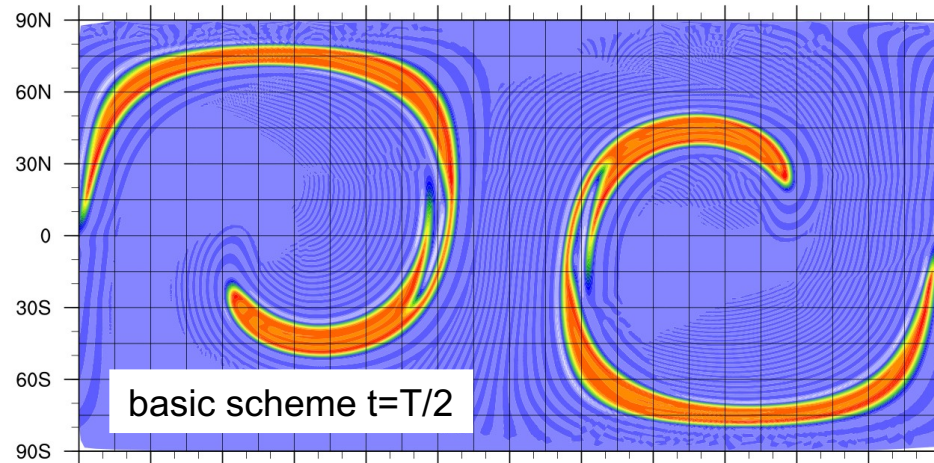
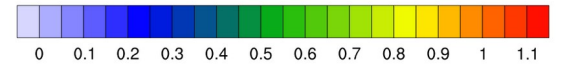


FIG. 7. Deformational flow test case results at time  $T$  using (11) with different values of the filter parameter  $\beta$ . The simulations were performed on the 40962-cell grid.



163842 cells, ~ 60 km cell spacing (~ 1/2 deg), Cr max ~ 0.8



## Configuring the dynamics

### Transport

namelist.atmosphere

```
&nhyd_model
  config_time_integration_order = 2
  config_dt = 720.0
  config_start_time = '2010-10-23_00:00:00'
  config_run_duration = '5_00:00:00'
  config_split_dynamics_transport = true
  config_number_of_sub_steps = 2
  config_dynamics_split_steps = 3
  config_horiz_mixing = '2d_smagorinsky'
  config_visc4_2dsmag = 0.05
  config_scalar_advection = true
  config_monotonic = true
  config_coef_3rd_order = 0.25
  config_epssm = 0.1
  config_smdiv = 0.1
```

*Upwind coefficient (0 <-> 1),  
> 0 increases damping.  
= 0, 4<sup>th</sup> order scheme,  
> 0, 3<sup>rd</sup> order scheme.*

/

# Operators on the Voronoi Mesh

## *Resolved and turbulent transport*

$$\frac{\partial(\rho\phi)}{\partial t} = \underline{-\nabla \cdot \mathbf{V} \phi}$$

Transport by the resolved flow

$$= \underline{\nabla \cdot (\rho K \nabla \phi)}$$

Turbulent transport, e.g. Smagorinsky  
 $K$  is an eddy viscosity ( $\text{m}^2/\text{s}$ )

$$= \underline{-\nabla \cdot (\rho \nu_4 \nabla (\nabla \cdot \nabla \phi))}$$

4<sup>th</sup>-order filter cast as a  
turbulent transport  
 $\nu_4$  is a hyperviscosity ( $\text{m}^4/\text{s}$ )



## Operators on the Voronoi Mesh *Resolved and turbulent transport*

continuous  
operators

discrete  
operators

$$\nabla \cdot \mathbf{V} \phi$$



$$\frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\mathbf{V} \cdot \mathbf{n}_{e_i}) \phi}$$

$$\nabla \cdot (\rho K \nabla \phi)$$

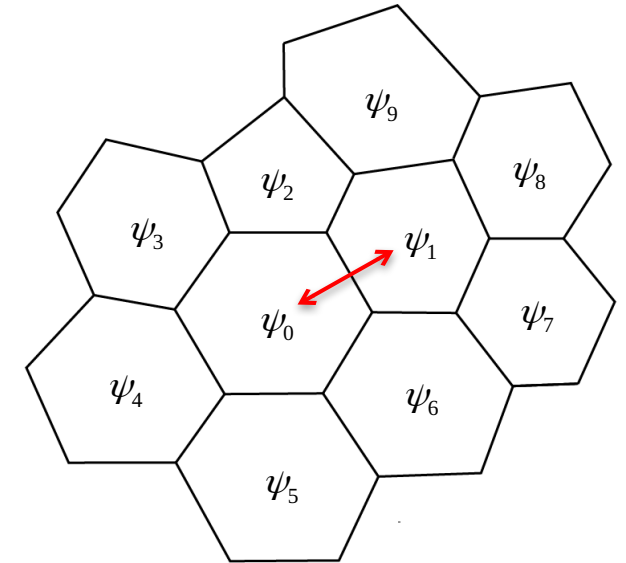


$$\frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{\rho K} (\mathbf{n}_{e_i} \cdot \nabla \phi)$$

$$\nabla \cdot (\rho \nu_4 \nabla (\nabla \cdot \nabla \phi))$$



$$\frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{\rho \nu_4} \left( \mathbf{n}_{e_i} \cdot \nabla \left[ \frac{1}{A_j} \sum_{n_{e_j}} d_{e_j} (\mathbf{n}_{e_j} \cdot \nabla \phi) \right] \right)$$



## Operators on the Voronoi Mesh *Filters for horizontal momentum*

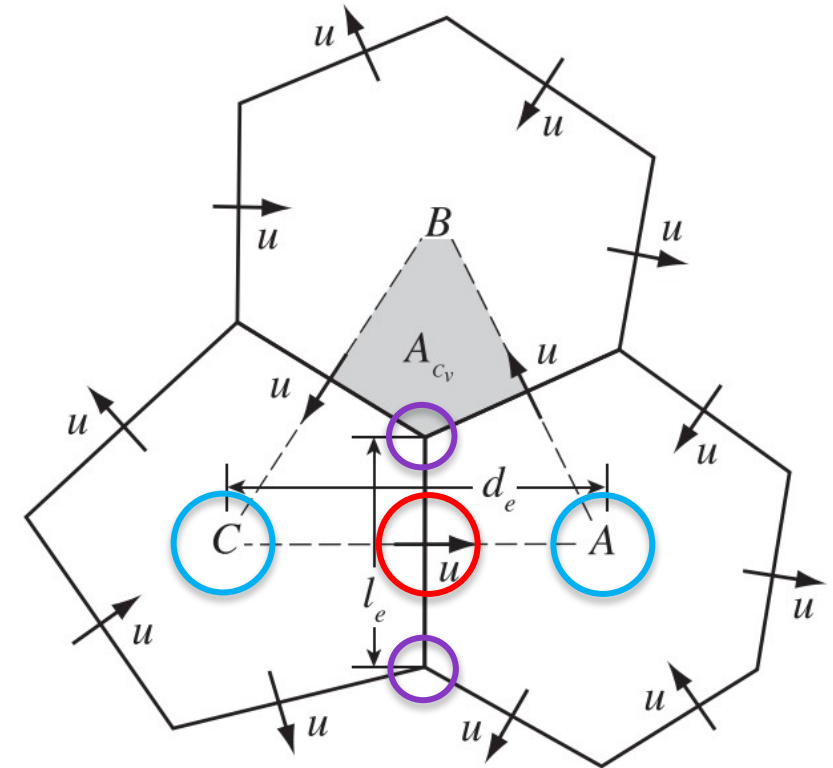
2<sup>nd</sup> order filter

$$\frac{\partial u_i}{\partial t} = \dots + K_u \nabla^2 u_i$$

$$\nabla^2 u_i = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \mathbf{v} - \frac{\partial \eta}{\partial x_j}$$

discrete form in MPAS.  
 $\eta$  is the vertical vorticity

$$\nabla^2 u_i = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \mathbf{v} - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \mathbf{v})]$$



## Operators on the Voronoi Mesh *Filters for horizontal momentum*

4<sup>th</sup> order filter

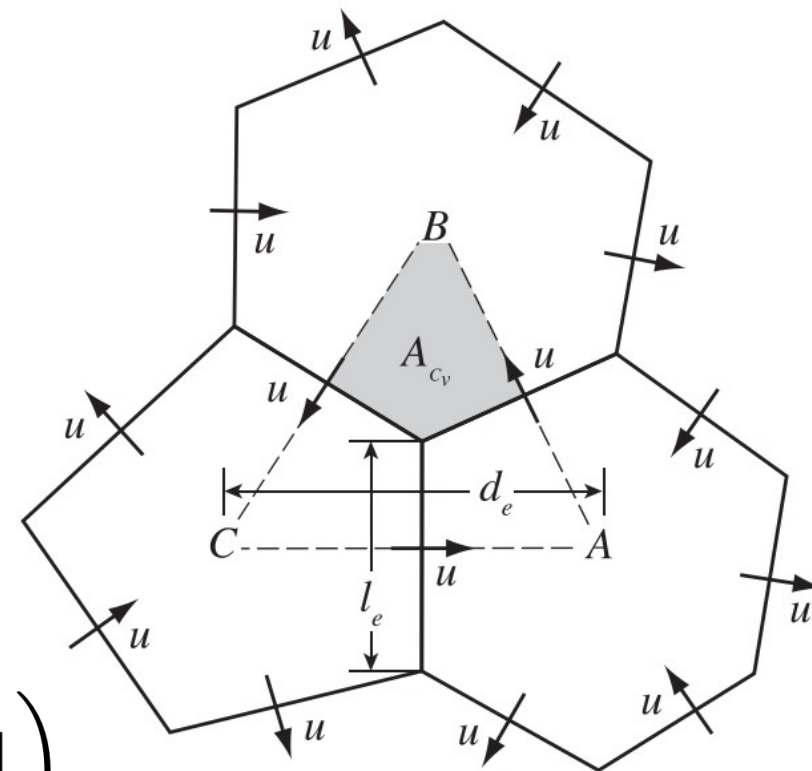
$$\frac{\partial u_i}{\partial t} = \dots - \nu_4^u \nabla^4 u_i$$

$$\nabla^4 u_i = \nabla^2 (\nabla^2 u_i)$$

$$\nabla^4 u_i = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \nabla^2 u_i - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \nabla^2 u_i)]$$

In MPAS

$$\frac{\delta u_i}{\delta t} = -\nu_4 \left( \gamma_u \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \nabla^2 u_i - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \nabla^2 u_i)] \right)$$



## Configuring the dynamics

### Dissipation

#### namelist.atmosphere

&nhyd\_model

```
config_time_integration_order = 2
config_dt = 720.0
config_start_time = '2010-10-23_00:00:00'
config_run_duration = '5_00:00:00'
config_split_dynamics_transport = true
config_number_of_sub_steps = 2
config_dynamics_split_steps = 3
config_horiz_mixing = '2d_smagorinsky'
config_visc4_2dsmag = 0.05
config_scalar_advection = true
config_monotonic = true
config_coef_3rd_order = 0.25
config_epssm = 0.1
config_smdiv = 0.1
```

/

$$\nu_4 \text{ (m}^4\text{/s)} = \Delta x^3 \times \text{config\_visc4\_2dsmag}$$

*The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars. We anticipate activating these options for scalars in a future release*

*Alternately  
"2d\_fixed"*

*4<sup>th</sup> order background  
filter coef, used with  
2d\_smagorinsky*



## Configuring the dynamics

### Dissipation

#### namelist.atmosphere

```
&nhyd_model
  config_time_integration_order = 2
  config_dt = 720.0
  config_start_time = '2010-10-23_00:00:00'
  config_run_duration = '5_00:00:00'
  config_split_dynamics_transport = true
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  config_dynamics_split_steps = 3
  config_horiz_mixing = '2d_smagorinsky'
  config_visc4_2dsmag = 0.05
  config_scalar_advection = true
  config_monotonic = true
  config_coef_3rd_order = 0.25
  config_epssm = 0.1
  config_smdiv = 0.1
  config_del4u_div_factor = 10.
```

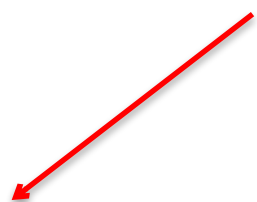
$$v_4 \text{ (m}^4\text{/s)} = \Delta x^3 \times \text{config\_visc4\_2dsmag}$$

*The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars. We anticipate activating these options for scalars in a future release*

For the horizontal momentum:

$$v_{4,D} \text{ (m}^4\text{/s)} = v_4 \times \text{config\_del4u\_div\_factor}$$

*Hidden in the MPAS V8 namelist.atmosphere  
config\_del4u\_div\_factor = 10 (default)*



## Configuring the dynamics Dissipation

### namelist.atmosphere

&nhyd\_model

```
config_h_mom_eddy_visc2 = 0  
config_h_mom_eddy_visc4 = 0  
config_v_mom_eddy_visc2 = 0  
config_h_theta_eddy_visc2 = 0  
config_h_theta_eddy_visc4 = 0  
config_v_theta_eddy_visc2 = 0  
config_horiz_mixing = "2d_fixed"
```

*Hidden in the MPAS V8  
namelist.atmosphere*

*fixed viscosity ( $m^2s^{-1}$ )*

*Fixed hyper-viscosity ( $m^4s^{-1}$ )*

*The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars.*

2d\_fixed option is used primarily in idealized cases.

# Spatial Discretization in MPAS

## *references*

### Dynamics

Skamarock, W. C, J. B. Klemp, M. G. Duda, L. Fowler, S.-H. Park, and T. D. Ringler, 2012: A Multi-scale Nonhydrostatic Atmospheric Model Using Centroidal Voronoi Tesselations and C-Grid Staggering. Mon. Wea. Rev., 140, 3090-3105. doi:10.1175/MWR-D-11-00215.1

### Transport

Skamarock, W. C. and A. Gassmann, 2011: Conservative Transport Schemes for Spherical Geodesic Grids: High-Order Flux Operators for ODE-Based Time Integration. Mon. Wea. Rev., 139, 2562-2575, doi:10.1175/MWR-D-10-05056.1