# Simulation of the time resolution of a 50 $\mu$ m low-gain avalanche detector.

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### Abstract

In this paper we report simulation results on the timing resolution of a 50  $\mu$ m low-gain avalanche detector (LGAD). The simulation includes: sensor fluctuations, front-end electronics, and quantization. Comparisons on the performance for different front-end electronics (FEE) bandwidths (BWs) are presented, as well as the dependance on singal-to-noise ratio (SNR). Two approaches to measure the timestamp are considered: leading edge (LE) and constant fraction (CF). Aditionally, the time resolution is studied as function of the irradiation of the sensor. Simulated LGAD pulses before irradiation, and after neutron fluences of  $5 \times 10^{14}$  n/cm<sup>2</sup> and  $1 \times 10^{15}$  n/cm<sup>2</sup>, are studied. The time resolution a 50  $\mu$ m LGADs was found to be 35 ps for FE electronics BWs larger than 350 MHz and SNRs larger than 30. The time resolution at a SNR of 30 for fluences of  $5 \times 10^{14}$  n/cm<sup>2</sup> and  $1 \times 10^{15}$  n/cm<sup>2</sup> were found to be 31 ps and 37 ps, respectively.

- 8 Key words:
- 9 Silicon, Timing, LGAD

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## 23 1. Introduction

LGADs are envisioned to be used in the CMS and ATLAS experiment upgrades for HL-LHC in order to overcome the event reconstruction challenges posed by the high rate of concurrent collisions per beam crossing. The implemented regions of pseudorapidity  $(\eta)$  are:  $|\eta| > 1.5$ , and  $2.4 < |\eta| < 4.2$  for CMS and ATLAS, respectively. In order to achieve the desired timing precision across a large area of the detectors, the sensors will need to provide high uniformity of signal response and timing resolution. Beam test measurements have provided encouraging results towards achieving such detectors [1].

In this paper, we report simulation results on the timing resolution of a 50  $\mu$ m low-gain avalanche detector (LGAD) which includes the effects of the sensor fluctuations, front-end electronics (FEE), and quantization. Our results indicate that for FEE analog bandwidths (BWs) larger than 350 MHz (shaping times < 1 ns) and signal-to-noise ratios (SNRs) larger than 30, time resolutions of 30-37 ps and 34-47 ps are obtained when using constand fraction (CF) and leading edge (LE) discrimintators, respectively. These results are compatible with previous measurements on LGAD timing resolutions carried out in laboratory and beam test conditions [1–3]. We study the time resolution of four different FEE shaping times: 0.5 ps, 1.0 ps, 2.0 ps, and 4.0 ps; three SNR: 20, 30, 100; and three irradiation levels: pre-radiation,  $5 \times 10^{14}$  n/cm<sup>2</sup>, and  $1 \times 10^{15}$  n/cm<sup>2</sup>. For every point in this scan we evaluate the time resolution for LE and CFD.

The paper is organized as follows: the simulation is described in Sec. 2; algorithms used in the timing reconstruction and analysis are described in Sec. 3; simulation results are presented in Sec. 4, followed by the conclusion in Sec. 5.

### 5 2. Simulation Framework

The simulation framework is based on c++ programing language. The LGAD pulses are obtained from Weightfield2 (WF2), a 2-dimensional silicon simulator [4]. WF2 provides sets of 1000 LGAD pulses which models the response of the sensor to minimum ionizing particles (MIPs). We generated 3 sets of LGAD pulses for a 50  $\mu$ m LGAD: pre-irradiation, and after neutron fluences of  $5 \times 10^{14}$  n/cm<sup>2</sup> and  $1 \times 10^{15}$  n/cm<sup>2</sup>. The simulation framework takes the LGAD pulses (from WF2) and adds gaussian white noise (hereafter white noise). At this point the LGAD pulses with the added white noise are fed into the simulation of the FEE (see Fig. 1). The output of the FEE simulation is the convolution of the impulse response function and the input signal at the FEE. We consider four shaping constants for the impulse response of the FEE: 0.5, 1.0, 2.0, and 4.0 ns (the FEE simulation is described in Sec. 2.1). At the output of the FEE block we have a simulated LGAD pulse which includes the effects of sensor fluctuations, shaping of the FEE, and noise. A waveform analysis is performed with the pulses obtained at the output of the FEE block. We assign timestamps to each pulse by using algorithms that

emulate an ideal LE and CF discriminators. For each threhold we obtain a LE and CF timestamp as well as the corresponding time-over-theshold (ToT) of the pulse. The SNR is defined as the ratio of the most probable value (MPV) of the amplitude distribution to the width of the amplitude distribution at a fixed sample (where only noise is present). We study 3 SNR scenarios: 20, 30, and 100. A schematic diagram of the simulation is shown in Fig. 1.

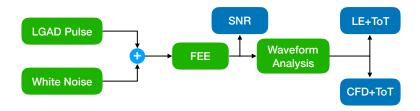


Figure 1: A schematic diagram of the simulation. Each simulation configurable block is shown in green. The most relevant outputs of the simulation are shown in blue.

### 2.1. Fron-end electronics and noise injection

The front-end simulation is implemented in c++ programing language. It combines analytical calculations when possible but it mostly relies on numerical methods. We implement most calculations in the time domain, while the frequency domain is mostly used to cross-check noise and the FEE expected responses. Sections 2.1.1 and 2.1.2 detail the front-end and noise implementation in the simulation.

# 2.1.1. front-end implementation

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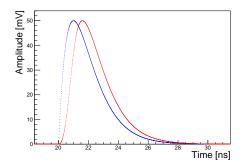
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The fron-end simulation is based on a single amplification stage. We focus on the BW of such amplifier rather than variations thereof. The FEE is a second order low-pass filter which transfer function and impulse response are given by equations 1 and 2, respectively.

$$H(S) = \frac{\frac{1}{\tau_s^2}}{(S + 1/\tau_s)^2} \tag{1}$$
  $h(t) = \frac{t}{\tau_s^2} e^{-t/\tau_s}$ 

The output pulse of the FEE is the convolution (in time domain) of the pulse from the LGAD library and the FEE impulse response (see Eq. 2). The time base for the pulses and the convolution is 10 ps – this sampling time is used throughout the simulation. As stated above we focus the study on the BW of the FEE, to that end we scan the  $\tau_s$  paremeter in Eq. 2 in the following set: $\{0.5, 1, 2, 4\}$  ns, this parameter is hereafter referred to as shaping time (ST). Figure 2 (left) shows the comparison of the impulse and LGAD responses for a ST of 1 ns while Figure 2 (right) shows the LGAD response for all STs studied. We obseve that the LGAD response is delayed with respect to the impulse response, and that pulse slew rate is decreased in the first nanosecond of the pulse. We also observe the expected behavior when comparing the LGAD responses for the different STs, pulse risetimes scale with the ST and the decay time is dominated by the ST. The measured 10 - 90% risetimes are shown in Tab. 1.



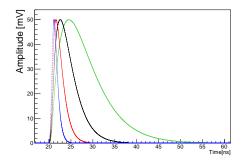


Figure 2: (Left) Comparison of impulse and LGAD reponses for the a shaping time (ST) of 1 ns. (Right) LGAD response for the four shaping times studied: {0.5, 1, 2, 4} ns. All pulses have been nomalized to achive a peak amplitude of 50 mV. Legends for the shaping times are shown in the plots.

Shaping time (ns)	0.5	1.0	2.0	4.0
Risetime (ns)	$0.7 \pm xx$	$0.9 \pm xx$	$1.4 \pm xx$	$2.5 \pm xx$

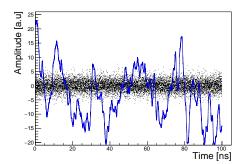
Table 1: Measured risetime for all shaping times studied:  $\{0.5, 1, 2, 4\}$  ns. Risetime is the 10% - 90% time difference as measured by the CFD algorithm described in Sec. 3.1.

### 2.1.2. noise injection

Gaussian white noise is simulated by sampling the full time window (0 - 100 ns) in 10 ps intervals. Each sampled time is assign a random amplitude which is drawn from from a gaussian distribution with zero mean and width corresponding to the SNR under study. It is important to note that the width of the gausian parameter is not exactly the SNR and needs to be adjusted depending on the ST of the FEE. The left panel of Figure 3 shows the gaussian white noise before and after a 1 ns FEE. The expected behavior for the noise is observed. The left panel of Figure 3 shows the output of the FEE block, with a 1 ns ST, for a pre-radiation LGAD pulse when noise has been injected. The injected noise is such that the SNR is 30. SNR is defined ratio of the landau peak of the maximum amplitude (MPV) to the the r.m.s of the 100th sample over an ensemble of 1000 pulses.

# 3. Timing Reconstruction and Analysis

The time reconstruction is based on a waveform analysis. We generate an ensamble of 1000 pulses sampled every 10 ps. Each pulse is interpolated using a the Whittaker-Shannon formula  $(\sin(x)/x)$ , using the interpolated pulse we assign a timestamp by finding when a voltage threshold has been crossed. The theshold can be a constant value (LE) or a constant fraction of the maximum amplitude of pulse (CF), more details about the algorithms are given in Sec. 3.1. The time resolution is estimated by the width parameter of a gaussian fit to the timestamps obtain for a particular theshold. We apply a time time-walk correction based on the time-over-threshold of the pulse, we note that this correction has a large improvement on the time resolution measured using the LE algorithm while the CF algorithm is mostly insentive to this correction (see Fig. 4). Details



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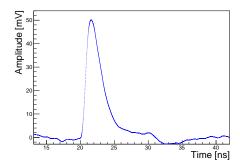


Figure 3: (Left) Comparison of gaussian white noise before and after the FEE. (Right) Example pulse at the output of the FEE block with a SNR of 30. Both figure use a shaping time (ST) of 1 ns. Legends for the shaping times are shown in the plots.

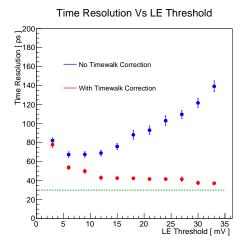
about this correction are covered in Sec. 3.2. The timestamps are measured with a 20 ps binning while the time-over-thershold is measured with a 100 ps in order to simulate the effect of quantization. We scan the LE and CF threshold such that we find the one with the lowest jitter.

### 3.1. Leading edge and constant fraction discriminators

The leading edge and constant fraction discriminator algorithms are ideal in the sense that they don't simulate the effect of electronics in a real implementation. Our approach is to sample the pulses every 10 ps and subsequently interpolate them using a the Whittaker-Shannon formula  $(\sin(x)/x)$  to more accurately find the threshold crossing. In the LE case the theshold is scanned from 3 - 60 mV, while the CFD is scanned from 5 - 90 % of the current pulse maximum amplitude. For each thershold we obtain two timestamps: when the pulse first crosses the threshold  $(t_0)$  and when it crosses the second time  $(t_1)$ , now in the opposite direction. The time-over-thershold is defined as the difference of the two timestapms (ToT =  $t_1 - t_0$ ). The first timestamp,  $t_0$ , is used to determine the time resolution at given threshold. The time resolution is defined as the width of a gaussian fit to the  $t_0$  distribution binned with a bin-width of 20 ps. The time resolution is obtained in two cases: before and after a time-walk correction. The timewalk correction aims to correct the known drift effect on the timestamps when dealing with pulses of different amplitudes. The time walk correction is based on the measured ToT and explained in detail in Sec. 3.2. Fig. 4 shows the time resolution as a function of the threshold required for a pre-radiation LGAD with a ST of 1 ns and a SNR of 30. We note that the effect of the time-walk correction is large for LE and almost negligible for CFD. Fig. 5 shows a typical  $t_0$  distribution, using the LE and CF algorithms, for the pre-radiation LGAD after the ToT correction has been applied. The time resolution  $(\sigma_t)$ is measured to be  $37.3 \pm 1.4$  and  $33.0 \pm 1.4$  for the LE and CF, respectively.

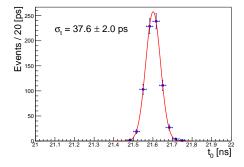
### 3.2. Time-walk correction and time-over-threshold

A time-walk correction is applied in order to correct the timestamp drift when dealing with pulses of varying amplitudes. The correction is based on the measured time-over-therhold:  $ToT = t_1 - t_0$ . We observe, as expected, that ToT correction is large for the



# Time Resolution Vs CFD Threshold 200 8 180 No Timewalk Correction 80 140 With Timewalk Correction 80 40 40 40 50 60 70 80 CFD Threshold [%]

Figure 4: (Left) Comparison of gaussian white noise before and after the FEE. (Right) Example pulse at the output of the FEE block with a SNR of 30. Both figure use a shaping time (ST) of 1 ns. Legends for the shaping times are shown in the plots.



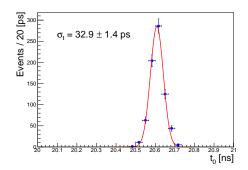


Figure 5: (Left) timestamp  $(t_0)$  distribution for a 30 mV threshold using a leading edge discriminator. (Left) timestamp  $(t_0)$  distribution for a 35% threshold using a constant fraction discriminator. Both figures include the time-walk correction based on the measured ToT. Both figures use a shaping time (ST) of 1 ns and correspond to SNR of 30.

LE case and negligible for CF (see Fig. 4). Fig. 6 (left) shows a typical two dimensional map of  $t_0$  and ToT for the LE algorith, wherein a clear correlation between  $t_0$  and ToT is observed. The time-walk correction is obtain by measuring the average  $t_0$  in each ToT bin and subsequently fitting a 2th-order polinomial (see Fig. 6 (right)). The resulting analytical expression after the fit is then used to correct the dependence of  $t_0$  on ToT. The time-walk correction is expressed in Eq. 3, where  $p_2$  and  $p_1$  are the quadratic and linear coefficients of the 2th-oder polinomial fit. The procedure is updated every time any parameter on the simulation changes, i.e ST, SNR, and LGAD library inputs. As shown in Fig. 4 (left) the effect of the time-walk dependes on the threshold used and correcting for it can yield significant improvements in the measured time resolution.

$$t_0 = t_0 - (p_2 \text{ToT}^2 + p_1 \text{ToT})$$
 (3)

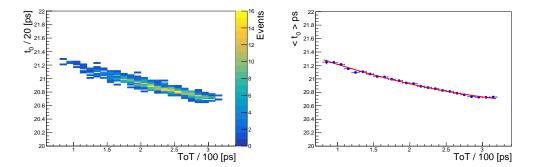


Figure 6: (Left) two dimensional map of the timestamp  $(t_0)$  and ToT  $(t_1-t_0)$ . (Right) one dimensional projection of the timestamp  $(t_0)$  dependence on ToT, the red curve is the 2th-order polinomial fit that ultimately is used to correct  $t_0$ . Both figures use a shaping time (ST) of 1 ns and correspond to a SNR of 30.

### 4. LGAD Front-end Electronics Performance

Herein we present a number of studies for a 50  $\mu$ m LGAD. We study the time resolution as a function of irradiation for three different scenarios: pre-radiation, and after neutron fluences of  $5 \times 10^{14}$  n/cm<sup>2</sup> and  $1 \times 10^{15}$  n/cm<sup>2</sup>. We also quantify the effect of the BW of the FEE by varying the ST ( $\tau_s$ ), four STs are considerd: 0.5, 1, 2, and 4 ns. Additionally, we study the effect of noise by varying the SNR in all the scenarios described above. We consider three SNR: 20, 30, and 100. Sec. 4.1 summarizes the effects of the shaping time and SNR, and and Sec. 4.2 summarizes the effect of irradiation.

# 4.1. Front-end electronics shaping time and SNR studies

We scan the ST of the FEE and the SNR. The results for the pre-radiation sensor are summarized in Table. 4.1. We observe that the best results are consitently obtained by the 0.5 ns and 1.0 ns STs regardless of the SNR. We observe that longer STs are more affected by less favorable SNR, e.g for and SNR of 20 the time resolution is 37 ps and 100 ps for a 0.5 ns and 4.0 ns ST, respectively. We note that CF consitently outperforms

# Time Resolution (ps)

		Leading Edge	Constant Franction			
ST (ns)	SNR = 20	SNR = 30	SNR = 100	SNR = 20	SNR = 30	SNR = 100
0.5	$38.4 \pm 2.1$	$34.9 \pm 1.7$	$28.8 \pm 1.0$	$37.2 \pm 1.9$	$34.5 \pm 1.6$	$29.8 \pm 1.9$
1.0	$45.4 \pm 2.2$	$37.3 \pm 1.4$	$28.7 \pm 1.7$	$36.4 \pm 1.8$	$33.0 \pm 1.4$	$25.9 \pm 1.3$
2.0	$63.4 \pm 2.5$	$47.6 \pm 2.0$	$30.7 \pm 1.2$	$47.6 \pm 1.9$	$34.3 \pm 1.6$	$28.7 \pm 1.7$
4.0	$103.0 \pm 4.1$	$75.3 \pm 2.8$	$37.6 \pm 2.0$	$73.8 \pm 3.1$	$54.8 \pm 2.1$	$32.1 \pm 1.3$

Table 2:  $50 \mu m$  pre-radiation LGAD sensor simulation: summary of best time resolution obtained for SNRs of 20, 30, and 100. Leading edge and constant fraction results are shown.

## Time Resolution (ps)

		Leading Edg	Constant Franction			
ST (ns)	SNR = 20	SNR = 30	SNR = 100	SNR = 20	SNR = 30	SNR = 100
0.5	$36.8 \pm 1.9$	$32.0 \pm 1.3$	$26.0 \pm 1.2$	$32.5 \pm 1.4$	$30.6 \pm 1.2$	$25.1 \pm 1.2$
1.0	$40.9 \pm 1.4$	$33.8 \pm 1.1$	$29.2 \pm 1.0$	$33.4 \pm 1.5$	$30.9 \pm 0.9$	$26.1 \pm 1.3$
2.0	$56.9 \pm 2.4$	$45.3 \pm 2.2$	$30.1 \pm 1.1$	$43.7 \pm 1.6$	$36.9 \pm 1.3$	$24.4 \pm 1.0$
4.0	$93.3 \pm 3.6$	$67.9 \pm 2.5$	$36.5 \pm 1.3$	$70.8 \pm 2.8$	$52.4 \pm 1.9$	$29.9 \pm 1.9$

Table 3: 50  $\mu$ m LGAD sensor simulation after neutron fluence of  $5 \times 10^{14}$  n/cm<sup>2</sup>: summary of best time resolution obtained for SNRs of 20, 30, and 100. Leading edge and constant fraction results are shown.

LE, this effect is clearly observed for less favorable SNR and slower ST. Comparing CF and LE for the 1.0 ns ST with SNR of 20 yields a difference in performance of 26 ps (when subtrated in quadrature). Aditionally, we observe that time resolutions better than 25 ps could not be achieved which is consitent with the known intrinsic LGAD jitter. The latter is taken into account by the WF2 pulse library and confirmed in our simulation, we use a SNR of 1000 and obtained a time resolution consistent with 25 ps. Finally, in the case of the pre-radiation sensor we obseved that time resolutions of 35 ps are achievable for STs between 0.5 - 1.0 ns and a SNR of 30.

# 4.2. Timing performace as a function of irradiation

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We study the effect of irradiation on the time resolution of a 50  $\mu$ m sensor, we employ LGAD simulation files that include the effect of radiation damage. We consider two cases besides pre-radiation: neutron fluences of  $5 \times 10^{14}$  n/cm<sup>2</sup> and  $1 \times 10^{15}$  n/cm<sup>2</sup>. We perform the same studies as in the pre-radiation case and covered in Sec. 4.1. The results for

### Time Resolution (ps)

		Leading Edge	Constant Franction			
ST (ns)	SNR = 20	SNR = 30	SNR = 100	SNR = 20	SNR = 30	SNR = 100
0.5	$47.8 \pm 2.0$	$37.6 \pm 2.0$	$26.6 \pm 1.3$	$41.9 \pm 1.9$	$34.3 \pm 1.1$	$24.1 \pm 1.0$
1.0	$59.9 \pm 2.3$	$46.8 \pm 1.8$	$28.1 \pm 1.5$	$46.5 \pm 1.9$	$36.8 \pm 1.3$	$23.1 \pm 0.9$
2.0	$89.7 \pm 3.5$	$68.2 \pm 2.6$	$32.3 \pm 1.4$	$64.7 \pm 2.8$	$49.6 \pm 2.1$	$27.3 \pm 0.9$
4.0	$147.3 \pm 5.1$	$109.0 \pm 4.3$	$42.6 \pm 1.9$	$118.6 \pm 4.0$	$84.1 \pm 3.2$	$33.8 \pm 1.1$

Table 4:  $50 \mu m$  LGAD sensor simulation after neutron fluence of  $1 \times 10^{15}$  n/cm<sup>2</sup>: summary of best time resolution obtained for SNRs of 20, 30, and 100. Leading edge and constant fraction results are shown.

the irradiated LGAD are presented in Tab. 4.1 and Tab. 4.1 for neutron fluences of  $5 \times 10^{14} \text{ n/cm}^2$  and  $1 \times 10^{15} \text{ n/cm}^2$ , respectively. We observe similar trends to those of the pre-radiation sensor described in Sec. 4.1. We note that when using STs between 0.5 - 1.0 ns and a SNR of 30, time resolutions of the order of 31 ps and 37 ps are obtained for  $5 \times 10^{14} \text{ n/cm}^2$  and  $1 \times 10^{15} \text{ n/cm}^2$ , respectively.

# 5. Conclusion

We study the time resolution of a 50  $\mu$ m LGAD using a simulation. We focus on the shaping time and sigal-to-noise ratio of the fron-end electronics and its interplay with the irradiation of the sensor. We reproduce the known LGAD jitter of 25 ps for fast STs and large SNRs. We observe a clear degradation of the time resolution with SNR and slower STs. The best results are obtained using a ST of 0.5 ns and using CF discriminator – similar results are obtained with a ST of 1.0 ns. For a SNR of 30 and for STs betwen 0.5-1.0 ns we obtain time resolutions between 30 - 37 ps for the 3 irradiations considered. The reduction in gain with irradiation could bring the SNR for the most irradiated LGAD  $(1 \times 10^{15} \text{ n/cm}^2)$  to 20 and thus worsen the time resolution to 42 - 47 ps. We note a clear gain in performace of CF over LE discriminators, particularly at low SNR and largest irradiation level. For the 1.0 ns at SNR = 30, the performance improvement of CF over LE is 26ps for the pre-radiation sensor while 37ps for  $1 \times 10^{15} \text{ n/cm}^2$ . Overall our simulation results indicate that time resolutions better than 45 ps are accessible for a 50  $\mu$ m LGADs up to irradiations of  $1 \times 10^{15} \text{ n/cm}^2$ .

# 199 Acknowledgment

We thank the FTBF personnel and Fermilab accelerator's team for very good beam conditions during our test beam time. We also appreciate the technical support of the Fermilab SiDet department for the rapid production of wire-bonded and packaged LGAD assemblies. We would like to thank Alan Prosser and Ryan Rivera for their critical help in setting up the DAQ and trigger chain. We thank Ned Spencer, Max Wilder, and Forest McKinney-Martinez for their technical assistance, and the CNM and HPK manufacturing team. We acknowledge the help of V. Cindro and I. Mandic with the neutron irradiations.

This document was prepared using the resources of the Fermi National Accelerator Laboratory (Fermilab), a U.S. Department of Energy, Office of Science, HEP User Facility. Fermilab is managed by Fermi Research Alliance, LLC (FRA), acting under Contract No. DE-AC02-07CH11359. Part of this work was performed within the framework of the CERN RD50 collaboration.

This work was supported by the Fermilab LDRD 2017.027; by the United States Department of Energy grant DE-FG02-04ER41286; by the California Institute of Technology High Energy Physics under Contract DE-SC0011925; by the European Union's Horizon 2020 Research and Innovation funding program, under Grant Agreement no. 654168 (AIDA-2020) and Grant Agreement no. 669529 (ERC UFSD669529); by the Italian Ministero degli Affari Esteri and INFN Gruppo V; and by the Spanish Ministry of Economy, Industry and Competitiveness through the Particle Physics National Program (ref. FPA2014-55295-C3-2-R and FPA2015-69260-C3-3-R) co-financed with FEDER funds.

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