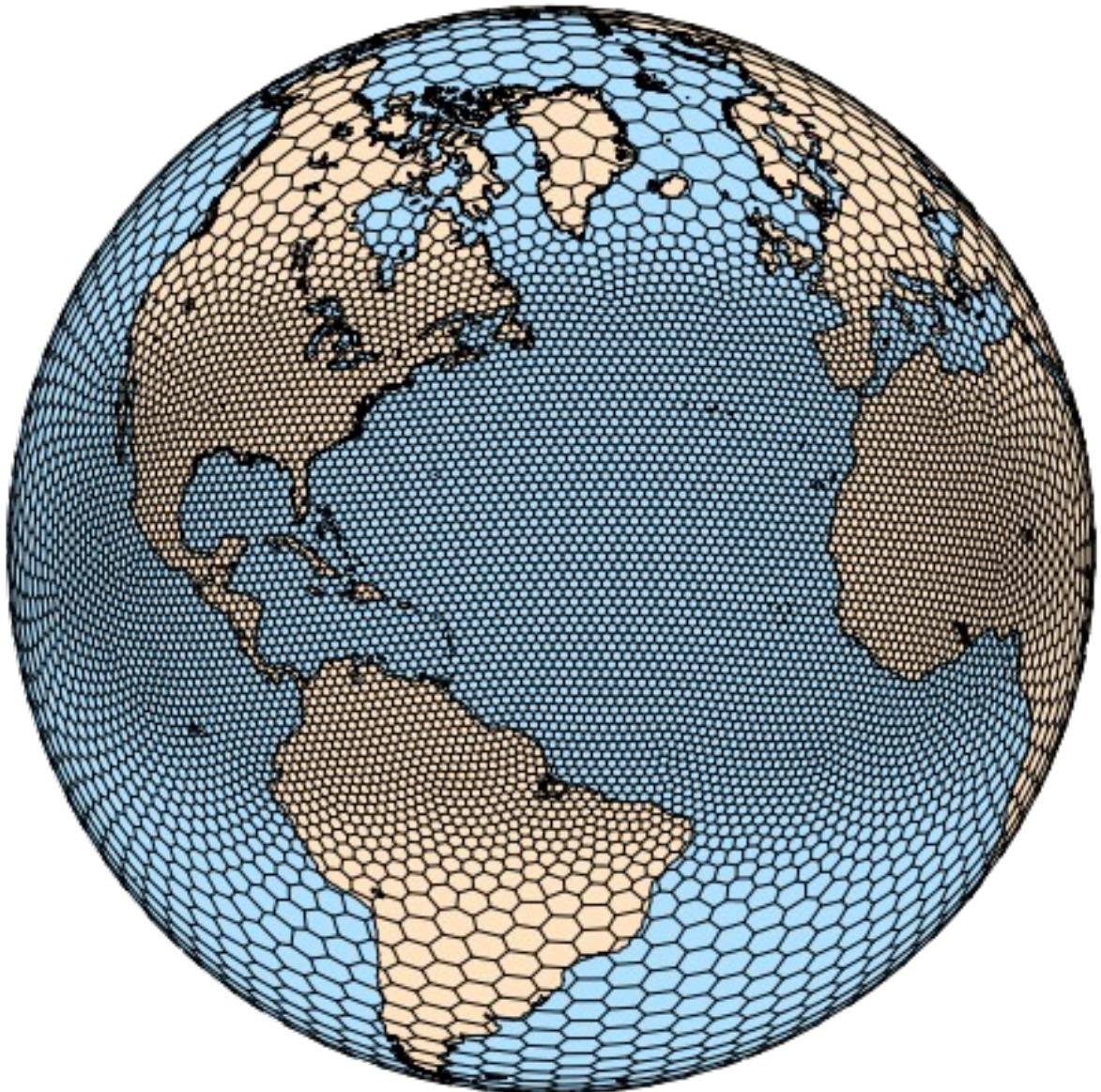
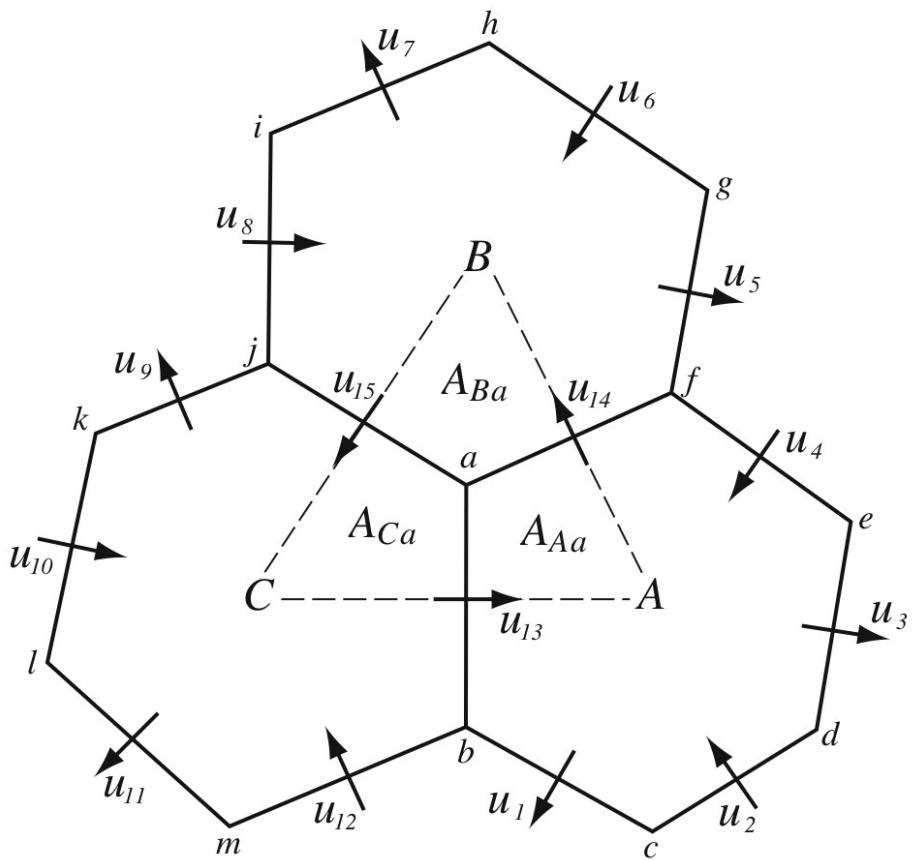


Dynamical Core

- *Spatial discretization*
 - *Transport*
 - *Filters*
 - *Namelist parameters*
 - *References*

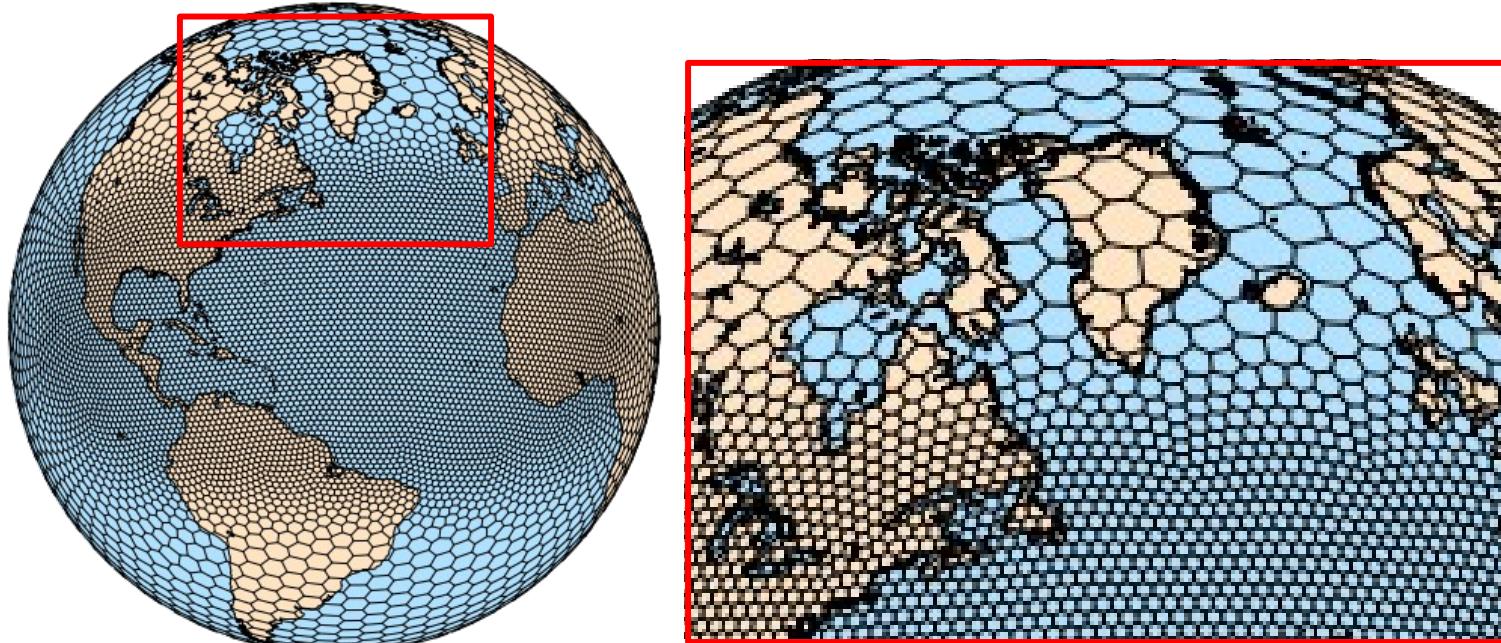


MPAS Horizontal Mesh



Unstructured spherical centroidal Voronoi meshes

- Mostly hexagons, some pentagons (5-sided cells) and heptagons (7-sided cells).
- Cell centers are at cell center-of-mass (centroidal).
- Cell edges bisect lines connecting cell centers; perpendicular.
- C-grid staggering of velocities (velocities are perpendicular to cell faces).
- Uniform resolution – traditional icosahedral mesh.



Equations

- Prognostic equations for coupled variables.
- Generalized height coordinate.
- Horizontally vector-invariant equation set.
- Continuity equation for dry air mass.
- Thermodynamic equation for coupled potential temperature.

MPAS Nonhydrostatic Atmospheric Solver

Variables: $(U, V, \Omega, \Theta, Q_j) = \tilde{\rho}_d (u, v, \omega, \theta, q_j)$ $\tilde{\rho}_d = \rho_d / \zeta_z$

Vertical coordinate: $z = \zeta + A(\zeta)h_s(x, y, \zeta)$

Prognostic equations:

$$\frac{\partial \mathbf{V}_H}{\partial t} = -\frac{\rho_d}{\rho_m} \left[\nabla_\zeta \left(\frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_H p}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{v}_H$$

$$- \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} + \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H}$$

$$\frac{\partial W}{\partial t} = -\frac{\rho_d}{\rho_m} \left[\frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W$$

$$\frac{\partial \Theta_m}{\partial t} = -(\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m}$$

$$\frac{\partial \tilde{\rho}_d}{\partial t} = -(\nabla \cdot \mathbf{V})_\zeta$$

$$\frac{\partial Q_j}{\partial t} = -(\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j}$$

Dry-air flux divergence

Flux divergence

$$\frac{\rho_m}{\rho_d} = 1 + q_v + q_c + q_r + \dots$$

$$p = p_0 \left(\frac{R_d \zeta_z \Theta_m}{p_0} \right)^\gamma$$

$$\theta_m = \theta [1 + (R_v/R_d) q_v]$$

Diagnostics and definitions:

Operators on the Voronoi Mesh

Flux divergence and transport

Transport equation,
conservative form:

$$\frac{\partial(\rho\psi)}{\partial t} = -\nabla \cdot \mathbf{V}(\rho\psi)$$

Finite-Volume formulation,
Integrate over cell:

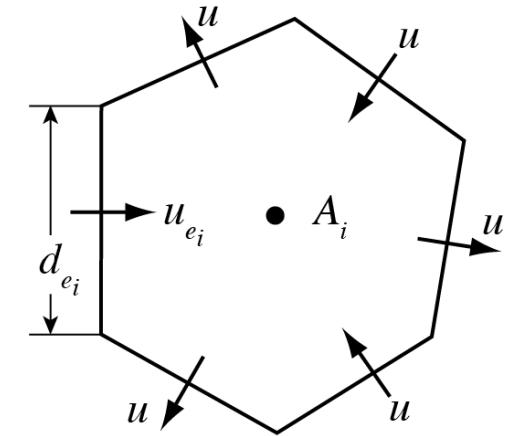
$$\int_D \left[\frac{\partial}{\partial t}(\rho\psi) = -\nabla \cdot \mathbf{V}(\rho\psi) \right] dV$$

Apply divergence theorem:

$$\frac{\partial(\overline{\rho\psi})}{\partial t} = -\frac{1}{V} \int_{\Sigma} (\rho\psi) \mathbf{V} \cdot \mathbf{n} \, d\sigma$$

Discretize in time and space:

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \psi}$$



Velocity divergence operator is
2nd-order accurate for
edge-centered velocities.

Operators on the Voronoi Mesh

Flux divergence and transport

Transport equation,
conservative form:

$$\frac{\partial(\rho\psi)}{\partial t} = -\nabla \cdot \mathbf{V}(\rho\psi)$$

In MPAS, the mass flux is a prognostic variables at the cell edge.

Finite-Volume formulation,
Integrate over cell:

$$\int_D \left[\frac{\partial}{\partial t}(\rho\psi) = -\nabla \cdot \mathbf{V}(\rho\psi) \right] dV$$

Scalar mixing ratios are defined at cell centers. Their definition at the cell edges defines the *transport scheme*.

Apply divergence theorem:

$$\frac{\partial(\overline{\rho\psi})}{\partial t} = -\frac{1}{V} \int_{\Sigma} (\rho\psi) \mathbf{V} \cdot \mathbf{n} d\sigma$$

More generally, a transport scheme defines the temporally and spatially integrated scalar mass flux through the edge over timestep Δt .

Discretize in time and space:

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} (\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \psi$$

Operators on the Voronoi Mesh

Flux divergence and transport

Runge-Kutta time integration

$$\phi^t \rightarrow \phi^{t+\Delta t}$$

$$\phi^* = \phi^t + \frac{\Delta t}{3} RHS(\phi^t)$$

$$\phi^{**} = \phi^t + \frac{\Delta t}{2} RHS(\phi^*)$$

$$\phi^{t+\Delta t} = \phi^t + \Delta t RHS(\phi^{**})$$

$$(\overline{\rho\psi})_i^{t+\Delta t} = (\overline{\rho\psi})_i^t - \Delta t \left[\frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} (\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \psi \right]$$

Transport – Unstructured MPAS Mesh

$$\frac{\partial \mathbf{V}_H}{\partial t} = - \frac{\rho_d}{\rho_m} \left[\nabla_\zeta \left(\frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_H p}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{V}_H$$

$- \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} - \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H}$

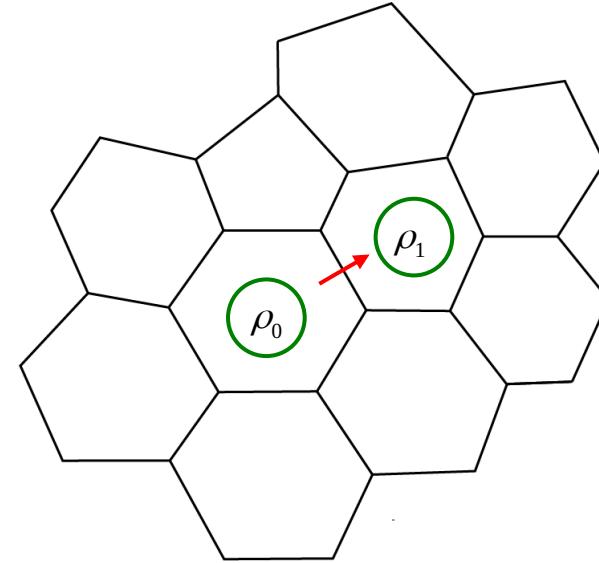
$$\frac{\partial W}{\partial t} = - \frac{\rho_d}{\rho_m} \left[\frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W$$

$$\frac{\partial \Theta_m}{\partial t} = - (\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m}$$

$$\frac{\partial \tilde{\rho}_d}{\partial t} = - (\nabla \cdot \mathbf{V})_\zeta$$

$$\frac{\partial Q_j}{\partial t} = - (\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j}$$

$$\mathbf{V} = \rho \mathbf{v}; \quad \mathbf{v} = (u, w)$$



For the horizontal dry-air mass flux, the value of the density ρ_d at a cell face is set equal to the average of the densities from the two cells sharing the face:

$$\rho_{\text{edge}} = (\rho_0 + \rho_1)/2, \quad \mathbf{V}_{\text{edge}} = u_e (\rho_0 + \rho_1)/2$$

Equations

- Prognostic equations for coupled variables.
- Generalized height coordinate.
- Horizontally vector-invariant equation set.
- Continuity equation for dry air mass.
- Thermodynamic equation for coupled potential temperature.

MPAS Nonhydrostatic Atmospheric Solver

Variables: $(U, V, \Omega, \Theta, Q_j) = \tilde{\rho}_d (u, v, \omega, \theta, q_j)$ $\tilde{\rho}_d = \rho_d / \zeta_z$

Vertical coordinate: $z = \zeta + A(\zeta)h_s(x, y, \zeta)$

Prognostic equations:

$$\frac{\partial \mathbf{V}_H}{\partial t} = -\frac{\rho_d}{\rho_m} \left[\nabla_\zeta \left(\frac{p}{\zeta_z} \right) - \frac{\partial \mathbf{z}_H p}{\partial \zeta} \right] - \eta \mathbf{k} \times \mathbf{v}_H$$

$$- \mathbf{v}_H \nabla_\zeta \cdot \mathbf{V} - \frac{\partial \Omega \mathbf{v}_H}{\partial \zeta} - \rho_d \nabla_\zeta K + \mathbf{F}_{V_H}$$

$$\frac{\partial W}{\partial t} = -\frac{\rho_d}{\rho_m} \left[\frac{\partial p}{\partial \zeta} + g \tilde{\rho}_m \right] - (\nabla \cdot \mathbf{v} W)_\zeta + F_W$$

$$\frac{\partial \Theta_m}{\partial t} = -(\nabla \cdot \mathbf{V} \theta_m)_\zeta + F_{\Theta_m}$$

$$\frac{\partial \tilde{\rho}_d}{\partial t} = -(\nabla \cdot \mathbf{V})_\zeta$$

$$\frac{\partial Q_j}{\partial t} = -(\nabla \cdot \mathbf{V} q_j)_\zeta + F_{Q_j}$$

Flux divergence

$$\frac{\rho_m}{\rho_d} = 1 + q_v + q_c + q_r + \dots$$

$$p = p_0 \left(\frac{R_d \zeta_z \Theta_m}{p_0} \right)^\gamma$$

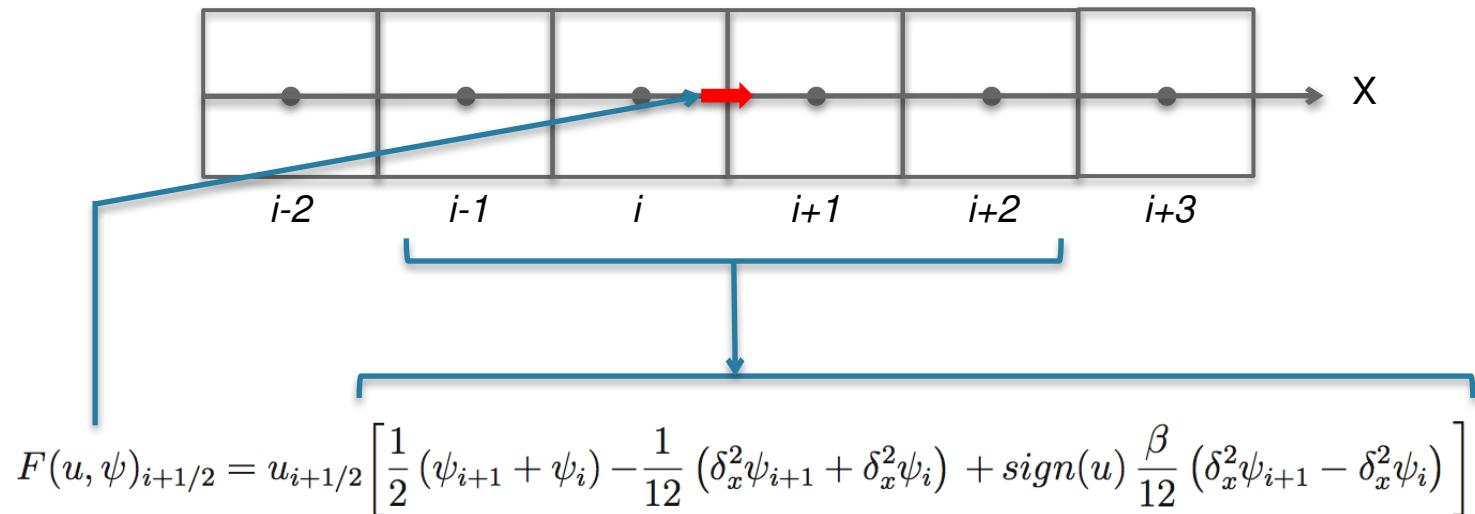
$$\theta_m = \theta [1 + (R_v/R_d) q_v]$$

Diagnostics and definitions:

Operators on the Voronoi Mesh

Flux divergence and transport

How do we define the edge mixing ratio on the MPAS unstructured mesh?
 First consider a structured mesh - WRF 3rd and 4th-order fluxes



(Hundsdorfer et al, 1995; Van Leer, 1985)

$\beta = 0$, fourth-order; $\beta = 1$ third
order

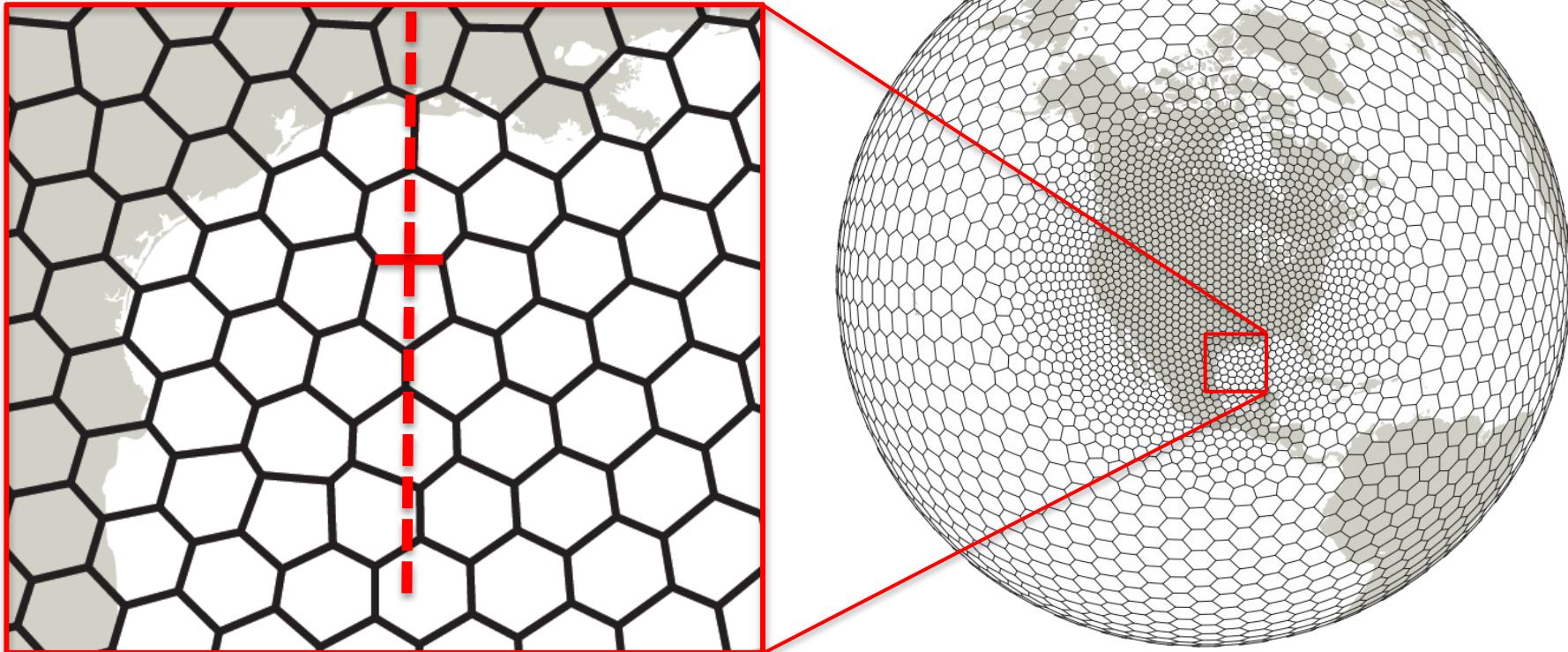
Operators on the Voronoi Mesh

Flux divergence and transport

3rd and 4th-order WRF fluxes:

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

The coordinates are not continuous in MPAS.



Transport – Unstructured MPAS Mesh

3rd and 4th-order fluxes (e.g. WRF):

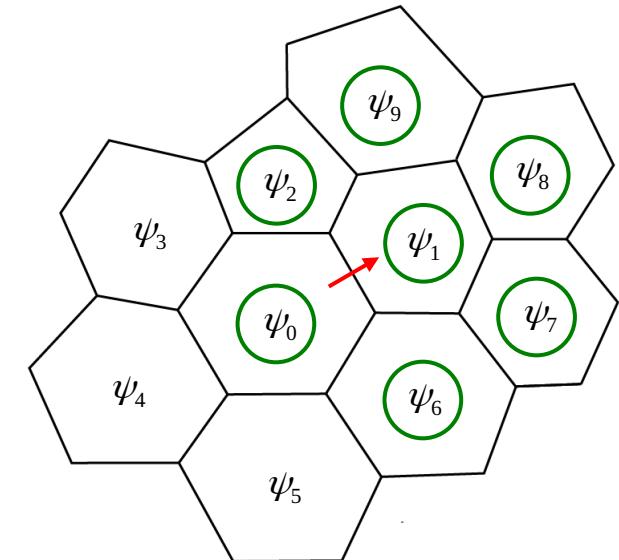
$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

where $\delta_x^2 \psi_i = \psi_{i-1} - 2\psi_i + \psi_{i+1}$ (Hundsdorfer et al, 1995; Van Leer, 1985)

Recognizing $\delta_x^2 \psi = \Delta x^2 \frac{\partial^2 \psi}{\partial x^2} + O(\Delta x^4)$ we recast the 3rd and 4th order flux as

$$\begin{aligned} F(u, \psi)_{i+1/2} = u_{i+1/2} & \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \underbrace{\left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1}}_{\psi_1} + \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right. \\ & \left. + \text{sign}(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \underbrace{\left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1}}_{\psi_1} - \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right] \end{aligned}$$

where x is the direction normal to the cell edge and i and $i+1$ are cell centers. We use the least-squares-fit polynomial to compute the second derivatives.



Transport – Unstructured MPAS Mesh

3rd and 4th-order fluxes (e.g. WRF):

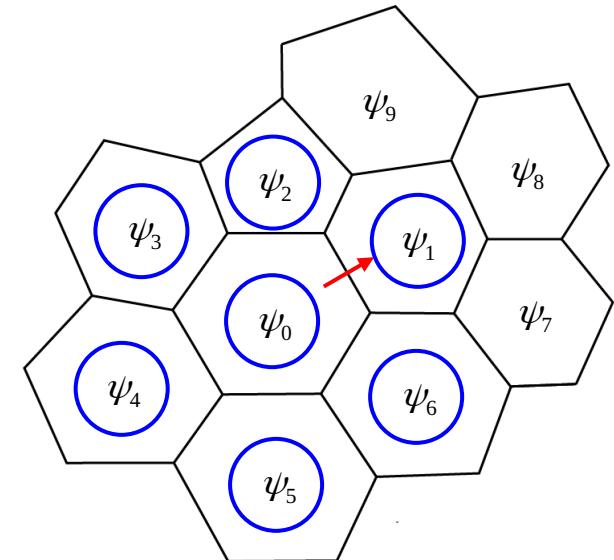
$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \frac{1}{12} (\delta_x^2 \psi_{i+1} + \delta_x^2 \psi_i) + \text{sign}(u) \frac{\beta}{12} (\delta_x^2 \psi_{i+1} - \delta_x^2 \psi_i) \right]$$

where $\delta_x^2 \psi_i = \psi_{i-1} - 2\psi_i + \psi_{i+1}$ (Hundsdorfer et al, 1995; Van Leer, 1985)

Recognizing $\delta_x^2 \psi = \Delta x^2 \frac{\partial^2 \psi}{\partial x^2} + O(\Delta x^4)$ we recast the 3rd and 4th order flux as

$$\begin{aligned} F(u, \psi)_{i+1/2} = u_{i+1/2} & \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \underline{\left(\frac{\partial^2 \psi}{\partial x^2} \right)_i} \right\} \right. \\ & \left. + \text{sign}(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \underline{\left(\frac{\partial^2 \psi}{\partial x^2} \right)_i} \right\} \right] \end{aligned}$$

where x is the direction normal to the cell edge and i and $i+1$ are cell centers. We use the least-squares-fit polynomial to compute the second derivatives.

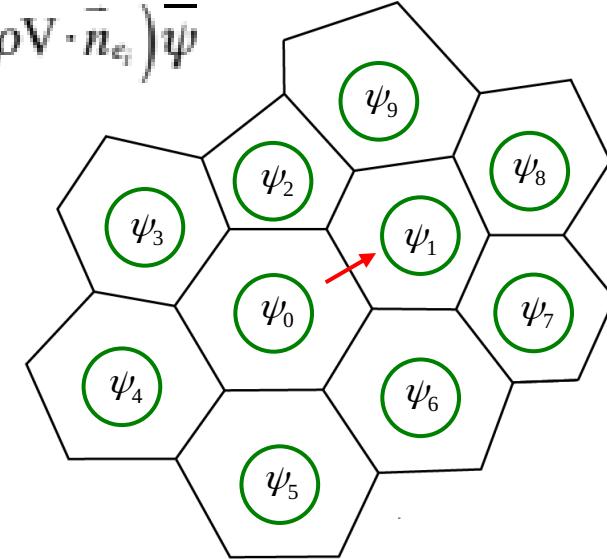


Flux divergence, transport, and Runge-Kutta time integration

Scalar transport equation for cell i :

$$\frac{\partial(\rho\psi)_i}{\partial t} = L(\mathbf{V}, \rho, \psi) = -\frac{1}{A_i} \sum_{e_i} d_{e_i} (\rho \mathbf{V} \cdot \bar{n}_{e_i}) \bar{\psi}$$

1. Scalar edge-flux value ψ is the weighted sum of cell values from cells that share edge and all their neighbors.
2. Each edge-flux is used to update the two cells that share the edge.
3. Three edge-flux evaluations and cell updates are needed to complete the Runge-Kutta timestep.
4. Weights are pre-computed and stored for use during the integration.

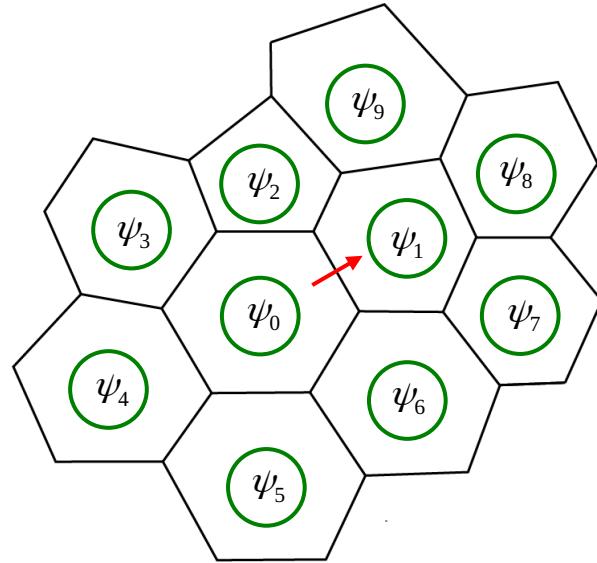


$$(\rho\psi)^* = (\rho\psi)^t + \frac{\Delta t}{3} L(\mathbf{V}, \rho, \psi^t)$$

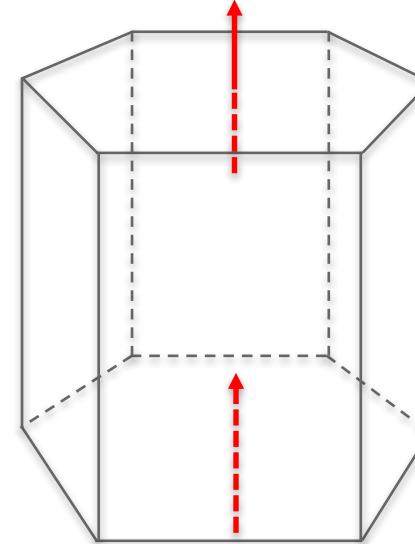
$$(\rho\psi)^{**} = (\rho\psi)^t + \frac{\Delta t}{2} L(\mathbf{V}, \rho, \psi^*)$$

$$(\rho\psi)^{t+\Delta t} = (\rho\psi)^t + \Delta t L(\mathbf{V}, \rho, \psi^{**})$$

Flux divergence and transport. Conservation



Horizontal (scalar) mass fluxes



Vertical (scalar) mass fluxes

The mass (or scalar mass) flux on a cell edge (face) is used to update both cells sharing that edge (face), thus mass (and scalar mass) is conserved exactly.

Scalar transport: Positive-definite and monotonic renormalization

Scalar update, last RK3 step:

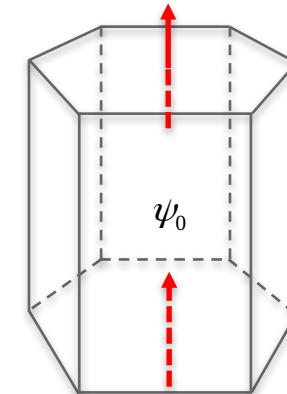
$$(\rho\phi)_i^{t+\Delta t} = (\rho\phi)_i^t - \frac{1}{V_i} \sum_{n_{e_i}} \underbrace{A_{e_i} \overline{(\rho \mathbf{V} \cdot \mathbf{n}_{e_i}) \phi}}_{\text{fluxes } f_i} \quad (1)$$

Renormalization

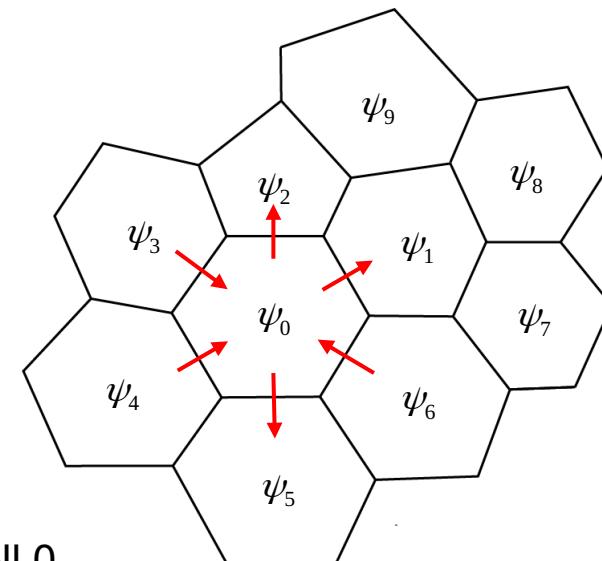
- (1) Decompose flux: $f_i = f_i^{upwind} + f_i^c$
- (2) Renormalize high-order correction fluxes f_i^c such that solution is positive definite or monotonic:

$$f_i^c = R(f_i^c)$$
- (3) Update scalar equation (1) using

$$f_i = f_i^{upwind} + R(f_i^c)$$



$n = 8$ in this example, 6 horizontal fluxes and 2 vertical fluxes to update cell 0



Conservative Transport with RK3 Time Integration: Examples

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right. \right. \\ \left. \left. + sign(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right] \right]$$

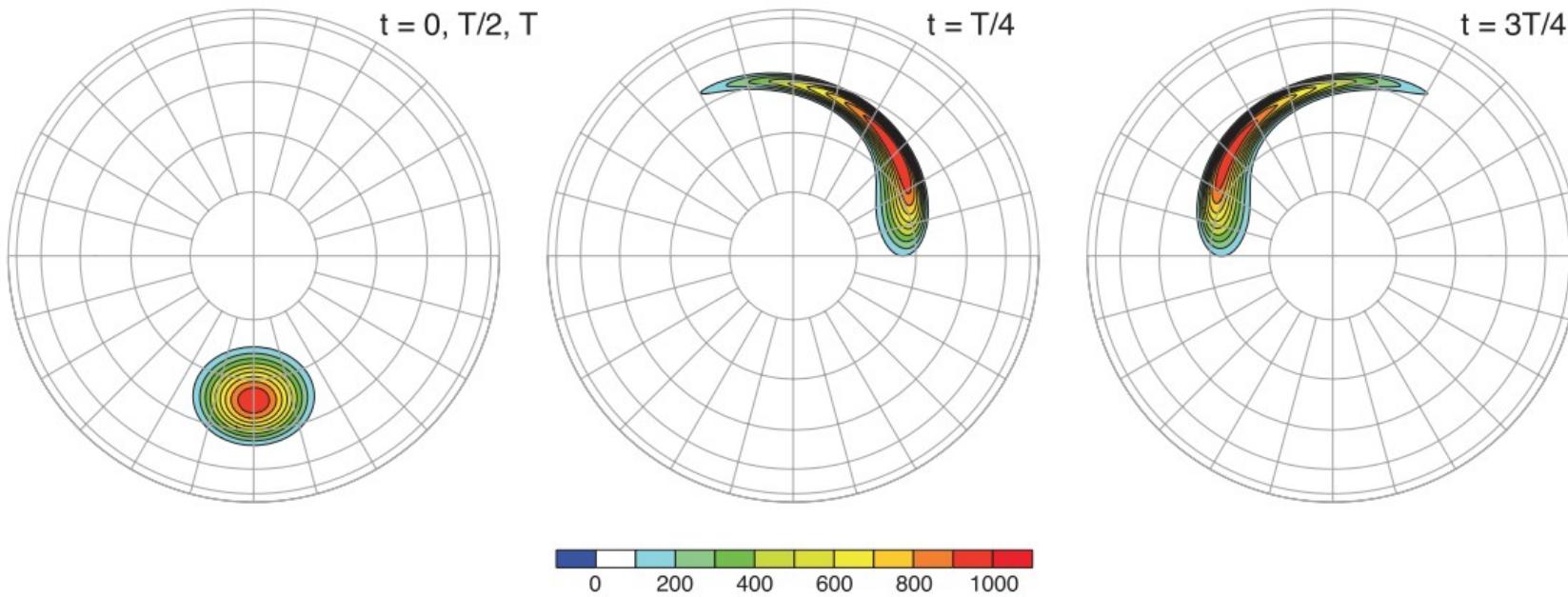


FIG. 5. Exact solution for the Blossey and Durran (deformational flow) test case adapted to the sphere, from Skamarock and Menchaca (2010).

Conservative Transport with RK3 Time Integration: Examples

$$F(u, \psi)_{i+1/2} = u_{i+1/2} \left[\frac{1}{2} (\psi_{i+1} + \psi_i) - \Delta x_e^2 \frac{1}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} + \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right. \right. \\ \left. \left. + sign(u) \Delta x_e^2 \frac{\beta}{12} \left\{ \left(\frac{\partial^2 \psi}{\partial x^2} \right)_{i+1} - \left(\frac{\partial^2 \psi}{\partial x^2} \right)_i \right\} \right] \right]$$

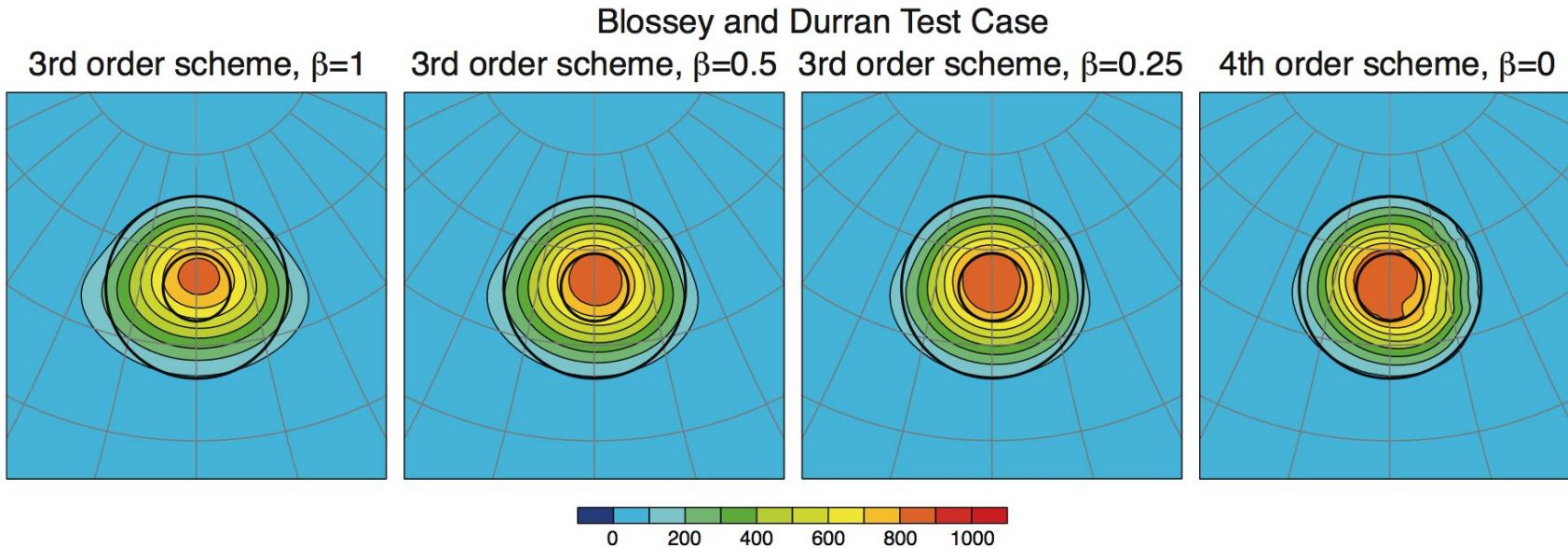
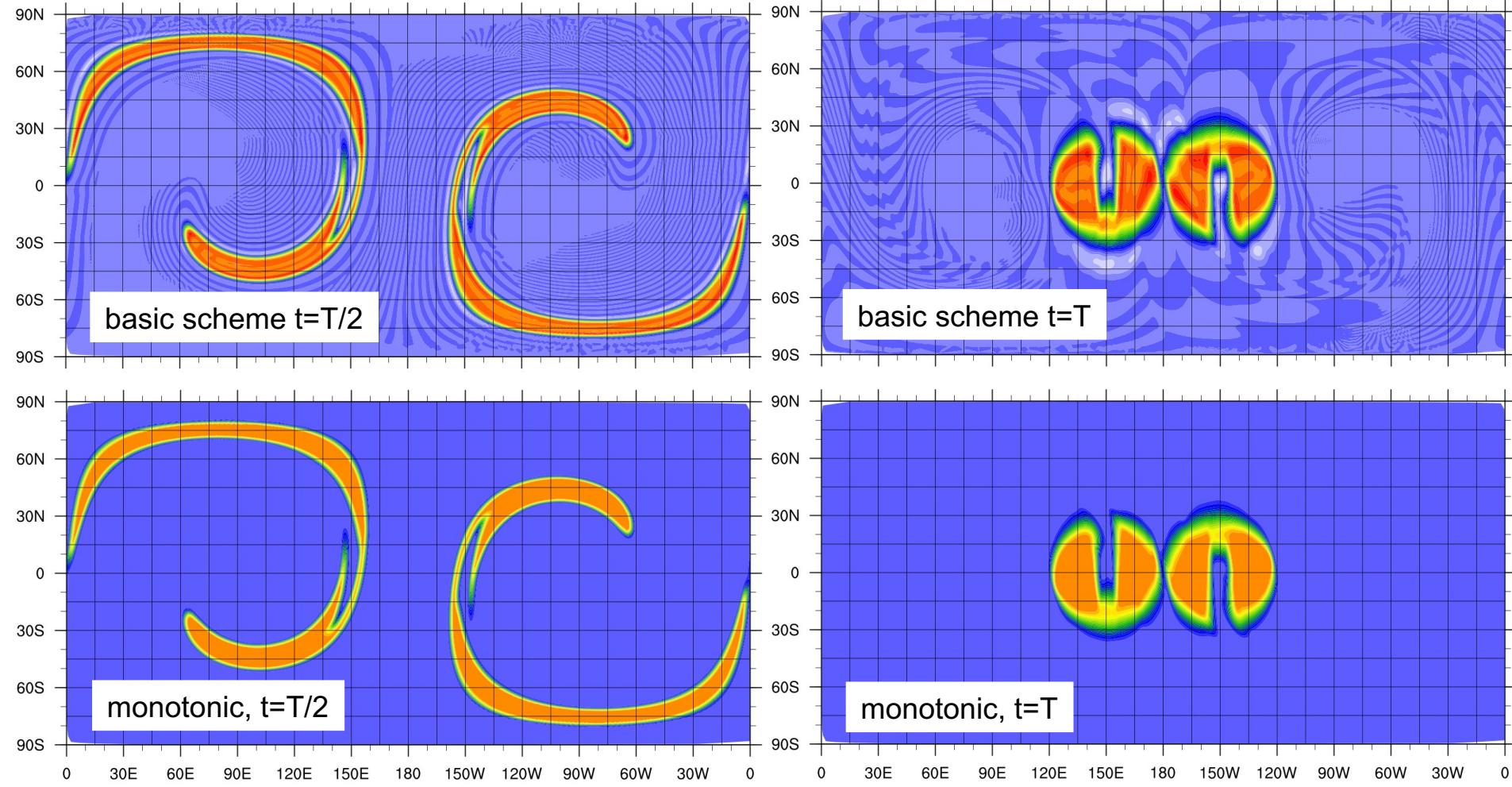
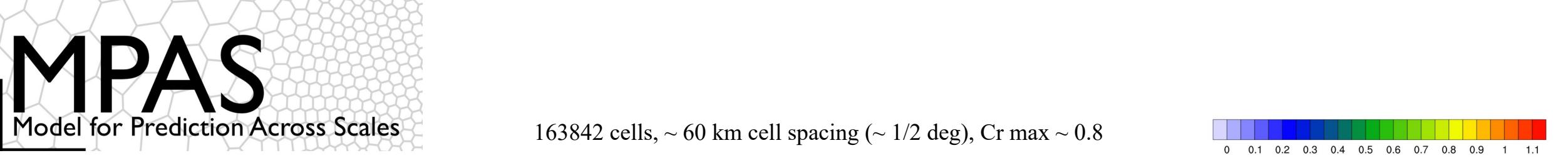


FIG. 7. Deformational flow test case results at time T using (11) with different values of the filter parameter β . The simulations were performed on the 40962-cell grid.



Configuring the dynamics

Transport

namelist.atmosphere

```
&nhyd_model
    config_time_integration_order = 2
    config_dt = 720.0
    config_start_time = '2010-10-23_00:00:00'
    config_run_duration = '5_00:00:00'
    config_split_dynamics_transport = true
    config_number_of_sub_steps = 2
    config_dynamics_split_steps = 3
    config_horiz_mixing = '2d_smagorinsky'
    config_visc4_2dsmag = 0.05
    config_scalar_advection = true
    config_monotonic = true
    config_coef_3rd_order = 0.25
    config_epssm = 0.1
    config_smdiv = 0.1
```

/

*Upwind coefficient ($0 \leftrightarrow 1$),
 > 0 increases damping.
 $= 0$, 4th order scheme,
 > 0 , 3rd order scheme.*

Operators on the Voronoi Mesh

Resolved and turbulent transport

$$\frac{\partial(\rho\phi)}{\partial t} = \underline{-\nabla \cdot \mathbf{V}\phi}$$

Transport by the resolved flow

$$= \underline{\nabla \cdot (\rho K \nabla \phi)}$$

Turbulent transport, e.g. Smagorinsky
 K is an eddy viscosity (m^2/s)

$$= \underline{-\nabla \cdot (\rho \nu_4 \nabla (\nabla \cdot \nabla \phi))}$$

4th-order filter cast as a
turbulent transport

ν_4 is a hyperviscosity (m^4/s)

Operators on the Voronoi Mesh

Resolved and turbulent transport

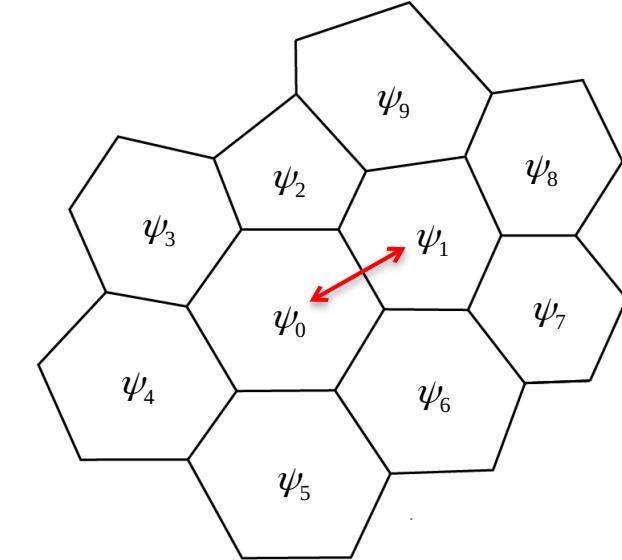
continuous
operators

discrete
operators

$$\nabla \cdot \mathbf{V} \phi \xrightarrow{\text{red arrow}} \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{(\mathbf{V} \cdot \mathbf{n}_{e_i}) \phi}$$

$$\nabla \cdot (\rho K \nabla \phi) \xrightarrow{\text{red arrow}} \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{\rho K} (\mathbf{n}_{e_i} \cdot \nabla \phi)$$

$$\nabla \cdot (\rho \nu_4 \nabla (\nabla \cdot \nabla \phi)) \xrightarrow{\text{red arrow}} \frac{1}{A_i} \sum_{n_{e_i}} d_{e_i} \overline{\rho \nu_4} \left(\mathbf{n}_{e_i} \cdot \nabla \left[\frac{1}{A_j} \sum_{n_{e_j}} d_{e_j} (\mathbf{n}_{e_j} \cdot \nabla \phi) \right] \right)$$



Operators on the Voronoi Mesh

Filters for horizontal momentum

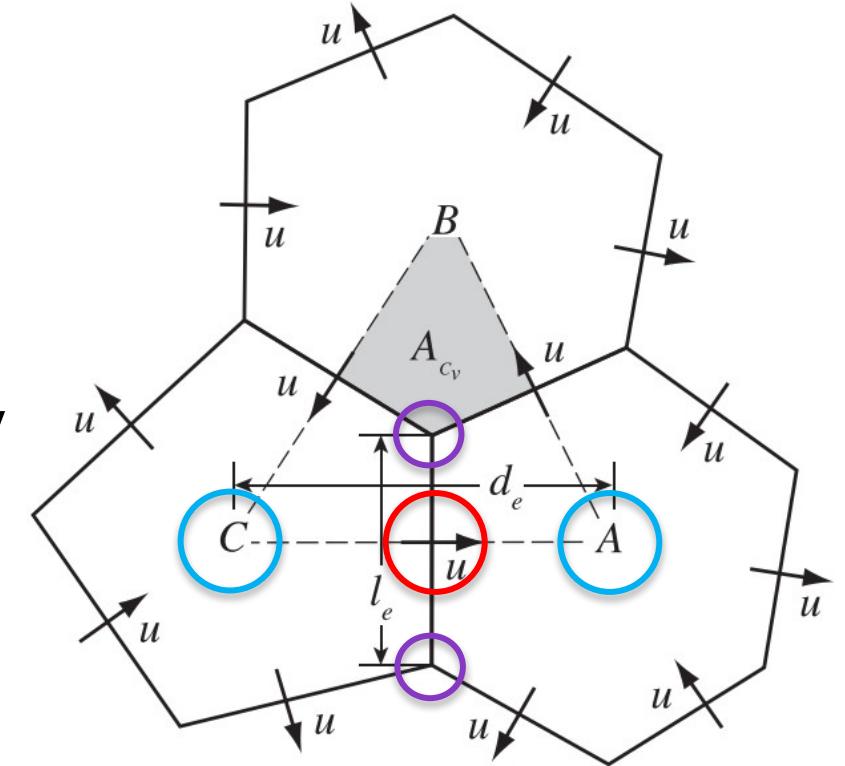
2nd order filter

$$\frac{\partial u_i}{\partial t} = \dots + K_u \nabla^2 u_i$$

$$\boxed{\nabla^2 u_i} = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \mathbf{v} - \frac{\partial \eta}{\partial x_j}$$

discrete form in MPAS.
 η is the vertical vorticity

$$\nabla^2 u_i = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \mathbf{v} - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \mathbf{v})]$$



Operators on the Voronoi Mesh

Filters for horizontal momentum

4th order filter

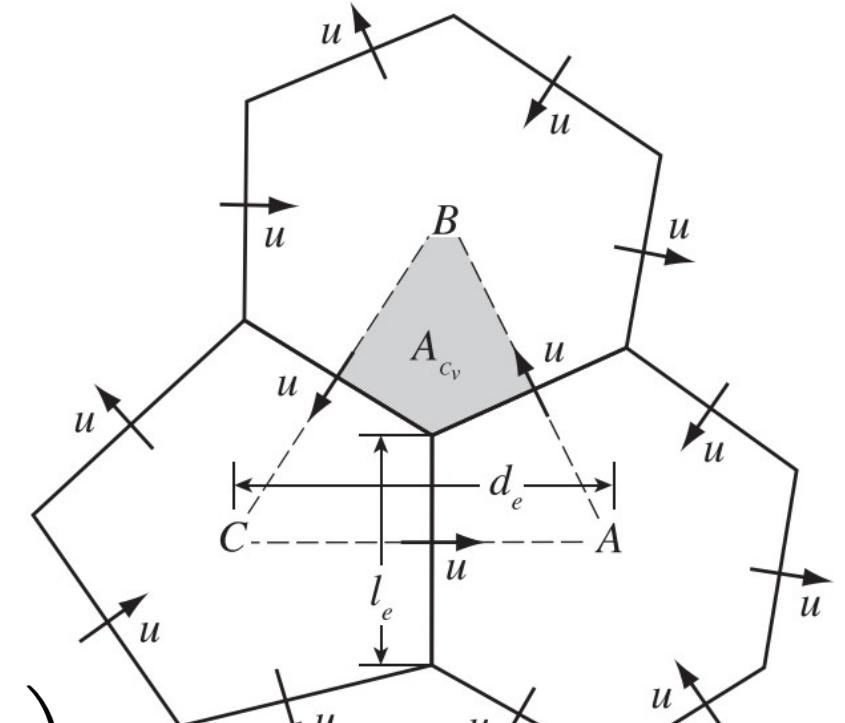
$$\frac{\partial u_i}{\partial t} = \dots - \nu_4^u \nabla^4 u_i$$

$$\nabla^4 u_i = \nabla^2 (\nabla^2 u_i)$$

$$\nabla^4 u_i = \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \nabla^2 u_i - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \nabla^2 u_i)]$$

In MPAS

$$\frac{\delta u_i}{\delta t} = -\nu_4 \left(\gamma_u \frac{\partial}{\partial x_i} \nabla_\zeta \cdot \nabla^2 u_i - \frac{\partial}{\partial x_j} [\mathbf{k} \cdot (\nabla \times \nabla^2 u_i)] \right)$$



Configuring the dynamics

Dissipation

namelist.atmosphere

```

&nhyd_model
    config_time_integration_order = 2
    config_dt = 720.0
    config_start_time = '2010-10-23_00:00:00'
    config_run_duration = '5_00:00:00'
    config_split_dynamics_transport = true
    config_number_of_sub_steps = 2
    config_dynamics_split_steps = 3
    config_horiz_mixing = '2d_smagorinsky' ←
    config_visc4_2dsmag = 0.05 ←
    config_scalar_advection = true
    config_monotonic = true
    config_coef_3rd_order = 0.25
    config_epssm = 0.1
    config_smdiv = 0.1
/

```

$$\nu_4 \text{ (m}^4/\text{s)} = \Delta x^3 \times \text{config_visc4_2dsmag}$$

The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars. We anticipate activating these options for scalars in a future release

Alternately
"2d_fixed"

4th order background
filter coef, used with
2d_smagorinsky

Configuring the dynamics

Dissipation

namelist.atmosphere

```

&nhyd_model
    config_time_integration_order = 2
    config_dt = 720.0
    config_start_time = '2010-10-23_00:00:00'
    config_run_duration = '5_00:00:00'
    config_split_dynamics_transport = true
    config_number_of_sub_steps = 2
    config_dynamics_split_steps = 3
    config_horiz_mixing = '2d_smagorinsky'
    config_visc4_2dsmag = 0.05
    config_scalar_advection = true
    config_monotonic = true
    config_coef_3rd_order = 0.25
    config_epssm = 0.1
    config_smdiv = 0.1
    config_del4u_div_factor = 10.
  /

```

$$\nu_4 \text{ (m}^4/\text{s)} = \Delta x^3 \times \text{config_visc4_2dsmag}$$

The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars. We anticipate activating these options for scalars in a future release

For the horizontal momentum:

$$\nu_{4,D} \text{ (m}^4/\text{s)} = \nu_4 \times \text{config_del4u_div_factor}$$

Hidden in the MPAS V8 namelist.atmosphere
 $\text{config_del4u_div_factor} = 10$ (default)

Configuring the dynamics

Dissipation

namelist.atmosphere

*Hidden in the MPAS V8
namelist.atmosphere*

```
&nhyd_model
  config_h_mom_eddy_visc2 = 0
  config_h_mom_eddy_visc4 = 0
  config_v_mom_eddy_visc2 = 0
  config_h_theta_eddy_visc2 = 0
  config_h_theta_eddy_visc4 = 0
  config_v_theta_eddy_visc2 = 0
  config_horiz_mixing = "2d_fixed"
```

fixed viscosity ($m^2 s^{-1}$)

Fixed hyper-viscosity ($m^4 s^{-1}$)

The dissipation options are not applied to the scalar integration. MPAS V8 relies on the monotonic limiter to filter the scalars.

2d_fixed option is used primarily in idealized cases.

Spatial Discretization in MPAS *references*

Dynamics

Skamarock, W. C., J. B. Klemp, M. G. Duda, L. Fowler, S.-H. Park, and T. D. Ringler, 2012: A Multi-scale Nonhydrostatic Atmospheric Model Using Centroidal Voronoi Tesselations and C-Grid Staggering. *Mon. Wea. Rev.*, 140, 3090-3105. doi:10.1175/MWR-D-11-00215.1

Transport

Skamarock, W. C. and A. Gassmann, 2011: Conservative Transport Schemes for Spherical Geodesic Grids: High-Order Flux Operators for ODE-Based Time Integration. *Mon. Wea. Rev.*, 139, 2562-2575, doi:10.1175/MWR-D-10-05056.1